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Article

Experimental Study on Remediation of Lead-Contaminated Soil with Citric Acid as Cleaning Agent

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Abstract: Soil washing is a rapid and efficient method for heavy metals removal. In this study, in order to prove the feasibility of leaching remediation technology for remediation of lead-contaminated soil around a smelter, intermittent oscillating washing tests and extensive continuous tests were conducted to remediate Pb contaminated soils. Plant growth tests with wheat (Bainong Aikang 58) were also conducted to investigate the effects of leaching on plant growth and the Pb content of stems and leaves. The results revealed that in soils, Pb mainly exists in the forms of PbCO₃, Pb₅(PO₄)₃Cl₂, PbSO₄, and in small amounts of PbS. The intermittent oscillating washing tests showed that a lower liquid–solid(L/S) ratio and a higher leaching temperature and time were related to increased Pb removal efficiency. The Pb removal efficiency rates in the oscillating washing tests and the extensive continuous tests were 72.50% and 69.94%, respectively. In addition, the chemical and physical characteristics of the soil were basically unchanged after the leaching regimes. The results of the plant growth tests showed that the leaching regimes did not have a negative effect on the survival rate and growth of the wheat, and the heavy metal contents of the stem and leaf were effectively reduced. This study provides a reference for the large-scale remediation of contaminated soils.

Keywords: Pb contaminated soils; repair; soil washing; intermittent and continuous experiments

1. Introduction

Heavy metal(loid)s are both biologically and industrially important, but the increased demand for these resources have often translated into the unscrupulous exploitation of heavy metal minerals[1]. During the last few decades, human activities have altered the nature of the surface soil environment[2,3], increasing the contamination of soils with heavy metal(loid)s worldwide[4]. Shahid et al. [5–8] have studied the influence of heavy metal(loid)s in the soil on soil physico-chemical properties, including the soil pH, electrical conductivity, cation exchange capacity, soil mineralogy, and microbial and biological conditions, some of which pose a significant threat to human health[9–13].

There are eight heavy metal(loid)s commonly present in soils: copper(Cu), lead(Pb), zinc(Zn), cadmium(Cd), arsenic(As), chromium(Cr), nickel(Ni), and mercury(Hg)[14–17]. Among these heavy metal(loid)s, As, Pb, Cd, and Hg are included in the top 20 hazardous substances listed by the Agency for Toxic Substances and Disease Registry(ATSDR,2012) and the United States Environmental Protection Agency(US EPA). It has been reported that Pb has a soil persistence period of 150–5000 years[18]. Pb can cause human ailments such as stomach aches, headaches, and tremors. Therefore, remediating Pb contaminated soils is of vital importance to human and soil health.

In addition, increasing awareness of the impact of soil heavy metal contamination on human and environmental health will improve existing technologies and help to develop new technologies for the contamination remediation. Numerous Pb contaminated soil remediation techniques have been developed during the last two decades[19–21], such as soil replacement[22], soil isolation[23],

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vitrification[24], electrokinetic remediation[25,26], immobilization techniques[27], encapsulation[28], soil washing[4,6,29], and biological remediation[30]. Soil washing refers to the removal of heavy metal(loid)s from the soil using various reagents and extractants that can leach the heavy metal(loid)s from the soil[29,31–34]. Soil washing is frequently used for remediating heavy-metal-contaminated sites because it has a number of potential advantages, such as cost-effectiveness, the complete removal of metals, faster, and it meets specific regulation criteria and reduces long-term liability[29,32–34]. Moreover, soil washing technology has certain limitations, such as the possibility of changing the physicochemical properties of the soil[35], damaging the ecological structure of the soil[36], and residues of detergents[37]. Therefore, the selection of a detergent with high metal removal rate, low toxicity and low damage to soil properties is the key to enable the application of the washing technology. Commonly used drenching agents include[37–40] inorganic washing agents(acid, base, and salt)[41–43], chemical (synthetic) surfactants[44,45], biosurfactants (natural surfactants)[39], Synthetic chelators[46–49], Low-molecular-weight organic acids, and citric acid has a high metal removal rate and is easily biodegradable[47,49–51], which has broad application prospects. This article finally chose citric acid as the leaching agent for detailed experiments.

Target farmland soils are affected by the atmospheric deposition of Pb smelting enterprises, and some heavy metal(loid)s in the soil exceed human health standards, which threatens food security. In this study, batch oscillating washing tests for remediating Pb contaminated soil are studied using soil washing. In addition, extensive continuous tests and plant growth tests were conducted to illustrate the larger-scale applicability of the soil washing technology.

The objectives of this study were to (1) select and compare the leaching effects of different leaching agent, select an environmentally friendly CA with a relatively high efficiency; (2) investigate the effects of different dosage, S/L, temperature and contact times ratios on CA for removing Pb; (3) conduct Extensive continuous tests to verify experimental indicators; and (4) assess changes in physicochemical properties and plant growth before and after soil washing.

2. Materials and Methods

2.1. Soil samples

All experiments were carried out on soil samples contaminated by the metallurgical industry. The sampling point is located in the woodland in the southeast of the smelter, 500~2000m away from the smelter chimney, with 50m as a gradient grid format sampling(E112°57′19″; N35°13′75″) located in Jiyuan (China), multi-point sampling mix, sampling method is soil sampler drilling, sampling depth of 20cm. The main chemical and physical characteristics of the Pb contaminated soil are presented in Table 1.

Table 1. Chemical and physical characteristics of the heavy metal contaminated soil sample.

Characteristics	Value	
pH-H ₂ O	7.55	
Density (g/cm³)	2.17	
Granulometry		
>0.125 mm	8.49%	
0.125–0.075 mm	16.26%	
0.075–0.045 mm	13.10%	
0.045–0.0385 mm	12.66%	
<0.0385 mm	49.49%	
\sum	100.00%	
Elemental composition		
Total iron (Fe)	3.38%	
Magnesium (Mg)	1.37%	
Phosphorus (P)	0.066%	
Calcium (Ca)	2.17%	

Sodium (Na)	0.99%		
Potassium (K)	1.93%		
Copper (Cu)	105 mg/kg		
Lead (Pb)	2290 mg/kg		
Zinc (Zn)	199 mg/kg		
Cadmium (Cd)	8.30 mg/kg		
Mercury (Hg)	0.902 mg/kg		
Arsenic (As)	10.50 mg/kg		
Chromium (Cr)	67.90 mg/kg		
Nickel (Ni)	38.80 mg/kg		

The soil samples were heavily contaminated with Pb (Pb 2290 mg·kg-¹), while the contents of the other heavy metal(loid)s were within the acceptable range: Cu 105 mg/kg, Zn 199 mg/g, Cd 8.30 mg/kg, Hg 0.902 mg/kg, As 10.50 mg/kg, Cr 67.90 mg/kg, and Ni 38.80 mg/kg.

The fine fraction (<0.0385 mm) largely contributed to the size composition of the soil samples, that is, 49.49% (W·W-1) of the total soil. The 0.045–0.0385 mm, 0.075–0.045 mm, 0.125–0.075 mm, and >0.125 mm fractions represented 12.66%, 13.10%, 16.26%, and 8.49% (W·W-1) of the total soil, respectively. The size distribution of the soil analysis above shows that the soil sample was a fine clay soil, and the influence of fine soil particles should be considered in the remediation tests.

The mineral composition of the soil samples was analyzed by X-ray diffraction (XRD). According to the XRD analysis, the main mineral components in the soil samples were quartz, albite, clinochlore, muscovite, microcline, dolomite, and calcite (Figure 1). However, Pb minerals were not detected, which was most likely because the Pb content of the remediated soil sample was lower than the lower limit of detection of the D/max-2500PC (D/max-2500PC, Japan).

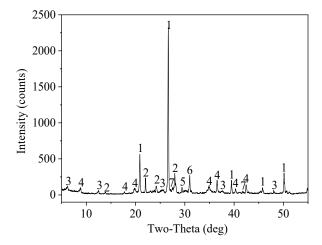


Figure 1. XRD of the soil sample (1-Quartz, 2-Albite, 3-Clinochlore, 4-Muscovite, 5-Calcite, 6-Dolomite, and 7-Microcline).

The soil samples were fine grained. In addition, the flue gas and dust significantly contributed to the heavy metal(loid)s contamination of the soil sample, which came from the metallurgical industry and fine-grained particles[52,53]. Therefore, both spherical and square Pb were occasionally found under the condition of strong exposure of the scanning background (Figure 2a–c). Pb was mainly present in spherical, square, and irregular forms (Figure 2d–f) after elutriation, which indicates that elutriation removed the dust and fine Pb-containing pollutants and concentrated the Pb.

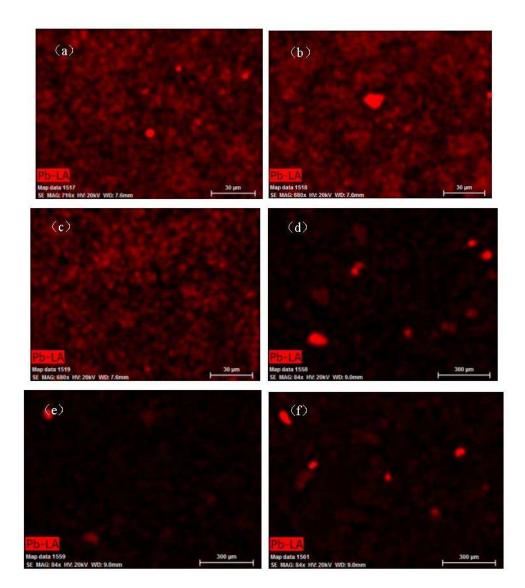
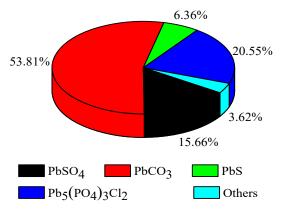


Figure 2. EDS surface scans of the soil sample ((a) \sim (c) the original soil sample; (d) \sim (f) the heavy fractions after elutriation).

The phase analysis of the Pb showed that the Pb was mainly present as PbCO $_3$ (53.82%), followed by Pb $_5$ (PO $_4$) $_3$ Cl $_2$ (20.55%) and PbSO $_4$ (15.66%), and a small amount of PbS (6.36%). This correlated with the flue gas from the Pb smelters, which mainly contained spherical monomer Pb particles. Due to its small specific surface area and high activity, it easily forms PbSO $_4$ in the presence of SO $_2$ and forms square PbS in the presence of S. When PbSO $_4$ is subjected to a carbonic acid solution, it forms PbCO $_3$ as a secondary product.



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Figure 3. Pb element chemical phase analysis.

2.2. Washing agents

The washing agent used in effects of different washing agents was a combination of analytical grade citric acid (CA), tartaric acid (TA), oxalic acid (OX), and acetic acid (HAc), all of which were purchased from the Tianjin Hengxing chemical reagent manufacturing Co., Ltd., and all of the chemicals used in the experiments were analytical grade. While, CA was selected as the washing agent for subsequent experiments through leaching tests. In addition, it should be noted that deionized water was used in the experiments.

2.3. Oscillating batch washing tests

The soil sample was air dried and sieved to remove debris, stones, and visible plant materials. It was then crushed (Φ 200×125 mm, Wuhan Exploration Machinery Factory) and mixed (Figure 4). We used a constant temperature shaking table (QYC-211, Shanghai Fuma Test Equipment Co., Ltd) in the soil washing test. First, a certain concentration of washing agent (0.1 mol/L, 0.2 mol/L, 0.3 mol/L, 0.4 mol/L, 0.5 mol/L) and 10 g soil samples were prepared. The detergent was mixed with the soil sample at a certain liquid-solid(L/S) ratio using a conical flask, and the mixture was placed on a constant temperature shaker to control the test parameters such as detergent concentration, L/S ratio, reaction temperature and reaction time. The washed mixture was filtered through 0.45 mm membrane filters (XTLZ-260, Sichuan Bureau of Geology and Mineral Resources), dried at 80°C overnight in a vacuum oven (GZX-9146 MBE, Shanghai Boxun Industrial Co., Ltd) before being weighed, ground (XPM – Φ 120×3, Wuhan Exploration Machinery Factory), and content of Pb in washed solid was determined using inductively-coupled plasma optical emission spectroscopy (ICP-OES, Agilent 5100 SVDV ICP-OES, America Agilent Technologies) at the analysis center of Henan Province Rock and Minerals Testing Center. The Pb leaching efficiency was evaluated using Eq.1:

Pb leaching efficiency =
$$1 - \frac{\text{Mass after} \times [\text{Me}] \text{after}}{\text{Mass before} \times [\text{Me}] \text{before}} \times 100\%$$
 (1)

The mass after and mass before are the weight (in g) of the soil after washing and before washing, respectively; [Me] after and [Me] before are the heavy metal contents of the soil (in mg/kg) after washing and before washing, respectively.

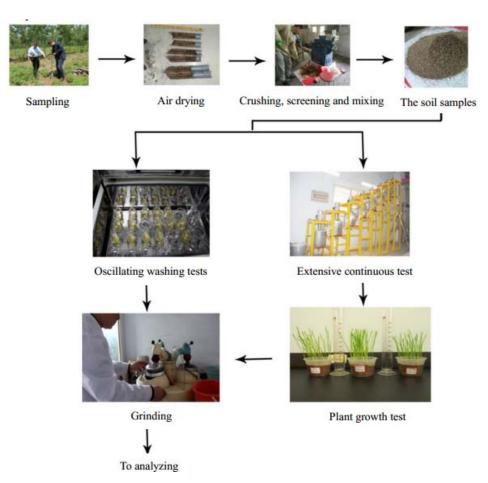


Figure 4. Experimental flow diagram.

2.4. Extensive continuous tests

The air-agitation leaching system (Figure 5), which was developed through independent research, was used in the soil washing extensive continuous tests. These tests involved eight stirring and leaching tanks (15 L), two buckets (200 L) for soil mixing and washing agent mixing, two peristaltic pumps (BT100S, Baoding leifu fluid technology Co., LTD) for accurately controlling the feeding speed, and one settling tank.

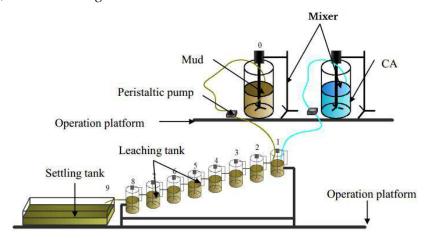


Figure 5. The air-agitation leaching system.

As can be seen from Figure 5, a large volume mixture of washing agent and mud(mixture of soil and water) was prepared with a CA concentration of 0.8 M and a L/S ratio of 20:2. Secondly, the washing agent was mixed with an equal volume of mud, and the stirring and leaching tanks were

filled completely. Third, the peristaltic pump parameters were adjusted to accurately control the feeding speed to 50 ml/min, and the valves between the tanks were adjusted to balance the speed of the mud (100 ml/min). It took 2.5 hours to fill a 15 L container and 20 hours to fill eight 15 L containers. Finally, after 24 hours of steady operation, the samples in each drum were separately processed by being filtered, dried, sufficiently ground, determined (as same as 2.3) and analyzed (Eq.1). The final sample, which was discarded into the settling tank, was used for the plant growth tests.

2.5. Plant growth test

After washing the soil with the extensive continuous test, the soil samples were air dried, crushed, and mixed. Then, 500 g of soil samples taken before and after washing were placed in separate pots (D 20cm and H 15cm). One hundred wheat seeds were planted in each pot to investigate the effects of soil Pb-remediation on wheat growth. After 30 days of growth, the stems and leaves of the wheat were collected, dried at 80°C overnight in a vacuum oven, sufficiently ground, and Pb contents been determined (as same as 2.3). The survival rate of the winter wheat was evaluated using Eq.2:

The survival rate =
$$\frac{\text{The number of wheat seedlings}}{\text{The number of wheat seeds}} \times 100\%$$
 (2)

3. Results and Discussion

3.1. Oscillating batch washing tests

3.1.1. Effects of different washing agents on Pb removal efficiency

Batch experiments were performed to determine the removal efficiency of different washing agents. With increasing concentrations of oxalic acid (OX), tartaric acid (TA), and acetic acid (HAc), the removal efficiency of Pb was low, while the CA concentration had a significant impact on the Pb removal efficiency (Figure 6). As the concentration of CA increased, the removal efficiency gradually increased. The removal efficiency was 54.55% and 77.27% for CA concentrations of 0.1M and 0.5M, respectively. However, this increase was not significant after a CA concentration of 0.4 M, making 0.4 M the optimal concentration. By a comprehensive comparison, CA had a significant effect on Pb removal efficiency compared with OX, TA, and HAc (Figure 7). CA has betterPb removal efficiency mainly because, firstly, it can release hydrogen ions by ionization, thus promoting the dissolution of heavy metals through proton competition[47]; secondly, CA is with carboxyl (-COOH) and hydroxyl (-OH) groups, which can complex heavy metals in soil to form water-soluble metal complexes[48,54,55]. As the optimum washing agent, CA (0.4 M) was used in the other tests.

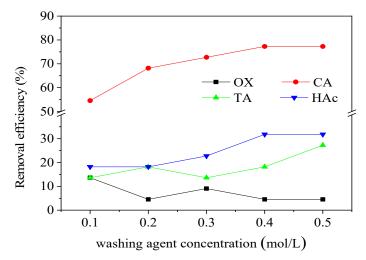


Figure 6. Pb removal efficiency versus washing agent concentration (liquid solid ratio 20:1, 25°C, leaching time 20 h, speed 150 r/min).

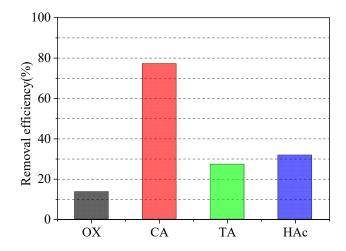


Figure 7. Pb removal efficiency of different washing agents. (0.1 M OX, 0.4 M CA, 0.5 M TA, 0.4 M HAc; L/S ratio 20:1, 25°C, leaching time 20 h, speed 150 r/min).

3.1.2. Effect of L/S ratio on Pb removal efficiency

The S/L ratio is another important factor affecting the removal of heavy metals[56]. In this study, the effect of the L/S ratio on Pb removal efficiency was determined. As the L/S ratio decreased, the Pb removal efficiency gradually decreased, this is due to the fact that, as the liquid-to-solid ratio increases, the number of drencher functional groups increases during the reaction, which can provide more chelate sites to interact with heavy metals and thus improve the removal efficiency[42,57]. Which indicated that a low L/S ratio was not conducive to a high Pb removal efficiency (Figure 8). The removal efficiency was 71.82% for a L/S ratio of 20:1, while the Pb removal efficiency decreased to 66.36% for a L/S ratio of 20:2. As the L/S ratio continued to decrease, the Pb removal efficiency also decreased significantly. When the L/S ratio was 20:5, the Pb removal efficiency was only 50.0%. However, a higher L/S ratio was not conducive to increasing the treatment capacity. Given the efficiency test results, detailed small-scale tests were conducted with a L/S ratio of 20:1.

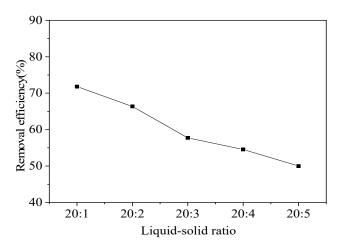


Figure 8. Pb removal efficiency versus L/S ratio (0.4 M CA, room temperature 25°C, leaching time 10 h, speed 150 r/min).

3.1.3. Effect of L/S ratio on Pb removal efficiency

Temperature is known to have an effect on metal(loid) removal efficiency. Thus, tests were conducted to determine the effect of temperature on Pb removal efficiency (Figure 9). As the leaching temperature increased, the Pb removal efficiency in the contaminated soil gradually increased, but the rate of increase was small. The removal efficiency was 70.0% at 25°C, and when the temperature

was increased to 30°C, the efficiency only increased to 71.34%. As the temperature continued to increase, the Pb removal efficiency rate increased slightly, when the temperature was increased to 50°C, the Pb removal efficiency was 73.36%. The results of the temperature tests indicated that increasing the leaching temperature was marginally effective at increasing the Pb removal efficiency, but heating increased the treatment cost. Thus, the subsequent leaching tests were conducted at room temperature.

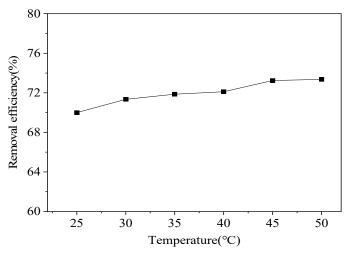


Figure 9. Pb removal efficiency versus temperature. (0.4 M CA, concentration L/S ratio 20:1, leaching time 10 h, speed 150 r/min).

3.1.4. Effects of leaching time on Pb removal efficiency

In the tests conducted on the contaminated soil, as the leaching time increased, the Pb removal efficiency gradually increased (Figure 10). There was a significant difference in the removal efficiency of Pb up to a leaching time of 12 h. The removal efficiency was 59.55% for a leaching time of 1 h, but when the leaching time was increased to 12 h, the Pb removal efficiency increased significantly to 70.45%. With a 20 h leaching time, the Pb removal efficiency only reached 72.50%. After 20 h, the Pb removal efficiency stabilized, and continuing to increase the leaching time was not helpful. The equilibration time of washing may be related to the limited rate of heavy metal dissolution and desorption[58], and heavy metal desorption/dissolution kinetics may be a more important factor in the heavy metal washing process[59]. Thus, the ideal leaching time was about 20 h, and a leaching time of 20 h was used in the extensive continuous tests.

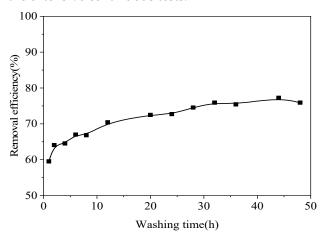


Figure 10. Pb removal efficiency versus leaching time (CA concentration of 0.4 M, L/S ratio 20:1, room temperature 25°C, speed 150 r/min).

The Pb removal efficiency increased gradually with increased leaching time in the leaching tanks (Figure 11). CA concentration in the stirring and leaching tanks was 0.4 M, L/S ratio in the stirring and leaching tanks was about 20:1, room temperature 25°C, stirring speed of 1000 r/min, 0 indicates taken from the bucket and a leaching time of 0 h. The numbers 1–8 indicate taken from stirring and leaching tanks 1–8 and leaching times of 0–2.5 h, 2.5–5.0 h, 5.0–7.5 h, 7.5–10.0 h, 10.0–12.5 h, 12.5–15.0 h, 15.0–17.5 h, and 17.5–20.0 h, respectively. Leaching tank 9 indicates the sample taken from the discharge port of the last stirring and leaching tank after a leaching time of 20.0 h. There was a significant difference in the Pb removal efficiency efficiencies of the first two leaching tanks, which meant that the rapid reaction stages occurred in the first 5 hours. The Pb removal efficiency was 63.76% in the second leaching tank, this is the so-called rapid response stage[42,57,60], while the Pb removal efficiency in the third leaching tank (69.94%) experienced a slower increase compared to that of the second leaching tank. As the stirring and leaching tank number continued, the Pb removal efficiency increased slightly. After moving through three tanks with a total leaching time of approximately 7.5 h, the Pb removal efficiency stabilized, and increasing in leaching time the process was not effective. Thus, the optimum leaching time used in the extensive continuous test was 7.5 h.

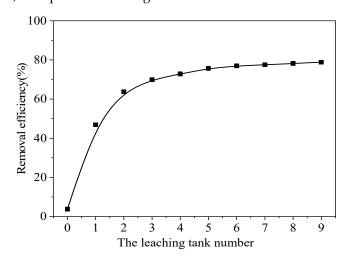


Figure 11. Pb removal efficiency at different sampling points.

3.3. Mechanism analysis

In Figure 12, the bright areas in panels (a)–(d) corresponds to the distribution of Pb, S, Cl, and P in the contaminated soil, while the bright areas in panels (e)–(h) corresponds to the distribution of Pb, S, Cl, and P in the soil after leaching. As can be seen in Figure 12a-d, the positions of the Pb and S basically overlap, which indicated that Pb and S were highly correlated. In addition, based on the fact that the bright areas were irregular, we can deduce that the Pb present mainly existed in the form of PbSO₄. Pb also partially overlapped with Cl and P, which indicated that Pb was also correlated with Cl and P. This was consistent with the phase analysis results (Pb₅(PO₄)₃Cl₂, 20.55%). The surface scanning of the soil remediation from the Pb leaching results exhibits no bright areas (Figure 12e), which indicates that the Pb was removed from the contaminated soil. The surface scanning results for S also exhibited no bright areas, which indicated that PbS and PbSO4 were removed from the contaminated soil through chemical reactions. The surface scanning results for P exhibited bright areas, but P was not correlated with Pb. Many factors can affect the reaction involved in the leaching of Pb contamination, including the oxygen content and the pH value. Based on the results of the EDS surface scan of the soil samples, PbSO₄, Pb5(PO₄)3Cl₂, and PbCO₃ reacted with CA to form Pb citrate, while PbS was produced by the oxidation of PbO, which also reacted with CA to form Pb citrate. The reaction can be described as follows:

$$3PbCO_3 + 2C_6H_8O_7 = (C_6H_5O_7)_2Pb_3 + 3H_2O + 3CO_2$$

$$3PbSO_4 + 2C_6H_8O_7 = (C_6H_5O_7)_2Pb_3 + 3H_2SO_4$$
$$3PbO + 2C_6H_8O_7 = (C_6H_5O_7)_2Pb_3 + 3H_2O$$
$$3Pb_5(PO_4)_3Cl_2 + 5C_6H_8O_7 = 5(C_6H_5O_7)_2Pb_3 + 3H_2O$$

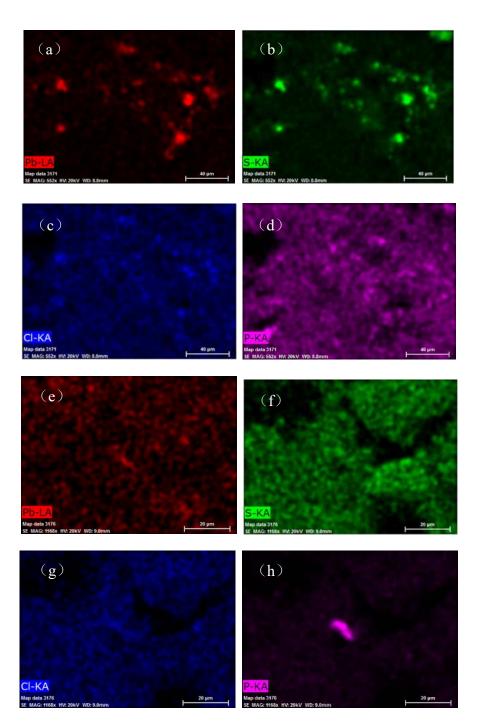


Figure 12. EDS surface scan of the soil sample ((a)–(d) the original soil sample; (e)–(h) the soil after remediation).

3.4. Chemical and physical characteristics before and after the washing treatment

The particle size characteristics of the soil after the washing treatment were slightly different compared to those of the original soil (Figure 13). The d50 and d90 of the original soil were 21.90 μ m

and $62.00~\mu m$, respectively, while those of the soil after the washing treatment were $18.90~\mu m$ and $58.10~\mu m$, respectively. The results of the particle size analysis indicated that the leaching remediation had little effect on the particle size composition of the soil; therefore, leaching remediation had a minimal effect on the relative soil permeability. The XRD spectrum of the soil sample before and after the washing treatment is shown in Figure 14. The peak types were basically the same, which indicated that the washing treatment did not have a significant impact on the mineral composition of the soil in this study. However, the washing treatment did have a negative effect on the soil, i.e., some of the nutrients were lost during the leaching process (Table 2).

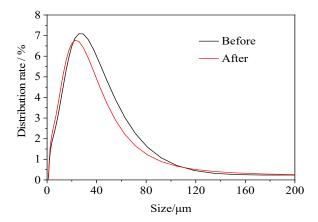


Figure 13. Size characteristic curve of the soil sample before and after the washing treatment.

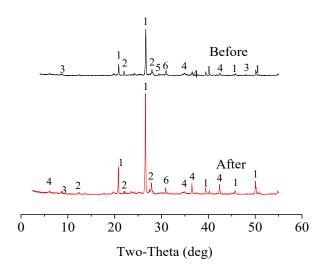


Figure 14. XRD spectrum of the soil sample before and after the washing treatment (1-Quartz, 2-Albite, 3-Clinochlore, 4-Muscovite, 5-Calcite, and 6-Dolomite).

Table 2. Chemical characteristics of the soil sample before and after the washing treatment.

Characteristics	Before (%)	After (%)	Change (%)
Total iron (Fe)	3.38	3.28	-2.96
Magnesium (Mg)	1.37	1.22	-10.95
Phosphorus (P)	0.066	0.052	-21.21
Calcium (Ca)	2.17	1.12	-48.39
Sodium (Na)	0.99	1.11	+12.12
Potassium (K)	1.93	1.96	+1.55

3.5. Plant growth

The remediation of the contaminated soil was beneficial to the survival and growth of winter wheat. Before washing, the survival rate was only 70% due to the influence of heavy metal(loid)s and Pb in the soil. After washing, the survival rate of the winter wheat increased significantly to 80%. As can be seen in Figure 15, the plant height of the winter wheat grown in soils after the leaching restoration was slightly lower compared with the winter wheat potted in un-remediated soil, but the growth was still good.

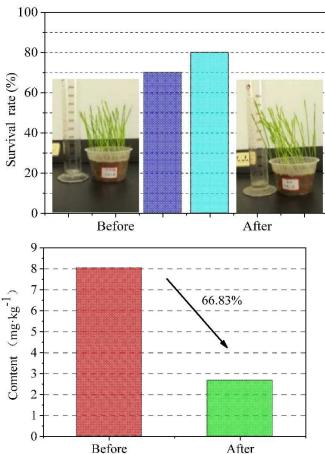


Figure 15. (a) Survival rate of the wheat planted in soils before and after the washing treatment; (b) Pb contents of the stems and leaves of the wheat growing in the soil before and after the washing treatment.

After 30 days of maintenance and growth, the stems and leaves of the winter wheat were cut and dried, and the contents of the heavy metal(loid)s and Pb were determined. The results indicated that the Pb content of the stems and leaves of the wheat grown in the un-remediated soil (before the washing treatment) was 8.05 mg/kg, while the plants grown in the remediated soil (after the washing treatment) was 66.83% lower (2.67 mg/kg), in Figure 16.

In conclusion, the leaching technology used in this study does not have a negative impact on the survival rate of winter wheat, and theoretically, it will not have a negative impact on the survival rate of other crops. In addition, this leaching technology could reduce the accumulation of Pb in plants. We propose that the leaching technology used in this study is feasible for larger scale agriculture on contaminated soils.

4. Conclusions

Both the leaching regimes used in the batch oscillating washing tests and the extensive continuous test effectively removed Pb from the soil, thereby decreasing the environmental risk from heavy metal(loid) pollution. The PbSO₄, Pb₅(PO₄)₃Cl₂, PbCO₃, and PbS all reacted with the CA to form

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Pb citrate, which led to a Pb removal efficiency of 72.50% in the oscillating washing tests and 69.94% in the extensive continuous tests. The chemical and physical characteristics of the soil (soil mineralogy, the size characteristic curve, and the major element concentrations) were basically unchanged by the leaching regimes. Besides, the remediation of contaminated soil does not reduce the survival rate of winter wheat (before or after restoration, 70% and 80%, respectively). The Pb content of the stems and leaves of the winter wheat grown in soil before and after the washing treatment was 8.05 mg/kg and 2.67 mg/kg, respectively, demonstrating that the washing treatment resulted in a 66.83% decrease in the Pb content of the stems and leaves. This study demonstrated the feasibility of using citric acid (CA) as a leachate in the remediation of Pb contaminated soil and provides a reference for larger-scale remediation of contaminated soils in the future. However, the repeatability of achieved results and the possibility of field application should be verified in further study.

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