

Article

Not peer-reviewed version

---

# Effect of Hole Size on Open Hole Tensile (OHT) and Flexural Strength (OHF) of Aramid-Basalt Fibre Reinforced Polymer Composites

---

Oshin Fernandes , Jyoti Dutta , [Yogeesha Pai](#) \* , Mahesha G T , [Ravishanker Baliga](#)

Posted Date: 2 November 2023

doi: 10.20944/preprints202311.0136.v1

Keywords: Open hole tensile test; Hybrid composite; Damage mechanism; Hole diameter; SEM



Preprints.org is a free multidiscipline platform providing preprint service that is dedicated to making early versions of research outputs permanently available and citable. Preprints posted at Preprints.org appear in Web of Science, Crossref, Google Scholar, Scilit, Europe PMC.

Copyright: This is an open access article distributed under the Creative Commons Attribution License which permits unrestricted use, distribution, and reproduction in any medium, provided the original work is properly cited.

Disclaimer/Publisher's Note: The statements, opinions, and data contained in all publications are solely those of the individual author(s) and contributor(s) and not of MDPI and/or the editor(s). MDPI and/or the editor(s) disclaim responsibility for any injury to people or property resulting from any ideas, methods, instructions, or products referred to in the content.

## Article

# Effect of Hole Size on Open Hole Tensile (OHT) and Flexural Strength (OHF) of Aramid-Basalt Fibre Reinforced Polymer Composites

Oshin Fernandes, Jyoti Dutta, Yogeesh Pai <sup>\*</sup>, Mahesha G T and Ravishanker Baliga B

Department of Aeronautical and Automobile Engineering, Manipal Institute of Technology, Manipal Academy of Higher Education (MAHE), Manipal, Karnataka, India- 576 104

<sup>\*</sup> Correspondence: yogish.pai@manipal.edu; Tel.: (+91-9916953709)

**Abstract:** The open hole tensile and flexural test of composites holds immense importance in aerospace and structural engineering. These tests provide critical insights into how composites perform under real-world conditions, allowing for the development of materials that meet rigorous standards, thereby ensuring the safety and durability of aircraft and other applications. This study investigates the influence of hole size on the open hole tensile (OHT) and flexural properties (OHF) of plane woven aramid/epoxy (AFRP), basalt/epoxy (BFRP), and aramid-basalt/epoxy (ABFRP) sandwiched laminates. Specimens with three different hole sizes viz., 4 mm, 6 mm, 8 mm were prepared and tested according to ASTM D5766 and ASTM D7264 for OHT and OHF performance respectively. Results indicated that the hybridization of aramid-basalt layers in a sandwich lay up significantly improved the mechanical performance when compared to only aramid laminate. However, with the increase in hole size the mechanical properties declined irrespective of the material. Basalt fibres showed higher hole sensitivity under tensile loading due to its brittle fracture mechanism while aramid fibres exhibited higher hole sensitivity under flexural loading which can be attributed to its the poor compressive strength. The effect of hole size on the damage mechanism has also been highlighted through scanning electron microscope (SEM). Major failure modes observed are delamination around the hole edges, ductile and brittle fibre fractures, and delamination.

**Keywords:** open hole tensile test; hybrid composite; damage mechanism; hole diameter; SEM

## 1. Introduction

Over the recent years, there has been substantial attention in the field of materials science, and aircraft applications, towards fiber-reinforced composites owing to their superior strength and stiffness-to-weight ratios in contrast to conventional materials such as metals or alloys[1–3]. In addition, the growing concern for environmental issues and regulations by authorities has promoted the employment of eco-friendly fibres in polymer reinforced composites. This development has given way to the emergence of a relatively novel category of hybrid materials, incorporating both synthetic and natural fibers or blends of different natural fibers, with the objective of producing eco-friendlier composite materials[4–6]. The natural, eco-friendly basalt fibres have recently gained attention as a potential substitute for glass or carbon reinforcements and are found in volcanic rocks originating from frozen lava[7,8]. This new generation of basalt fibers boasts advantageous characteristics such as effective sound insulation, superior heat resistance surpassing that of glass, robust resistance against chemical exposure, and minimal water absorption[9,10]. The impressive mechanical strength of basalt fibers, coupled with their cost-effectiveness, positions this material as a potential alternative to glass fibers in diverse industrial sectors such as aerospace, automotive, transportation, and shipbuilding[11–13]. Unfortunately, the exceptional stiffness and strength of these composites are accompanied by reduced toughness[14–17]. Given the urgent demand for innovative lightweight materials with enhanced toughness, there is a resurgence in research interest surrounding the concept

of "hybridization"[18,19]. Hybrid composites are produced by incorporating multiple types of fibers into a single matrix, yielding a novel material with exceptional characteristics. These hybrid composites showcase unique attributes that can effectively address a variety of conflicting design needs in a more economically efficient manner than traditional composites[20,21]. Previous investigations have revealed that impact properties of basalt fibres can be enhanced by incorporating aramid fibres which have higher ductility[22–25].

Hybrid composite structures reinforced with aramid and basalt have found extensive applications in aerospace, military, protective apparel, and marine industries. However, one of the primary factors affecting the design of composite structure is the load carrying capacity of the composite joints. Mechanical joints such as bolts, pins, screws, and rivets are the preferred choice for assembling primary structural composite components[26–28]. These joints require notches such as holes and slots to be drilled into the structures during practical applications to install necessary components. Holes may also form during the service life of the component due to impact damage. Hence, holes in composites create structural weaknesses, leading to reduced strength and shorter service life due to stress concentration near the notched areas[29,30]. Ensuring safety and dependability in service makes it imperative to accurately measure residual properties and assess failure responses. Bandaru et al.[31] examined the influence of hybridization on the mechanical performance of polypropylene composites embedded with Kevlar and basalt fibres. According to the authors, hybridization enhanced the tensile behavior and increased the tensile modulus by 13.77% in comparison to Kevlar laminates. Sarasini et al.[32–34] studied the impact behavior of epoxy composites reinforced with carbon/basalt, glass/basalt, and aramid/basalt fibres. The findings revealed that hybrid laminates with a sandwich-like structure (intercalated) displayed enhanced flexural performance and greater absorption of impact energy compared to non-hybrid configurations. Previous studies have demonstrated that hybrid laminates with aramid fibres as outer plies are better at withstanding delamination damage when exposed to impact loads. This is in contrast to inner aramid plies, which are less effective in this regard[35]. Adding aramid layers as surface plies can provide protection to the primary load-bearing basalt plies (0°/90°) against impact damage[36]. In the event of an impact, the external aramid layer disperses the damage across a wider surface area starting from the impact point, effectively managing the risk of delamination within the plies. Pai et al.[37] explored the mechanical strengths of aramid-basalt/epoxy sandwich laminate with different orientation angle of surface aramid layer. The findings indicated that aramid fabrics positioned on the surface with a (0°/90°) orientation displayed superior mechanical properties when compared to alternative orientations. As a result, creating hybrid composites that incorporate these two types of fibers can effectively achieve a favorable equilibrium among tensile, flexural, and impact properties. Although several studies have investigated the mechanical properties of aramid-basalt hybrid composite, only a limited number of studies have documented the open-hole tensile (OHT) behavior and the mechanisms of failure in hybrid composites. Currently, as the use of brittle-toughness fibre structures and fabric reinforcements continues to expand, there is a need for further research. This study is crucial for gaining a deeper understanding of how these structures perform under open-hole conditions, ultimately ensuring their safety and reliability during service.

A primary limitation of FRP composites lies in their vulnerability to out-of-plane forces and the reduction in strength when subjected to notches and holes [38]. Numerous research endeavors have delved into examining the strength and failure patterns in laminated composites under open-hole tension conditions. These investigations encompass aspects such as fiber orientations, stacking order, ply thickness, and machining methods, all of which impact the composite's mechanical properties[39–42]. Previous research into notched laminates has primarily concentrated on attributes related to the notches, encompassing aspects such as their quantity, hole profile, and dimensions. Cunningham et al.[43] explored how the arrangement of holes influenced the tensile behavior of laminates reinforced with glass fiber. Beyene et al.[44] explored how different notch configurations, including circular holes, transverse ellipses, longitudinal ellipses, and slot geometry, affected the flexural performance of glass/epoxy composites. The study revealed that notch geometry with sharp curvature changes, such as the rectangular slot geometry, results in greater stress concentration. This, in contrast to circular geometry, leads to a higher loss of strength. Yu et al.[45] investigated the OHT

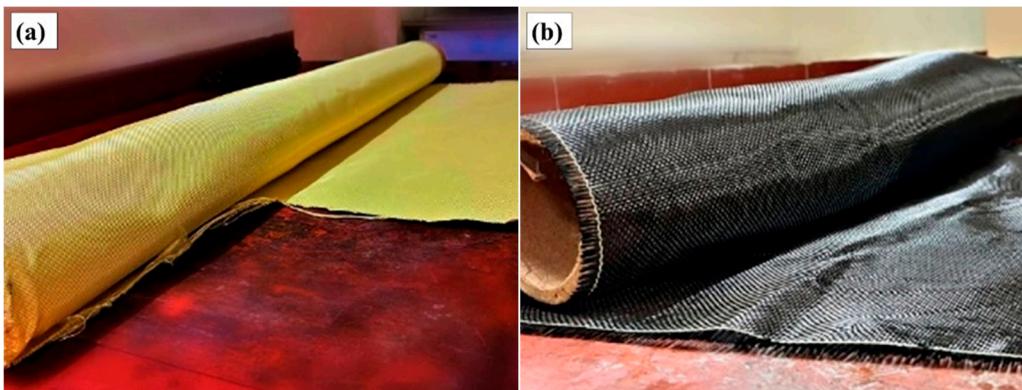
behavior and failure mechanisms in carbon/epoxy, glass/epoxy and carbon-glass/epoxy hybrid laminates. The outcomes revealed that the incorporation of glass fibers into carbon/glass hybrid composites led to a notable enhancement in fracture strain and strength when compared to carbon fiber composites alone. The addition of glass fiber layers also altered the failure modes in hybrid structures, effectively impeding the rapid propagation of cracks. Belgacem et al.[46] investigated how varying the diameter of notches and the number of plies affected the mechanical characteristics of interply epoxy composites reinforced with carbon and glass fibres. The outcomes indicated that the decrease in ultimate strength of the samples correlated with the rise in the geometric ratio (notch size/width). Additionally, the performance of the composites declined with an increasing number of glass layers. Sun et al.[47] studied the open hole tensile performance of carbon/epoxy and basalt/epoxy composites with different hole sizes. The author concluded that large hole sizes resulted in significant strength reduction. Shaari et al.[48,49] studied the OHT behavior of Kevlar-glass/epoxy laminates with various hole sizes and stacking sequences. Results indicated that the hybrid specimens with alternate layers of fibre improved the bonding between the lamina and thus increased the tensile characteristics. In addition, it was reported that the failure mechanism changed with increase in hole size with more delamination zone around larger holes. TA sebaey[50] studied the flexural characteristics of notched carbon-aramid/epoxy laminates for five-hole diameters using a four-point bending test and concluded that the hybridization methodology affected the flexural response.

Studying the mechanical behaviors of open-hole hybrid laminates under different loading conditions remains a challenging task, mainly because of the intricate nature of their damage mechanisms and failure modes. To the authors best knowledge, the mechanical behavior of aramid-basalt/epoxy hybrid interply laminate with drilled hole has not been explored in the existing research. Therefore, this paper outlines experimental studies on the tensile and flexural behavior of epoxy composites reinforced with aramid and basalt fibres, containing open hole (OH). Three different composite systems were considered for the study viz., aramid laminate (AFRP), basalt laminate (BFRP) and interply aramid-basalt hybrid laminate (ABFRP), in which a core of basalt layers is sandwiched between layers of aramid fibre. Three different hole diameters viz. 4 mm, 6 mm and 8 mm are examined to study the influence of hole size on the tensile and flexural properties of the manufactured laminates. Further the damage modes of the fractured specimens have also been discussed.

## 2. Materials and Testing Procedure

### 2.1. Materials and Fabrication

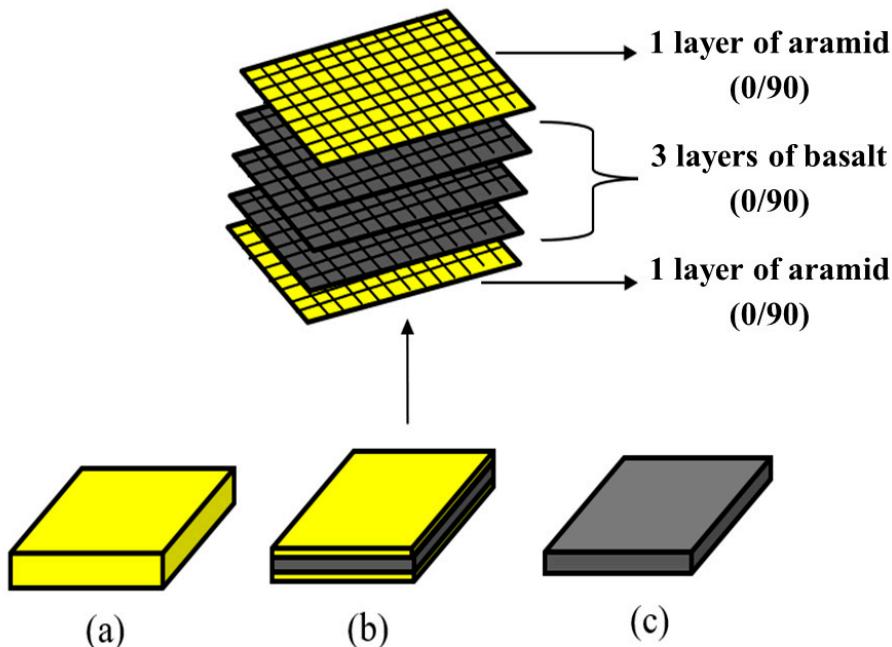
The materials used for the composite fabrication are plain woven bidirectional (2-D) basalt and aramid fabrics as shown in Figure 1, while the binding materials used are CT/E 556 liquid epoxy resin, and CT/H 951 hardener. The materials were supplied by M/S Composite Tomorrow, Gujarat, India. The Material details are provided in Table 1. The resin and hardener were mixed in the ratio of 100:10 and applied to the fabrics by hand lay-up followed by compression molding process. The five layered composite fabrication was carried out on a mild steel plate with dimensions of 350 x 350 mm. Thick metallic spacers were kept on all four sides of the plates to maintain a thickness of 2.8 mm. Three different laminates were fabricated viz., basalt/epoxy laminate (BFRP), aramid/epoxy laminate (AFRP) and aramid-basalt/epoxy interply hybrid laminate (ABFRP) as depicted in Figure 2. The ABRP comprised of a core of three layers of basalt fibres sandwiched between surface aramid piles. The laminates were retained under compression molding machine for a curing period of 24 hours at room temperature. The detailed process of fabrication and the computation of void percentage of the laminates have been previously documented in[25].



**Figure 1.** Plain woven bidirectional fabrics (a) aramid (b) basalt.

**Table 1.** Physical properties of the reinforcements and matrix used.

Material	Surface Density (g/m <sup>2</sup> )	Density (g/cm <sup>3</sup> )	Elastic modulus (GPa)
Basalt	400	1.44	89
Aramid	480	2.8	>72
Resin (CT/E 556)	-	1.15	-
Hardener (CT/H 951)	-	0.97	-

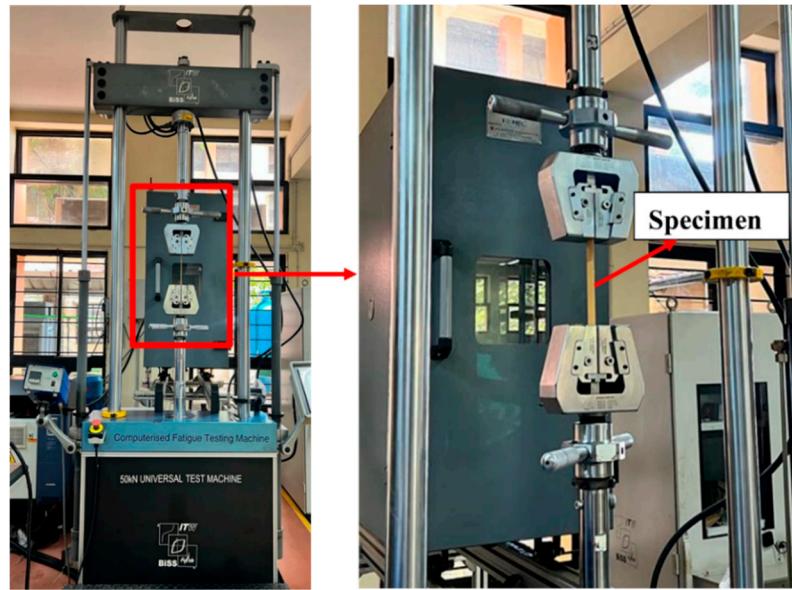


**Figure 2.** Schematic of five layered laminates (a) AFRP (b) ABFRP and (c) BFRP.

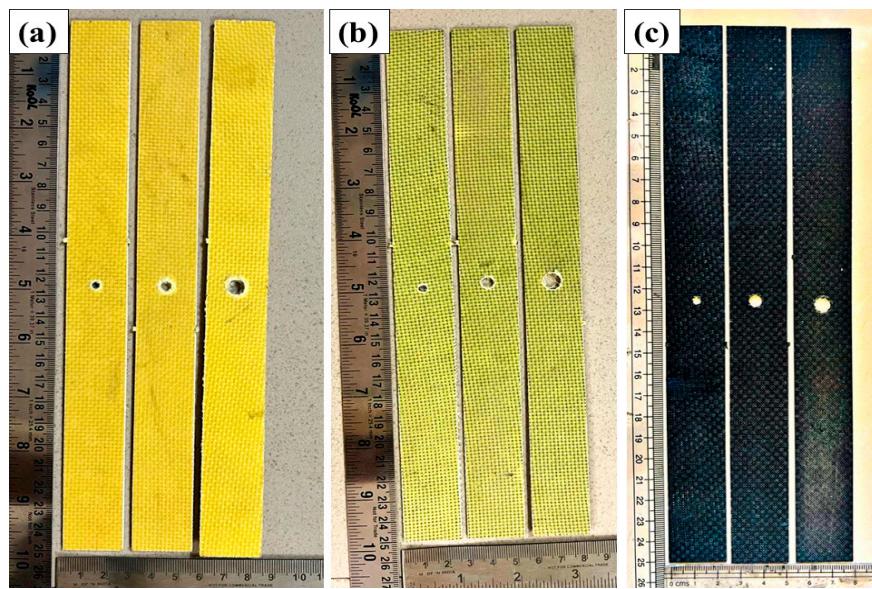
## 2.2. Tensile test set up

Tensile testing was conducted using an Indian-manufactured BiSS Universal Testing Machine (UTM) with a maximum loading capacity of 50 kN, as shown in Figure 3. Specimens were cut following the guidelines outlined in the ASTM D3039[51] and ASTM D5766[52] standard. The span dimension remained fixed at 150 mm, and the overall dimensions of the specimens were 250 mm in length and 25 mm in width. A circular shaped open hole with the diameters, viz., 4, 6 and 8 mm were drilled at the centre of each sample as shown in Figure 4. The crosshead speed was maintained at a

constant rate of 2 mm/min. The Data Acquisition System was employed to record both the applied force and specimen elongation, allowing for the subsequent calculation of the corresponding tensile properties. Five specimens were considered for test in each hole category.



**Figure 3.** Tensile test setup.



**Figure 4.** OHT specimens (a) AFRP (b) ABFRP and (c) BFRP for three different hole diameters of 4 mm, 6 mm and 8 mm respectively.

### 2.3. Flexural test setup

The three point bending test was conducted following the ASTM D7264[53] and ASTM D790[54] standard, using an Indian-manufactured UNITEK-9450 Universal Testing Machine (UTM) with a maximum loading capacity of 50 kN as illustrated in Figure 5. A total of five specimens in each hole category, with a standard span to thickness ratio of 32:1 and 25 mm in width, were subjected to the experiment. The overall length was maintained at 20% greater than span length. A circular shaped open hole with diameters viz., 4, 6 and 8 mm were drilled at the centre of each sample as shown in Figure 6. The flexural coupons were securely positioned between a pair of supports, and a centrally applied load at a rate of 1 mm/min was applied at the midpoint of the specimen. The displacement at the loading point was measured, and the corresponding flexural properties were calculated.

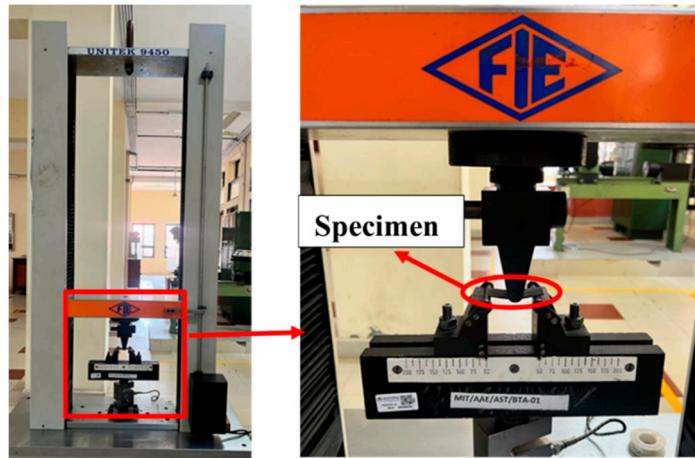


Figure 5. Three-point bending test set up.

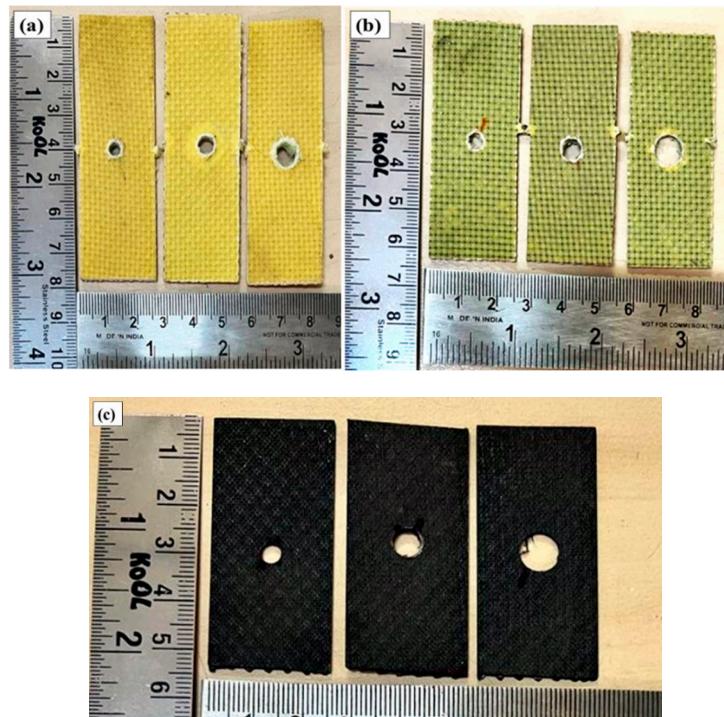
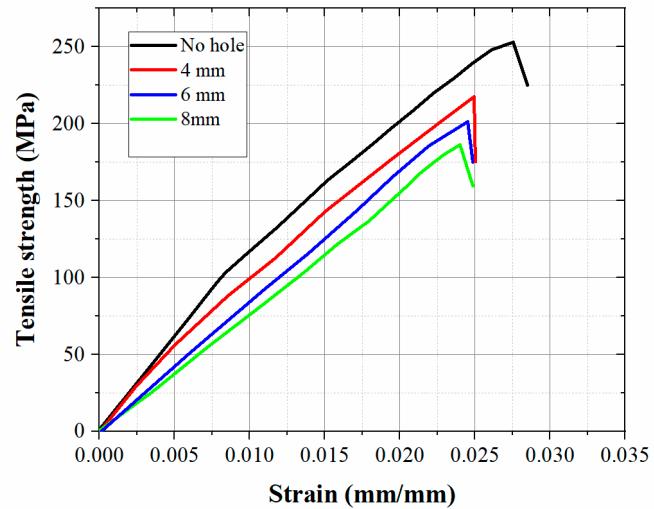


Figure 6. Aramid-basalt/epoxy OHF specimen with hole diameter a) 4 mm b) 6 mm c) 8 mm.

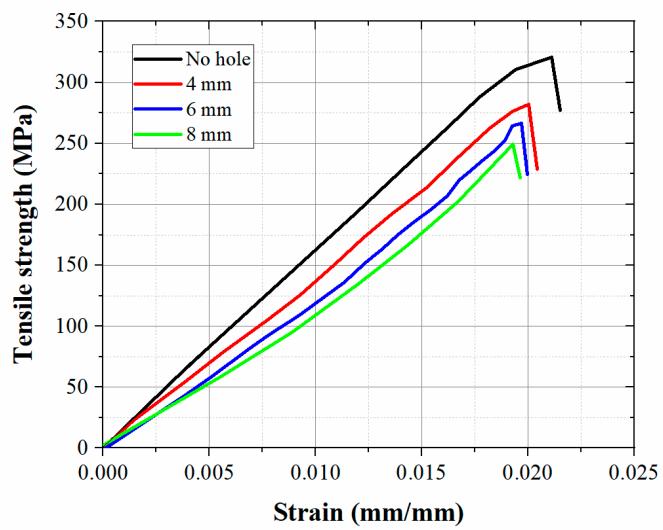
### 3. Results and Discussions

#### 3.1. Tensile behavior

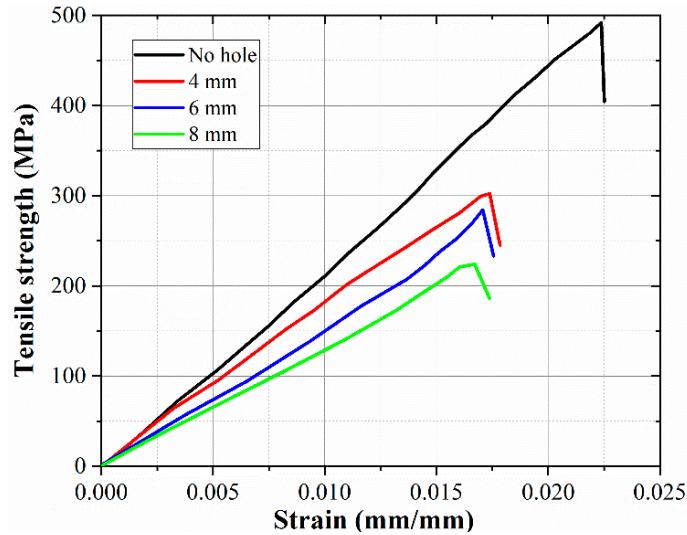
Figure 7 illustrates the stress vs strain response of different composite systems for varying hole sizes. FRPs have linear elastic mechanical characteristics without a significant yielding stage, which reduces failure strain and elongation rates. The brittle elastic behavior of all laminates was evident, even when a notch was present. The sharp drop in load depicted in this curve, as specified in ASTM D3039 [51], indicates significant damage occurring, ultimately leading to specimen fracture. Figure 7 also illustrates that the findings in this study align well with typical observations seen in the majority of FRP composites. Elastic modulus, tensile strength, and strain at failure were estimated using stress-strain curves in accordance with ASTM standards. Table 2 shows the tensile characteristics of the tested laminates for various open hole diameters. A comparison between the mechanical performance of different composite systems as well as with increasing hole size is discussed in the next section.



(a)



(b)



(c)

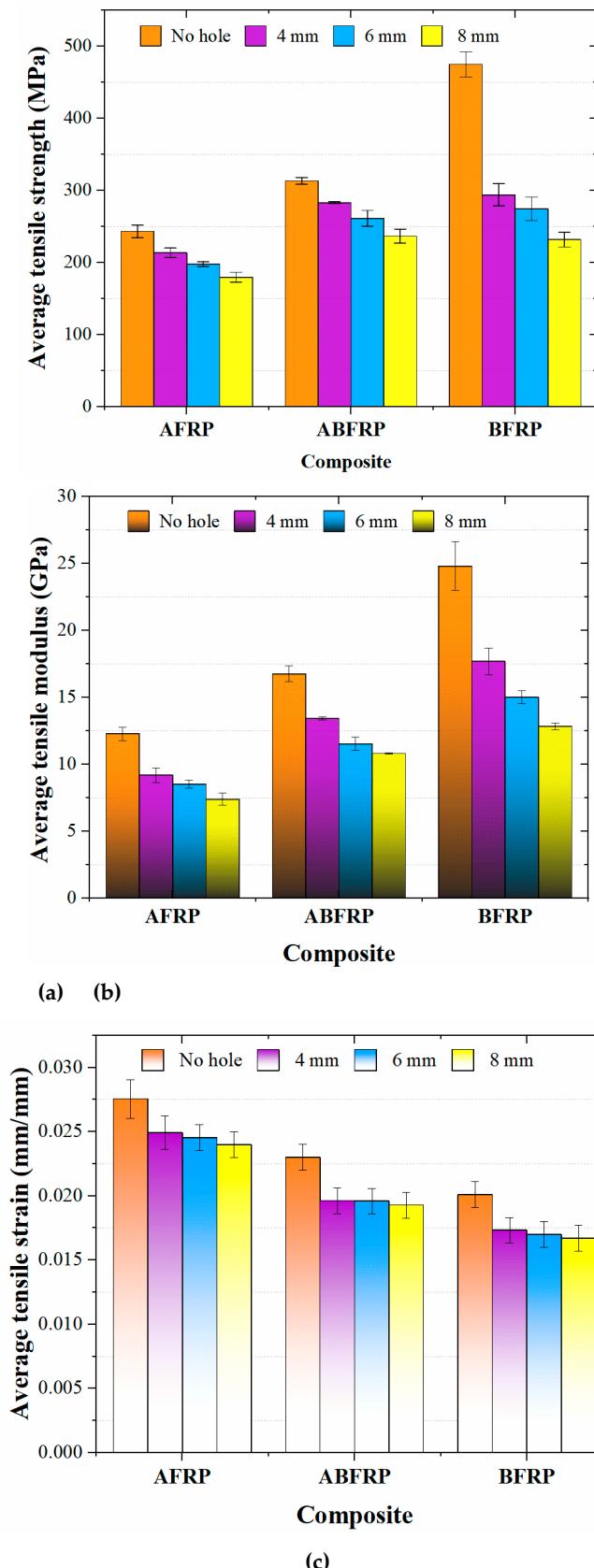
**Figure 7.** Effect of hole size on stress-strain response of (a) AFRP (b) ABFRP and (c) BFRP composites.

**Table 2.** Tensile properties of AFRP, ABFRP and BFRP composite systems corresponding to varying hole size.

Mechanical properties	Hole diameter (mm)	AFRP	ABFRP	BFRP
Average tensile strength (MPa)	0	243.11 ± 8.74	313.12 ± 4.80	474.54 ± 17.52
	4	213.52 ± 6.52	282.9 ± 1.56	293.83 ± 15.52
	6	197.84 ± 3.20	261.2 ± 11.10	274.39 ± 16.20
	8	179.68 ± 6.73	241.58 ± 9.64	231.65 ± 10.19
Young's modulus (GPa)	0	12.28 ± 0.41	16.74 ± 0.59	24.8 ± 1.83
	4	9.18 ± 0.55	13.43 ± 0.11	17.68 ± 0.99
	6	8.51 ± 0.31	11.52 ± 0.5	15.02 ± 0.47
	8	7.39 ± 0.44	10.8 ± 0.05	12.83 ± 0.23
Failure strain	0	0.0275	0.0211	0.0223
	4	0.0249	0.0196	0.0173
	6	0.0245	0.0196	0.0170
	8	0.0239	0.0192	0.0167
Strength retention (%)	4	87.83	90.35	61.88
	6	81.38	83.41	57.79
	8	73.91	75.55	48.78

### 3.2. Tensile properties

Figure 8 (a-c) depicts the affect of hole size on the tensile properties of the composite systems considered. Regardless of hole size, introducing basalt layers to aramid increases the tensile strength of the ABFRP laminate. BFRP displayed almost twice the tensile strength of the AFRP for the no hole case. Similar observation has been reported in [55,56]. This phenomenon can be elucidated by prior research, which demonstrated that blending high elongation/low modulus fibers like Kevlar or glass with low elongation/high modulus and rigid synthetic fibers such as carbon or basalt leads to a well-balanced hybrid composite laminate[57,58]. This interchangeably incorporates the desired mechanical properties from each reinforcement while minimizing undesired behavior[18,23].

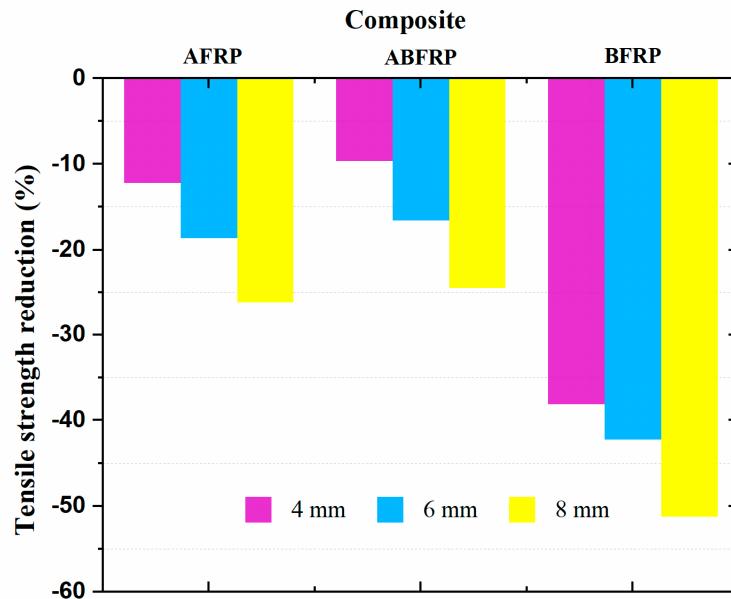


**Figure 8.** Variation of tensile characteristics with hole size (a) Average tensile strength (b) Average tensile modulus (c) Average failure strain.

Basalt fibre is known to offer high strength and modulus but being brittle in nature it is often hybridized with ductile aramid fibres [59,60]. Ductile materials like aramid absorb most of the

applied load in the form of plastic deformation, hence they attain lower tensile strength. In contrast brittle materials are resistant to deformation and do not dissipate the applied energy before failure, thereby achieving higher strength. Bazan et al. [61] has also stated that the positive hybrid effect of aramid-basalt reinforcement is contributed by the aramid fibres tendency to delaminate but not brittle break when stretched and the high strength characteristics of basalt fibres. The higher tensile strength may also be associated with the higher density of the basalt fibres as reported in [56]. Therefore hybridization resulted in intermediate strength which was also explained by Hayashi et al. [62] on the basis of synergistic effect called hybridization. The no hole ABFRP showed an increase of 28.97% in ultimate strength compared to AFRP. The improved mechanical performance due to aramid-basalt hybridization has been confirmed by various literatures [10,22,31,63].

The effect of hole size on the tensile strength is evident since ultimate strength decreased as hole size increased regardless of the material. To clearly examine the effect of hole diameter on the tensile performance of each material, strength retention was calculated and reported as  $\frac{\sigma_{\text{hole}}}{\sigma_{\text{no hole}}}$  shown in Table 2. Figure 9 shows the percentage loss in tensile strength compared to the no hole case for increasing hole sizes. The hybrid ABFRP laminates were found to record the least loss in strength as the hole size increased when compared to AFRP and BFRP laminates. However, BFRP showed the highest tensile strength at all hole sizes while AFRP showed the lowest tensile strength.



**Figure 9.** Tensile strength reduction of AFRP, ABFRP and BFRP laminates.

The strength retention observed was in the order of ABFRP > AFRP > BFRP. This also indicates the higher hole sensitivity of BFRP laminates. Due to its greater ductility and failure strain, AFRP can reduce stress concentration at the hole's edge, redistribute loads away from the hole, and delay crack propagation, thus showing lower hole sensitivity than BFRP. While the basalt fibres being more brittle and less ductile, it resulted in faster fracture growth at low strain or earlier failure, which reduced strength retention. This indicates that basalt fibre is highly hole sensitive compared to other composite systems. At a hole size of 8 mm, BFRP lost more than 50% of its strength.

BFRP shows the highest tensile modulus for all hole sizes and AFRP shows the lowest modulus. Owing to the brittle nature of basalt fibres it resists deformation which is responsible for the higher modulus. The positive effect of hybridization is seen with the tensile modulus of hybrid ABFRP being intermediate [18,62]. An increase in tensile modulus of 36.31% is seen in ABFRP compared to AFRP considering the no hole case. Increase in hole size had a negative effect on elastic modulus of the material. With the increase in hole size, modulus decreased regardless of the material. This decrease in modulus may be associated with stress concentration in the vicinity of the hole edge. The occurrence of hole introduces discontinuity in the fibres or in other words the woven fabrics are torn

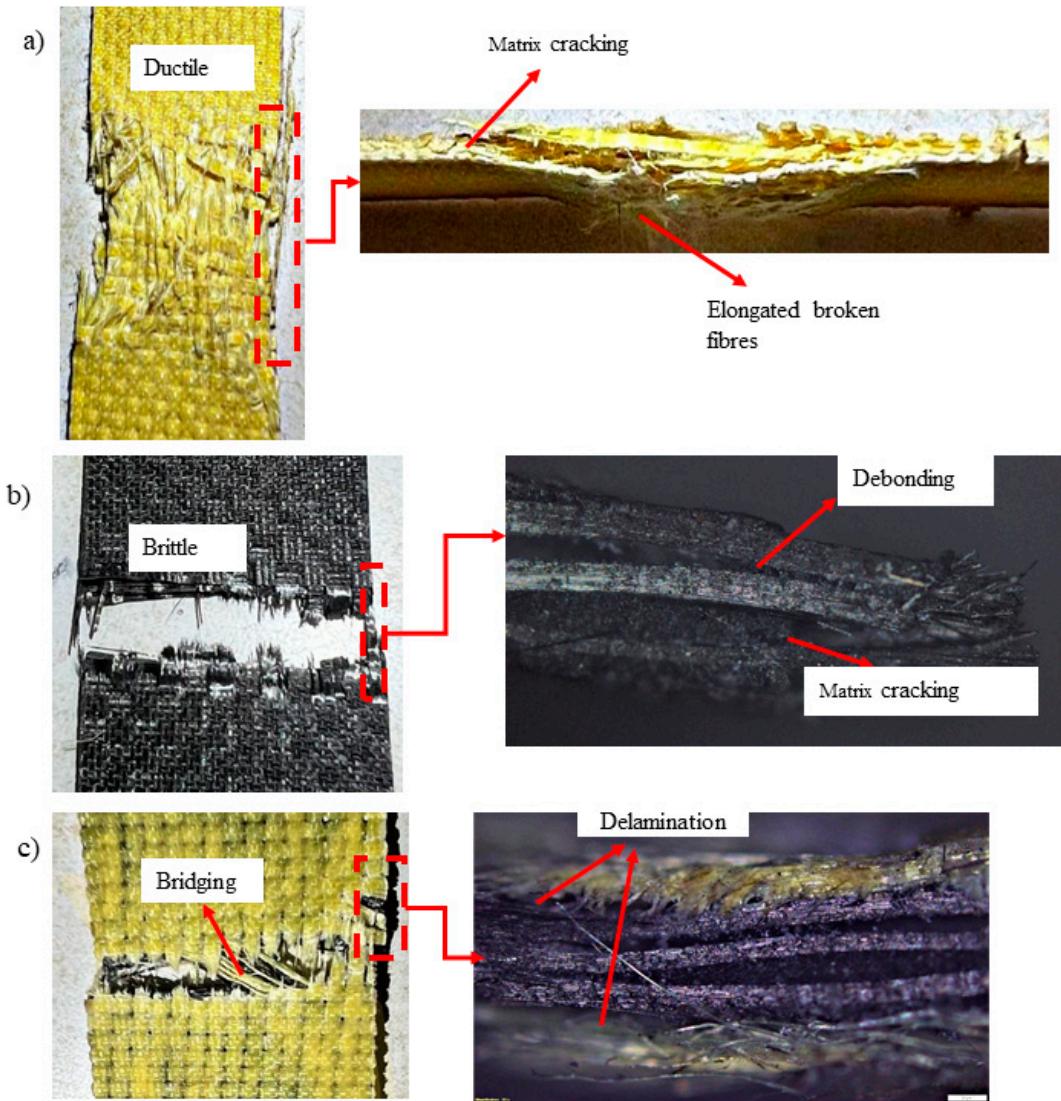
or damaged when a hole is drilled, thus causing a strong anisotropy in the laminate which deteriorates the modulus [46]. Larger holes induce greater anisotropy which explains greater loss in modulus [30]. The introduction of an 8 mm hole showed a tensile modulus loss of 48.2%, 39.8% and 35.4% in BFRP, AFRP and ABFRP laminates respectively.

AFRP showed the highest tensile strain owing to its high ductility as mentioned in the previous section while BFRP showed the least tensile strain due to its brittle fracture behavior. The tensile strain of AFRP is 25.5% higher than BFRP laminate for the no hole case. An increase in strain is observed in basalt fibres with the insertion of aramid layers. Since the damage first initiated in the basalt fibres and transfer of stress to surface aramid fibres took place closer to failure load the stretching and bridging effect offered by aramid fibres allowed the hybrid ABFRP laminate to fail at a higher strain than in the case of only basalt fibres [18]. Therefore, ABFRP laminate showed intermediate performance. Introduction of hole decreased the failure strain of the material. Presence of hole results in lesser area to support the stress which leads to early failure [64]. The 4 mm hole caused a large decrease in strain compared to specimen without hole. Strain values of other hole sizes were only slightly reduced from this value. 8 mm hole size led to a decrease of 12.9%, 16.1% and 16.9% in tensile strain of AFRP, ABFRP and BFRP laminate respectively.

### 3.3. *Damage assessment of fractured tensile specimens*

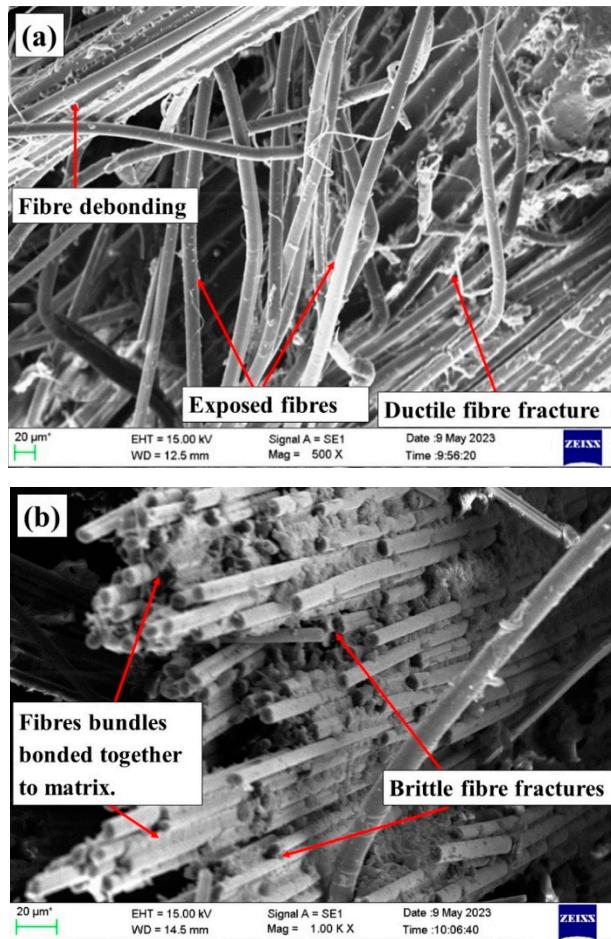
#### 3.3.1. Specimens without hole

Figure 10 (a) indicates the various failure modes observed in three different composites without the hole. The AFRP laminate exhibited significant elongation before fibre breakage in the tensile loading direction at the fracture surface, indicating a ductile fracture. The greater strain response observed in aramid fibres is attributed to their high ductility. While the BFRP laminates showed smooth fracture surface which corresponds to brittle fracture as depicted in Figure 10 (b). The hybrid ABFRP laminate in Figure 10 (c) showed the intervention of both these properties with the bridging effect from the top and bottom surface aramid layers. This failure mechanism accounts for the moderate strain response achieved through hybridization.



**Figure 10.** Fractured surfaces (top view and side view) of tensile specimens (a) AFRP (b) BFRP and (c) ABFRP composites.

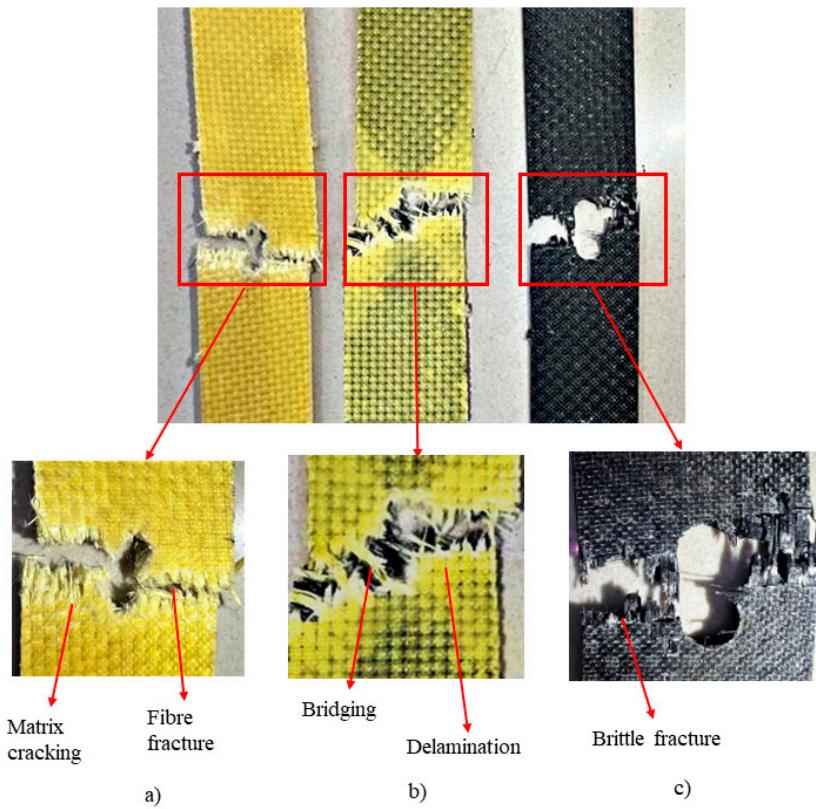
SEM investigations were performed to comprehend the damage processes involved in AFRP and BFRP laminates as shown in Figure 11. Interfacial adhesion examination through SEM is also useful to compare the mechanical strength between the different materials. In Figure 11 (a) the elongated aramid fibres at the region of fracture confirm the ductile failure mode of the AFRP laminate. Additionally, the fibres in the fibre bundles are no longer bonded to the matrix and have been completely exposed at the surface. This indicates a weak bond between aramid fibres and the epoxy matrix. In contrast Figure 11 (b) confirms the brittle failure mode of the BFRP laminate as it shows smoother cut of fibre breakage. The fibres show relatively better bonding with matrix since the epoxy is still adhering around the fibres hence holding them together which explains the superior mechanical properties of BFRP as compared to AFRP.



**Figure 11.** SEM images of fractured tensile specimens (a) AFRP and (b) BFRP.

### 3.3.2. Open hole specimens

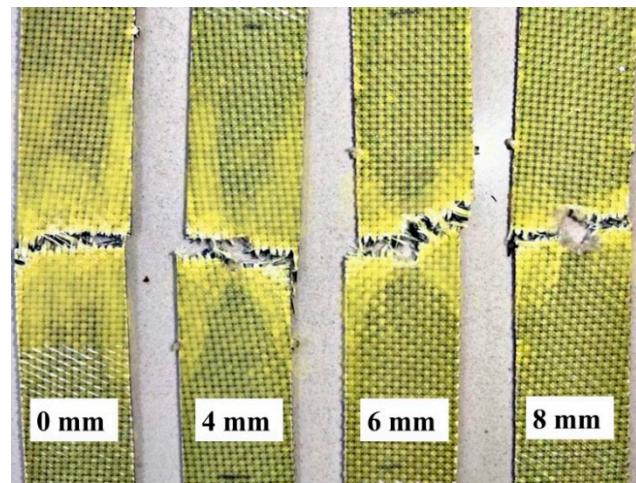
A close-up view of the fractured specimens for 6 mm hole size are shown in Figure 12. The existence of the hole, serves as a stress riser in the specimen, is responsible for the localized rupture in the area around the hole. The hole causes an interruption in the continuity fibres, changing the stress distribution along the fibre orientation. Stress concentration causes the detachment of discontinuous fibre tips from the matrix at very low loads. This results in microcracks in the material, which, when subjected to additional loading, progress into larger cracks, eventually leading to fibre-matrix debonding and delamination. Ultimately, fibre breakage occurs resulting in complete fracture of the specimen at the failure load.



**Figure 12.** Fracture surface of open hole specimens of (a) AFRP (b) ABFRP and (c) BFRP laminates.

The fracture was seen to begin at the perimeter of the hole and grow transverse to the direction of tensile loading along the specimen width. Figure 12 (a) shows stretched fibres which can be attributed to the high ductile nature of aramid fibres. Failure initiated with a matrix crack forming around the hole's edge, subsequently propagating across the width, and ultimately resulting in fibre-matrix debonding and, eventually, fibre breakage. While in the case of hybrid ABFRP in Figure 12 (b) the basalt fibres fractured first and were bridged by the surrounding ductile aramid fibres. This allowed for the stronger and stiffer basalt fibres to reach its ultimate strength giving rise to enhanced tensile strength of the hybrid structure. Delamination can be observed as whitish-yellow appearance due to the exposed aramid fibres separated from the basalt layer. BFRP laminate showed smoother fracture surface with damage is still confined to the area around the hole, confirming brittle fracture mechanism as shown in Figure 12 (c). Failure initiated with matrix cracks originating at the hole's edge, then extending across the width. Subsequently, fibre breakage ensued, resulting in sudden fracture of the specimen into two pieces.

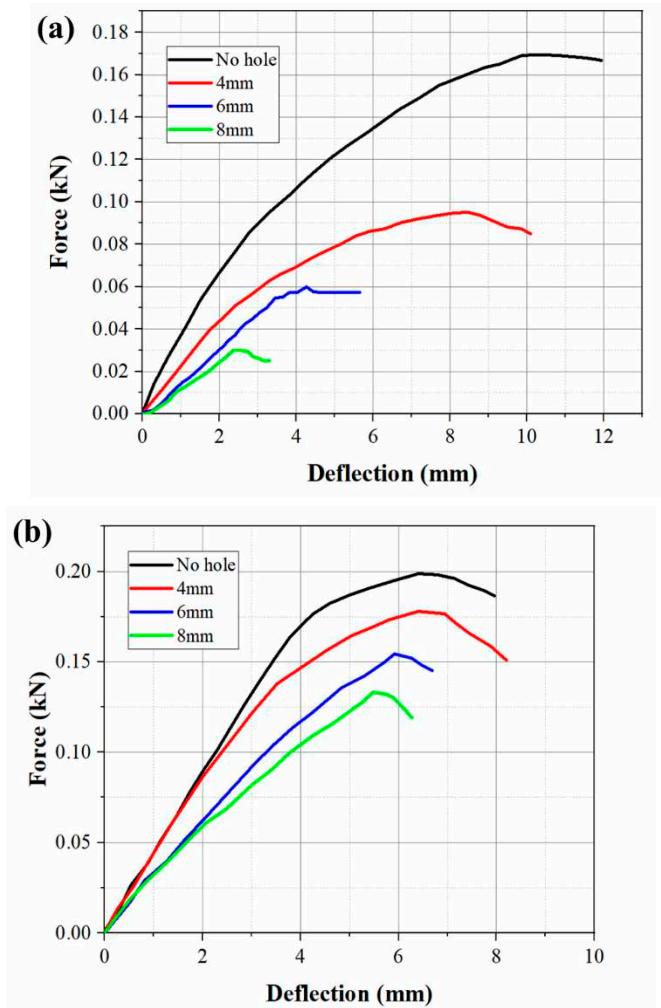
Delamination was evident in the hybrid ABFRP as whitish-yellow appearance on the top and bottom surface. This is due to matrix damage which debonds the surface aramid layer from the core basalt exposing the aramid fibres. Figure 13 shows that the delamination zone around the open hole decreased with the increase in hole size [29,46,49,65]. This is because for a specimen with small hole size, more loads are required to be applied before failure can occur. Moreover, when the diameter is smaller the transverse cracks initiating from the hole edge can easily link up and propagate to larger available area between hole edge and specimen edge [29,65].

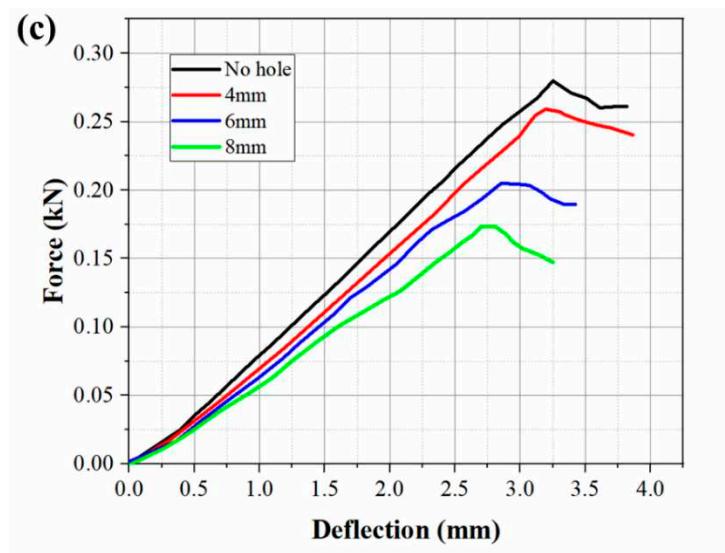


**Figure 13.** Influence of hole size on the delamination zone.

### 3.4. Flexural behavior

Figure 14 depicts the flexural load vs deflection curves of different composite systems for varying hole sizes.





**Figure 14.** Force vs deflection response of a) AFRP b) ABFRP and c) BFRP composites.

Figure 14 (a) indicates that the flexural curve of aramid laminate is relatively nonlinear due to the nonlinear compressive behavior of aramid fibres [66]. From load vs deflection plots it can be deduced that with increase in load, deflection also increases and at a certain deflection it attains peak load after which it starts to decline. There is no sharp decline in the load instead, a plateau is seen at the peak load until the specimen completely fails [50]. Such a behavior is an indication of stable propagation of damage unlike BFRP laminate which shows a specific peak followed by a rapid decline in peak load within a smaller range of deflection as depicted in Figure 14(c). This is associated with the brittle damage propagation of basalt fibres which has also been substantiated in the following sections. The load vs. deflection curve also demonstrates the coupling effect of hybridizing aramid and basalt fibres. Since the laminate features aramid layers on the surface, it effectively prevents catastrophic failure. Stress transfer occurs between the two reinforcements, allowing the hybrid laminate to exhibit intermediate performance. Figure 14(b) indicates the pseudo ductile behavior[67] of hybrid system comprising of initial linear response which then turns into nonlinear region owing to the plastic deformation in aramid layers.

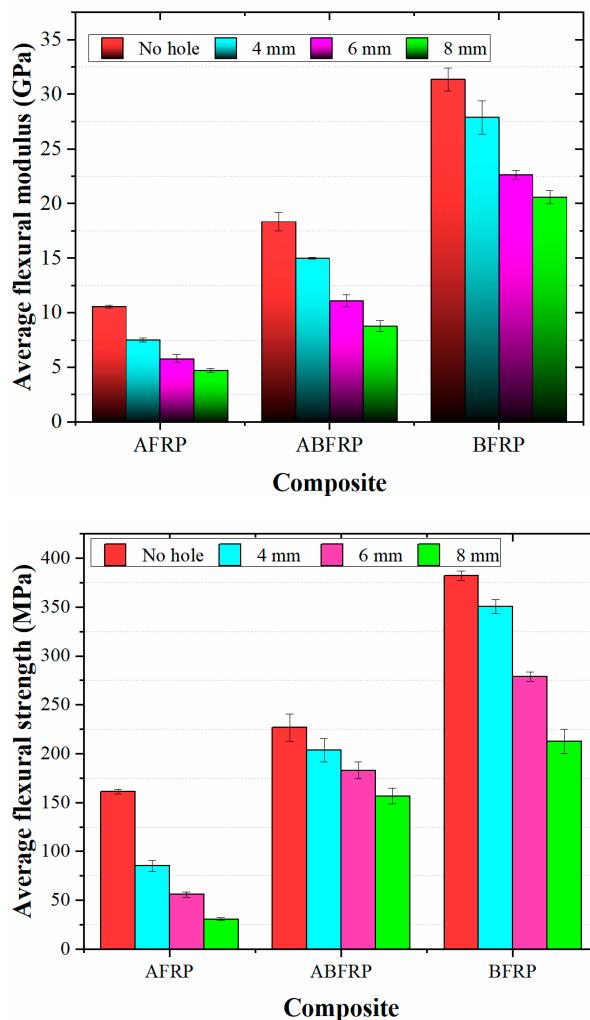
**Table 3.** Flexural properties of composite systems for varying hole sizes.

Mechanical properties	Hole diameter (mm)	AFRP	ABFRP	BFRP
	0	160.96 ± 2.42	226.68 ± 14.05	382.27 ± 4.87
Average flexural strength (MPa)	4	85.12 ± 5.78	203.53 ± 11.75	350.31 ± 7.09
	6	56 ± 2.77	182.81 ± 8.62	278.95 ± 4.87
	8	30.43 ± 1.47	153.56 ± 7.99	212.60 ± 12.79
Young's modulus (GPa)	0	10.55 ± 0.12	18.33 ± 0.82	31.36 ± 1.05
	4	7.52 ± 0.18	14.98 ± 0.09	27.88 ± 1.52
	6	5.78 ± 0.36	11.10 ± 0.55	22.61 ± 0.43
	8	4.73 ± 0.18	8.75 ± 0.50	20.57 ± 0.59

	4	52.88	89.78	91.63
Strength retention (%)	6	34.79	80.64	72.97
	8	18.90	69.06	55.61

### 3.5. Flexural properties

Flexural strength and flexural modulus were calculated using load displacement curves in accordance with ASTM standards. Figure 15 (a), (b) illustrate the influence of hole size on the flexural properties of the composite.

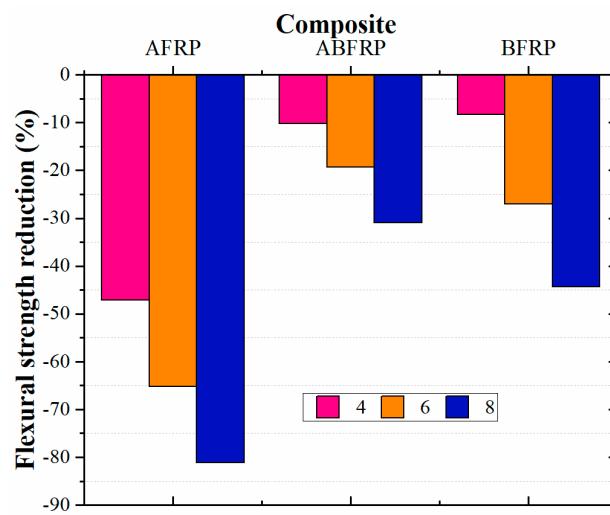


**Figure 15.** Variation of flexural properties (a) flexural strength and (b) flexural modulus of composites for different hole sizes.

It is obvious from the above results that the sandwiched hybrid specimen shows the highest strength retention. This is due to hybrid specimens can sustain loads even after the breakage of the low elongation fibres by transferring the load to the high elongation fibres at the surface [68]. The introduction of the 8 mm hole caused a decrease in strength of 44.3%, 32.25%, 81.09% for BFRP, ABFRP and AFRP respectively. AFRP showed higher hole sensitivity in flexural loading due to its poor compressive and bending properties [32,35,55]. This indicates that 8 mm hole diameters mark an important hole dimension since it led to a significant reduction in strength. This is due to the larger amount of material removed, resulting in a reduced load-bearing area and consequently a greater decrease in strength. In addition, larger holes with specimen dimension or width are kept constant, the edge effect also comes into play. The higher proximity of the hole edge to the specimen edge

facilitates instantaneous crack propagation to the edge of the specimen and cause early failure[32,35,55].

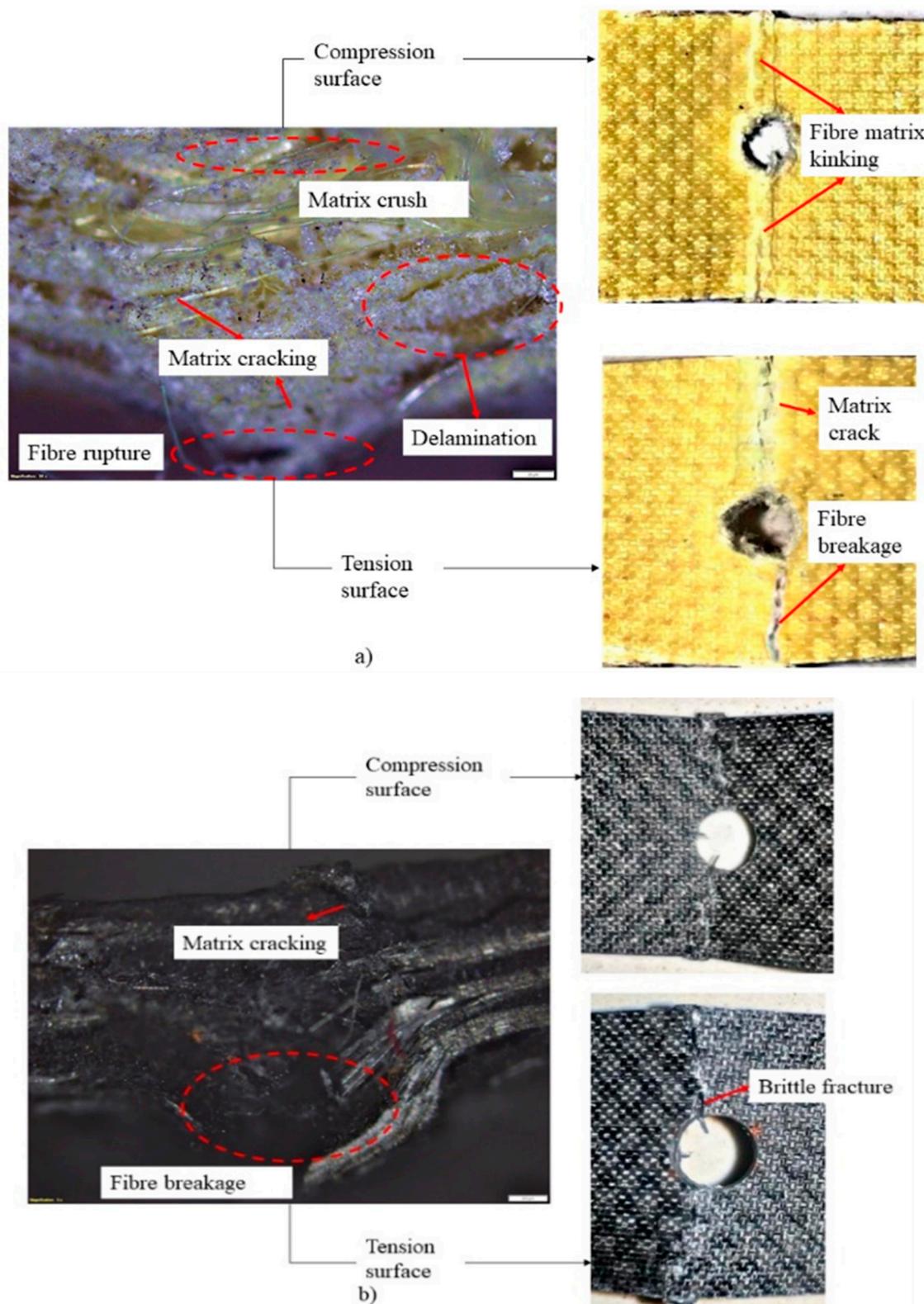
Figure 16 illustrates the loss in flexural strength with increasing hole size. Figure indicates that the presence of holes causes the flexural modulus to decrease. The flexural modulus decreases with increasing hole diameter due to the presence of holes causing a discontinuity in the fibre orientation, which, in turn, reduces the stiffness[64]. Hybrid composite laminates displayed an elevation in flexural modulus when compared to AFRP composite laminate. The presence of high strength basalt layers increased the flexural modulus. The flexural modulus of BFRP laminate is nearly 3 times while the flexural modulus of ABFRP laminate is almost twice that of AFRP laminate.

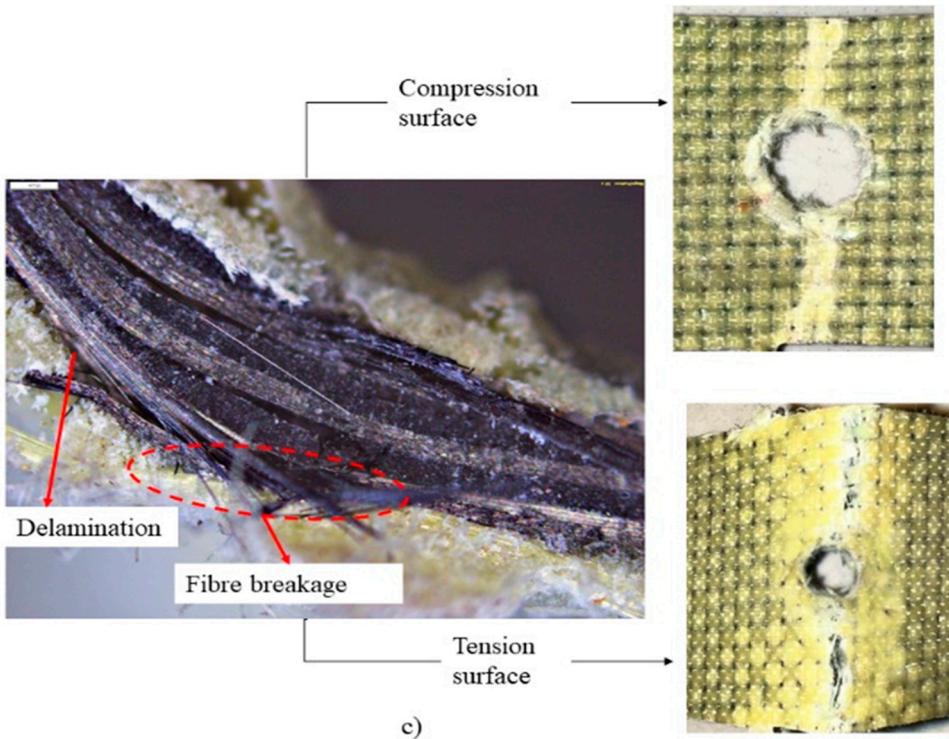


**Figure 16.** Loss in flexural strength with increasing hole size.

### 3.6. Damage assessment of fractured flexural specimens

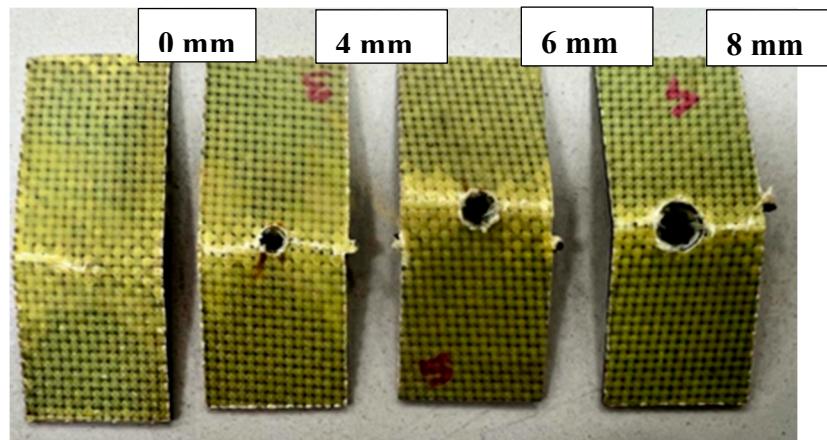
Compressive, tensile, shear, and/or delamination failures are commonly associated mechanisms in flexural loading[71]. Tensile forces act on the support face of the specimens during flexural loading, while compressive forces act on the loading face. The surface layers undergo maximum stress in the process. The fractured specimens with 6 mm hole damage modes are shown in Figure 17. High stress concentrations which began at the hole's edge and extended to the free edge were the root cause of all the specimens' failures. The final failure occurred due to fibre breakage on the bottom surface. The bottom surface of fractured specimens showed more damage than the top surface indicating tensile failure of aramid fibres, which are known for their high toughness and ductility. Hence, aramid fibres tend to delaminate but not brittle break as shown in Figure 17 (a). The appearance of kinks or whitish areas near the loading point in composite materials reinforced with aramid fibres is the result of compressive failure of the fibres[72]. Due to the brittle fracture behavior of basalt fibres, increased crack propagation and fibre breakage are observed as shown in Figure 17 (b). In the hybrid specimen, Figure 17(c), it is evident that matrix cracking first initiated in the lower basalt layers, subsequently leading to fibre rupture. This behavior has been elucidated by Kretsis [73] stating that in hybrid laminates, lower-strain fibres tend to break before higher-strain fibres. Thus, enabling the fibre with a lower strain and greater strength to approach its maximum strength. This indicates that the hybrid specimen's flexural strength is higher than that of a laminate made entirely of aramid. Debonding and delamination occurred at the interface between the aramid and basalt layers due to a difference in the mechanical properties.





**Figure 17.** variation in damage mechanism for 6mm hole.

A decrease in delamination zone is observed with an increase in the diameter of the hole as indicated in Figure 18. Similar observation has been reported in the previous section under tensile test. In comparison to smaller hole sizes, the catastrophic process zone is quite wide since it redistributes the stress concentration.



**Figure 18.** Influence of hole size on delamination zone.

In conclusion, while the higher load carrying capacity of the basalt layers benefits the aramid layers, the higher tolerance to damage and ductile fracture properties of aramid fibres benefits basalt layers. These combined effects lead to improved flexural performance and delays the occurrence of final failure. Larger holes function as an adequate stress riser to cause failure, which causes an early fracture with a smaller delamination zone. Therefore, it can be said that fibre fracture is a dominant failure mechanism in large holes while matrix cracking and delamination are the dominant failure mechanism in small holes.

#### 4. Conclusions

In this investigation, open hole tensile and flexural behavior were evaluated for aramid/epoxy (AFRP), basalt/epoxy (BFRP), and hybrid aramid-basalt/epoxy (ABFRP) composites for three different hole sizes 4 mm, 6 mm, and 8 mm respectively. The following findings can be drawn from the experimental evaluations:

- The inclusion of basalt layers significantly enhanced the tensile strength and modulus of the hybrid composite laminate. The surface aramid layers in the sandwich type lay-up sequence allowed for larger failure strain by allowing a more ductile failure.
- The stress concentration effect at the hole boundary reduced the material's tensile properties. Strength retention deteriorated for larger holes in the order of AFRP > ABFRP > BFRP.
- BFRP laminates were more hole sensitive due to their brittle damage mechanism. Hybrid laminates showed delamination as a major failure mode due to the poor interfacial bonding and difference in mechanical properties between the aramid and basalt fibres.
- Larger holes exhibited smaller delamination area. Matrix cracking, fibre fracture and fibre pull out were the mode of damage observed in the open hole specimens.
- For specimens without holes, BFRP laminates displayed a flexural strength of 382 MPa, which is higher than that of ABFRP (226 MPa), and AFRP (160 MPa). As the hole diameter increases, the flexural strength reduces significantly. However, the introduction of 8 mm hole caused a decrease in strength of 44.3 %, 32.25 %, 81.09 % for BFRP, ABFRP and AFRP respectively.
- Aramid fibres exhibited a more pronounced decline in flexural strength with an increase in hole size due to their poor compression and bending properties. However, due to their ability to absorb higher energy and high ductility, resulted in considerable increase in failure strain of the hybrid laminate accompanied by stable failure than BFRP.
- The results obtained from this research on open hole aramid-basalt/epoxy tensile and flexural specimens offer critical data that can be directly applied in engineering and industry to optimize the design and performance of composite structures, enhancing their durability, safety, and overall efficiency.

**Author Contributions:** Conceptualization, O.F., Y.P. and J.D.; methodology, O.F. and J.D.; software, Y.P., M.G.T. and R.S.B.; investigation, Y.P., M.G.T. and R.S.B.; resources, Y.P., M.G.T., and R.S.B.; data curation, O.F., Y.P. and J.D.; writing—original draft preparation, O.F., Y.P. and J.D.; writing—review and editing, Y.P., M.G.T., R.S.B.; supervision, Y.P.

**Funding:** This research received no external funding

**Acknowledgments:** The authors acknowledge “Department of Aeronautical and Automobile Engineering, Manipal Institute of Technology, Manipal” for providing Advanced Composite laboratory facility to carry out this research.

**Conflicts of Interest:** The authors declare no conflict of interest.

#### References

1. Mallick, P.K. *“Fiber-Reinforced Composites Materials, Manufacturing and Design”*; Third Edit.; CRC Press Taylor & Francis Group, 2007; ISBN 9780849342059.
2. K.K. Chawla. *Composite Materials: Science and Engineering*; Third Edit.; Springer Science & Business Media: New York, 2012;
3. Agarwal B D and Broutman L J *Analysis and Performance of Fiber Composites*; Second Edi.; John Wiley & Sons Inc., 1990;
4. Neto, J.; Queiroz, H.; Aguiar, R.; Lima, R.; Cavalcanti, D.; Banea, M.D. A Review of Recent Advances in Hybrid Natural Fiber Reinforced Polymer Composites. *Journal of Renewable Materials* **2022**, *10*, 561–589, doi:10.32604/jrm.2022.017434.
5. Pandita, S.D.; Yuan, X.; Manan, M.A.; Lau, C.H.; Subramanian, A.S.; Wei, J. Evaluation of Jute/Glass Hybrid Composite Sandwich: Water Resistance, Impact Properties and Life Cycle Assessment. *Journal of Reinforced Plastics and Composites* **2014**, *33*, 14–25, doi:10.1177/0731684413505349.

6. CHICHANE, A.; BOUJMAL, R.; EL BARKANY, A. Bio-Composites and Bio-Hybrid Composites Reinforced with Natural Fibers: Review. *Materials Today: Proceedings* **2023**, *72*, 3471–3479, doi:10.1016/j.matpr.2022.08.132.
7. Fiore, V.; Scalici, T.; Di Bella, G.; Valenza, A. A Review on Basalt Fibre and Its Composites. *Composites Part B: Engineering* **2015**, *74*, 74–94, doi:10.1016/j.compositesb.2014.12.034.
8. Czigány, T.; Vad, J.; Pölöskei, K. Basalt Fiber as a Reinforcement of Polymer Composites. *Periodica Polytechnica Mechanical Engineering* **2005**, *49*, 3–14.
9. Elmahdy, A.; Verleysen, P. Mechanical Behavior of Basalt and Glass Textile Composites at High Strain Rates : A Comparison. *Polymer Testing* **2020**, *81*, 106224, doi:10.1016/j.polymertesting.2019.106224.
10. Sarasini, F.; Tirillò, J.; Valente, M.; Ferrante, L.; Cioffi, S.; Iannace, S.; Sorrentino, L. Hybrid Composites Based on Aramid and Basalt Woven Fabrics: Impact Damage Modes and Residual Flexural Properties. *Materials and Design* **2013**, *49*, 290–302, doi:10.1016/j.matdes.2013.01.010.
11. Bandaru, A.K.; Sachan, Y.; Ahmad, S.; Alagirusamy, R.; Bhatnagar, N. On the Mechanical Response of 2D Plain Woven and 3D Angle-Interlock Fabrics. *Composites Part B: Engineering* **2017**, *118*, 135–148, doi:10.1016/j.compositesb.2017.03.011.
12. Czigány, T. Special Manufacturing and Characteristics of Basalt Fiber Reinforced Hybrid Polypropylene Composites: Mechanical Properties and Acoustic Emission Study. *Composites Science and Technology* **2006**, *66*, 3210–3220, doi:10.1016/j.compscitech.2005.07.007.
13. Dorigato, A.; Pegoretti, A. Flexural and Impact Behaviour of Carbon/Basalt Fibers Hybrid Laminates. *Journal of Composite Materials* **2014**, *48*, 1121–1130, doi:10.1177/0021998313482158.
14. Zubair, M.; Pai, Y. Review on Impact Response of Polymer Composites. *Journal of Mechanical Engineering Research and Developments* **2019**, *42*, doi:10.26480/jmerd.04.2019.238.242.
15. Pai, Y.; Pai, K.D.; Kini, M.V. A Review on Low Velocity Impact Study of Hybrid Polymer Composites. *Materials Today: Proceedings* **2021**, doi:10.1016/j.matpr.2021.05.390.
16. Fernandes, O.; Dutta, J.; Pai, Y. Effect of Various Factors and Hygrothermal Ageing Environment on the Low Velocity Impact Response of Fibre Reinforced Polymer Composites- a Comprehensive Review. *Cogent Engineering* **2023**, *10*, doi:10.1080/23311916.2023.2247228.
17. Agarwal, S.; Pai, Y.; Pai, D.; Mahesha, G.T. Assessment of Ageing Effect on the Mechanical and Damping Characteristics of Thin Quasi-Isotropic Hybrid Carbon-Kevlar / Epoxy Intraply Composites and Damping Characteristics of Thin Intraply Composites. *Cogent Engineering* **2023**, *10*, doi:10.1080/23311916.2023.2235111.
18. Swolfs, Y.; Gorbatikh, L.; Verpoest, I. Composites : Part A Fibre Hybridisation in Polymer Composites : A Review. *COMPOSITES PART A* **2014**, *67*, 181–200, doi:10.1016/j.compositesa.2014.08.027.
19. Gupta, M.K.; Srivastava, R.K. A Review on Characterization of Hybrid Fibre Reinforced Polymer Composite. *Gupta MK American Journal of Polymer Science & Engineering* **2016**, *4*, 1–7.
20. Phillips, L.N. The Hybrid Effect - Does It Exist? *Composites* **1976**, *7*, 7–8, doi:10.1016/0010-4361(76)90273-1.
21. Pandya, K.S.; Veerraju, C.; Naik, N.K. Hybrid Composites Made of Carbon and Glass Woven Fabrics under Quasi-Static Loading. *Materials and Design* **2011**, *32*, 4094–4099, doi:10.1016/j.matdes.2011.03.003.
22. Pai, Y.; Pai K, D.; Kini, M.V. Experimental Investigations on the Moisture Absorption and Mechanical Behaviour of Basalt-Aramid/Epoxy Hybrid Interply Composites under Different Ageing Environments. *Cogent Engineering* **2022**, *9*, 0–20, doi:10.1080/23311916.2022.2080354.
23. Wang, X.; Hu, B.; Feng, Y.; Liang, F.; Mo, J.; Xiong, J.; Qiu, Y. Low Velocity Impact Properties of 3D Woven Basalt/Aramid Hybrid Composites. *Composites Science and Technology* **2008**, *68*, 444–450, doi:10.1016/j.compscitech.2007.06.016.
24. Pai, Y.; Pai, D.K.; Kini, M.V. Evaluation of the Mechanical Characteristics of Hygrothermally Aged 2-D Basalt-Aramid/Epoxy Hybrid Interply Composites. *Journal of Physics: Conference Series* **2021**, *2070*, doi:10.1088/1742-6596/2070/1/012234.
25. Pai, Y.; Dayananda Pai, K.; Vijaya Kini, M. Effect of Ageing Conditions on the Low Velocity Impact Behavior and Damage Characteristics of Aramid-Basalt/Epoxy Hybrid Interply Composites. *Engineering Failure Analysis* **2023**, *152*, 107492, doi:10.1016/j.engfailanal.2023.107492.
26. Jule, L.T.; Ramaswamy, K.; Nagaprasad, N.; Shanmugam, V.; Vignesh, V. Design and Analysis of Serial Drilled Hole in Composite Material. *Materials Today: Proceedings* **2021**, *45*, 5759–5763, doi:10.1016/j.matpr.2021.02.587.
27. Caminero, M.A.; Lopez-Pedrosa, M.; Pinna, C.; Soutis, C. Damage Monitoring and Analysis of Composite Laminates with an Open Hole and Adhesively Bonded Repairs Using Digital Image Correlation. *Composites Part B: Engineering* **2013**, *53*, 76–91, doi:10.1016/j.compositesb.2013.04.050.
28. Guo, Q.; Zhang, Y.; Li, D.; Lv, Q.; Sun, X.; Ma, M.; Chen, L. Experimental and Numerical Investigation of Open-Hole Tensile Properties and Damage Mechanisms of 3D Woven Composites under Weft-Loading. *Thin-Walled Structures* **2021**, *161*, 107455, doi:10.1016/j.tws.2021.107455.
29. Green, B.G.; Wisnom, M.R.; Hallett, S.R. An Experimental Investigation into the Tensile Strength Scaling of Notched Composites. *2007*, *38*, 867–878, doi:10.1016/j.compositesa.2006.07.008.

30. Kumar, S.A.; Rajesh, R.; Pugazhendhi, S. A Review of Stress Concentration Studies on Fibre Composite Panels with Holes/Cutouts. *Proceedings of the Institution of Mechanical Engineers, Part L: Journal of Materials: Design and Applications* **2020**, *234*, 1461–1472, doi:10.1177/1464420720944571.
31. Kumar, A.; Patel, S.; Sachan, Y.; Ahmad, S.; Alagirusamy, R. Composites : Part A Mechanical Behavior of Kevlar / Basalt Reinforced Polypropylene Composites. *Composites Part A* **2016**, *90*, 642–652, doi:10.1016/j.compositesa.2016.08.031.
32. Sarasini, F.; Tirillò, J.; Valente, M.; Valente, T.; Cioffi, S.; Iannace, S.; Sorrentino, L. Effect of Basalt Fiber Hybridization on the Impact Behavior under Low Impact Velocity of Glass/Basalt Woven Fabric/Epoxy Resin Composites. *Composites Part A: Applied Science and Manufacturing* **2013**, *47*, 109–123, doi:10.1016/j.compositesa.2012.11.021.
33. Sarasini, F.; Tirillò, J.; Ferrante, L.; Valente, M.; Valente, T.; Lampani, L.; Gaudenzi, P.; Cioffi, S.; Iannace, S.; Sorrentino, L. Drop-Weight Impact Behaviour of Woven Hybrid Basalt-Carbon/Epoxy Composites. *Composites Part B: Engineering* **2014**, *59*, 204–220, doi:10.1016/j.compositesb.2013.12.006.
34. Sarasini, F.; Tirillò, J.; D'Altilia, S.; Valente, T.; Santulli, C.; Touchard, F.; Chocinski-Arnault, L.; Mellier, D.; Lampani, L.; Gaudenzi, P. Damage Tolerance of Carbon/Flax Hybrid Composites Subjected to Low Velocity Impact. *Composites Part B: Engineering* **2016**, *91*, 144–153, doi:10.1016/j.compositesb.2016.01.050.
35. Dorey, G.; Sidey, G.R.; Hutchings, J. Impact Properties of Carbon Fibre / Kevlar 49 Fibre Hybrid Composites. *Composites* **1978**, *9*, 25–32, doi:https://doi.org/10.1016/0010-4361(78)90514-1.
36. Vasudevan, A.; Senthil Kumaran, S.; Naresh, K.; Velmurugan, R.; Shankar, K. Advanced 3D and 2D Damage Assessment of Low Velocity Impact Response of Glass and Kevlar Fiber Reinforced Epoxy Hybrid Composites. *Advances in Materials and Processing Technologies* **2018**, *4*, 493–510, doi:10.1080/2374068X.2018.1465310.
37. Pai, Y.; Kini, M.V.; Engineering, A. Effect of Aramid Fabric Orientation Angle on the Mechanical Characteristics of Basalt-Aramid / Epoxy Hybrid Interply Composites. *Materials Research* **2021**, *24*, doi:DOI: https://doi.org/10.1590/1980-5373-MR-2021-0209 Effect.
38. Kanitkar, Y.M.; Kulkarni, A.P.; Wangikar, K.S. Investigation of Flexural Properties of Glass-Kevlar Hybrid Composite. **2016**, *1*, 25–29.
39. Chuaqui, T.R.C.; Nielsen, M.W.D.; Colton, J.; Butler, R.; Rhead, A.T. Effects of Ply Angle and Blocking on Open-Hole Tensile Strength of Composite Laminates : A Design and Certification Perspective. *Composites Part B* **2021**, *207*, 108582, doi:10.1016/j.compositesb.2020.108582.
40. Oz, F.E.; Mehdikhani, M.; Ersoy, N.; Lomov, S. V In-Situ Imaging of Inter- and Intra-Laminar Damage in Open-Hole Tension Tests of Carbon Fibre Reinforced Composites. *Composite Structures* **2020**, *244*, 112302, doi:10.1016/j.compstruct.2020.112302.
41. Kannan, T.G.; Mou, C.; Bing, K. Composites : Part B Influence of Laminate Lay-up , Hole Size and Coupling Agent on the Open Hole Tensile Properties of Flax Yarn Reinforced Polypropylene Laminates. *Composites Part B* **2014**, *57*, 80–85, doi:10.1016/j.compositesb.2013.09.042.
42. Vaidya, R.S.; Klug, J.C.; Sun, C.T. Effect of Ply Thickness on Fracture of Notched Composite Laminates Introduction. **1998**, *36*.
43. Cunningham, D.; Harries, K.A.; Bell, A.J. Open-Hole Tension Capacity of Pultruded GFRP Having Staggered Hole Arrangement. *Engineering Structures* **2015**, *95*, 8–15, doi:10.1016/j.engstruct.2015.03.042.
44. Beyene, A.T.; Belingardi, G.; Koricho, E.G. Effect of Notch on Quasi-Static and Fatigue Flexural Performance of Twill E-Glass / Epoxy Composite. *Composite Structures* **2016**, *153*, 825–842, doi:10.1016/j.compstruct.2016.05.094.
45. Yu, J.; Pan, Z.; Cai, Q.; Zhang, F.; Wu, Z. Open Hole Tensile Behavior of Plain Woven Carbon/Glass Hybrid Composites. *International Journal of Mechanical Sciences* **2023**, *246*, 108142, doi:10.1016/j.ijmecsci.2023.108142.
46. Belgacem, L.; Ouinas, D.; Aurelio, J.; Olay, V.; Argüelles, A. Experimental Investigation of Notch Effect and Ply Number on Mechanical Behavior of Interply Hybrid Laminates ( Glass / Carbon / Epoxy ). *Composites Part B* **2018**, *145*, 189–196, doi:10.1016/j.compositesb.2018.03.026.
47. Sun, G.; Wang, L.; Chen, D.; Luo, Q. International Journal of Mechanical Sciences Tensile Performance of Basalt Fiber Composites with Open Circular Holes and Straight Notches. *International Journal of Mechanical Sciences* **2020**, *176*, 105517, doi:10.1016/j.ijmecsci.2020.105517.
48. Shaari, N.; Jumahat, A.; Abdullah, S.A.; Hadderi, A.Z. Effect of Hybridization on Open-Hole Tension Properties of Woven Kevlar/Glass Fiber Hybrid Composite Laminates. *Jurnal Teknologi* **2015**, *76*, 91–96, doi:10.11113/jt.v76.5684.
49. Shaari, N.; Jumahat, A. Hole Size Effects on the Open Hole Tensile Properties of Woven Kevlar-Glass Fibre Hybrid Composite Laminates. **2017**, *25*, 309–318.
50. Sebaey, T.A.; Wagih, A. Flexural Properties of Notched Carbon – Aramid Hybrid Composite Laminates. **2019**, doi:10.1177/0021998319855773.
51. ASTM D3039 / D3039M-14 Standard Test Method for Tensile Properties of Polymer Matrix Composite; ASTM International, West Conshohocken, PA, 2014;

52. ASTM D3171 Standard Test Methods for Constituent Content of Composite Materials. **2011**, 1–11, doi:10.1520/D3171-15.2.

53. D7264, A. *Standard Test Method for Flexural Properties of Polymer Matrix Composite*; 2020;

54. ASTM D790 Standard Test Methods for Flexural Properties of Unreinforced and Reinforced Plastics and Electrical Insulating Materials 2021, 1–6.

55. Bozkurt, Y. Hybridization Effects on Tensile and Bending Behavior of Aramid / Basalt Fiber Reinforced Epoxy Composites. **2015**, doi:10.1002/pc.

56. Velumayil, R. Hybridization Effect on Mechanical Properties of Basalt / Kevlar / Epoxy Composite Laminates. **2022**.

57. Vara, V.; Talupula, S. ScienceDirect A Review on Reinforcement of Basalt and Aramid ( Kevlar 129 ) Fibers. *Materials Today: Proceedings* **2018**, 5, 5993–5998, doi:10.1016/j.matpr.2017.12.202.

58. Safri, S.N.A.; Sultan, M.T.H.; Jawaid, M.; Jayakrishna, K. Impact Behaviour of Hybrid Composites for Structural Applications: A Review. *Composites Part B: Engineering* **2018**, 133, 112–121, doi:10.1016/j.compositesb.2017.09.008.

59. Chowdhury, I.R.; Nash, N.H.; Portela, A.; Dowd, N.P.O.; Comer, A.J. Analysis of Failure Modes for a Non-Crimp Basalt Fiber Reinforced Epoxy Composite under Flexural and Interlaminar Shear Loading. *Composite Structures* **2020**, 245, 112317, doi:10.1016/j.compstruct.2020.112317.

60. Bulut, M. Mechanical Characterization of Basalt/Epoxy Composite Laminates Containing Graphene Nanopellets. *Composites Part B* **2017**, doi:10.1016/j.compositesb.2017.04.013.

61. Bazan, P.; Wierzbicka-miernik, A. A Novel Hybrid Composites Based on Biopolyamide 10 . 10 with Basalt / Aramid Fibers : Mechanical and Thermal Investigation. **2021**, 223, doi:10.1016/j.compositesb.2021.109125.

62. Hayashi T. On the Improvement of Mechanical Properties of Composites by Hybrid Composition. In Proceedings of the In: Proc 8th int reinforced plastics conference; 1972; pp. 149–152.

63. Pai, Y.; Pai K, D.; Kini, M.V. Effect of Aramid Fabric Orientation Angle on the Mechanical Characteristics of Basalt-Aramid/Epoxy Hybrid Interply Composites. *Materials Research* **2021**, 24, doi:10.1590/1980-5373-mr-2021-0209.

64. Khashaba, U.A.; Selmy, A.I.; Megahed, M. GFR / EPOXY Composites under Static and Fatigue Loads. **2007**, 81, 606–613, doi:10.1016/j.compstruct.2006.11.005.

65. Wisnom, M.R.; Khan, B.; Hallett, S.R. Size Effects in Unnotched Tensile Strength of Unidirectional and Quasi-Isotropic Carbon/Epoxy Composites. *Composite Structures* **2008**, 84, 21–28, doi:10.1016/j.compstruct.2007.06.002.

66. Z. Carl The Flexural Strength of Aramid Fiber Composites. **1978**, 12, 422–430.

67. Czél, G.; Wisnom, M.R. Demonstration of Pseudo-Ductility in High Performance Glass/Epoxy Composites by Hybridisation with Thin-Ply Carbon Prepreg. *Composites Part A: Applied Science and Manufacturing* **2013**, 52, 23–30, doi:10.1016/j.compositesa.2013.04.006.

68. Basha, M.; Wagih, A.; Melaibari, A.; Lubineau, G.; Eltaher, M.A. Microporous and Mesoporous Materials On the Impact Damage Resistance and Tolerance Improvement of Hybrid CFRP / Kevlar Sandwich Composites. **2022**, 333, 1–11.

69. Wisnom, M.R.; Hallett, S.R. The Role of Delamination in Strength, Failure Mechanism and Hole Size Effect in Open Hole Tensile Tests on Quasi-Isotropic Laminates. *Composites Part A: Applied Science and Manufacturing* **2009**, 40, 335–342, doi:10.1016/j.compositesa.2008.12.013.

70. Mariatti, M.; Nasir, M.; Ismail, H. *The Effects of Hole Locations and Hole Sizes on Damaged Behaviour of Woven Thermoplastic Composites*; 2001; Vol. 20;

71. Subagia, I.D.G.A.; Kim, Y.; Tijing, L.D.; Sang, C.; Kyong, H. Composites : Part B Effect of Stacking Sequence on the Flexural Properties of Hybrid Composites Reinforced with Carbon and Basalt Fibers. *COMPOSITES PART B* **2014**, 58, 251–258, doi:10.1016/j.compositesb.2013.10.027.

72. Bazhenov, S.L. Bending Failure of Aramid Fibre-Reinforced Composite. *Composites* **1995**, 26, 757–765.

73. Kretsis, G. A Review of the Tensile, Compressive, Flexural and Shear Properties of Hybrid Fibre-Reinforced Plastics. *Composites* **1987**, 18, 13–23, doi:10.1016/0010-4361(87)90003-6.

**Disclaimer/Publisher's Note:** The statements, opinions and data contained in all publications are solely those of the individual author(s) and contributor(s) and not of MDPI and/or the editor(s). MDPI and/or the editor(s) disclaim responsibility for any injury to people or property resulting from any ideas, methods, instructions or products referred to in the content.