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Article

Experimental Investigations on the Ferromagnetic Resonance and Absorbing Properties of a Ferrofluid in the Microwave Range

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Abstract: Measurements of complex magnetic permeability, $\mu(f,H)=\mu'(f,H)-i\mu''(f,H)$ and dielectric permittivity $\epsilon(f,H)=\epsilon'(f,H)-i\epsilon''(f,H)$, in the frequency range, f of (0.4-7) GHz, and polarizing field, H of (0-135) kA/m, were performed, for a kerosene-based ferrofluid with magnetite nanoparticles. Based on these measurements, the phenomenon of ferromagnetic resonance was highlighted and some microwave propagation parameters of the ferrofluid were determined: the attenuation constant, $\alpha(f,H)$, and the reflection coefficient, $R(f,H)$, at the air-material interface. Knowing these parameters we proposed a theoretical model establishing for the first time a new equation that allows the calculation of the overall reflection coefficient, $R_w(f,H)$, of a ferrofluid with thickness d , deposited on a totally reflective support, following multiple internal reflections of the electromagnetic wave in the material. The results show that by increasing both, H , and d , the parameter, $R_w(f,H)$ presents a minimum that decreases from 0.90 (for $d=2$ mm) to 0.64 (for $d=10$ mm), at frequency $f=5$ GHz, which indicates an increase in the absorption of the electromagnetic wave by the ferrofluid. The obtained results are useful in the study of some materials that could be used as electromagnetic absorbers in the microwave range, by the determination of the overall reflection coefficient, $R_w(f,H)$, controlled both by the thickness, d , of the absorber and by the external applied field, H .

Keywords: ferrofluid; complex dielectric permittivity; complex magnetic permeability; the attenuation constant; the reflection coefficient; absorbing properties

1. Introduction

Ferrofluids are colloidal systems of single-domain magnetic nanoparticles, having a distribution of sizes between (3-15) nm being dispersed in a carrier liquid and coated with a surfactant to prevent their agglomeration [1]. Each particle can be in a state of uniform magnetization with the magnetic moment, $m=MsV_m$, where Ms is the spontaneous magnetization of the bulk material from which the particles come, and V_m is the magnetic volume of the particle.

It is known that, due to anisotropy, single-domain particles can have more than one axis of anisotropy, but the particle presents a minimum energy along a preferential axis called the principal axis. As a result, in the theoretical investigations of the magnetic properties of ferrofluids, it is assumed that the single-domain particles in a ferrofluid have uniaxial anisotropy [1] and the effective anisotropy constant, K_{eff} , is the result of the combination of magnetocrystalline, shape or surface anisotropy [2,3]. For the single-domain particle with uniaxial anisotropy, the anisotropy field, H_A is given by the relation [2,4]:

$$H_A = \frac{2K_{eff}}{\mu_0 M_s} \quad (1)$$

where μ_0 is the magnetic permeability of free space.



Measurements of the complex magnetic permeability, $\mu(f, H)$ in the microwave range and in presence of a polarizing magnetic field H , allow the determination of the real $\mu'(f, H)$ and imaginary $\mu''(f, H)$ components [5–7], which are very useful both for highlighting the phenomenon of ferromagnetic resonance and for evaluating the anisotropy field H_A , and other magnetic parameters of nanoparticles in ferrofluids. Starting from the Landau–Lifshitz equation [4], which describes the movement of the magnetic moment m of the particle, in a magnetic field H , for a strong polarizing magnetic field ($H \gg H_A$), the resonance condition is written in the form [8]:

$$2\pi f_{res} = \gamma(H + H_A) \quad (2)$$

This equation shows a linear dependence between the resonant frequency, f_{res} and H , whose slope is γ , (called the gyromagnetic ratio of the particle), and is given by the following relation:

$$\gamma = \mu_0 g \gamma_e (1 + \alpha_L^2)^{1/2} \quad (3)$$

In Eq. (3), g is the spectroscopic splitting factor; $\gamma_e = 8.791 \times 10^{10} \text{ s}^{-1} \text{T}^{-1}$ is the electronic gyromagnetic ratio and α_L is the damping parameter of the Landau–Lifshitz equation [4]. In the ferromagnetic resonance range, knowing these parameters of the nanoparticles in the ferrofluid is very important in some microwave applications [9]. Among the practical applications based on microwaves, we can mention the wireless connection, through radio waves, global positioning system (GPS), radar and mobile telephony, and with the progress made in these applications, the problem of electromagnetic interference appears, thus requiring the finding of materials with electromagnetic absorbing properties [10], which are very necessary in the field of electromagnetic shielding [11]. At the same time, the increased use of electronic devices leads to significant pollution with electromagnetic waves, so that the study of electromagnetic wave absorbers (EMAs) is appropriate [12–14]. The results reported in [15] clearly show that composite materials are effective in reducing electromagnetic interference (EMI) pollution, with special attention being paid to the development of new nanocomposite materials with high electromagnetic absorbing properties.

Ferrofluids are considered to be nanocomposite systems and may show special electromagnetic properties which differ from the typical properties of the individual constituent components [16]. To design devices with specific microwave properties, such as the electromagnetic absorbers [15,17], it is necessary to undertake an analysis regarding the propagation of the electromagnetic waves in ferrofluids and the determination of propagation parameters correlated with possible absorbing properties of the ferrofluid in the microwave field.

It is known that in the case of plane wave propagation [18] through an electromagnetic medium along the Oz axis, the complex temporal expressions of the electric (\vec{E}) and magnetic (\vec{H}) components of the electromagnetic field are given by the relations:

$$\vec{E} = \vec{e}_x E_0 e^{-\alpha z} e^{i(\omega t - \beta z)} \quad (4)$$

$$\vec{H} = \vec{e}_y \frac{E_0}{Z_m} e^{-\alpha z} e^{i(\omega t - \beta z)} \quad (5)$$

where, \vec{e}_x and \vec{e}_y are unit vectors on the Ox and Oy axes and $i = \sqrt{-1}$; $(\omega t - \beta z)$ represents the phase of the electromagnetic wave, β being the phase constant and ω the angular frequency. Also, $E_0 e^{-\alpha z}$ and $(E_0/Z_m) e^{-\alpha z}$ are the amplitudes of the electric and magnetic components of the electromagnetic wave, where α and Z_m represent the attenuation constant and the intrinsic impedance of the propagation medium, respectively, which are given by the relations [19]:

$$\alpha = \frac{\sqrt{2\pi f}}{c} \sqrt{(\mu_r'' \epsilon_r'' - \mu_r' \epsilon_r') + \sqrt{(\mu_r'' \epsilon_r'' - \mu_r' \epsilon_r')^2 + (\mu_r' \epsilon_r'' + \mu_r'' \epsilon_r')^2}} \quad (6)$$

$$Z_m = \sqrt{\frac{\mu_0}{\epsilon_0}} \cdot \sqrt{\frac{\mu_r}{\epsilon_r}} = Z_0 \sqrt{\frac{\mu_r}{\epsilon_r}} \quad (7)$$

In these relations, f is the frequency of electromagnetic wave; $c = 3 \times 10^8 \text{ m/s}$ is the speed of electromagnetic waves in free space and $Z_0 = (\mu_0 / \epsilon_0)^{1/2} = 377 \Omega$ is the intrinsic impedance of free space

(ϵ_0 being the dielectric permittivity of free space). Considering the complex form of the relative magnetic permeability, $\mu_r = \mu'_r - i\mu''_r$ as well of the relative dielectric permittivity, $\epsilon_r = \epsilon'_r - i\epsilon''_r$, the following expression for calculating the intrinsic impedance of the medium is obtained from equation (7):

$$Z_m = Z_0 \sqrt{\frac{1}{\epsilon_r'^2 + \epsilon_r''^2} \sqrt{(\mu'_r \epsilon'_r + \mu''_r \epsilon''_r)^2 + (\mu''_r \epsilon'_r - \mu'_r \epsilon''_r)^2}} \quad (8)$$

Let's assume that an electromagnetic wave comes from medium 1 and is reflected on the surface of medium 2 (Figure 1).

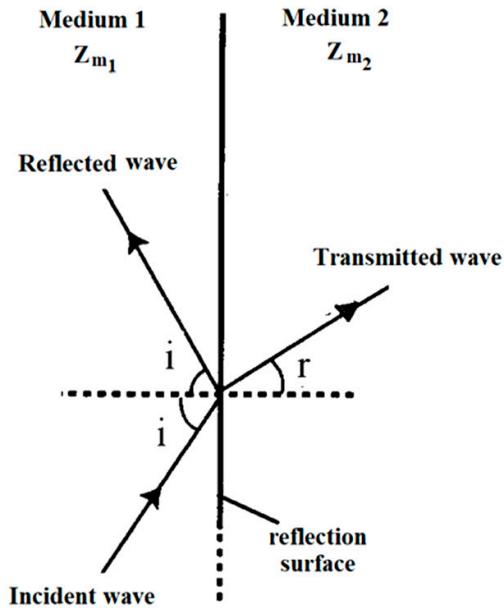


Figure 1. Schematic representation of the reflected and transmitted wave, on the separation surface between two electromagnetic media.

It is known that the modulus of the reflection coefficient R , on the reflection surface, is defined as the ratio between the complex amplitude of the reflected wave and the complex amplitude of the incident wave [15,20], and in the case of the field perpendicular to the plane of incidence, the reflection coefficient, R , is given by the relation [20]:

$$R = \frac{\left| \frac{\mu_{r1} \epsilon_{r2}}{\mu_{r2} \epsilon_{r1}} - 1 \right|}{\left| \frac{\mu_{r1} \epsilon_{r2}}{\mu_{r2} \epsilon_{r1}} + 1 \right|} \quad (9)$$

Considering the definition of the intrinsic impedance of a medium (Eq. (7)), R can be written as:

$$R = \frac{\left| \frac{Z_{m2} - Z_{m1}}{Z_{m2} + Z_{m1}} \right|}{\left| \frac{Z_{m2} + Z_{m1}}{Z_{m2} - Z_{m1}} \right|} \quad (10)$$

where Z_{m1} and Z_{m2} are the intrinsic impedances of the medium 1 and medium 2 respectively.

The absorbing properties of the propagation medium can be highlighted both by the attenuation constant, α and by the reflection coefficient R . As a result, the aim of the work presented here, was to investigate the microwave absorption properties of a ferrofluid sample, by determining the

parameters α , and R , at different H values and sample thicknesses d . For this, we performed measurements of $\mu(f,H)$ and $\varepsilon(f,H)$, in the microwave range (0.4 - 7) GHz and at different values H , (0 - 135) kA/m, for a ferrofluid sample. At the same time we proposed a theoretical model for computing the overall reflection coefficient, $R_w(f, H)$ of a plane wave absorber with a single layer supported by a perfect conductor, following multiple internal reflections, valid for any material/composite system that has absorbing properties in microwave range, applied to the investigated ferrofluid sample.

2. Theoretical model of the overall reflection coefficient

Another important parameter relating to electromagnetic absorbers is the overall reflection coefficient, R_w , of a material with thickness d , through which an electromagnetic wave propagates. To define R_w , consider a thin layer of an absorbent material (having the attenuation constant α and reflection coefficient R), deposited on a metal support (total reflective support) (Figure 2). We consider that the incident wave (E_i) comes from medium 1 (air) and on the air-material interface, at point A, is reflected (R_i wave) and simultaneously, is transmitted (E_t wave) in the material (medium 2).

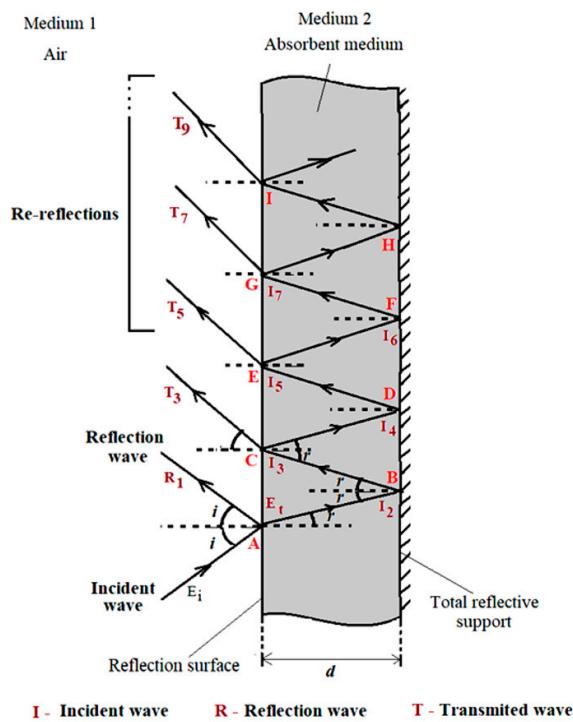


Figure 2. Schematic representation of the electromagnetic wave absorption and reflection through an absorbent material deposited on a total reflective support.

The absorption of the wave is performed during its passage through medium 2, both before and after total reflection on the reflective support, at point B. By returning to the interface air-material, at point C, both reflection in material (medium 2) and transmission in air (medium 1) of the wave (see Figure 2) occurs. Similarly, at point C, there will be several internal reflections of the wave in the absorbing medium, followed by its return to medium 1. All reflected waves and re-reflections at the interface air-absorbing material, which reach medium 1 (air) (see Figure 2), will thus determine the overall reflection coefficient, R_w , of the absorbing material.

It is known that the modulus of the transmission coefficient, T , in absorbent material, is defined as the ratio between the complex amplitude of the transmitted wave and the complex amplitude of

the incident wave [15,20]. At the same time, the reflection (R) and transmission (T) coefficients at the air-material interface are related by the relation, $T+R=1$ [15]. Keeping these definitions in mind, both the wave reflected and transmitted through the material at point A can be written mathematically with the relations:

$$E_{R1(A)} = RE_i \quad (11)$$

$$E_{t(A)} = (1-R)E_i \quad (12)$$

where, with $E_{R1(A)}$ and $E_{t(A)}$, are the reflected and transmitted wave respectively, at point A (see Figure 2).

The $E_{t(A)}$ wave travels through the absorbent material and will arrive, attenuated at point B on the total reflective metallic support, and is then reflected. As a result,

$$E_{i2(B)} = E_{t(A)} \exp(-\alpha d) = (1-R)E_i \exp(-\alpha d) \quad (13)$$

Due to the total reflection on the reflective metallic support, the reflected wave, $E_{r2(B)}=E_{i2(B)}$, will then travel through the absorbing material (medium 2) and will arrive attenuated at point C ($E_{i3(C)}$ wave), on the air-absorbing material incident surface (see Figure 2); $E_{i3(C)}$ being expressed by the relation:

$$E_{i3(C)} = E_{r2(B)} \exp(-\alpha d) = (1-R)E_i \exp(-2\alpha d) \quad (14)$$

where Eq. (13) was considered.

At point C, the incident wave $E_{i3(C)}$ will be reflected in medium 2 and at the same time will be transmitted in medium 1 (air) (Figure 2). On incident surface at the point C, the transmission coefficient T, will be the same as at point A, so that the following relation can be written for the transmitted wave $E_{t3(C)}$:

$$E_{t3(C)} = (1-R)E_{i3(C)} \quad (15)$$

Considering relation (14), equation (15) becomes:

$$E_{t3(C)} = (1-R)^2 E_i \exp(-2\alpha d) \quad (16)$$

Following the same reasoning, we determined the expressions of the re-reflected waves in medium 1 (air), T5, T7, T9,.....(see Figure 2). Result:

$$E_{t5(E)} = R(1-R)^2 E_i \exp(-4\alpha d) \quad (17)$$

$$E_{t7(G)} = R^2(1-R)^2 E_i \exp(-6\alpha d) \quad (18)$$

$$E_{t9(I)} = R^3(1-R)^2 E_i \exp(-8\alpha d) \quad (19)$$

As a result, on the incident surface (air-absorbent material), after the repeated passes of the wave through the material and returning to medium 1 (air), the following relation can be written:

$$E_{eff} = R_w E_i \quad (20)$$

where,

$$E_{eff} = E_{R1(A)} + E_{t3(C)} + E_{t5(E)} + E_{t7(G)} + E_{t9(I)} + \dots \quad (21)$$

represents the sum of all reflected waves and re-reflections from medium 1, after the electromagnetic wave has been totally reflected an infinite number of times, on the metal support by passing through the absorbing medium. Considering relations (12), (14), (17) - (21), the overall reflection coefficient R_w , at normal incidence is given by the following equation:

$$R_w = R + (1-R)^2 \exp(-2\alpha d) + (1-R)^2 \sum_{k=1}^{\infty} R^k \exp[-2(k+1)\alpha d] \quad (22)$$

Unlike other papers [21,22], relation (22) represents a new equation that allows a much more precise determination of the overall reflection coefficient R_w , which takes into account the multiple total reflections of the electromagnetic wave on the reflective metal support, when the wave passes

through absorbent material, being valid for any material/composite system that has electromagnetic wave absorption properties.

3. Sample and experimental setup

The investigated sample was a ferrofluid with magnetite nanoparticles dispersed in kerosene and stabilized with oleic acid using the new technique of hydrophobization in the absence of the dispersion medium [23]. The obtained magnetic material was dispersed in kerosene and then filtered in a magnetic field gradient in order to remove aggregates and large particles [23,24].

The static magnetization curve of the ferrofluid sample (Figure 3) was determined using an inductive method [25] and it shows a Langevin-type dependence [1]. Based on the magneto-granulometric analysis of Chantrell [26] and the $M(H)$ dependence from Figure 3, we have determined the following parameters for the ferrofluid sample, assuming the particles to be of spherical shape: the saturation magnetization of the ferrofluid, $M_{sat}=22.47\text{ kA/m}$; the mean magnetic diameter of a particle, $d_m=8.03\text{ nm}$; the particles concentration, $n=12.44\cdot10^{22}\text{ m}^{-3}$ and initial susceptibility $\chi_{in}=1.048$.

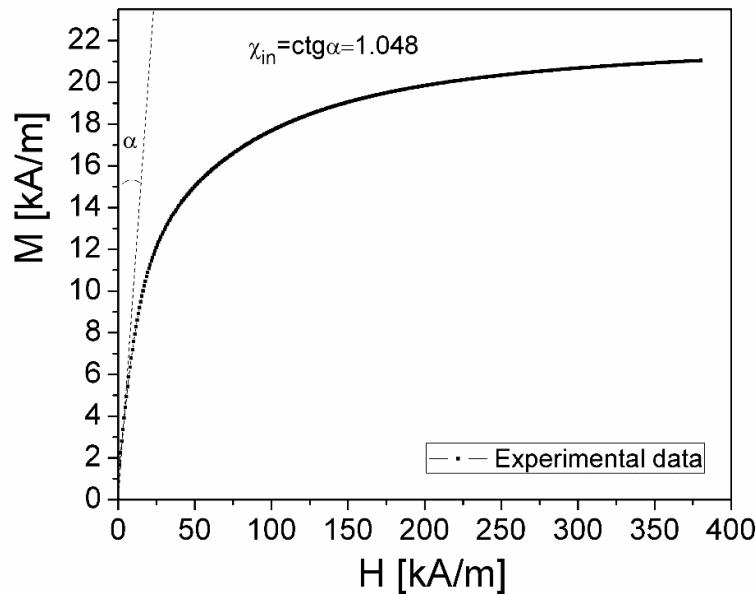


Figure 3. Magnetization curve of the ferrofluid sample.

$\mu(f,H)$ and $\epsilon(f,H)$, of the sample were measured using the short-circuited (SC) or open-circuited (OC) coaxial transmission line technique [27,28], over the frequency range (0.4–7) GHz and at values of H , between 0 to 135 kA/m. For this, we have used a Hewlett Packard (HP) 50W coaxial line incorporating a coaxial cell, containing the ferrofluid sample, in conjunction with the HP 8753C network analyzer [28]. The coaxial cell was placed between the poles of an electromagnet, the axis of cell being perpendicular to the polarizing magnetic field.

4. Results and discussions

Figure 4 shows the dependence on frequency f , and magnetic field H , of the components $\epsilon'(f,H)$ and $\epsilon''(f,H)$ of the complex dielectric permittivity and Figure 5 shows the dependence on frequency f and magnetic field H of the components of $\mu'(f,H)$ and $\mu''(f,H)$ of the complex magnetic permeability of the investigated ferrofluid sample.

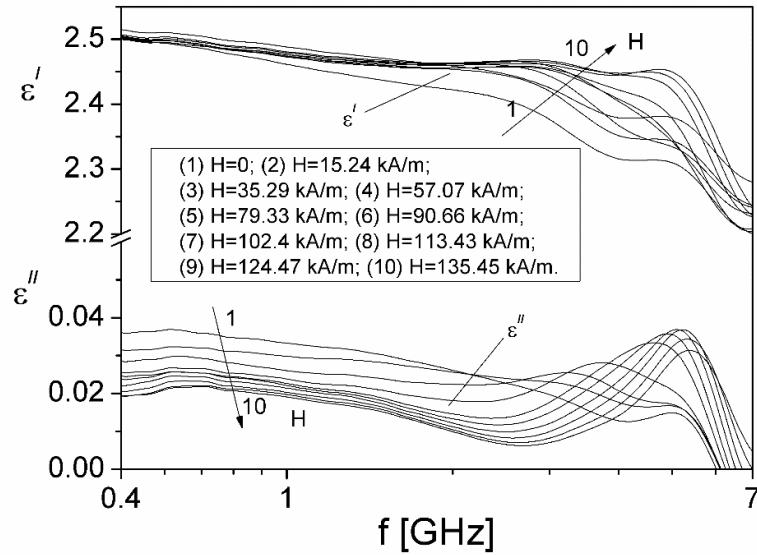


Figure 4. The frequency dependence of the complex dielectric permittivity components of the ferrofluid sample, for 10 different values of polarizing magnetic field, H .

As can be seen from Figure 4, for a constant frequency f , the real component $\epsilon'(f)$ increases between (2.2 - 2.5) with increasing H , and the imaginary component $\epsilon''(f)$ decreases with the increase of H . At the same time, $\epsilon''(f)$ displays a maximum in the frequency range between (3-5) GHz, for each H value of the magnetic polarizing field, which indicates a relaxation process attributed to the interfacial polarization mechanism [29]. Also, the maximum amplitude of the imaginary component $\epsilon''(f)$, of the complex dielectric permittivity increases with the magnetic field for the first seven values of H , and then, for the next 3 values, it decreases with H , this behavior being characteristic of the formation of the particle agglomerations in the ferrofluid sample [30].

From Figure 5, it is observed that the investigated ferrofluid sample presents the ferromagnetic resonance phenomenon, highlighted by the transition of the real part of the complex magnetic permeability, $\mu'(f)$, from a superaunit value to a subunit value at the resonant frequency, f_{res} [8,28]. By increasing the polarizing magnetic field H , the f_{res} frequency moves to higher values from 1.245 GHz (for $H=0$) to 6.170 GHz (at $H=135.45$ kA/m). At the same time, from Figure 5 it is observed that the imaginary component, $\mu''(f)$, has a maximum at the frequency f_{max} , very close to the f_{res} frequency, named the maximum absorption frequency, which moves to higher values with increasing H , from 0.942 GHz (for $H = 0$) to 6.048 GHz (for $H=135.45$ kA/m).

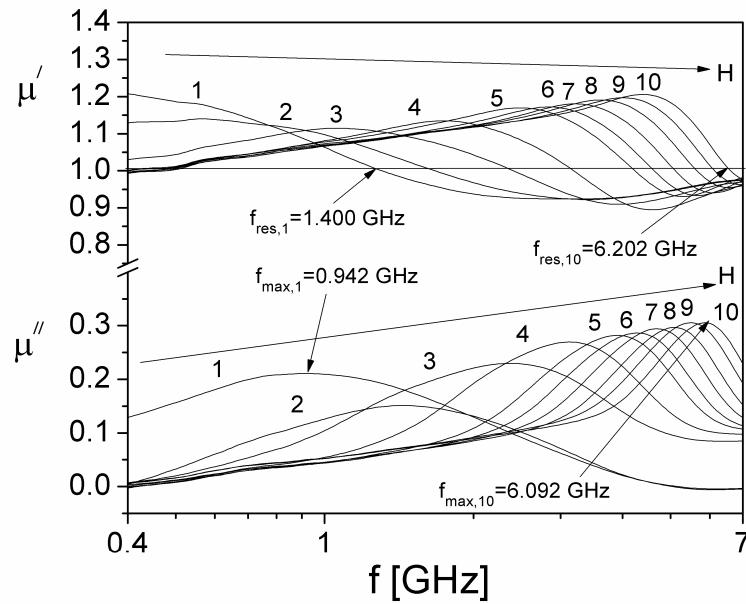


Figure 5. The frequency dependence of the complex magnetic permeability components of the ferrofluid sample, for 10 different values of polarizing field, H , corresponding to, (1) $H = 0$; (2) $H = 15.24$ kA/m; (3) $H = 35.28$ kA/m; (4) $H = 57.07$ kA/m; (5) $H = 79.33$ kA/m; (6) $H = 90.66$ kA/m; (7) $H = 102.40$ kA/m; (8) $H = 113.43$ kA/m; (9) $H = 124.47$ kA/m; (10) $H = 135.45$ kA/m.

Knowing the values of the f_{res} , corresponding to each H value, from Figure 5, we were able to obtain the dependence of f_{res} on H , which is linear, as can be seen in Figure 6, being in accordance with equation (2).

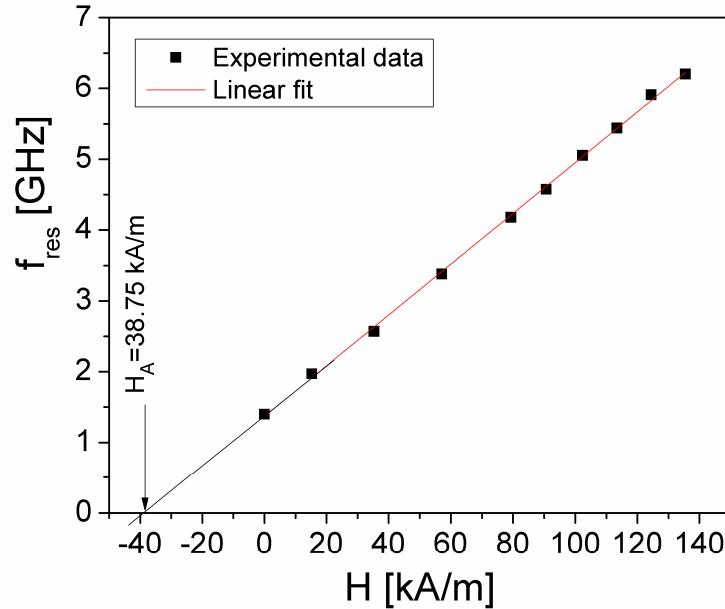


Figure 6. The polarizing magnetic field dependence, of the resonance frequency $f_{res}(H)$, for ferrofluid sample.

By fitting with a straight line, the experimental dependence $f_{res}(H)$ from Figure 6, we were able to determine the anisotropy field H_A and the gyromagnetic ratio of the particle γ ; the values obtained being: $H_A=38.75$ kA/m and $\gamma=2.25 \times 10^5$ s⁻¹A⁻¹m. From Eq (1), we determine that the effective anisotropy constant, $K_{eff}=1.16 \cdot 10^4$ J/m³ which agrees with the values obtained in the literature [31,32] for magnetite particles. Taking into account both the value obtained for γ , and the relation (3) valid for high values of the magnetic field $H>H_A$, we were able to determine the damping parameter of the Landau–Lifshitz equation α_L , and using the value $g=2$, specific to a kerosene-based ferrofluid with magnetite particles [5,8,33], we obtained the value, $\alpha_L=0.194$. As shown in the paper [34], high values obtained for the α_L parameter ($\alpha_L>0.1$) can be due either to the polydispersity of the nanoparticle systems [35], or to the interactions between the particles [36], in presence of a high polarizing magnetic field.

Based on the experimental values obtained for $\epsilon'(f,H)$ and $\epsilon''(f,H)$ (Figure 4) and components $\mu'(f,H)$ and $\mu''(f,H)$ (Figure 5), the frequency dependence of the attenuation constant of the electromagnetic wave, $\alpha(f)$ at different values of magnetic field H , was computed using the Eq. (6). The results are presented in Figure 7.

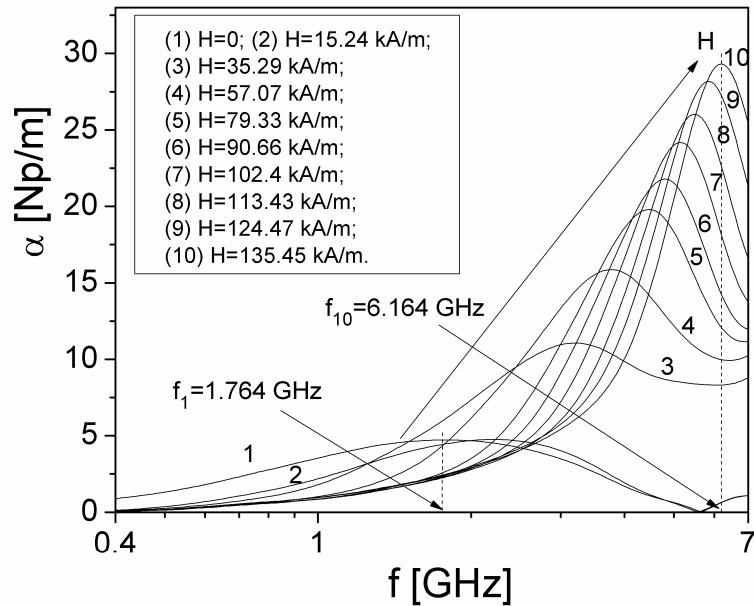


Figure 7. Frequency dependence of the attenuation constant α at different values of polarizing magnetic field, H .

From Figure 7 it is observed that the attenuation constant α , at microwave frequencies in a ferrofluid sample, has a maximum at a frequency f_m , for each value of H , which shifts from 1.764 GHz (for $H=0$) to 6.164 GHz (for $H=135.45$ kA/m). For frequencies less than 1.764 GHz, the attenuation constant α decreases with increasing H and for a frequency greater than 6 GHz, the α increases with increasing H .

Figure 8 shows the dependence of α , on H , at four frequencies, f , of the electromagnetic field, in the range (1–6) GHz. From Figure 8 it is observed that α presents a maximum at a value of H_{max} , which moves to higher values from 40 kA/m (at $f=2$ GHz) to 109 kA/m (at $f=5$ GHz), over the frequency range of (1.764–6) GHz. Also, for $H>H_{max}$, α decreases with increasing H (Figure 8). This result is very useful in magnetically controlled electromagnetic absorbers applications because it provides information on the maximum limit of the magnetic field applied for control of α , at different frequencies.

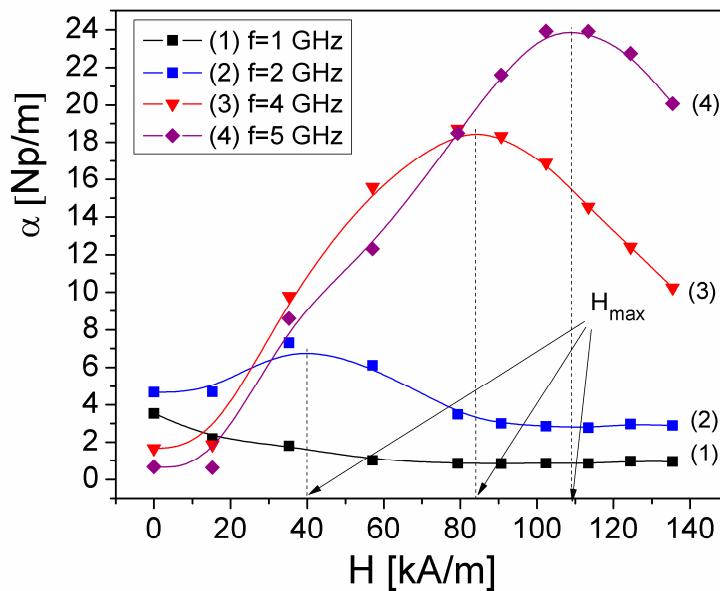


Figure 8. A plot of the attenuation constant α of microwaves in ferrofluid, against the polarizing magnetic field, H , at different frequencies.

Using the Eqs. (8) and (10) and experimental values of the components $\epsilon'(f,H)$ and $\epsilon''(f,H)$ of (Figure 4) and components $\mu'(f,H)$ and $\mu''(f,H)$ of (Figure 5), the frequency dependence of the reflection coefficient at the interface air-ferrofluid, R , at different values of magnetic field H , was computed and the results are presented in Figure 9.

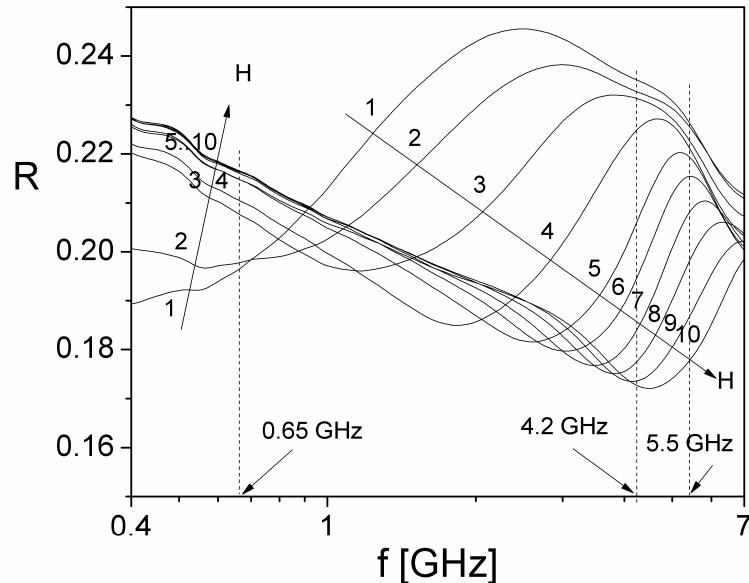


Figure 9. Frequency dependence of the reflection coefficient R at the interface air-ferrofluid for normal incidence at various magnetic field values: (1) 0 kA/m, (2) 15.24 kA/m, (3) 35.29 kA/m, (4) 57.07 kA/m, (5) 79.33 kA/m, (6) 90.66 kA/m, (7) 102.4 kA/m, (8) 113.43 kA/m, (9) 124.47 kA/m, (10) 135.45 kA/m.

As can be seen from Figure 9, for the reflection coefficient at the interface air–ferrofluid for normal incidence $R(f,H)$, two regions of interest for applications are distinguished: the first region corresponding to frequencies lower than 0.65 GHz when $R(f,H)$ increases with the increase of the H field and the second region in the domain of ferromagnetic resonance (4.2 -5.5 GHz), in which $R(f,H)$ decreases with the increase of H . Knowing the values of $R(f,H)$ at the interface air–ferrofluid for normal incidence (Figure 9) and the attenuation constant $\alpha(f, H)$ at microwaves in ferrofluid sample (Figure 7), based on Eq. (22) we calculated the overall reflection coefficient $R_w(f, H)$ for 3 values of the thickness d of the ferrofluid sample: 2mm, 5mm and 10 mm. For the third term in equation (22), in R_{eff} 's calculation, we considered only the terms corresponding to $k=1$ and $k=2$, because for $k \geq 3$, the calculated values decrease very quickly, tending towards zero, being thus negligible. The calculation relations for the third term in Eq. (22) corresponding to the values $k=1, 2, 3, 4$ are as follow:

$$k=1 \quad , \quad T_{3(1)} = R(1-R)^2 \exp[-4\alpha d] \quad (23)$$

$$k=2 \quad , \quad T_{3(2)} = R^2(1-R)^2 \exp[-6\alpha d] \quad (24)$$

$$k=3 \quad , \quad T_{3(3)} = R^3(1-R)^2 \exp[-8\alpha d] \quad (25)$$

$$k=4 \quad , \quad T_{3(4)} = R^4(1-R)^2 \exp[-10\alpha d] \quad (26)$$

In Table 1, the values computed with relations (23) – (26), for $k=1, 2, 3, 4$ corresponding to the frequencies of 2 GHz, 4 GHz and 5 GHz, both in zero field ($H=0$) and in the presence of the magnetic field ($H=135.45 \text{ kA/m}$), are listed, for the three considered thicknesses d of the sample.

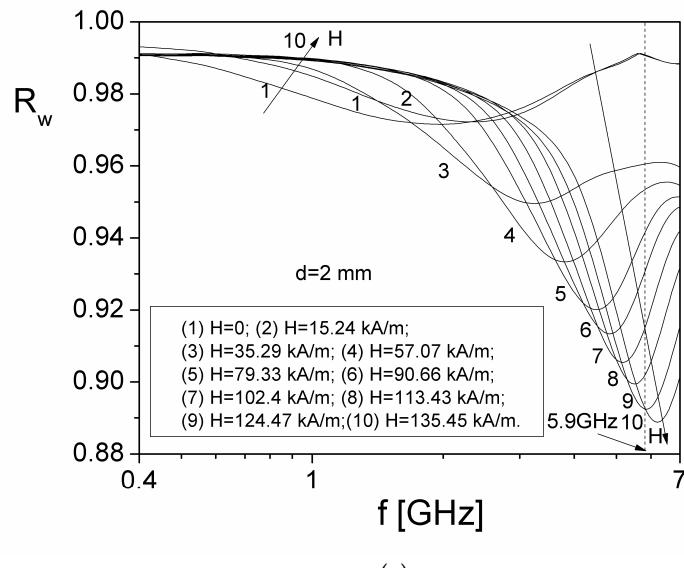
Table 1. The values computed with Eqs. (23) - (26) of the terms $T_{3(1)}$, $T_{3(2)}$, $T_{3(3)}$ and $T_{3(4)}$.

Thickness $s d$		2 mm			5 mm			10mm		
Frequenc y f [GHz]		2	4	5	2	4	5	2	4	5
$T_{3(1)}$ for $H=0$		0.1341 8	0.1359 7	0.1358 2	0.1268 7	0.1332 9	0.1348 3	0.1155 7	0.1289 5	0.1332
$T_{3(1)}$ for $H=135.45$ kA/m		0.1229 1	0.1094 2	0.1005 3	0.1186 2	0.0967 6	0.0781 8	0.1118 0.1118	0.0788 4	0.0514 1
$T_{3(2)}$ for $H=0$		0.0320 3	0.0318 9	0.0312 3	0.0294 5	0.0309 6	0.0308 9	0.0256 0.0256	0.0294 6	0.0303 3
$T_{3(2)}$ for $H=135.45$ kA/m		0.0235 9	0.0182 2	0.0161 8	0.0222 1	0.0152 6	0.0110 9	0.0203 9	0.0111 8	0.0059
$T_{3(3)}$ for $H=0$		0.0076 4	0.0074 8	0.0071 8	0.0068 3	0.0071 9	0.0070 8	0.0056 7	0.0067 3	0.0069 1
$T_{3(3)}$ for $H=135.45$ kA/m		0.0044 9	0.0030 6	0.0025 9	0.0041 9	0.0023 9	0.0015 6	0.0037 2	0.0015 9	0.0006 7
$T_{3(4)}$ for $H=0$		0.0018 2	0.0017 5	0.0016 5	0.0015 9	0.0016 7	0.0016 2	0.0012 6	0.0015 4	0.0015 7

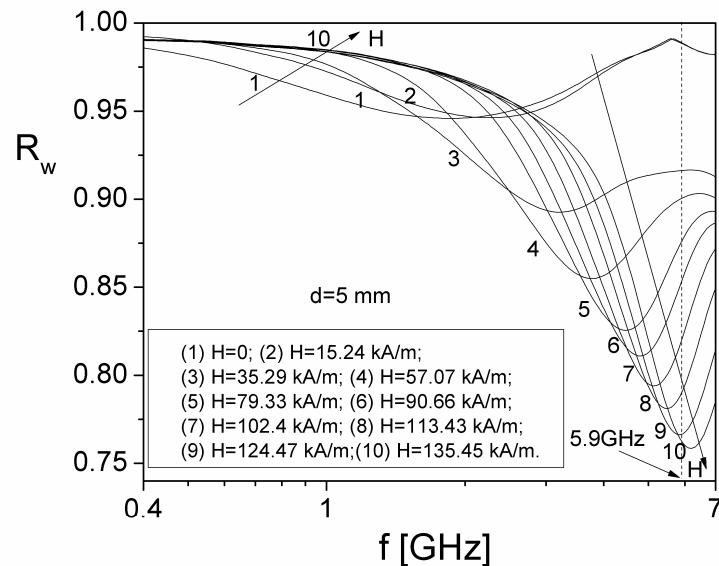
$T_{3(4)}$ for $H=135.45$ kA/m	0.0044 4	0.0029 3	0.0023 8	0.0040 6	0.0021 6	0.0012 7	0.0035 9	0.0012 9	0.0004 4
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From Table 1 it can be seen that the terms $T_{3(3)}$ and $T_{3(4)}$, corresponding to $k=3$ and $k=4$ respectively, are much smaller than the terms $T_{3(1)}$ and $T_{3(2)}$, corresponding to $k=1$ and respectively $k=2$, for all frequencies f and all thicknesses d considered, of the sample, both in the zero field and in the presence of the H field. At the same time, as the thickness of the sample d increases, the value of the terms $T_{3(3)}$ and $T_{3(4)}$, becomes very small close to zero, so that the contribution to the calculation of the R_{eff} parameter, with Eq. (22) of all terms starting with $k \geq 3$, was neglected.

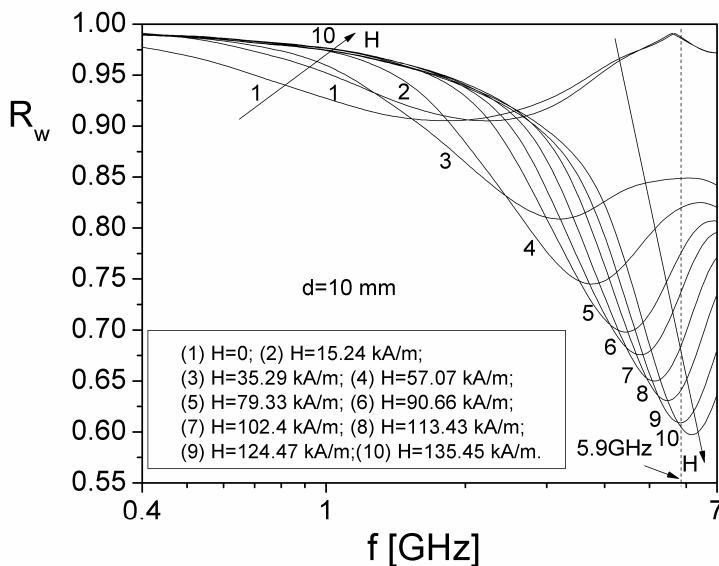
Based on the computations, the overall reflection coefficient R_w , for 3 values of the thickness d of the ferrofluid sample, 2mm, 5mm and 10 mm, the frequency and magnetic field dependencies of the overall reflection coefficient, $R_w(f,H)$, of the ferrofluid deposited on a totally reflective support, for normal incidence, are presented in Figure 10 a), b) and c).



(a)



(b)



(c)

Figure 10. Frequency dependence of the overall reflection coefficient, R_w , at various magnetic field H values for a thickness of ferrofluid, $d=2 \text{ mm}$ (a), $d=5 \text{ mm}$ (b) and $d=10 \text{ mm}$ (c).

From Figure 10 a), b) and c), it can be observed that for all three thicknesses d of the investigated ferrofluid sample, the coefficient $R_w(f, H)$ decreases with the increase of the magnetic field at frequencies higher than 5.9 GHz, while at frequencies below approximately 1 GHz, the overall reflection coefficient, $R_w(f, H)$ increases with increasing H .

Figure 11 shows the dependence of the overall reflection coefficient R_w , on the magnetic field H , at three frequencies, f , of the electromagnetic field, in the range (1–6) GHz, for the three considered thicknesses d of the ferrofluid sample deposited on a totally reflective support, for normal incidence.

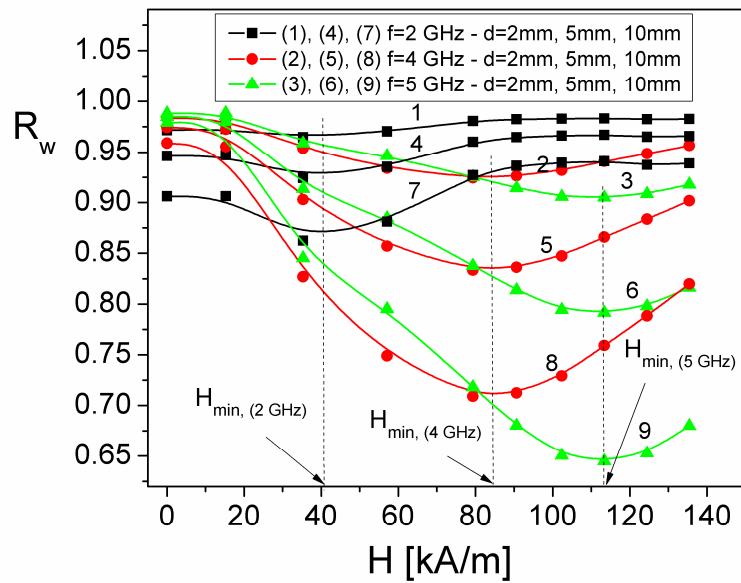


Figure 11. The plot of the overall reflection coefficient, $R_w(f, H)$, against the polarizing magnetic field H , at different frequencies f .

For each frequency f , of the electromagnetic field (2 GHz, 4 GHz and 5 GHz), from Figure 11 it can be observed that with increasing magnetic field, H , the overall reflection coefficient R_w presents a minimum that is accentuated by increasing the thickness d , of the ferrofluid sample. Thus, at $f=2$ GHz, the minimum of R_w appears at the same value of the polarizing magnetic field, $H_{min,(2\text{ GHz})}=40$ kA/m, decreasing from the value 0.93 (for $d=2$ mm) to 0.87 (for $d=10$ mm), while at $f=5$ GHz the minimum of R_w appears at the constant value of the field, $H_{min,(5\text{ GHz})}=109$ kA/m, decreasing from the value 0.90 (for $d=2$ mm) to 0.64 (for $d=10$ mm) (see Figure 11). At the same time, for $H>H_{min}$, R_w increases with increasing H (Figure 11), for any value d of the sample thickness. As a result, obtaining a value as low as possible for the overall reflection coefficient R_w , indicates that the investigated material is a good absorber of the electromagnetic wave. The obtained result is useful in the study of some materials/composite systems with possible absorbing properties in microwaves, by determination of the overall reflection coefficient $R_w(f, H)$ controlled both by the thickness d of the absorber and by the external field H applied, at different frequencies from the range (1-6) GHz.

5. Conclusions

Based on the complex magnetic permeability and complex dielectric permittivity measurements in the microwave frequency range (0.4-7) GHz and in presence of a polarizing magnetic field, H of (0-135) kA/m, for a kerosene-based ferrofluid with magnetite nanoparticles, the ferromagnetic resonance phenomenon was highlighted and the most important propagation parameters of the electromagnetic wave through ferrofluid, were determined: namely the attenuation constant, $\alpha(f, H)$ and the reflection coefficient, $R(f, H)$ at the air-material interface. The dependence $\alpha(H)$ at different frequencies, f , in the range (1-6) GHz shows that the parameter α , presents a maximum at a value of polarizing magnetic field, H_{max} , which moves to higher values from 40 kA/m (at $f=2$ GHz) to 109 kA/m (at $f=5$ GHz), while for $H>H_{max}$, α decreases with increasing H . The obtained result is very important in applications of electromagnetic absorbers because it provides information on the maximum limit of the magnetic field H , for control of attenuation constant α , at different frequencies. Also, in this paper, we defined another parameter, namely the overall reflection coefficient, R_w , of a ferrofluid with thickness d and the attenuation constant α , through which the electromagnetic wave propagates. For this, we proposed a theoretical model for computing the overall reflection coefficient, $R_w(f, H)$ of a

plane wave absorber with a single layer deposited on a perfect conductor, following multiple internal reflections, valid for any material/composite system that has absorbing properties in the microwave range. Using this model, we established for the first time a new equation for the computation of $R_w(f,H)$ for 3 values of the thickness d of the ferrofluid sample: 2 mm, 5 mm and 10 mm, which takes into account, the multiple total reflections of the electromagnetic wave on the reflective metal support, when the wave passes through the ferrofluid. The dependence of $R_w(H)$ at different frequencies, f , in the range (1–6) GHz shows that the parameter R_w presents a minimum at a value of polarizing magnetic field, H_{min} , which moves to higher values from 40 kA/m (at $f=2$ GHz) to 113 kA/m (at $f=5$ GHz), for all values d of thickness of sample, while for $H > H_{min}$, R_w increases with increasing H . On the other hand, at a fixed frequency, such as $f=5$ GHz, the minimum of R_w decreases from 0.90 (for $d=2$ mm) to 0.64 (for $d=10$ mm) which shows an increase in the absorption of the electromagnetic wave in the ferrofluid. The result is very useful in the study of some materials/composite systems that could be used as electromagnetic absorbers in microwave range.

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