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Posted Date: 28 September 2025

doi: 10.20944/preprints202509.2322.v1

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Article

# Long-Lasting Hydrophilicity of Al<sub>2</sub>O<sub>3</sub> Surfaces via Femtosecond Laser Microprocessing

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#### **Abstract**

We explore the wettability modulation induced on alumina ( $Al_2O_3$ ) targets by femtosecond laser texturing to demonstrate a stable and durable hydrophilic character of the surface. Specifically, we identify a suitable operational regime to tailor micro-nanostructures onto  $Al_2O_3$  plates and accurately assess the ablation threshold in our experimental conditions. A periodic geometry with triangular patterns of various groove depths was optimized for establishing a long-term wetting response. The latter was monitored on daily basis over a time interval of six-weeks by collecting contact angle measurements of samples with and without a post-process thermal annealing, here adopted to stabilize the surface wettability soon after the laser treatment. Results show that deeper grooves significantly enhance and maintain the hydrophilic character, particularly in samples without post-process thermal annealing, where super-hydrophilicity is demonstrated to persist throughout the entire time under test. These findings disclose the potential for an effective fine-tuning of the alumina wettability, thus opening to specific applications requiring long-term control of surface-liquid interactions, such as biomedical implants, orthopedic and dental prostheses.

**Keywords:** femtosecond laser microprocessing; laser surface texturing; superhydrophilicity; alumina ceramic (Al<sub>2</sub>O<sub>3</sub>); surface wettability

#### 1. Introduction

Aluminum oxide ( $Al_2O_3$ ), commonly known as alumina, is a ceramic material widely used in numerous technological and industrial applications due to its excellent physical and mechanical properties [1]. Typically, alumina exhibits low density and exceptional hardness, good thermal conductivity, high resistivity, and notable dielectric strength [2,3]. Moreover, from a chemical standpoint, alumina is highly resistant to corrosion and oxidation, showing excellent wear resistance and a high degree of biocompatibility [4]. These properties make alumina an ideal candidate for cutting-edge applications in automotive, aerospace, and biomedicine, where the control of surface wettability is particularly challenging [5–7].

Alumina surfaces with hydrophobic behavior, characterized by contact angles greater than 90°, have attracted a lot of attention due to their potential applications in microfluidics, lab-on-chip devices and as functional surfaces for the aerospace and automotive industries [8]. Conversely, alumina hydrophilicity, typically associated with contact angles lower than 90°, has been exploited to promote cell adhesion and osseointegration [9,10], or in crucial aspects of biomedical applications such as joint prostheses (e.g., dental or hip implants) [11,12]. In this context, a comprehensive study of long-term hydrophilicity of alumina appears to be still missing in the current scientific literature.

Over the years, several methods have been developed to adjust the wettability response of alumina via surface modifications, including polymer coatings, UV irradiation, chemical-assisted and

plasma treatments [13–15]. However, those approaches often present some limitations in terms of process complexity and fabrication times. Laser processing is known to overcome these disadvantages and intrinsically guarantees improved precision, efficiency, and surface quality [16,17]. Noteworthy, laser processing has been proven to be highly effective in producing hydrophilic surfaces. Triantafyllidis et al. [19] experimentally studied the impact of CO2 induced melting and resolidification of refractory Al<sub>2</sub>O<sub>3</sub> composite ceramics, observing a decrease of the fluid contact angle from 41.4° to 26.9°, which they attributed to an increase in surface roughness in relation to the laser power density. However, the authors exclusively focused on analyzing the initial modification of the contact angle, without evaluating the long-term stability of the laser-induced hydrophilicity. Jagdheesh et al. [8] incidentally observed highly hydrophilic properties on Al<sub>2</sub>O<sub>3</sub> surfaces immediately after laser texturing with picosecond pulses and Kunz et al. [19] used femtosecond laser pulses to modify the wetting behavior on composite alumina, reporting a significant contact angle reduction but no evidence on hydrophilicity evolution over time. Cao et al. [20] and Wang et al. [21] reported on their experimental investigations with femtosecond laser pulses on alumina, demonstrating a threshold fluence of 10.39 J/cm<sup>2</sup> and 8.32 J/cm<sup>2</sup>, respectively, and a hydrophilic contact angle of 57.9° after 240 hours and 56° after 360 hours. However, their results on timedependent hydrophilicity were limited to a period of few days, without addressing whether that would finally stabilize or decay over time.

In this work, we address the entire range of wettability, from hydrophobicity to hydrophilicity, induced by femtosecond laser pulses on alumina surfaces, focusing on the evolution and temporal persistence of surface hydrophilicity over a period of six weeks, without the application of additional surface treatments.

#### 2. Materials and Methods

The material used in this study was ADS-96R alumina ( $Al_2O_3$ ) from CoorsTek, a ceramic substrate widely adopted as an industrial standard [22]. Samples had dimensions of  $88.9 \times 88.9 \text{ mm}^2$  and a thickness of 0.64 mm. To remove surface impurities, all samples were cleaned before laser texturing by ultrasonication in acetone (AR, > 99.5%), ethanol (AR, 95%), and distilled water for 15 minutes each. Finally, the samples were air-dried at 70 °C.

To modify the morphology of the sample surface, we carried out laser direct writing in ambient air by employing a versatile solid-state laser Pharos SP 1.5 femtosecond laser system (Light Conversion), which offered a wide range of adjustable parameters (pulse duration, fluence, repetition rate, etc.) and significant flexibility for experimental optimization. The pulse duration was set to 190 fs, with a central wavelength of 1030 nm, and the laser repetition rate could be varied from single-shot operation up to 1 MHz. The emitted beam was nearly diffraction-limited ( $M^2 = 1.3$ ) and linearly polarized. The laser beam was directed onto the sample surface using a galvo scanner (IntelliSCANN 14, SCAN-LAB) combined with a telecentric f-theta lens of 100 mm focal length, enabling precise control over the scanning process. The beam waist was measured to be 13.2  $\pm$  0.1  $\mu$ m ( $1/e^2$  peak intensity) by a CCD camera FireWire BeamPro (Model 2523 by Photon Inc.).

In the following section, we determined the ablation threshold of alumina  $(Al_2O_3)$  in our experimental conditions and optimized the surface morphology to demonstrate for the first time to our best knowledge a stable and durable hydrophilicity induced by femtosecond laser micronanotexturing.

#### 3. Experimental Section

#### 3.1. Ablation Threshold of Alumina with Femtosecond Laser Pulses

We have estimated the ablation threshold of alumina in our experimental conditions using the Liu method [23], which is based on measuring the diameters of laser-induced craters formed on the surface of our samples. According to this method, the relationship between the ablation threshold fluence for N consecutive pulses and the crater sizes is expressed by the following equation:



$$D^{2} = 2 * \omega_{0}^{2} * \ln \left( \frac{F_{0}}{F_{th}(N)} \right)$$
 (1)

where F<sub>0</sub> is the peak fluence, defined as:

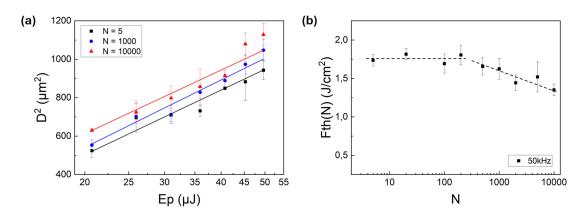
$$F_0 = \frac{2 * E_p}{\pi * \omega_0^2} \tag{2}$$

and  $\omega_0$  is the Gaussian beam radius at  $1/e^2$ ,  $E_P$  is the pulse energy. Through linear fitting of Equation (1), the radius of the Gaussian laser beam and the threshold fluence for multiple pulses,  $F_{th}(N)$ , were evaluated for each number of pulses N and repetition rate in Table 1. Specifically, seven series of ablation craters were generated, each consisting of five matrices produced at different pulse energies. Within each matrix, each row was ablated with an increasing number of laser pulses, and the repetition frequency was kept constant and upper limited to 50 kHz by the maximum pulse energy available in our experiments. All parameters used for each series, matrix, and row are summarized in Table 1.

**Table 1.** Experimental parameters used to evaluate the threshold fluence for multiple pulses,  $F_{th}(N)$ , using the Liu method [23].

Parameters	Values	
Repetition rates [kHz]	50 - 25 - 10 - 5 - 1	
Number of pulses (N)	5 - 20 - 100 - 200 - 500 - 1000 - 2000 - 5000 - 10000	
Pulse energy (E <sub>p</sub> ) [μJ]	49.6 - 45.3 - 40.8 - 35.9 - 31 - 25.9 - 20.7	

Figure 1(a) shows the semi-logarithmic graph of the squared crater diameter ( $D^2$ ) as a function of pulse energy ( $E_P$ ) for different pulse numbers (N) at the highest repetition rate (i.e. 50 kHz). Morphological and optical characterization of the craters were carried out using a Nikon Eclipse ME600 optical microscope equipped with ImageJ software.



**Figure 1.** (a) Squared crater diameter (D<sup>2</sup>) as a function of pulse energy ( $E_p$ ) for different numbers of pulses (N). The linear fit shows an R<sup>2</sup> value higher than 0.97. (b) Multi-pulse ablation threshold fluence,  $F_{th}(N)$ , as a function of the number of laser pulses (dashed line is a guide for the eye only). All data refers to a fixed repetition frequency of 50 kHz, which is upper limited by the maximum pulse energy available in our experiments.

It was observed that as both pulse energy and the number of pulses increased, the squared crater diameter increased linearly, indicating that the ablation area also increased with higher energy. By extrapolating the ablation threshold fluence for each pulse number from the intercept of the linear fitting in Figure 1(a), we calculated an average ablation threshold of  $1.63 \pm 0.16 \,\text{J/cm}^2$ .

Figure 1(b) shows the relationship between multi-pulse ablation threshold fluence  $F_{th}(N)$  and number of laser pulses N at the same repetition frequency of 50 kHz. It was observed that for N values less than or equal to 200 pulses, the threshold fluence  $F_{th}(N)$  remained nearly constant, in

accordance with results shown by Andriukaitis *et al.* [24], who analyzed the threshold fluence in similar conditions to reveal a rapid saturation in the range  $100 \div 1000$  fs-pulses, both in single-pulse and in MHz/GHz burst regime. Nonetheless, a slight decrease in the multi-pulse ablation threshold fluence was shown in Figure 1(b) for N > 200 pulses, which can be rather interpreted as the incubation effect [25–27].

#### 3.2. Role of Femtosecond Laser Microtexturing on Alumina Wettability

We employed an effective strategy of laser processing [28,29] to access various wettability regimes on  $Al_2O_3$  targets and establish a long-term stability of their hydrophilic character. Specifically, we modified the surface morphology with femtosecond laser pulses to create an optimal periodic geometry, which was induced by overlapping cross scanning patterns to generate square-shaped structures, separated by a hatch of 150  $\mu$ m, followed by a 45° square-shaped pattern.

Figure 2 shown a representative contour plot of those micro-nanostructures as taken by a profilometer (CountourGT InMotion; Bruker, USA), with laser parameters being optimized at the maximum available pulse energy of 49.6  $\mu$ J for a fixed rep. rate of 50 kHz. The beam scanning speed was set at 20 mm/s to inscribe periodic grooves with a depth of 17.1  $\pm$  0.1  $\mu$ m relative to the intact surface, which in turn featured a roughness of about 3.4  $\pm$  0.1  $\mu$ m. In the 3D image, different regions of the textured surface are highlighted: the pristine substrate and three areas labeled bottom-1, bottom-2, and bottom-3, corresponding to one, two, and four laser passes over the same spot, respectively. This variation in the number of laser passes was intentionally set in accordance with our laser strategy. Consequently, some areas received multiple overlaps of laser exposure, leading to different groove depths and roughness.

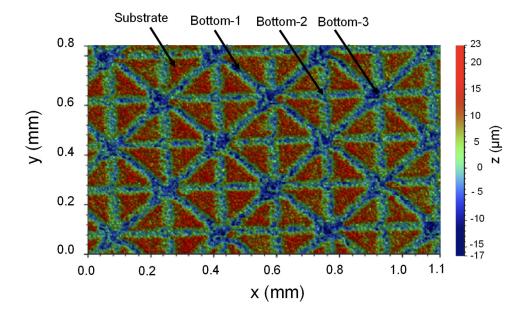


Figure 2. Representative 3D topography of laser-inscribed patterns on  $Al_2O_3$  surface, featuring a triangular lattice with a texture percentage above 70%. The beam scanning speed was set at 20 mm/s and the depth of the periodic grooves were  $17.1 \pm 0.1$  µm relative to the intact surface. Different regions of the textured surface are highlighted: the unetched substrate (in red), and three areas labeled bottom-1, bottom-2, and bottom-3, corresponding respectively to one, two, and four laser passes over the same spot.

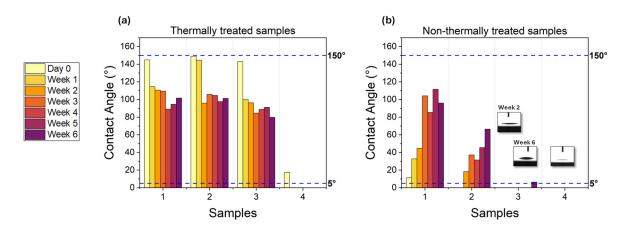
We investigated various scanning speeds (ranging from 20 to 750 mm/s) at a fixed pulse energy and repetition frequency, aiming to fine-tune the groove depth only. In Table 2, we summarized the outcome: the groove depth became progressively shallower with increasing scanning speed, as expected [29].

**Table 2.** Correlation between laser-induced groove depths and beam scanning speed at a fixed pulse energy of  $49.6 \mu J$  and repetition rate of 50 kHz.

Sample	Depth [µm]	Scan Speed [mm/s]
1	$3.2 \pm 0.1$	750
2	$4.3 \pm 0.1$	250
3	$13.2 \pm 0.1$	80
4	$17.1 \pm 0.1$	20

Figure 3 shows how the wetting response of our samples in Table 2 would evolve over a time-interval of 6 weeks in air atmosphere. Specifically, the wettability dynamics of laser-textured surfaces with increasing groove depth (see labels 1 to 4 in Figure 3) was assessed by static water contact angle measurements using an Optical Contact Angle Goniometer (OCA 25 by Dataphysics). To ensure a metrological grade measurement, a set of 3  $\mu$ L water droplets were deposited on several areas of each sample, and the average value of the resulting contact angles was evaluated. Noteworthy, samples were stored at room temperature between consecutive measurements, and the contact angles were monitored on daily basis, from day 0 to week 6, although only weekly values have been plotted in Figure 3 for clarity.

The comparison between contact angle dynamics of both thermally and non-thermally treated samples is shown in Figure 3(a) and 3(b), respectively. The thermal treatment consisted of heating the samples at  $120 \pm 1$  °C for 3 hours in ambient air, as widely employed to promote the wettability stabilization of similar laser-textured structures [28–31]. This thermal aging procedure, with rather mild annealing conditions, was here purposely adopted to accelerate the surface enrichment with oxides and organic contaminants, and to expedite the settlement of the wetting response immediately after laser texturing (i.e., without waiting for a standard room temperature aging period of tens of days).



**Figure 3.** Evolution of the contact angle over time for: (a) thermally and (b) non-thermally treated samples, with the aging time ranging from day 0 to week 6. Dashed lines indicate the reference threshold angle for superhydrophobic (150°) and superhydrophilic (5°) regimes, respectively. Inset in Figure 3(b) shows representative images of contact angle measurements (barely above the instrument sensitivity) on the alumina surface at week 2 (i.e.,  $3.2 \pm 0.1^{\circ}$ ) and week 6 (i.e.,  $5.6 \pm 0.1^{\circ}$ ), respectively.

Initially, samples 1–3 in Figure 3(a) exhibited an almost superhydrophobic regime induced by the thermal treatment, with contact angles as high as  $148.9 \pm 0.1^{\circ}$ , in accordance with results previously observed by Lang *et al.* in similar conditions [32]. However, such a hydrophobic character was not persistent, with contact angles progressively drifting to a saturation value around 90° within 6 weeks of testing. This behaviour is consistent with the time-dependent chemistry stabilization expected at the surface of thermally treated samples [28,30]. Similarly, a comparable trend of monotonic reduction in the contact angle was revealed on pristine (i.e. unstructured) samples

subjected to thermal annealing, which displayed an initial contact angle of  $83.4 \pm 0.1^{\circ}$  reaching a plateau point of  $46.3 \pm 0.1^{\circ}$  after few days. Analogously, a plateau point of  $46.1 \pm 0.1^{\circ}$  was measured on unstructured and non-thermally treated samples (not shown in Figure 3).

Remarkably, sample 4 in Figure 3(a) displayed an unexpected hydrophilicity on day 0, rapidly evolving into a steady super-hydrophilic regime which lasted all over the testing time and featured an average contact angle always below 5°. We ascribed this behavior to the laser-induced morphology at the surface and speculated on the role played by grooves with certain depth and roughness, which may accommodate more fluid into the microstructures, thus promoting a hydrophilic character of the sample.

Figure 3(b) shows wettability dynamics on non-thermally treated samples: a gradual increase of the contact angle from day 0 to the sixth week was plausibly due to natural aging and surface contamination in air atmosphere. Despite such a gradual increase, all samples except for sample 1 maintained a contact angle below 90° throughout the observation period, demonstrating a persistent hydrophilicity of  $Al_2O_3$  surfaces via femtosecond laser texturing. Noteworthy, samples 3 and 4 exhibited a long-lasting superhydrophilic regime (< 5°), with their specific morphology fostering very-low contact angles in time, with values even below the instrument sensitivity. Although the comparison with sample 3 in Figure 3(a) may appear to some extent controversial, these preliminary results validated the explicit correlation between fs-laser strategy and long-term superhydrophilicity of alumina, opening to more refined design of micro-nanostructure at the surface to establish a robust control on the  $Al_2O_3$  wettability.

### 4. Conclusions

In summary, this study demonstrates that femtosecond laser micro-nanoprocessing can effectively modulate the wettability of alumina surfaces, enabling long-lasting hydrophilicity on  $Al_2O_3$  substrates without the need for additional chemical or physical treatments.

The average ablation threshold was accurately determined under our experimental conditions to identify an optimal operational strategy for fs-laser tailoring the surface morphology of alumina. By fine-tuning the pattern design and systematically varying groove depth and roughness, we established a direct correlation between surface morphology and wetting response of alumina. Notably, non-thermally treated samples maintained a super- or hydrophilic state throughout the entire testing period, except for samples with shallow grooves. Aging period and fs-laser strategy may be refined to settle hydrophilicity endurance on thermally treated samples, except for samples with deep grooves.

These preliminary outcomes provide a valuable starting point for future investigations and address key gaps in the current scientific literature, demonstrating a long-term stability of hydrophilic behavior on alumina over much longer period than previously reported. Such a capability to control and stabilize hydrophilic states on alumina opens new opportunities for biomedical applications. In particular, the enhanced and durable hydrophilicity can promote cell adhesion and osseointegration, which are critical for joint prostheses, such as dental or hip implants, where long-term stability and reproducibility of wetting properties are essential.

**Author Contributions**: Conceptualization, A.S. and F.P.M.; methodology, A.S., F.P.M., C.G.; software, A.S.; formal analysis, A.S., F.P.M., C.G.; L.P., M.P.; investigation, A.S. L.P., M.P.; writing—original draft preparation, A.S., F.P.M; writing—review and editing, F.P.M., C.G, A.V. and A.A.; visualization, A.S., L.P., M.P.; supervision, F.P.M.; All authors have read and agreed to the published version of the manuscript.

**Funding:** This work was supported by MUR in the framework of the PRIN 2022 PNRR Project "Surface and Interface acoustic wave-driven Microfluidic devices BAsed on fs-laser technology for particle sorting (SIMBA)" (grant number: Prot. P2022LMRKB) and the project "Quantum Sensing and Modeling for One-Health (QuaSiModO)" (CUP: H97G23000100001).

Data Availability Statement: Data will be made available on request.



**Conflicts of Interest:** The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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