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Article

Designing Advanced Multistatic Imaging Systems with Optimal 2D Sparse Arrays

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Abstract: This study introduces an innovative optimization method to identify the optimal configuration of a sparse symmetric 2D array for applications in security, particularly multistatic imaging. Utilizing Genetic Algorithms (GA) in a sophisticated optimization process, the research focuses on achieving the most favorable antenna distribution while mitigating the common issue of secondary lobes in sparse arrays. The main objective is to determine the ideal configuration from specific design parameters, including hardware specifications such as number of radiating elements, minimum spacing, operating frequency range, and image separation distance. The study employs a cost function based on the the point spread function (PSF), the system response to a point source, with the goal of minimizing the secondary lobe levels and maximizing their separation from the main lobe. Advanced simulation algorithms based on Physical Optics (PO) are used to validate the presented methodology and results.

Keywords: Submillimeter wavelength imaging; multistatic imaging; backpropagation imaging; genetic algorithm (GA).

1. Introduction

Active millimeter and sub-millimeter-wave radar systems have become indispensable tools for enhancing civil security in airports, bus stations, crowded areas, and other public places [1]. These non-destructive testing (NDT) systems play a key role in security screening, imaging concealed objects and detecting weapons and drugs, providing effective and safe solutions. However, current monostatic or quasi-monostatic radar systems [2] face limitations in complex geometries due to shadow regions caused by specular reflections falling outside the receiving area.

To overcome this limitation, our proposal integrates multiple wideband millimeter-wave transmitters and receivers to obtain high-resolution radar images in real time [3,4]. Multistatic systems offer several advantages, such as improved detection of stealth objects, reduced susceptibility to interference, and the ability to acquire information from multiple angles. This approach also allows the use of a lower spatial sampling frequency than conventional systems by taking advantage of the cancellation of the secondary lobes.

This paper presents a novel methodology for identifying the optimal 2D sparse matrix configuration to generate multi-static images based on predefined design parameters. Section 2 introduces the architecture, the imaging procedure, and the function that will be used to evaluate possible solutions. In Section 3, we provide an introduction to GAs and explain their specific application to this work. The simulation process is defined in Section 4, while Section 5 presents the obtained results, including a compelling comparison between optimized and non-optimized approaches. Finally, in Section 6 we summarize the achieved objectives and outline potential future approaches to further enhance the efficiency of imaging systems.

2. Multistatic architecture

The architecture of the system relies on multiple transmitters (tx_m) and receivers (rx_n) , positioned at t_m and r_n , respectively [5,6]. Typically, these systems employ large, densely sampled arrays (Eq. 1) to ensure sufficient Fourier space (k-space) coverage, which aids in achieving high resolution by minimizing the presence of secondary lobes.

$$d_{elements} \le \frac{\lambda_{min}}{2} \tag{1}$$

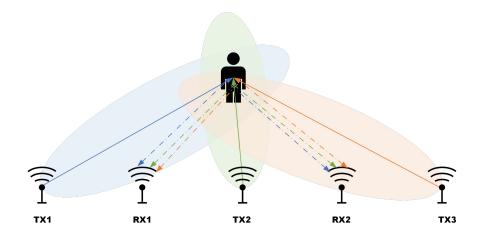
The main purpose of these systems is to be used in real-time personnel security and surveillance applications. Hence, it is crucial to minimize the number of required elements.

2.1. Baseline configuration

This work serves as a prelude to the production of a prototype, which is already in the construction phase. As a result, design constraints have been defined by considering the available hardware and its specific characteristics. Our focus is on analyzing a specific architecture consisting of a 2-D sparse array with 64 transmit antennas (NTX) and 49 receive antennas (NRX) positioned in front of an Object Under Test (OUT). The transmit antennas are spaced equidistantly at a distance of d_{tx} cm, while the receive antennas are also equidistantly spaced at a distance of d_{rx} cm. To ensure symmetrical responses with respect to both the X=0 and Z=0 axes, this equidistance is maintained in both the horizontal and vertical directions. The system operates in the frequency range of 120 to 150 GHz using only 12 different frequencies, which corresponds to a minimum working wavelength (λ_{min}) of 2 mm.

2.2. Imaging

The imaging process implies generating an image for each transmitting antenna, with each image being formed by coherently summing the contributions from individual receptors. The final image is obtained by coherently combining these transmitter images. Figure 1 provides a graphical representation of the described procedure on a simplified system with NTX = 3 and NRX = 2.



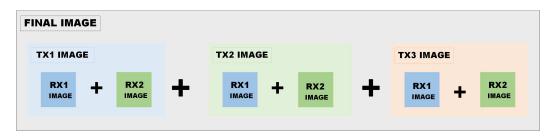


Figure 1. Graph of the imaging process in a simplified system with NTX = 3 and NRX = 2.

2.3. Point spread function

One of the most useful parameters to characterize the behavior of an imaging system is the PSF, which describes the response of a system to a point source target. Based on the reciprocity theorem, the total PSF of the system when focused at the point p_i can be calculated from the PSFs of the transmit and receive arrays as follows [4]:

$$PSF_{rx}(\mathbf{p}_i) = \sum_{l,n} e^{-j\kappa_l |\mathbf{r}_n - \mathbf{p}_i|}$$
(2)

$$PSF_{tx}(\mathbf{p}_i) = \sum_{l,m} e^{-j\kappa_l |\mathbf{t}_m - \mathbf{p}_i|}$$
(3)

$$PSF_{total}(\mathbf{p}_i) = PSF_{rx}(\mathbf{p}_i) \times PSF_{tx}(\mathbf{p}_i)$$
(4)

where multiple frequencies f_l are used to generate the images in an Ultra Wide Band (UWB) radar configuration, and κ_l is the wavenumber at the l-th frequency. The PSF calculation is employed to determine the optimal array size for the imaging system.

Knowledge of the PSF is invaluable in many ways. It plays a key role in determining the resolution of the system, which represents the size of the main beam, and also provides valuable information about the dimensions and position of the secondary lobes surrounding the main beam. The presence of secondary lobes is a critical factor because it directly affects the quality of the images produced by the imaging system. To achieve the desired results, it is important to identify a configuration with a minimum number of secondary lobes. It has been observed that it is also beneficial to place these secondary lobes as far away from the main lobe as possible. This helps reduce aliasing between responses and increases the field of view (FoV) of the system, improving its imaging capabilities.

3. Genetic Algorithm

GAs have proven to be effective in finding solutions to real-world problems [7,8]. They operate on a population of individuals, where each individual represents a potential solution to the problem at hand. The fitness of each individual is evaluated based on its ability to solve the problem. Highly fit individuals are given the opportunity to reproduce by mating with other individuals in the population, resulting in an offspring that inherits certain characteristics from their parents. Through this process, less fit individuals are less likely to be selected for reproduction and eventually die out, leading to the emergence of a new population with potentially better solutions. The algorithm combines the best individuals from the current generation with recombination (crossover) and mutation to create a new set of individuals. As a result, successive generations tend to improve upon the previous ones as the best-performing individuals reproduce and exchange genetic information. By encouraging the combination of the most promising individuals and using mutations to avoid optimization stalling, genetic algorithms are able to efficiently explore the most favorable regions of the search space. The basic operation of GA is depicted in Figure 2.

A well-designed GA is capable of converging on an optimal solution to a given problem. A notable strength of GAs is their ability to handle diverse problem domains, including those that are traditionally challenging for other methods. Since GAs cannot guarantee to find the globally optimal solution due to their inherent randomness, there is a possibility that they will converge to a local minimum without reaching the optimum. Nevertheless, GAs are generally capable of quickly finding solutions that are good enough for practical purposes.

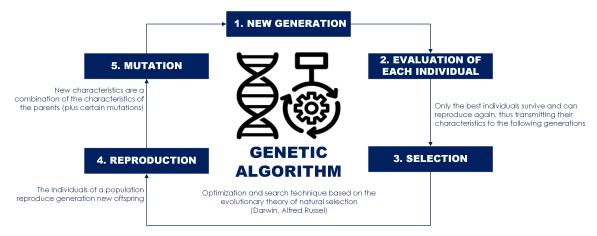


Figure 2. Basic GA operation.

3.1. Custom GA configuration

In this work, GA is used to compute the optimal value of the distance between the receiving elements (d_{rx}) while keeping the distance between the transmitting elements (d_{tx}) fixed. When we first started using GAs, attempts were made to optimize both variables simultaneously, but it turned out that setting the value of d_{tx} to cover the desired aperture and calculating the optimal value of d_{rx} proved to be more efficient.

To evaluate which values are most appropriate, a custom cost function is defined based on the PSF of the system. The best configuration will be the one with the lowest sidelobes. As stated in Section 2.1, this work corresponds to the pre-prototype phase, so the configurations must satisfy specific design constraints:

- The aperture size (horizontal and vertical) cannot exceed 100 cm.
- Due to hardware limitations, the minimum distance between elements is set to 2 cm.
- The array is symmetric on both the X and Z axes.
- Transmitter elements are equispaced in two dimensions (both horizontally and vertically). So are the receivers.

The process is computationally expensive as the GA solver needs to construct the corresponding architecture, calculate the PSF, and evaluate the cost function for each possible pair of d_{tx} - d_{rx} values. Despite this, utilizing GPU acceleration and MATLAB's vector computation capabilities allows us to obtain preliminary results quickly and efficiently. Fixing d_{tx} and optimizing only for d_{rx} yields results in less than 3 minutes and 18 seconds. If d_{tx} and d_{rx} are optimized simultaneously, the process takes approximately 15 minutes.

4. Simulation

A PO based simulator for THz imaging systems is used [9,10]. The simulator performs a two-step simulation of the electromagnetic response of the imaging system to an arbitrary OUT. In the first step, the simulator calculates the induced electric currents in the OUT by considering the interaction between the incident electromagnetic wave and the material properties and geometry of the OUT. By solving Maxwell's equations, the simulator determines the distribution of the induced currents on the surface of the OUT. The simulator then calculates the field received at each receiver from the field generated by the eddy currents. This process is repeated independently for each transmit antenna and each single frequency (f_l).

For radiation modeling, both the transmit and receive antennas are represented as ideal spherical sources. The OUTs are imported into the simulator as CAD models. Reflectivity images are obtained by applying SAR techniques, as referenced in [11]. The final reflectivity image is normalized to its maximum value for display purposes.

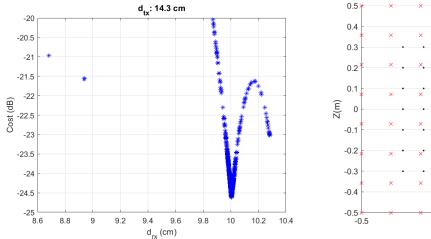
5. Results

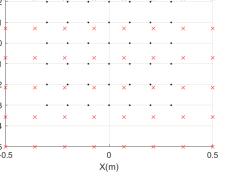
The results presented were obtained using the hardware described below:

- HW-1: Laptop
 - 12th Gen Intel® Core™ i7-12700H @ 2.70 GHz
 - RAM: 32 GB
 - Number of Cores: 14 (20 logical cores per physical)
 - $1 \times \text{NVIDIA}$ GeForce RTX 3070 Ti Laptop GPU
 - Memory: 8 GB (GDDR6 SDRAM) Number of CUDA Cores: 5888
- HW-2: Server GPU
 - 32×13 th Gen Intel® CoreTM i9-13900K @ 5.80 GHz
 - RAM: 128 GB
 - Number of Cores: 24 (32 logical cores per physical)
 - 1 × NVIDIA GeForce RTX 4090
 - Memory: 24 GB (GDDR6X)
 - Number of CUDA Cores: 16384

5.1. Optimal 2D-sparse array

To prove the performance of the method, an architecture with 64 transmitter elements (NTX) and 49 receiver elements (NRX) is used. The desired aperture size is 1 m, both in range and cross-range. To achieve the desired aperture size, d_{tx} is set to 14.3081 cm. Considering the physical characteristics of the array elements, a minimum spacing of 2 cm is maintained between them. As previously mentioned, the system operates in the frequency range of 120 GHz to 150 GHz. Considering all these design factors, the initial step involves using GA to determine the optimal d_{rx} . Figure 3 (a) shows the values taken by d_{rx} in a given optimization and the associated costs until the optimal value is reached. The optimization results yielded d_{rx} = 10.0103 cm, which is utilized to construct the optimal architecture (Figure 3 (b))





Receivers

(a) Values taken by d_{rx} during optimization and associated costs. GA convergence at 10.0103 cm

(b) Optimized architecture

Figure 3. Optimal 2D-sparse array architecture via GA ($\frac{d_{rx}}{d_{tr}} = 0.7$).

5.1.1. PSF

Figure 4 displays the PSF at 3 meters of the architecture that was constructed from the value obtained in the GA optimization. The presence of the secondary lobes is observed about \approx 13 cm from

the main lobe and with a magnitude 24.6 dB below that of the main lobe. Figure 4 shows the PSF in (a) XZ plane and (b) X cut when Z = 0.

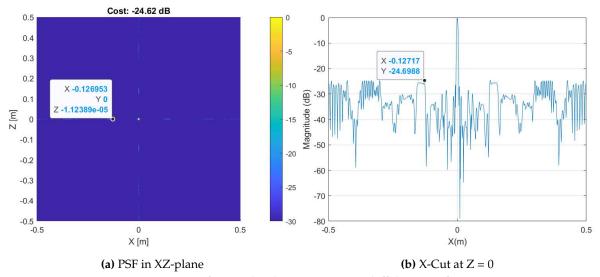


Figure 4. PSF of optimal architecture at a standoff distance of 3 m.

The nature of these architectures and the non-compliance with the Nyquist criterion make the presence of these diffraction lobes inevitable, which limits the FoV of the reconstruction and directly affects the quality of the images that the system can produce.

Without the aid of these tools, the most intuitive way to design the architecture would be to distribute the transmitters and receivers equidistantly along the X and Z axes. Thus, to achieve an aperture of 1 m, the distance between the elements should be 13.33 cm. Figure 5 (a) shows the resulting configuration and Figure 5 (b) shows the PSF response at 3m. The presence of several secondary lobes extremely close in magnitude to the main lobe is not a good sign, as it implies a significant degradation in the quality of the recovered images. The improvement of the optimized system over the non-optimized one is remarkable.

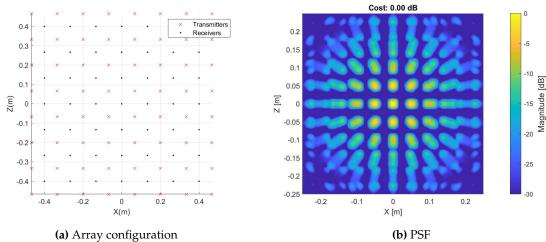


Figure 5. Non-optimized array configuration and its corresponding PSF.

5.1.2. Imaging

To validate the performance of the presented configuration, a model based on a 1951 USAF MIL-STD-150A resolution test chart was used as OUT. This type of geometry consists of several groups of bars (in this specific case modeled as metal plates) separated by a certain distance, and is widely used to analyze and validate imaging systems. The CAD model used in the following simulation is

shown in Figure 6 (a) and Table 1 specifies its geometry.

To perform the experiment, the OUT is placed at a standoff-distance of 3 m. As can be seen in Figure 6 (b), the reconstruction replicates all the details of the original image. This shows that the system has a very high resolution, since it is able to reconstruct all the elements of the two groups of bars, which indicates that it is able to detect targets with an accuracy of less than 1 mm.

RESOLUTION (rr) ANALYSIS		
DISTANCE BETWEEN BARS		
	GROUP NUMBER	
ELEMENT	-2	-1
1	2.5 cm	0.85 cm
2	1.75 cm	0.75 cm
3	1.5 cm	0.5 cm
4	1 cm	0.25 cm
5		0.2 cm
6		0.1 cm
Vertical spacing between elements		1 cm
Bar width (bw)		1 cm
Bar length (bl)		3bw + 2rr

Table 1. Custom 1951 USAF MIL-STD-150A model geometry definition.

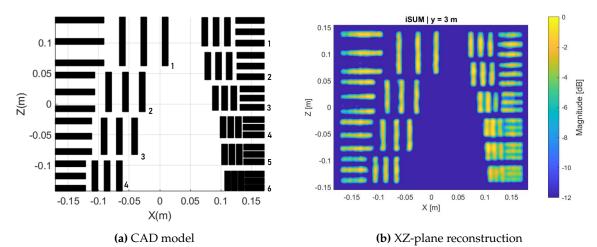


Figure 6. XZ-plane reconstruction of the USAF-based target located 3 m from the antenna array.

Runtime simulation performance

To perform the imaging, an XZ plane of $36.5 \text{ cm} \times 31 \text{ cm}$ is defined. A 2.5 mm discretization is used, so the image plane consists of 18375 pixels. As explained in Section 2.2, each tx_m - rx_n pair generates an individual image, leading to a total of 3.136 different images to combine for this architecture. HW-1 processes images in 0.03 seconds, but with HW-2, it achieves an impressive 0.008 seconds – a remarkable improvement. This exceptional performance is attributed to the utilization of GPU resources and MATLAB's vector computing capabilities.

Our commitment to achieving greater efficiency and faster processing speeds motivates us to constantly enhance the software. We strive to explore alternative approaches that optimize performance and push the boundaries of what is currently achievable.

6. Conclusions

This study introduces a method for designing 2D-sparse arrays, resulting in remarkable improvements in imaging performance. By integrating advanced electromagnetic simulation and

powerful mathematical optimization algorithms (GA), this approach yields highly satisfactory results. It demonstrates the capability to achieve superior reconstruction outcomes while utilizing less than 2% of the elements typically required by conventional full-density 2D arrays.

The significance of this method extends to the development of On-The-Move (OTM) imaging systems, enabling real-time 3D imaging of moving targets. The reduction in the number of elements, combined with optimized simulation codes utilizing vector computation in Matlab and harnessing the potential of GPU and parallelization resources, drastically minimizes the execution time of the simulations.

This study represents a remarkable advancement in imaging technology, offering promising possibilities for more efficient and agile imaging systems with unparalleled imaging quality. This research makes a significant contribution to the field of image processing and paves the way for future advances in the field.

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Conflicts of Interest: The authors declare no conflict of interest.

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