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Article

Numerical Simulation of a Valorisation-Oriented Hybrid Process for the Bio-Oil-Related Separation of Acetol and Acetic Acid

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Abstract: Biomass as a whole offers a more diverse potential for valorisation than any other renewable energy source. As one of the stages in the separation of bio-oil involves the liquid mixture of acetol and acetic acid, and as both components are particularly well suited for valorisation, a hybrid method has been developed for their separation with a high purity level through an approach combining liquid-liquid extraction and rectification. In order to design and simulate the flowsheet, the ChemCAD 7.0 simulation software has been used. Sensitive analyses have been carried out to investigate the influence of the different parameters in the rectification columns such as the reflux ratio, the feed stage location, and the vapour/bottom molar flow ratio. The effect of different extractants and of their excess on the separation process as well as the possibility of regenerating the extractant has also been studied. Tri-n-octylamine has accordingly been selected as a separating agent which has been fully recycled. The end result for separating an initial 48/52 wt% acetol/acetic-acid liquid mixture has been acetol with a purity of 99.4 wt% and acetic acid with a purity of 100 wt%.

Keywords: simulation; modelling; separation; bio-oil; acetol; acetic acid; extraction; distillation

1. Introduction

Environmental protection and sustainable development require to resort to every renewable energy source available, such as solar and wind, and the integration of these sources often requires interdisciplinary action [1–5]. For biomass, additional research into valorisation of the large range of diverse by-products is gaining more and more attention [3,4,6–9]. Biomass can indeed be used directly as a fuel but it can also be used to separate and valorise interesting molecules either present in the biomass structure, such as aromatics and sugars, or arising during a process such as pyrolysis. Pyrolysis, which is one of the most promising valorisation methods [8–11], gives rise to three product streams: gas, bio-oil, and biochar [6,12–15]. Bio-oil is made up of an organic fraction and an aqueous one, both containing a complex mixture of compounds [16–19]. The organic fraction of bio-oil contains mainly phenolic compounds and lignin derivatives [20,21] whereas the composition of the aqueous fraction is highly variable, depending mainly on the starting biomass and the pyrolysis conditions. Comprehensive studies of the aqueous phase of bio-oil from different biomasses show levoglucosan, acetic acid, furfural and acetol [22–24].

During the bio-oil separation process, a mixture of acetol and acetic acid (A/HAc) is obtained. Both components of the mixture are widely used in industry and households, which is the reason why they have been taken into consideration in the present study. Acetol, which is also known as hydroxyacetone, is one of the α -hydroxyketone compounds (1-hydroxy-2-propanone). Acetol is used as an organic intermediate because it contains both hydroxyl and carbonyl functional groups and it is mainly used to produce polyols, acrolein and heterocyclic compounds [25–27]. It is also widely

used as a dye and skin tanning agent. Furthermore, the commercially available acetol is made from petroleum which is incompatible with sustainable development and leads to high production costs. Acetic acid is the most widely used aliphatic carbonic acid. It is frequently used as a solvent in the manufacture of cellulose acetate and many pharmaceutical products [28–31]. The use of acetic acid in plants is also beneficial for improving drought tolerance and reducing growth inhibition in agricultural fields [32].

Within the pyrolysis oil, these two chemicals are among the high-added-value oxygenates which are the most present in substantial amounts, namely acetol (7.4%), acetic acid (12%), and glycolaldehyde (13%) [33,34]. Due to the poor thermal stability of the pyrolysis oil, direct distillation of these oxygenates is however not possible. In the case of the A/HAc mixture which has been chosen as the model fluid in this study, its separation proves difficult and requires a great deal of effort. Several methods have already been investigated for separating different compounds from the aqueous fractions of pyrolysis oil. The most common technique is liquid–liquid extraction with organic solvents or water extraction to extract the phenolic compounds from the bio-oil [33,35]. Liquid-liquid reactive extractions have been extensively studied for the recovery of acetic acid from aqueous solutions [36,37]. Conventional extraction techniques with organic solvents may be used but lead to a certain amount of the solvent ending up in the pyrolysis oil phase [38]. Other separation techniques such as fractional condensation [39], adsorption [40], or crystallisation [41] have also been proposed for extracting specific chemicals or separating certain chemical groups from bio-oil. The objective of this study has therefore been to develop a hybrid method for the A/HAc mixture separation with a high purity level based on a combination between liquid-liquid extraction and conventional distillation [42,43] with an appropriate choice of extractants.

Using the commercial simulation software ChemCAD, a steady-state computer model of the A/HAc mixture separation process has been implemented to design the flowsheet. Several technological options and optimisation and sensitivity analyses have been carried out in order to determine the optimal operating conditions. In this way, the study develops theoretical strategies for acetol/acetic-acid separation with a view to future application in industrial production.

2. Process and Flow Sheet Development

An analysis of the vapour-liquid equilibrium in the A/HAc system, as represented in Figure 1, serves as a starting point for selecting a separation method for this system.

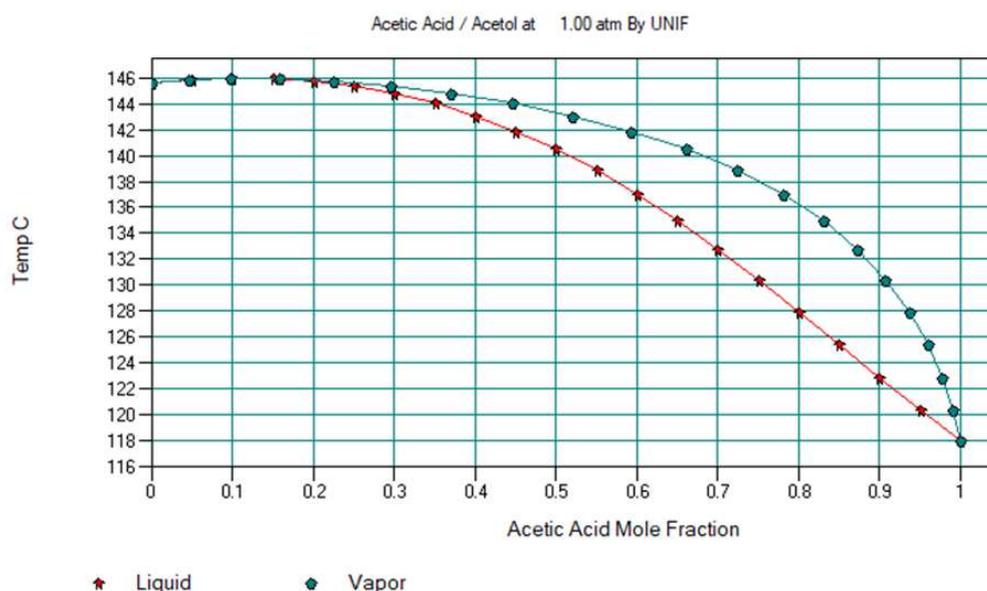


Figure 1. Equilibrium data for the A/HAc system.

It can be seen from Figure 1 that the two components do not form an azeotrope but, for acetic acid concentration below 25mol%, the vapour and liquid-phase curves are almost bonded, which makes the separation of these two substances very difficult by conventional distillation. It would indeed require columns with a large number of stages operated at high reflux ratio and requiring high energy operating costs.

In order to separate a binary mixture which is difficult or impossible to separate by ordinary means, a third component, namely a separating agent, must be added. To separate the A/HAc system, a combined process involving liquid-liquid extraction and distillation has accordingly been proposed. This process has been simulated by using the ChemCAD software. The flow diagram is shown in Figure 2.

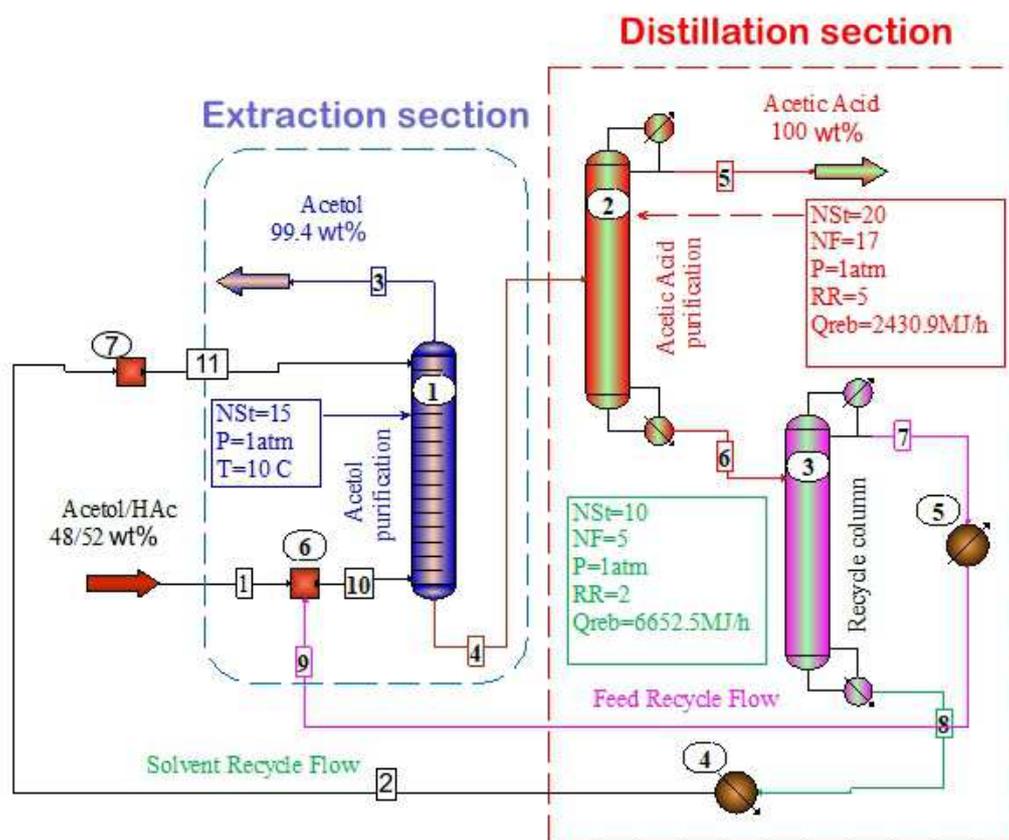


Figure 2. Flowsheet for A/HAc separation.

The extraction column 1 (stream 10) is fed with the A/HAc mixture and the HAc extraction is carried out at 10°C using the extractant. The upper part of the column, namely the light phase, produces pure acetol (stream 3). A mixture of extractant and acetic acid, also containing a small amount of acetol, (stream 4) is removed in the lower part of the column, namely the heavy phase, and then enters the distillation column 2. Pure HAc (stream 5) is distilled off at the top of column 2 and a mixture of extractant, HAc and acetol (stream 6) is separated as a residue in its lower part. This residue is then used for separation in the distillation column 3, after which a pure extractant (stream 8) is released as a residue at the bottom of column 3, which, after cooling in heat exchanger 4, returns to extraction column 1 (stream 2). A mixture of A/HAc (stream 7) is removed as a distillate from column 3, which, after cooling in heat exchanger 5 (stream 9), is mixed with the primary feed (stream 1) in mixture 6 in order to feed stream 10 in extraction column 1.

The extraction column is simulated using the liquid-liquid extraction module of the ChemCAD software. The module estimates the heat and mass transfer of a stagewise contact of two immiscible liquid mixtures. It can use up to five feeds and six products. This unit permits up to 300 stages and accommodates stage efficiencies. the Newton-Raphson simultaneous convergence technique is used

for the solution of this module. The Simultaneous Correction Distillation System (SCDS) module is used to simulate the distillation columns in the ChemCAD software. SCDS is a rigorous multi-stage vapour-liquid equilibrium module. It can be used to simulate any single column including distillation columns, absorbers, reboiled absorbers and strippers. In particular, the Murphree's tray efficiency can be entered and simulated. In order to estimate rigorously the derivatives of each equation, the Newton-Raphson convergence method is applied. Side products and side heaters/coolers can also be modelled rigorously by SCDS. This module is mainly designed to simulate non-ideal K-value chemical systems. SCDS switches columns with unlimited stages, five feed streams, and four side products. The rigorous simulation of the multiphase (two-phase or three-phase) distillation systems can be performed. If the calculation concerns a three-phase system, the user has the option to decant one of the liquid phases in the condenser, while refluxing the other.

3. Results and Discussion

3.1. Liquid-Liquid Extraction

To describe the liquid-liquid (LL) extraction process, a counter-current extraction column model with a theoretical number of stages has been used [44]. ChemCAD's Liquid-Liquid Extraction module calculates the heat and material balance of bringing two immiscible liquid mixtures into contact in stages. Up to five feeds and six products can be obtained with this unit. The extraction module uses the Newton-Raphson simultaneous convergence technique for its solution. As a first approximation, 15 theoretical stages have been set. A sensitive study of the influence of the number of theoretical stages on the separation efficiency of the system has been carried out.

Four factors mainly affect the results of the numerical experiments:

- the initial concentration of the liquid-liquid mixture;
- the thermodynamic equilibrium of the system;
- the type of separating agent (extractant);
- the amount of extractant.

The effect of each factor and its control are detailed in the subsequent subsections.

3.1.1. Initial Concentration of the Liquid-Liquid Mixture

The initial concentration of the separation mixture affects the final extraction results. This is related to the selectivity of the used extractant with respect to the individual components of the system. In this case, the extractants solvate basically HAc, but also the acetol in small amounts.

Therefore, at high concentrations of acetol in the feed mixture, it will be present not only in the light fraction (where acetol is the target product) but also at significant amount in the heavy phase (where acetol is an undesirable product). To take this phenomenon into account, the experiments have been divided into two identical series. In the first series, the concentration of acetol in the feed mixture is high, around 50 mol%, while in the second it is low, around 10 mol%.

As mentioned above, from the point of view of the separation of the A/HAc mixture, the unfavourable case is when the concentration of acetol in the feed mixture is high. Therefore, results for this case only are presented. In addition, the acetol concentration in the feed mixture of around 50 mol% corresponds to the more common case in practice. The optimal working conditions determined for this case will also be valid for the case where the concentration of acetol in the feed mixture is low.

3.1.2. Thermodynamic Equilibrium of the Liquid-Liquid System

A correct description of the thermodynamics of the LL system is very important for the accuracy of the final results. This can be well achieved when experimental equilibrium data for the binary LL system of the extractant and the compound in the mixture are available. In the numerical experiments, several organic solvents have been tested as extractants (see next section).

Finding or obtaining experimental data for all combinations of binary components is difficult and time consuming. For this reason, the UNIFAC 'LLE' model has been used as a first approximation to describe the thermodynamics of the system [45,46]. UNIFAC uses the functional groups present on the molecules that make up the liquid mixture to calculate activity coefficients. By using interactions for each of the functional groups present on the molecules, as well as some binary interaction coefficients, the activity of each of the solutions can be calculated. The UNIFAC 'LLE' model is based on the Gibbs excess energy description and is designed to theoretically predict liquid-liquid equilibria (LLE). In practice, the binary interaction parameters regressed from vapour-liquid equilibrium (VLE) data are insufficient to predict the LLE behaviour. The UNIFAC 'LLE' is obtained from the UNIFAC model which uses binary interaction parameters regressed from LLE data [47]. Although the UNIFAC 'VLE' model equations are used without change, the values of the group interaction parameters differ from the UNIFAC 'VLE' model. The LLE parameters have been regressed between 10 and 40°C since the model may not be relevant outside this range. Typically, a second liquid phase will not be present outside this range.

During numerical experiments, it was found that decreasing the temperature favoured the extraction process. The results presented in this study are therefore obtained from numerical experiments at 10°C.

3.1.3. Separating-Agent Selection

The type of extractant is essential for the final extraction result. In general, the extractant must have a high selectivity with respect to the target component and a high extraction capacity. It should preferably be non-toxic, easy to regenerate, inexpensive and do non-corrosive.

Our concept has been to determine an extractant that dissolves the acetic acid so that, after the liquid-liquid extraction process, pure acetol (light phase) and a mixture of acetic acid and extractant (heavy phase) would be obtained. According to literature [48–52], good solvents of HAc include tertiary amines, cyclopentane, and toluene. In this study, the following solvents have been used to carry out the numerical experiments: di-n-octylether; tri-n-octylamine; tributylamine; tri-n-pentylamine; cyclohexane; toluene; n-heptane; n-decane.

3.1.4. Amount of Extractant

The amount of extractant has a strong influence on the composition of the final products. In this case, the amount of extractant depends on two basic criteria:

1. producing acetol with a purity of 99 mol% in the light phase;
2. producing the smallest possible amount of acetol in the heavy phase.

In order to study the effect of the extractant amount while taking into account the above two criteria, a sensitive analysis has been carried out. All the numerical experiments have been performed with an initial compound feed rate of 1247 kg.h⁻¹ HAc and 1132 kg.h⁻¹ acetol (50-50 mol%). During the sensitive analyses, the amount of extractant varied from 1,000 to 10,000 kg.h⁻¹.

Figures 3 and 4 show the results of sensitive analysis using tri-n-octylamine as an extractant. Figure 3 shows the acetol amount in the extract (stream 4 in Figure 2) as a function of solvent flow rate. Since a larger amount means higher losses, acetol is an undesirable component there.

Figure 4 shows the concentration of acetol in the raffinate (stream 3 in Figure 2) as a function of solvent flow rate. Since stream 3 represents the yield of pure acetol, the concentration of acetol in this stream should be at a maximum (greater than 99%).

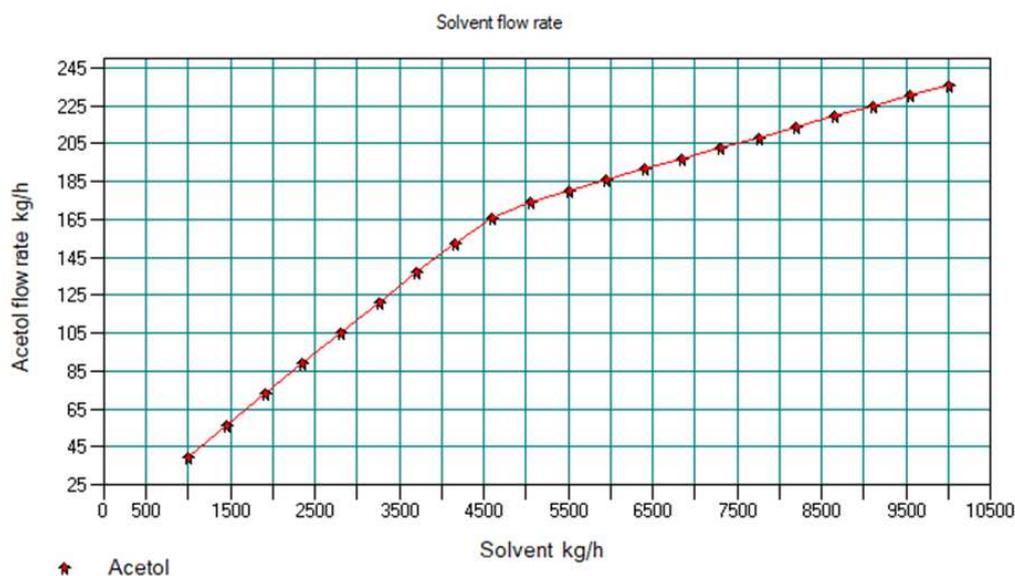


Figure 3. Acetol amount in the extract as a function of solvent flow rate.

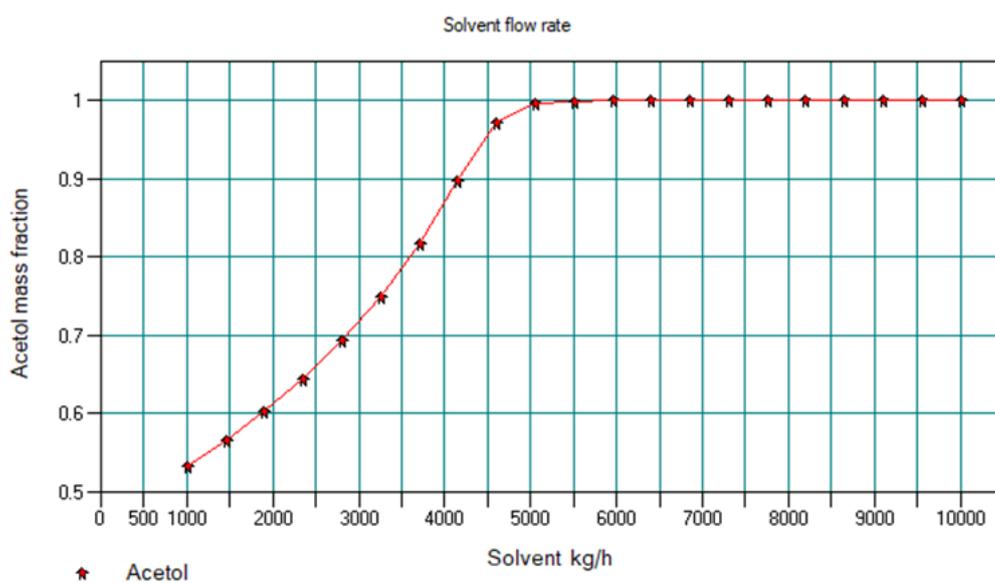


Figure 4. Acetol concentration in the raffinate as a function of solvent flow rate.

Figures 3 and 4 show that, by increasing the extractant flow rate, the purity of the upper-end product of column 1 (light phase) is improved while the amount of acetol in the heavy phase simultaneously increases. From the above, it can be concluded for instance that, for an optimal flow rate of tri-n-octylamine of $5000 \text{ kg}\cdot\text{h}^{-1}$, the amount of acetol in the lower-end product is $174.02 \text{ kg}\cdot\text{h}^{-1}$ and the acetol concentration in the upper-end product is 99,41 wt%. Similar analyses have been carried out for the other extractants used in this study. The results are summarised in Table 1.

Table 1. Numerical experiment results at initial composition A/HAc 50-50 mol%.

Solvent	Optimal Solvent Flow Rate [kg.h ⁻¹]	Upper-End Acetol Fraction [wt%]	Lower-End Acetol Flow Rate [kg.h ⁻¹]
di-n-octylether CAS 629-82-3	3200	99.46	155.12
tri-n-octylamine CAS 1116-76-3	5000	99.41	174.02
tri-n-butylamine CAS 102-82-9	3300	99.02	201.14
cyclohexane CAS 110-82-7	4000	95.89	97.35
tri-n-pentylamine CAS 621-77-2	3700	99.12	140.56
toluene CAS 108-88-3	6800	77.79	212.63
n-heptane CAS 142-82-5	4200	98.21	82.76
n-decane CAS 124-18-5	4400	99.01	61.20

As the toluene flow rate increases, the concentration of acetol in the extract increases, reaching a plateau with a maximum of 77.79 wt% of acetol. Since the desired purity of the acetol cannot be achieved with this extractant, it is unsuitable for use. The same applies to cyclohexane and n-heptane.

Table 1 shows that the best results are obtained with tri-n-octylamine and n-decane. Since tri-n-octylamine and n-decane require a flow rate of 5000 kg.h⁻¹ and 4400 kg.h⁻¹ respectively, n-decane proves to be more advantageous than tri-n-octylamine in that respect. Furthermore, the amount of acetol in the heavy phase (which has to be subsequently separated) is lower when n-decane is used. From this point of view, n-decane seems more appropriate. It can however be concluded that both solvents can be successfully used as extractants to separate the A/HAc system.

3.2. Acetic-Acid Purification

To regenerate the extractant, it is more convenient to use a distillation process. The possibility of regenerating the two selected extractants by distillation is discussed below. The equilibrium of the following ternary systems, tri-n-octylamine/A/HAc and n-decane/A/HAc, is modelled by the NRTL approach using the residual curve map topology. The general NRTL equation linking the activity coefficient γ_i to the molar concentrations x_j of the different components is:

$$\ln \gamma_i = \frac{\sum_{j=1}^{N_c} (\tau_{ji} F_{ji} x_j)}{\sum_{k=1}^{N_c} (F_{ki} x_k)} + \sum_{j=1}^{N_c} \left[\frac{(F_{ji} x_j)}{\sum_{k=1}^{N_c} (F_{ki} x_k)} \left(\tau_{ij} - \frac{\sum_{k=1}^{N_c} \tau_{kj} F_{kj} x_k}{\sum_{k=1}^{N_c} F_{kj} x_k} \right) \right] \quad (1)$$

where

$$F_{ji} = \exp(-\alpha_{ij} \tau_{ji}) \quad \text{and} \quad \tau_{ji} = a_{ij} + \frac{b_{ji}}{T}$$

α_{ij} is a non-randomness parameter, and a_{ij} and b_{ij} are the temperature-dependent and temperature-independent binary interaction parameters respectively.

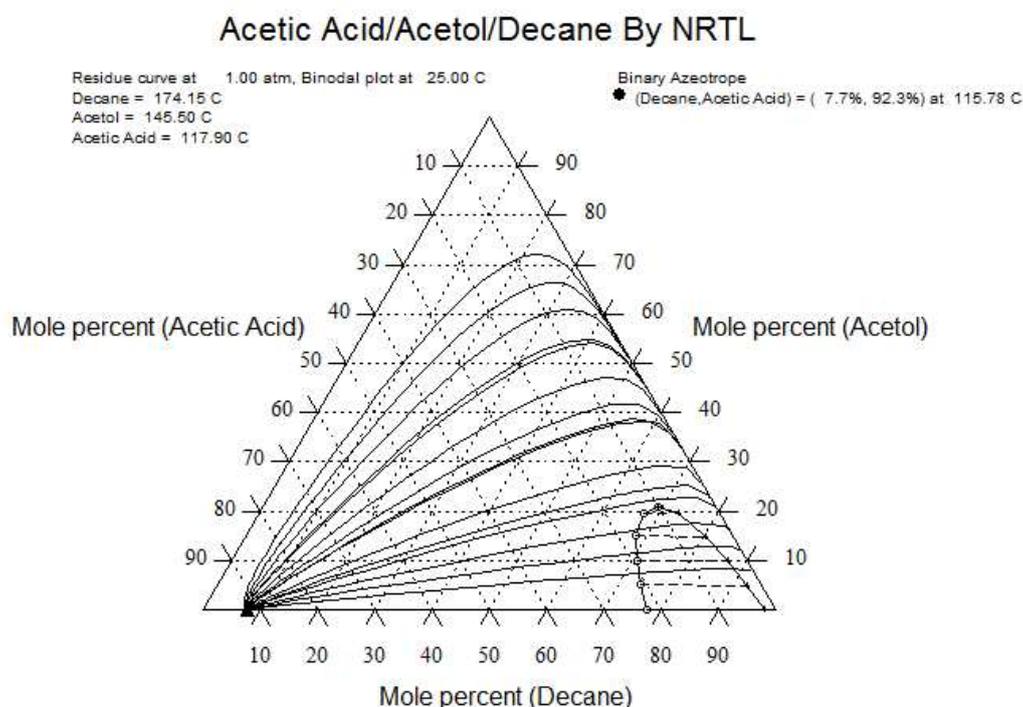
Experimental equilibrium data for binary vapour-liquid equilibria were taken from the literature for the acetic-acid/acetol system. For the other two systems, the binary equilibria were determined by the UNIFAC method. The coefficients are given in Table 2.

Table 2. Binary interaction parameters for the NRTL model.

System	α_{ij}	α_{ji}	b_{ij}	b_{ji}	α_{ij}	source
tri-n-octylamine /acetic acid	0	0	2099.406	-411.6049	0.3998	UNIFAC
acetic acid/acetol	0.531	-1.732	-543.900	1326.0000	0.3000	Ch. Stephan et al. [53]
tri-n-octylamine /acetol	0	0	2499.792	196.9379	0.2000	UNIFAC

Results are shown in Figures 5 and 6. From Figure 5, it can be seen that in the n-decane/A/HAc system, a double azeotrope is formed between n-decane and HAc. The composition of the azeotrope is 7.7 mol% n-decane and 92.3 mol% HAc with a boiling temperature of 115.78°C. Since the boiling temperature of pure HAc is 117.9°C, this azeotrope would accumulate in the distillate. As a result, the HAc obtained in the distillate would not be of sufficient purity. It is therefore not possible to separate HAc with a purity greater than 92.3 mol% using the conventional distillation process. Due to its inability to separate HAc, n-decane cannot be used as an extractant in this process.

Figure 6 shows that there is no such azeotrope in the octylamine/A/HAc system. It is therefore still possible to separate HAc from the extractant using a conventional distillation process.

**Figure 5.** Equilibrium predicted for the n-decane/A/HAc system.

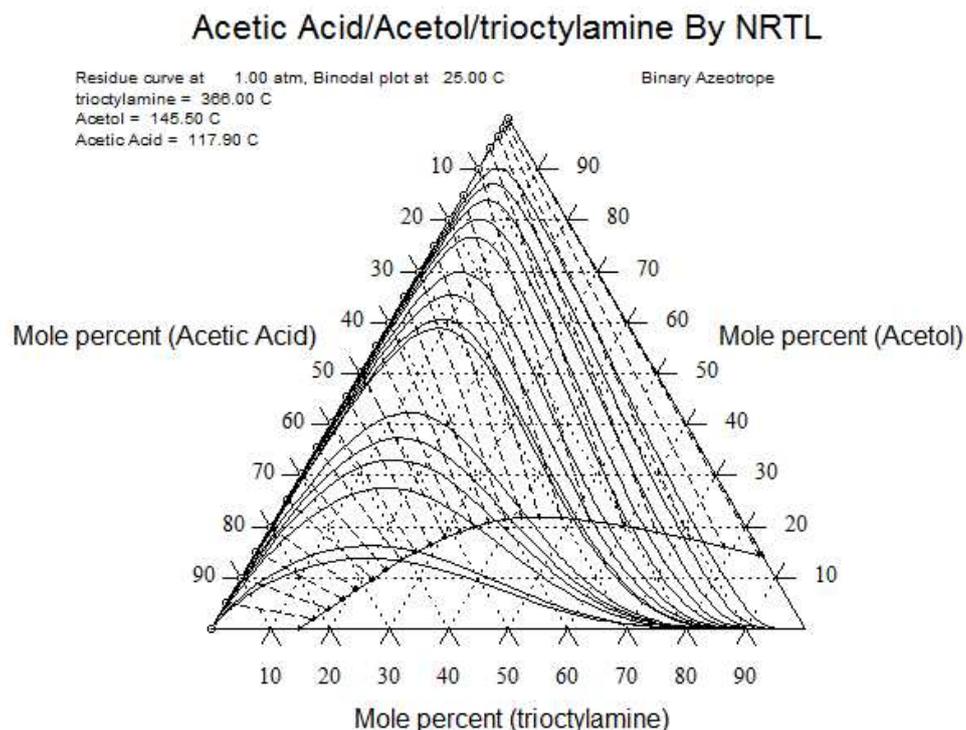


Figure 6. Equilibrium predicted for the tri-n-octylamine/A/HAc system.

3.2.1. Thermodynamic Equilibrium in Vapour-Liquid Systems

A correct modelling of the vapour-liquid equilibrium in the trioctylamine/A/HAc system is important for the final result. The classical UNIFAC method has been selected to describe the VLE.

3.2.2. Production of Pure Acetic Acid

Pure acetic acid is produced in distillation column 2 whose primary requirement is to produce pure HAc as a distillate at its upper end. In addition, the concentration of HAc in the residue (at the lower end of the column) must be low enough to promote further purification of the extractant in column 3. The results of the numerical experiments show that the optimal number of stages is 20 and the optimal feed stage location is 17.

Composition profiles can be accessed after the simulation in each column configuration window. Figures 7 and 8 show the concentration and temperature profiles in column 2 obtained after optimisation.

In order to optimise the performance of column 2, sensitive studies have been carried out by varying the reflux ratio and the vapour/bottom molar flow ratio. The best results obtained from these analyses are a reflux ratio of 5 and a vapour/bottom molar flow ratio of 2. Under these conditions, HAc with a purity of 100 wt% has been obtained whereas the residue from column 2 contains HAc (19.19 wt%), acetol (1.85 wt%), and tri-n-octylamine (78.95 wt%).

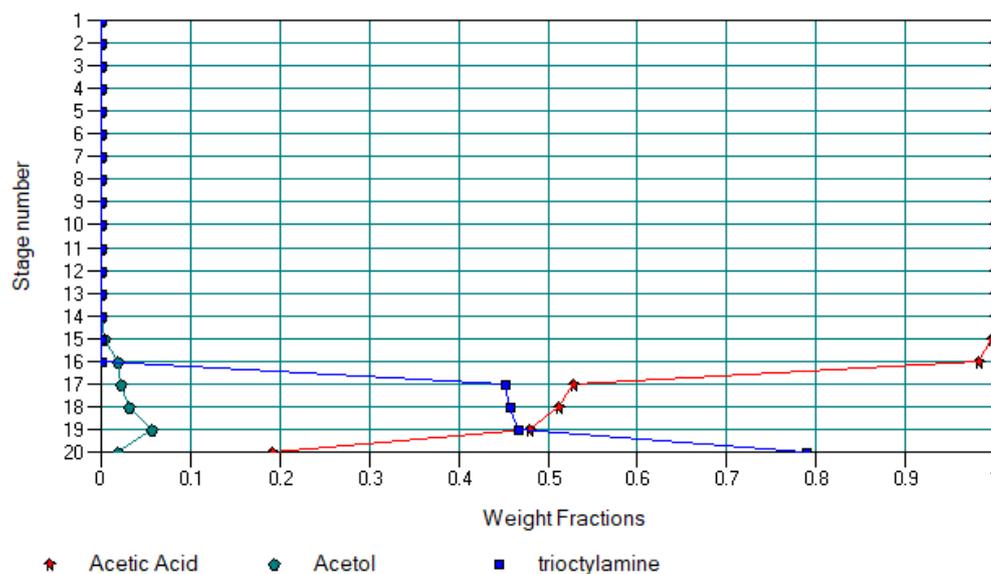


Figure 7. Tray liquid concentration profile in column 2.

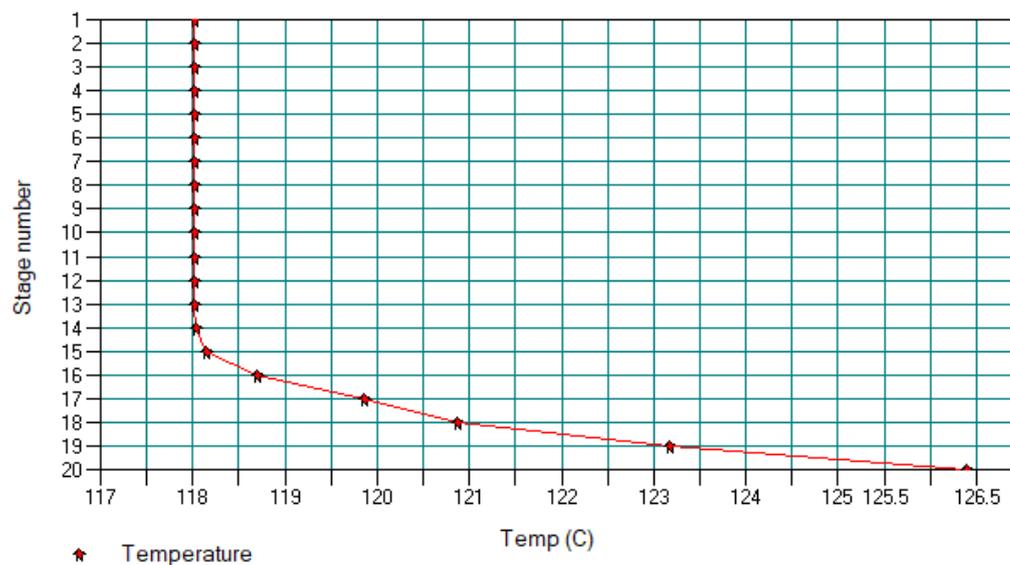


Figure 8. Tray temperature profile in column 2.

3.3. Extractant Regeneration

Before re-use, the extractant (tri-n-octylamine) must be purified from the residues of column 2 which also contain HAc and acetol. This is done in distillation column 3 (see Figure 2) where HAc (91.13 wt%) and acetol (8.87 wt%) are removed. After cooling in heat exchanger 5, this mixture is re-separated in column 1. Moreover, tri-n-octylamine is obtained as a residue of column 3 with a purity of 99.84 wt%. After cooling in heat exchanger 4 (stream 8), this purified extractant is returned to column 1 (stream 2).

Figures 9 and 10 show the concentration and temperature profiles in column 3. It can be seen from Figure 9 that tri-n-octylamine accumulates at the top of the column. The concentration of the

extractant down from the feed stage location (stage 5 in column 3 on Figure 2) decreases and at the bottom of the column reaches practically zero. Thus, practically 100% of the used tri-n-octylamine is regenerated.

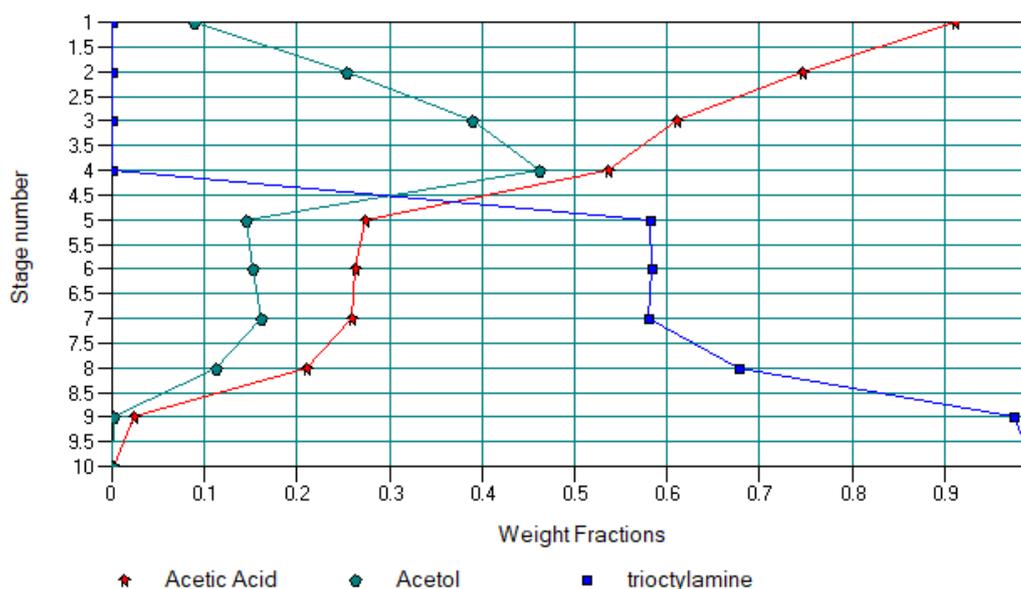


Figure 9. Tray concentration profile in column 3.

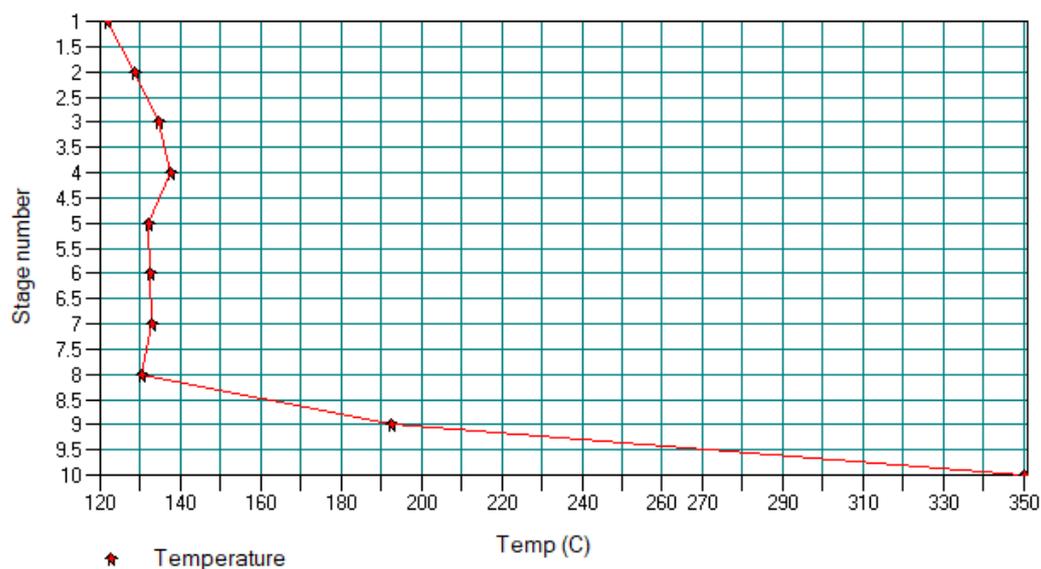


Figure 10. Tray temperature profile in column 3.

In order to optimise the performance of this column, sensitive analyses have been carried out by varying the reflux ratio and the location of the feed stage. The optimal result obtained is 10 stages, a reflux ratio of 2 and a lower-end product temperature of 350°C. The optimal location for the feed stage is 5. As a result, the treatment scheme designed for the separation of the A/HAc mixture is compact and ensures minimal equipment costs. The flowsheet is fed with the A/HAc mixture. The streams leaving the flowsheet are mostly acetol (99.4 wt%) and pure acetic acid (≈ 100 wt%). There is

therefore no by-product waste. All intermediate flows are included in recycling and are 100% recovered. The energy optimisation of the designed flowsheet is beyond the scope of this study and is therefore not included in this article.

4. Conclusions

This study can be seen within the wider context of valorisation and biomass processing, as the separation of a liquid mixture made up of components such as acetol and acetic acid shows by extension on the one hand that molecules with high added value deserve to be identified and, on the other hand, that separating those molecules may still be possible using a hybrid process when individual processes fail.

In the present case, the hybrid process has consisted of a combination of liquid-liquid extraction and distillation following a literature review of the possibilities for separating the liquid mixture, so that their advantages could be combined whereas their disadvantages would be minimised. A flowsheet combining one liquid-liquid extraction column and two distillation ones has been designed using the ChemCAD software and the NRTL and UNIFAC 'LLE' models have been used to determine the thermodynamic equilibrium of the liquid mixtures. Sensitive analyses have been carried out to determine the key end-product parameters for all columns. The effect of different extractants and of their excess on the separation process as well as the possibility of regenerating the extractant has also been studied. Tri-n-octylamine has accordingly been selected as a separating agent which has been fully recycled. As a final result, from the initial 48/52 wt% liquid mixture (2379 kg.h⁻¹), acetol (1132 kg.h⁻¹) with a purity of 99.4 wt% and acetic acid (1240.55 kg.h⁻¹) with a purity of 100 wt% have been obtained.

Based on the predictive results of this study, experiments on real systems can be carried out to determine the thermodynamic equilibrium data and hence the parameters of the binary interactions in the tri-n-octylamine/acetol/acetic-acid system. Laboratory experiments would definitively validate the scheme proposed in this study. Beyond this system, this case study paves the way to a much broader research field.

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