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# The Influence of Elevated Temperature on the Efficiency of Photovoltaic Modules

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Research

# Evaluation of the Impact Temperature Variations on the Output Power of Silicon-Based Photovoltaic Modules

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**Abstract:** A widely used material for the photovoltaic (PV) arrays is crystalline silicon. The PV conversion losses of a power plant as a yearly average, include: light reflection losses (3,1%), low radiation and shadowing losses (3,2%), DC board losses (1,2%), DC/AC conversion losses (4%), mismatching losses (5,7%), temperature losses (7,6%). It can be stated that the major fraction of losses is related to the temperature increase of the silicon solar cells. In real operating conditions, solar cells and modules operate at different temperatures, either due to changes in ambient temperature (atmospheric conditions changing with the seasons) and cooling rate, depending on wind speed and insolation, rain, snow, etc., or due to changes in the amount of heat (electrical power lost on the internal resistance of the cell), emitted during their operation. The possibility of operation of these devices in ground applications in the temperature range from -20 to +70°C should be taken into account. The given range, of course, does not apply to operation in the tropics. The detailed studies of the impact of temperature on the electrical parameters of crystalline silicon solar cells have been presented. The theoretical justification of the temperature influence mechanism on the exploitation parameters of the silicon solar cells has been submitted. The better photovoltaic cells and modules, the lower the values of temperature coefficients, in particular, attention should be paid to the decrease in maximum power with increasing temperature. The experimental results were compared with the theoretical predictions and the results, obtained by other authors and producers.

**Keywords:** photovoltaic solar cells; photovoltaic module; efficiency decrease; working temperature

## 1. Introduction

The surface of monocrystalline silicon photovoltaic cells enables almost 90% absorption of radiation and the highest efficiency of photoelectric conversion among silicon cells. The temperature of the cells and modules during operation depends on the intensity of the incident radiation, wind speed, air temperature, thermal properties of the installation components and may rise above 70°C at the irradiance of over 750 W/m<sup>2</sup> [1], and 30°C is reached by a typical building-integrated PV placed on the roof at the ambient temperature of 10.9°C and the radiation intensity of 381 W/m<sup>2</sup> [2].

Poulek et al. [3] determined the frequency of reaching different temperature values of photovoltaic modules during the year for various locations for free-standing and roof-integrated installations. The operating temperature of free-standing PV modules practically does not exceed 70°C in an annual cycle, with the exception of hot climates. However, for roof-integrated installations, the situation is worse: while module temperatures do not exceed 80°C in cold and temperate climates, temperatures of over 80°C for 200 hours have been recorded in hot climates, and peak temperatures of over 90°C have been recorded.

Dubey et al. [4] analyzed the performance of silicon photovoltaic cells and modules as a function of temperature for different locations and found that the efficiency of PV modules decreases with increasing latitude, although for high latitudes the efficiency is higher due to lower temperatures (southern Andes, Himalayan region and Antarctica). Therefore photovoltaic modules with less

sensitivity to temperature are preferable for the high temperature regions and those more responsive to temperature will be more effective in the low temperature regions.

An increase in temperature causes a decrease in PV conversion efficiency, a decrease in electrical output power and other physical parameters.

Thermal effects are described by specifying the NOCT (Nominal Operating Temperature) - the temperature of the module in SRE (Standard Reference Environment) conditions: at the incident radiation intensity of 800 W/m<sup>2</sup>, ambient temperature of 20°C and wind speed of 1 m/s and the temperature coefficients of the determined quantities characterizing electrical parameters of cells and modules.

NOCT is determined based on international standards, e.g. International Standard EN-61215 [5] for modules illuminated with light falling perpendicularly to their surfaces without load. All these standards are based on the fact that the difference between the temperature of the module and the ambient temperature is practically independent of the temperature of the surrounding air and the strength of the wind, and changes in direct proportion to the intensity of the incident radiation. The following conditions do not meet this assumption: incident radiation intensity below 400 W/m<sup>2</sup>, wind speed outside the range of 1±0.75 m/s, ambient temperature outside the range of 20±15°C or its fluctuations greater than 5°C within 10 minutes [5].

The temperature of the module is determined by the relation:

$$t_m = t_{amb} + (NOCT - 20) \cdot \frac{E}{800} \quad (1.1)$$

where E is the intensity of the incident radiation in W/m<sup>2</sup>,  $t_{amb}$  is the ambient temperature.

This relationship does not take into account the construction of the module and the cover material. Based on the standard [5], Alonso Garcia [6] determined the NOCT for the tested commercial modules of monocrystalline silicon photovoltaic cells from various manufacturers, obtaining a value of 49.2±1.1°C. The annual amount of electricity produced by a crystalline silicon photovoltaic module varies across Europe for different orientations (east to west) and tilt angles of the module (horizontal to vertical) as well as the use of modules with different NOCT values.

According to the formula (1.1), the module temperature is higher for modules with a higher NOCT value. The difference in NOCT values by 9°C translates into a difference in module temperature of 11.5°C (at 1000 W/m<sup>2</sup> radiation) [7].

As a result of changing the NOCT value from (NOCT +3°C) to (NOCT-3°C), the annual efficiency of the module increases by 1.3% (data obtained on the basis of simulations using a program developed by CIEMAT). This allows us to conclude that after insolation, the temperature is the second factor determining the output power obtained from the PV module [6].

With the change of temperature, the electrokinetic potential  $kT/e$  changes, and since it is present in most equations describing the properties of PV cells, one can talk about the direct influence of temperature changes on these properties. In the range of very low temperatures of PV cells, the thermal generation of electrons from the baseband to the conduction band practically does not occur, and the impurities are not ionized, so they do not provide charge carriers, i.e. the semiconductor does not conduct, and PV cells do not convert radiation into electric current. Along with the temperature change, the physical properties of the semiconductor material (silicon) from which the silicon cell is made also change. Hence, the relevant properties of PV cells and modules are indirectly changed. The basic physical aspects of the decrease in output power and energy conversion efficiency for silicon photovoltaic elements, related to the increase in temperature, mainly include:

- increase in the frequency and amplitude of crystal lattice vibrations with increasing temperature, leading to an increase in scattering of charge carriers - electrons and holes - on phonons,
- decrease in the mobility of charge carriers  $\mu_n$  and  $\mu_p$  with increasing temperature,
- voltage drop of the built-in p-n junction and its ability to separate electrons from holes in photogenerated pairs due to the very strong temperature dependence of carrier concentration ( $n_i^2$ ).

It should be noted, however, that many different quantities that determine the output electrical parameters of the operation of photovoltaic cells depend on the temperature and only some of them

can be treated as constant (their variability is negligibly small) in the entire operating range, i.e. the practical use of crystalline PV elements. silicon. Others depend on many factors at the same time and the description of their variability using temperature coefficients is insufficient. For example, the recombination rate decreases with increasing temperature, but its value strongly depends on the doping level [8].

The article presents research on the impact of temperature changes on the efficiency of photovoltaic conversion and on those parameters of crystalline silicon photovoltaic cells that have a decisive impact on this conversion. Thermally sensitive operating parameters of solar cells clearly determine the current-voltage characteristics and conversion efficiency of cells illuminated by a natural or artificial light source. The basic task was to perform accurate measurements and present the results of own research against the current state of knowledge on parameters such as: maximum output electrical power, short-circuit current and open-circuit voltage, series resistance, dark current, duty cycle of the current-voltage characteristic, efficiency, photovoltaic conversion of cells, as well as factors limiting the conversion efficiency and, consequently - the electrical power received by the user.

Theoretical considerations are also included regarding physical phenomena and quantum processes that determine the possible values of operating parameters of crystalline silicon photovoltaic cells, taking into account the effects related to heat transport in the cells during their operation.

It has been shown that the theoretical predictions resulting from the analysis of equations describing the mechanisms of photocurrent generation and flow are confirmed by the experimental studies carried out.

## 2. The temperature influence mechanism on the exploitation parameters of silicon solar cells

Quantum efficiency determines the efficiency of energy conversion of incident photons into photoelectric current. Also, determining the influence of the wavelength of the incident radiation on the photocurrent - spectral sensitivity - is a useful tool to determine the suitability of materials used in the production of photovoltaic cells. An increase in the cell temperature affects the spectral sensitivity: a shift of the maximum spectral sensitivity for the short-circuit current for silicon in the infrared range from 950 nm at  $t=5^{\circ}\text{C}$  to 1000 nm at  $t=83^{\circ}\text{C}$  is observed [9]. Shifting the point of maximum sensitivity of the cell with increasing temperature towards longer waves is of particular importance in the case of using anti-reflection optical coatings on the surface of cells operating at high temperatures. Spectral characteristics of the coating should be determined at cell temperature.

The width of the band-gap decreases with the temperature increase. This enables the semiconductor material (silicon) to absorb additional photons with a higher wavelength or - in other words - lower energy (Equation (2.1).) [10]:

$$\Delta\lambda_1 = hc \cdot \left[ \frac{1}{E_g(380K)} - \frac{1}{E_g(300K)} \right] = 1.126\mu\text{m} - 1.107\mu\text{m} = 19\mu\text{m} \quad (2.1)$$

In addition, charge carriers generated deeply inside the material are used more efficiently due to the increased diffusion length. These effects lead to an increase of the photo - current. On the other hand, with decreasing width of the band gap, more charge carriers can surmount the band-gap, just by means of their thermal excitation.

The energy gap  $E_g$  depends on the electronegativity of the atoms that make up the crystal. The  $E_g$  gap, which occurs in the complex band structure of a semiconductor, is formed as a result of splitting the energy levels of isolated atoms (or molecules) when they come together in the process of crystal formation (crystallization). Under given external conditions,  $E_g$  is determined by both the atomic composition and the type of crystal lattice. The existence of an approximately linear relationship between the thermodynamic properties of the lattice, including the enthalpy change, as well as the heat of atomization  $\Delta H$  (network energy), and the energy gap was found empirically:  $E_g = C\Delta H$ , with  $\Delta H = f(T)$  where  $C$  - coefficient of proportionality.

The bandgap width of semiconductors as a function of temperature in a limited temperature range is given by the formula:

$$E_g(T) = E_g(300K) + \left(\frac{dE_g}{dT}\right)(T - 300K) \text{ and } \frac{dE_g}{dT} = -2.3 \cdot 10^{-4} \frac{eV}{K}, \quad (2.2)$$

where  $E_g(300 K)$  is the band gap at 300 K, which for silicon is 1.12 eV [11].

On the other hand, a smaller energy gap can be overcome by a greater number of charge carriers generated by thermal activation, which results in an increase in the reverse saturation current, which is an important diode parameter and determines the change in the working parameters of the cells with temperature. Singh and Ravindra [12] showed that the reverse saturation current increases with increasing temperature, which causes a decrease in  $V_{oc}$ , FF and cell efficiency.

The absorption coefficient  $\gamma$  is closely related to the width of the energy gap, which changes linearly with the temperature in the region close to room temperature. It can be concluded that at higher temperatures, the depth of penetration of the cell material by photons is smaller, and consequently the cell sensitivity decreases with increasing temperature and at shorter wavelengths of the incident radiation [13].

The mobility of charge carriers depends on two factors: on the effective mass of the charge carrier and on their interaction with the lattice, and is strongly related to the concentration of impurities and changes in temperature. In a doped semiconductor, carrier scattering takes place on donors and acceptors that have a large scattering cross section. An increase in the concentration of impurities causes a significant decrease in the mean free path of charge carriers and their mobility. At high temperatures, lattice scattering of charge carriers on phonons plays an important role, and then the effect of impurity concentration is less significant.

Since, as indicated above, both the concentration of intrinsic charge carriers and their mobility depend on temperature, then the resistivity of a semiconductor is also a function of temperature. The effect of temperature change on resistivity is different in different temperature ranges and at different levels of doping. The greater the concentration of impurities, the lower the resistivity and the smaller the change in resistivity with temperature change. At intermediate temperatures in the operating range of photovoltaic cells, the decrease in carrier mobility causes an increase in resistivity. Also significant temperature changes of the Fermi level in this range result in a high temperature coefficient of resistivity.

The open-circuit voltage  $U_{oc}$  of silicon photovoltaic cells is a maximum of 0.72 V and is limited by the effects of spontaneous recombination [14]. It is also strongly dependent on the operating conditions of the silicon cell: both on the characteristics of the radiation incident on the surface of the cell, and on the temperature of this cell. The value of the open-circuit voltage is, apart from the intensity of the incident radiation, important for obtaining the maximum power on the load resistance. The open-circuit voltage as a function of temperature is described by the relation [15]:

$$U_{oc}(T) = U_{oc}(T_0) - \left[ \frac{E_{g0}}{e} - U_{oc}(T_0) \right] \left( \frac{T}{T_0} - 1 \right) - \frac{3kT}{e} \ln \frac{T}{T_0} \quad (2.3)$$

where  $E_{g0}=1.21$  eV is the bandgap width of silicon at 0 K. Assuming that during the operation of the photovoltaic cells their temperature increases to 340 K, then  $\ln \frac{T}{T_0} \approx 0.125$  at  $T_0=300$  K and the factor  $\frac{3kT}{e} \ln \frac{T}{T_0} \approx 10$  mV can be neglected as small compared to  $U_{oc} \approx 550$  mV for silicon (at AM 1.5), and from Equation (2.3) we obtain a linear relationship:

$$U_{oc}(T) \approx U_{oc}(300K) - \text{const}(T - 300K) \quad (2.4)$$

Differentiating Equation (2.2) one obtains the change in open-circuit voltage per one degree change in temperature:

$$\frac{dU_{oc}}{dT} = - \frac{\frac{E_{g0}}{e} - U_{oc}(T_0)}{T_0} - \frac{3k}{e} \cdot \left( \ln \frac{T}{T_0} + 1 \right) \quad (2.5)$$

At the temperature  $T_0 = 300$  K, assuming the typical value [7]  $U_{oc}(T_0) = 0.55V$  for a single-crystalline silicon cell, we obtain from Equation (2.5):



$$\frac{dU_{oc}}{dT} = -2.49 \frac{mV}{K} \text{ or: } \frac{1}{U_{oc}} \cdot \frac{dU_{oc}}{dT} \cong -0.45 \frac{\%}{K} \quad (2.6)$$

i.e. the value of the temperature coefficient in accordance with the one given by Green [16], to which the values declared by the manufacturers of photovoltaic modules can be compared, striving for the lowest possible values.

The electric current (photocurrent) is directly related to the number of photons  $N_\lambda$  of wavelength  $\lambda$  incident on the cell per unit of time and to the quantum efficiency  $\eta_\lambda$ :

$$I_{ph}(\lambda) = \eta_\lambda e N_\lambda [1 - r(\lambda)], \quad (2.7)$$

where  $r(\lambda)$  is the reflection coefficient from the upper surface absorbing the radiation. Introducing the expression for the irradiation power:

$$P_\lambda = N_\lambda \frac{hc}{\lambda} \quad (2.8)$$

from Equation (2.6) we get:

$$I_{ph}(\lambda) = \eta_\lambda \cdot e \frac{P_\lambda \lambda}{hc} \cdot [1 - r(\lambda)] \quad (2.9)$$

and:

$$I_{ph} = \frac{e}{hc} \int_0^{\lambda_g} \eta_\lambda [1 - r(\lambda)] P_\lambda \lambda d\lambda, \quad (2.10)$$

where:  $\lambda_g = \frac{hc}{E_g}$  is the limiting wavelength.

Temperature is one of the decisive factors, both for losses and efficiency of photovoltaic conversion of PV cells. The photovoltaic conversion efficiency is defined as the ratio of the maximum output electric power  $P_{max}$  to the total power of the incident radiation, thus according to the formula (2.10):

$$\eta = \frac{FF \cdot U_{oc} \cdot \frac{e}{hc} \cdot \int_0^{\lambda_g} P_\lambda \eta_\lambda [1 - r(\lambda)] \lambda d\lambda}{\int_0^\infty P_\lambda d\lambda} \quad (2.11)$$

where:  $FF$ - characteristic fill factor:

$$FF = \frac{U_{MPP} \cdot I_{MPP}}{U_{oc} \cdot I_{sc}}. \quad (2.12)$$

The characteristic fill factor is in practice the highest and close to unity for lower irradiation values and lower cell temperature and decreases both with the increase of irradiation and temperature. This is the result of an increase in the series resistance of the cell, associated with an increase in both of these parameters.

The  $FF$  can be determined with sufficient accuracy from the formula given by Green [17]:

$$FF_0 = \frac{\frac{eU_{oc}}{m_{id}kT} - \ln\left(\frac{eU_{oc}}{m_{id}kT} + 0.72\right)}{\frac{eU_{oc}}{m_{id}kT} + 1} \quad (2.13)$$

where  $FF_0$  is here the fill factor of the ideal cell characteristic, and:

$$FF = FF_0 \left(1 - \frac{r_s I_{sc}}{U_{oc}}\right), \quad (2.14)$$

which illustrates the influence of the series resistance  $r_s$  on the fill factor of the characteristic and why the cells show an unexpected degradation of both the open circuit voltage  $U_{oc}$  and the  $FF$  factor at higher series resistances.

According to the formula (2.13), the characteristic fill factor depends on the temperature both directly and indirectly through  $m_{id}$  and  $U_{oc}$ .

As the temperature increases, the silicon band gap  $E_g$  decreases, according to formula (2.2), which allows the absorption of additional photons with a longer wavelength. The charge carriers generated by these lower-energy photons penetrate deeper into the semiconductor - they can be used due to the longer diffusion path. This leads to a slight increase in the short-circuit current  $I_{sc}$ . On the other hand, with decreasing width of the band gap, more charge carriers can surmount the band-gap, just by means of their thermal excitation.

In the range of very low temperatures of PV cells, the thermal generation of electrons from the baseband to the conduction band practically does not occur, and the impurities are not ionized, so they do not provide charge carriers, i.e. the semiconductor does not conduct, and PV cells do not convert radiation into electric current.

### 2.1. Research methodology

Measurement stations were built to test the cells in isothermal conditions in a wide range of temperatures, typical for terrestrial applications, and a hybrid system of a photovoltaic module with a PV/T water solar collector:

- measurement station enabling temperature stabilization and regulation on the entire surface of the tested cell with temperature sensors and computer reading and data acquisition, - a stand for testing solar cells and silicon diodes in an optical darkroom with a temperature control and stabilization system [10],
- station for determining current-voltage characteristics when cells are illuminated with sunlight and artificial light (incident radiation intensity values from 600 to 800 W/m<sup>2</sup>) in the temperature range from 293 K to 353 K [24],
- a monochromator system with an optical darkroom and a halogen light source for measuring the spectral characteristics - the voltage of the open circuit of a crystalline silicon cell as a function of the wavelength of the incident radiation [25],
- a stand for testing the energy efficiency of a hybrid system in which the photovoltaic module is cooled with water [24].

The first experimental stand consisted of a 10 mm thick copper plate, the task of which was to ensure isothermality over the entire surface of the tested elements. The electric heater was powered by a stabilized DC power supply. The measurement of the temperature of the lower and upper surfaces of the tested PV cells or photodiodes was carried out using transistors (MOSFET) with computer reading and recording of data with an accuracy of  $\pm 0.1$  K. The light source was a halogen lamp with a power of 400 W, placed at the focus of the converging lens in order to uniform illumination of the tested elements. A class 0.1 decade resistor with a resistance of  $0.1\Omega$  to  $10k\Omega$  was used as the load resistance  $R_L$ .

At the station for determining the spectral characteristics, the light source was a halogen lamp with a monochromator system. A beam of white light from a halogen lamp, after passing through the monochromator, fell on the tested silicon cell. For different positions of the monochromator mirrors, the dependence of the open circuit voltage  $U_{oc}$  on the wavelength of the incident radiation  $\lambda$  was determined.

In order to determine the operating parameters of the silicon photovoltaic cell module as a function of temperature in the hybrid system, a photovoltaic module, consisting of 72 cells connected in a series-parallel system, was glued to an aluminum plate (3 mm thick), maintaining a distance of 8 mm. The capacity of the space between the cells and the plate was 11.88 dm<sup>3</sup>. Two aluminum stubs were welded to the aluminum plate at the top and bottom to supply and discharge thermostated cooling water, which is the working medium of the thermal collector. The system was built in an aluminum frame. The frame was mounted on wheels and it was possible to adjust the angle of inclination to set it perpendicular to the direction of the sun's rays. The absorber of the module (solar collector) obtained in this way is the dark blue surface of silicon cells placed between two glass plates. To increase this area, a panel with square cells was used, which - although more expensive - provides better space utilization than round cells. Current-voltage characteristics were determined for various values of the intensity of incident solar radiation by simultaneously measuring the water temperature

at the inlet and outlet of the collector using copper-constantan thermocouples with a computer data acquisition system and the flowing water stream.

The obtained results were compared with review articles: [20–22].

## 2.2. Influence of temperature increase on photovoltaic conversion efficiency of a PV cell – obtained results

An increase in temperature reduces the photovoltaic conversion efficiency of all types of solar cells except:

- organic cells, for which a weak maximum conversion efficiency is observed near 40°C,
- amorphous silicon cells (a-Si:H), which after heating have an inverse temperature dependence, i.e. the efficiency increases with the increase of temperature; however, after irradiation, their efficiency decreases again with increasing temperature and stabilizes at a lower level [18]. This Staebler-Wronski degradation effect causes the efficiency to drop to about 40% of the initial value.

Efficiency changes as a function of temperature can be quantified by the coefficient of relative temperature changes in efficiency:

$$\beta = \frac{1}{\eta} \cdot \frac{d\eta}{dT} \quad (2.15)$$

For small temperature changes near 300 K:

$$\eta(T) = \eta(300K) \cdot [1 + \beta(T - 300K)]. \quad (2.16)$$

## 3. Temperature coefficients of working parameters of photovoltaic cells

Measurements of temperature coefficients (TC) using various continuous light sources and the pulsed solar simulator SPIRE 240A were carried out by K. Emery [19]. He represented these coefficients with a common formula (3.1) and (3.2):

$$TC \left[ \frac{\text{unit}}{^{\circ}\text{C}} \right] = \frac{1}{Z} \frac{\partial Z}{\partial T} \Big|_{T_n=25^{\circ}\text{C}} \quad (3.1)$$

$$Z' = Z + \frac{TC \cdot Z(T' - T)}{1 - TC(T_n - T)} \quad (3.2)$$

where Z is the measured parameter.

For crystalline silicon, he obtained the following values on this basis:

$$\frac{1}{P_{max}} \frac{\partial P_{max}}{\partial T} = -0.4 \frac{\%}{^{\circ}\text{C}}, \quad (3.3)$$

$$\frac{1}{U_{oc}} \frac{\partial U_{oc}}{\partial T} = -0.3 \frac{\%}{^{\circ}\text{C}}, \quad (3.4)$$

$$\frac{1}{I_{sc}} \frac{\partial I_{sc}}{\partial T} = 0.025 \frac{\%}{^{\circ}\text{C}}, \quad (3.5)$$

$$\frac{1}{FF} \frac{\partial FF}{\partial T} = -0.15 \frac{\%}{^{\circ}\text{C}}, \quad (3.6)$$

while for example, one of the best: SunPower's solar modules have a power temperature coefficient of -0.34%/°C. This means is that for every 1°C above 25°C, the efficiency of SunPower's solar modules decreases by 0.37%.

King et al. [23] obtained coefficients for crystalline silicon calculated on the basis of measurements in natural conditions of sunlight illumination:

$$\frac{1}{P_{max}} \frac{\partial P_{max}}{\partial T} = -0.52 \frac{\%}{\text{K}}, \quad (3.7)$$



$$\frac{1}{U_{oc}} \frac{\partial U_{oc}}{\partial T} = -0.39 \frac{\%}{K'} \quad (3.8)$$

$$\frac{1}{I_{sc}} \frac{\partial I_{sc}}{\partial T} = 0.03 \frac{\%}{K'} \quad (3.9)$$

which is consistent with the measurements presented in article [10] and by Shell Solar and SOLARTEC manufacturers:

$$\frac{1}{P_{max}} \frac{\partial P_{max}}{\partial T} = -0.45 \frac{\%}{K'}. \quad (3.10)$$

Based on the data collected by a group of specialists from the University of Opole [24], the value of the open-circuit voltage temperature coefficient for silicon photovoltaic cells is:

$$\frac{1}{U_{oc}} \frac{\partial U_{oc}}{\partial T} = -0.352 \frac{\%}{K'} \quad (3.13)$$

which is consistent with the measurements presented in the article [10]:  $-0.38 \frac{\%}{K}$  and the data of the manufacturer Astro Power: also  $-0.38 \frac{\%}{K}$ .

The temperature coefficient of mobility of electrons and holes for silicon is, [11]:

$$\frac{d\mu_n}{dT} = -1.6 \cdot 10^{-4} \frac{m^2}{V \cdot s \cdot K'} \quad (3.11)$$

$$\frac{d\mu_p}{dT} = -4.3 \cdot 10^{-4} \frac{m^2}{V \cdot s \cdot K'} \quad (3.12)$$

which means that the mobility of carriers decreases monotonically with increasing temperature.

The temperature does not have a significant effect on the short-circuit current density [18], because, as results from the measurements of a single-crystalline silicon cell [10]:

$$\frac{1}{I_{sc}} \cdot \frac{\partial I_{sc}}{\partial T} = 3 \cdot 10^{-4} K^{-1}, \quad (3.13)$$

which is consistent with the measurements of Hall [18] and the cell manufacturer SOLARTEC, which states:  $9 \cdot 10^{-4} K^{-1}$  and the value provided by Shell Solar:  $4 \cdot 10^{-4} K^{-1}$  [26].

On the basis of measurements made in laboratory in a thermostatic system the temperature coefficient of efficiency for silicon solar cells, according to the Equation (2.16), the following was obtained:  $\beta = -8 \cdot 10^{-3} K^{-1}$  [27,28].

#### 4. Conclusions

Since solar energy is a clean, pollution-free and inexhaustible source of energy, research into photovoltaic power generation systems has received a lot of attention, especially in many terrestrial applications. In addition, due to the continuous reduction of production costs of photovoltaic modules and increasing their efficiency, the PV power generation system seems to be one of the comparable candidates for the energy source for humanity in the near future.

The physical aspect of the decrease in the efficiency of photovoltaic cells with increasing temperature involves two main factors: increase in the amplitude of crystal lattice vibrations, hindering the flow of charge carriers by reducing their mobility and loss of ability to separate photogenerated charges by the joint. The first factor limits the use of silicon cells already at room temperature, because then they work below their maximum efficiency.

The article showed a direct negative impact of temperature increase on individual parameters and the output power obtained as a result.

Solar cells and photovoltaic modules work best at a certain temperature, characteristic of the material from which they are made. Silicon is a good photovoltaic material at temperatures close to or below 298 K, at high temperatures the conversion efficiency of the cell decreases so that at 473 K it drops to 5% of the value corresponding to 298 K.

Due to the significant temperature dependence of the conversion efficiency of the silicon module, its cooling is beneficial as it results in the removal of the total thermal energy from absorption

of those photons that are not involved in the generation of electron-hole pairs, indirect and direct pair recombination and Joule's heat of the photoelectric current.

The obtained results provide practical advice for designers and users of photovoltaic installations, clearly indicating that it is beneficial to reduce the operating temperature of photovoltaic cells by cooling them. An effective way to counteract this unfavorable phenomenon is to remove thermal energy, which reduces their temperature and, consequently, increases the output power. It is worth considering the use of hybrid systems in which photovoltaic cell modules are cooled by water or air, and the heat carried by the cooling medium can be used in heating or air conditioning of buildings.

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## References

1. Garcia Alonso M.C., Balenzategui J.L., Estimation of photovoltaic module yearly temperature and performance based on Nominal Operation Cell Temperature calculations, *Renewable Energy* **2004**, Vol. 29, p. 1997; DOI: 10.1016/j.renene.2004.03.010.
2. Lee, W.M. and Infield, D.G. and Gottschalg, R. *Thermal modelling of building integrated PV systems*. In: 17<sup>th</sup> European Photovoltaic Solar Energy Conference and Exhibition, Munich, Germany, **2001**.
3. Poulek V. et al., Influence of increased temperature on energy production of roof integrated PV panels, *Energy & Buildings* **166** (2018) 418–425, DOI: 10.1016/j.enbuild.2018.01.063.
4. Dubey S., Sarvaiya J.N., Seshadri B., Temperature Dependent Photovoltaic (PV) Efficiency and Its Effect on PV Production in the World - A Review, *Energy Procedia* **33** (2013) 311 – 321, DOI: 10.1016/j.egypro.2013.05.072.
5. NORME INTERNATIONALE CEI IEC INTERNATIONAL STANDARD **61215**, Second edition 2005-04; [https://www.google.com/url?sa=t&rct=j&q=&esrc=s&source=web&cd=&ved=2ahUKEwih76u-7-CAAxU8FBAIHXXKRBLsQFnoECBMQAQ&url=https%3A%2F%2Fwebstore.iec.ch%2Fpreview%2Finfo\\_iec61215-1%257Bed2.0.RLV%257Den.pdf&usg=AOvVaw2-ksPDBkLl9Zcu9qay-k6y&opi=89978449](https://www.google.com/url?sa=t&rct=j&q=&esrc=s&source=web&cd=&ved=2ahUKEwih76u-7-CAAxU8FBAIHXXKRBLsQFnoECBMQAQ&url=https%3A%2F%2Fwebstore.iec.ch%2Fpreview%2Finfo_iec61215-1%257Bed2.0.RLV%257Den.pdf&usg=AOvVaw2-ksPDBkLl9Zcu9qay-k6y&opi=89978449) (accessed on 16 August 2023)
6. Garcia Alonso M.C., Balenzategui J.L., Estimation of photovoltaic module yearly temperature and performance based on Nominal Operation Cell Temperature calculations, *Renewable Energy* **2004**, Vol. 29, p. 1997; DOI: 10.1016/j.renene.2004.03.010
7. Bücher K., Kleiss G., Bätzner D., Photovoltaic Modules in Buildings: Performance and Safety, *Renewable Energy* **1998**, Vol. 15, p. 545; DOI: 10.1016/S0960-1481(98)00222-5
8. Macdonald D.H., Cuevas A., The trade-off between phosphorous gettering and thermal degradation in multicrystalline silicon, *16<sup>th</sup> European Photovoltaic Solar Energy Conference and Exhibition*, United Kingdom, Glasgow, 1-5 May **2000**, p. 1707.
9. Mosalam Shaltout M.A. i in., The temperature dependence of the spectral and efficiency behavior of Si solar cell under low concentrated solar radiation, *Renewable Energy* **2000**, Vol. 21 p. 445, DOI: 10.1016/S0960-1481(00)00075-6.
10. Klugmann-Radziemska E., Klugmann E.; Thermally Affected Parameters of the Current-Voltage Characteristics of Silicon Photocell, *Energy Conversion and Management* **2002**, Vol. 43/14 p. 1989; DOI: 10.1016/S0196-8904(01)00132-7.
11. Wolf H.F., *Semiconductors*, New York: Wiley-Interscience; First Edition, **1971**.
12. Singh P., Ravindra N.M., Temperature dependence of solar cell performance - an analysis, *Solar Energy Materials & Solar Cells* **101** (2012) 36–45, DOI:10.1016/j.solmat.2012.02.019.
13. Woronkova E.M. et al., *Optical materials for infrared technique*, Moscow: Nauka, **1965**.
14. Kerr M.J., Cuevas A., Campbell P., Limiting efficiency of crystalline silicon solar cells due to Coulomb-enhanced Auger recombination, *Progress in Photovoltaics: Research and Applications* **2003**, Vol. 11/2, p. 97-104; DOI: 10.1002/pip.464.
15. Carlson D., *Low-cost Power from Thin-Film PV*, Electricity, Ed. by Lund University Press, Lund **1989**.
16. Green M.A., *Solar Cells*, University of New South Wales, Kensington, UK **1992**.
17. Markvart T., Castanër L., *Practical Handbook of Photovoltaics*, Elsevier **2003**.
18. Shimizu T., Staebler-Wronski Effect in Hydrogenated Amorphous Silicon and Related Alloy Films, *Japanese Journal of Applied Physics* (2004) Vol. 43 pp. 3257-3268, DOI: 10.1143/JJAP.43.3257.
19. Emery K. et al., Temperature dependence of photovoltaic cells, modules and systems, *Conference Record of the Twenty Fifth IEEE Photovoltaic Specialists Conference - 1996*, Washington, DC, USA, **1996**, pp. 1275-1278, DOI: 10.1109/PVSC.1996.564365.

20. Singh P., Ravindra N.M., Temperature dependence of solar cell performance - an analysis, *Solar Energy Materials & Solar Cells* 101 (2012) 36–45, DOI:10.1016/j.solmat.2012.02.019
21. Sun Ch., Zou Y., Caiyan Qin C., Zhang B., Wu X.; Temperature effect of photovoltaic cells: a review; *Advanced Composites and Hybrid Materials* (2022) 5:2675–2699, DOI: 10.1007/s42114-022-00533-z
22. Dhass A. D., Natarajaa E., Lakshmi P.; An Investigation of Temperature Effects on Solar Photovoltaic Cells and Modules; *IJE TRANSACTIONS B: Applications* Vol. 27, No. 11, (November 2014) 1713-1722; DOI: 10.5829/idosi.ije.2014.27.11b.09
23. King D.L., Kratochvil J.A., Boyson W.E., Stabilization and performance characteristics of commercial amorphous-silicon PV modules, Technical Report 04/2000, Sandia Laboratories ([www.sandia.gov/pv](http://www.sandia.gov/pv))
24. Rodziejewicz T., Źdanowicz T., Ząbkowska- Waławek M., Cheap Sensor Made of Multicrystalline Silicon for Insolation and Temperature Measurements, *Ecological Chemistry and Engineering S* **2016**, 23(4), DOI: 10.1515/eces-2016-0041.
25. Hall R.N., Silicon photovoltaic cells, *Solid-State Electronics*, Vol. 24(7), **1981**, pp. 595-616, DOI: [10.1016/0038-1101\(81\)90188-X](https://doi.org/10.1016/0038-1101(81)90188-X).
26. Solar - Shell Sustainability Report 2021 <https://reports.shell.com> (accessed on 21<sup>th</sup> August 2023)
27. Klugmann E., Klugmann-Radziemska E., Lewandowski W.M., Influence of temperature on conversion efficiency of a solar module working in photovoltaic PV/T integrated system, 16<sup>th</sup> European Photovoltaic Solar Energy Conference and Exhibition, United Kingdom, Glasgow, 1-5 May **2000**, p. 2406.
28. Klugmann-Radziemska E.; The Effect of Temperature on the Power Drop in Crystalline Silicon Solar Cells, *Renewable Energy* **2003**, Vol. 28/1 pp. 1-12, DOI: 10.1016/S0960-1481(02)00015-0.

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