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## Article

# Effects of Quenching Temperature on the Microstructure and Mechanical Properties of a Medium-Mn Steel Processed by Quenching and Partitioning

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**Abstract:** A medium-Mn steel was processed by a route involving twin-roll strip casting, hot-rolling and quenching and partitioning with different quenching temperatures. The effects of quenching temperature on the microstructure and mechanical properties were studied. It was found primary martensite and retained austenite (RA) were obtained at the quenching temperature of 140–180 °C, while primary martensite, RA and secondary martensite were obtained when the quenching temperature was 220–300 °C. With increase in quenching temperature from 140 to 260 and to 300 °C, RA fraction first increased from 15.4% to 31.8% and then decreased to 16.6%. The sample at quenching temperature of 220 °C yielded the mechanical properties with yield strength of 992 MPa, tensile strength of 1159 MPa and total elongation of 20.4%. The superior mechanical properties were achieved by an optimum combination of high RA fraction (26.5 vol%), appropriate mechanical stability of RA and a small amount of secondary martensite.

**Keywords:** medium-Mn steel; twin-roll strip casting; quenching and partitioning; microstructure; mechanical properties

## 1. Introduction

Weight reduction and improved crashworthiness property are the urgent demands in the modern automotive industry [1]. The application of advanced high strength steels (AHSSs) to automobile is one of the most effective way to reduce weight and improve passenger safety [2, 3]. In recent years, medium-Mn steels (4–12 wt% Mn) have been received significant attention as typical third-generation AHSSs because of excellent combination of strength and ductility together with reasonable materials cost. A high volume fraction (~ 20%–60%) of retained austenite (RA) can be obtained in medium-Mn steels, leading to a superior PSE (product of tensile strength (TS) and total elongation (TE)) of ~ 20–60 GPa% through transformation-induced plasticity (TRIP) effect (or TRIP effect + twinning induced plasticity effect) [4–8].

It is well known that intercritical annealing (IA) is generally adopted as the main heat treatment to obtain an ultrafine-grained structure in medium-Mn steels [6–8]. The effects of IA conditions, such as IA temperature [9, 10], IA time [11, 12], heating rate [13, 14] and cooling rate [15], on the microstructure and mechanical properties of medium-Mn steels have been widely studied. Besides IA process, quenching and partitioning (QP) process is also attempted as an important processing route for medium-Mn steels. Seo et al. applied the QP process to a cold-rolled Fe–0.21C–4.0Mn–1.6Si–1.0Cr (wt%) medium Mn steel [16]. It was found that the RA with volume fraction of 33% was achieved at optimal quenching temperature and the PSE of ~ 24.5 GPa% with a high TS was obtained [16]. Zhao et al. explored the effect of austenitizing temperature on the mechanical properties of a cold-rolled Fe–0.28C–4.08Mn–1.42Si (wt%) medium-Mn steel [17]. The small size prior austenite

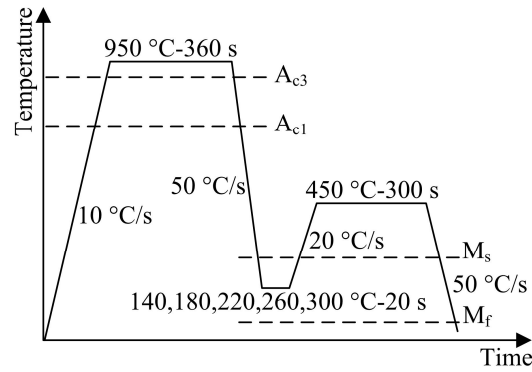
under the low austenitizing temperature resulted in a large volume fraction of RA and uniform microstructure [17]. De Moor et al. explored a cold rolled Fe-0.3C-5Mn-1.6Si (wt%) medium-Mn steel processed by QP process following IA, which exhibited TS of 1110–1175 MPa with TE of 7%–15% [18]. Cai et al. explored a cold-rolled Fe-0.16C-6.5Mn-1.1Al-0.05Nb-0.22Mo-0.03N medium-Mn steel processed by QP process and compared it with IA process [19]. The QP-processed sample showed relatively higher strength with relatively lower ductility than the IA-processed sample [19]. Although these previous studies on QP process of medium-Mn steels have been carried out, the microstructure and mechanical properties of medium-Mn steels containing different composition processed by QP process are still not clear because of limited studies.

Recently, our previous study has confirmed that twin-roll strip casting (TRSC) is a potential processing route to produce medium-Mn steels [20]. Excellent mechanical properties were obtained basing on the short processing route involving TRSC, hot rolling and IA [20]. However, the studies on the strip-cast medium-Mn steel processed by QP process have not been reported. In this study, a Fe-0.3C-4Mn-1.82Al-0.6Si (wt%) medium-Mn steel was attempted to be processed by a route involving TRSC, hot rolling and QP process. The effects of quenching temperature on the microstructure and mechanical properties were studied in detail.

## 2. Materials and Methods

A ~ 2.5 mm-thick as-cast strip of Fe-0.3C-4Mn-1.82Al-0.6Si (wt%) medium-Mn steel was produced by a vertical-type twin-roll strip caster available at the State Key Laboratory of Rolling and Automation and then the as-cast strip was hot-rolled to ~ 1 mm at 1000 °C. The detailed TRSC and hot rolling parameters were reported in our previous study [20]. The microstructures of the as-cast strip and hot-rolled sheet consisted of martensite together with a small amount of RA [20]. Finally, the hot-rolled sheet was subjected to QP process. The  $A_{c3}$ ,  $M_s$  and  $M_f$  temperatures were measured by a dilatometer equipment (DIL 805A/D), which were 880, 340 and 101 °C, respectively. In order to confirm the optimum austenitizing temperature, the hot-rolled sheet was first heated to 800, 850, 900 and 950 °C for 360 s and then quenched to room temperature (preliminary experiment). Basing on the result of preliminary experiment (see next section), the hot-rolled sheets were austenitized at 950 °C for 360 s in a tube type resistance furnace, quenched in a low-temperature salt bath furnace (initial quenching) of 140, 180, 220, 260 and 300 °C (quenching temperature) for 20 s, and then put in a middle-temperature salt bath furnace (partitioning process) of 450 °C (partitioning temperature) for 300 s followed by quenching to room temperature (final quenching). For convenience, the QP-processed samples subjected to different quenching temperatures were referred as Q140, Q180, Q220, Q260 and Q300, respectively.

The phase transformation behavior during the QP process was also studied using DIL 805 A/D dilatometer. The detailed QP process for dilatometry study is shown in Figure 1. Rectangular dilatometry specimens (length 10 mm, width 4 mm, thickness 1 mm) were prepared from the hot-rolled sheets. The microstructure was characterized by Zeiss Ultra-55 field emission scanning electron microscope (SEM) equipped with electron backscattered diffractometer (EBSD), JXA-8530F electron probe microanalyzer (EPMA) and Tecnai G2 F20 transmission electron microscope (TEM). EPMA specimens were first mechanically polished and then etched with 4 vol% nital solution (time 22 s). EBSD specimens were electropolished (current 0.7 A, time 20 s) using an electrolyte consisting of alcohol and perchloric acid in the proportion of 7:1 to remove the mechanically damaged layer. TEM specimen (diameter 3 mm, thickness ~ 45 μm) was twin-jet electropolished (voltage 32 V, temperature -22 °C) in a solution containing alcohol and perchloric acid in the proportion of 23:2.



**Figure 1.** Schematic diagram of the detailed QP process for dilatometry study.

The volume fraction of RA was measured by a Rigaku SmartLab X-ray diffractometer (XRD) (step rate 0.04 °/s, Cu K $\alpha$  radiation). XRD samples were electropolished using the same method of EBSD specimens. Integrated intensities of (200) $\alpha$ , (211) $\alpha$ , (200) $\gamma$ , (220) $\gamma$  and (311) $\gamma$  peaks were used to calculate the volume fraction of RA ( $V_\gamma$ ) using the following equation [21]:

$$V_\gamma = 1.4 I_\gamma / (I_\alpha + 1.4 I_\gamma) \quad (1)$$

where  $I_\gamma$  and  $I_\alpha$  are the average integral intensities of austenite and ferrite peaks, respectively. Besides, the carbon content of RA ( $x_C$ ) was calculated using the following equation [22]:

$$a_\gamma = 3.556 + 0.0453 x_C + 0.00095 x_{Mn} + 0.0056 x_{Al} \quad (2)$$

where  $a_\gamma$  is the lattice parameter of RA in Angstroms,  $x_C$ ,  $x_{Mn}$  and  $x_{Al}$  are the concentration of carbon, manganese and aluminum in RA in wt%, respectively. (200) $\gamma$ , (220) $\gamma$  and (311) $\gamma$  peaks were selected to calculate  $a_\gamma$  using the equation in reference [22].

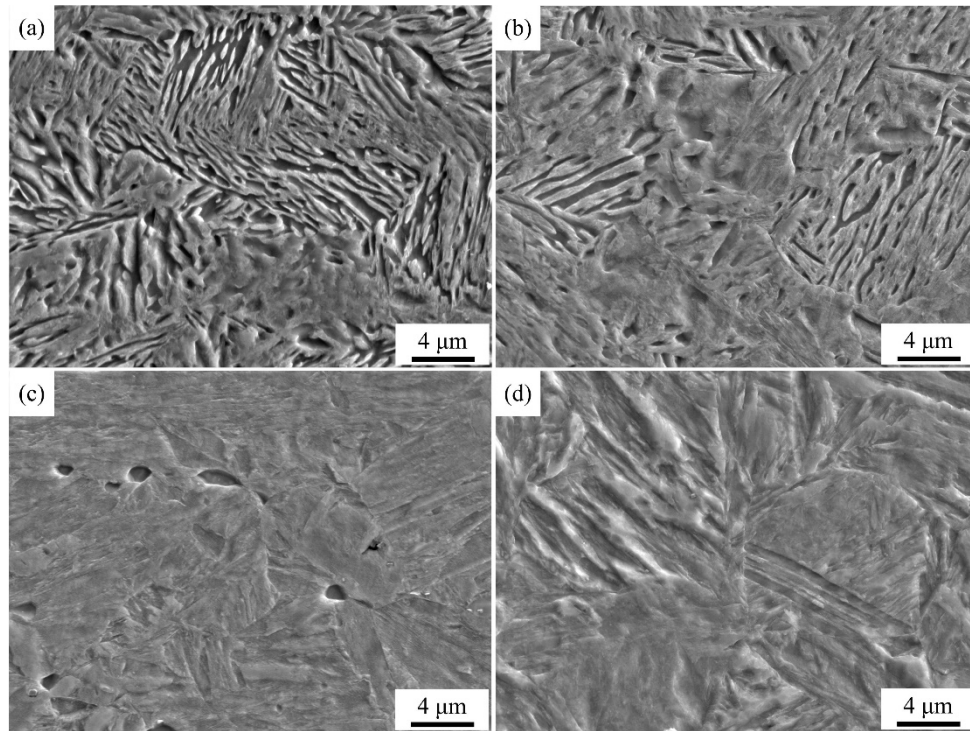
Dog-bone shaped tensile specimens of dimensions 10 mm (gauge length)  $\times$  5 mm (width) were machined with longitudinal axis parallel to hot rolling direction. The tensile tests were conducted using a SHIMADZU AG-X plus 100 kN testing machine (room temperature, crosshead speed 1 mm/min).

### 3. Results

#### 3.1. Microstructure of the Samples under Different Austenitizing Condition

Figure 2 shows secondary electron images of the samples under different austenitizing conditions. Lath ferrite was obtained in the samples quenched from 800 and 850 °C. This is because the two heat treatment temperatures are in the temperature range between  $A_{e1}$  and  $A_{e3}$  temperatures [20], such that austenite reversion from martensite occurred, leading to the formation of lath ferrite. When the sample was quenched from 900 °C, although the heat treatment temperature was higher than  $A_{e3}$  temperature, there was still some globular ferrite present at the prior austenite grain boundary. This may be related to the short holding time (360 s), which was not enough for ferrite completely transformed to austenite. No ferrite was observed in the sample quenched from 950 °C, such that 950 °C was selected as the austenitizing temperature of QP process.





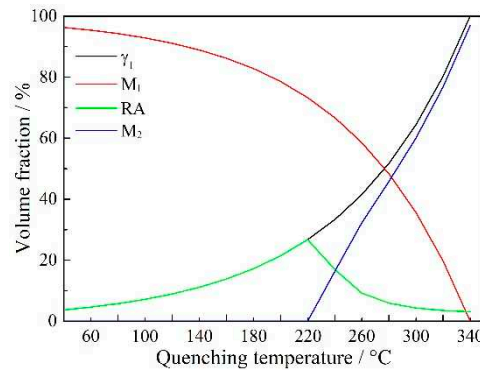
**Figure 2.** Secondary electron images of the samples under different austenitizing conditions, quenched from (a) 800 °C, (b) 850 °C, (c) 900 °C and (d) 950 °C.

### 3.2. Predicted Phase Fraction Basing on CCE Model

The CCE (constrained carbon equilibrium) model was considered as a well description for the thermodynamics of carbon partitioning process, which assumed that full carbon partitioned into untransformed austenite prior to the final quenching [23–25]. In the present study, different phase fractions in QP-processed samples were predicted basing on this model. The volume fractions of primary martensite (martensite formed during initial quenching), initial austenite (austenite retained after initial quenching and prior to partitioning), secondary martensite (martensite formed during final quenching) and RA under CCE model were determined by the Koistinen–Marburger equation [26]:

$$f_m = 1 - \exp[-0.011 \times (M_s - T_q)] \quad (3)$$

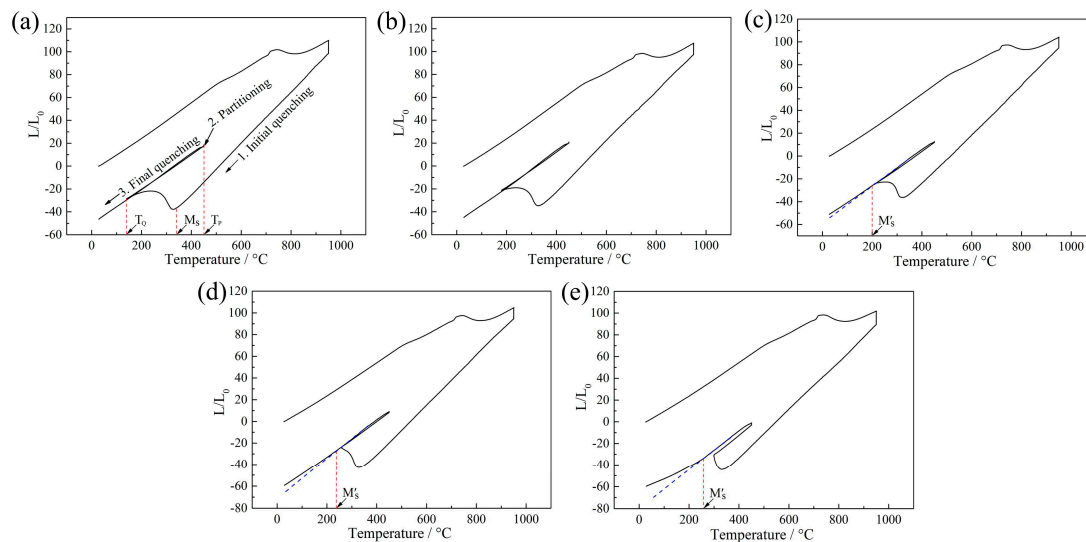
where  $T_q$  is the quenching media temperature and  $f_m$  is the fraction of martensite formed at  $T_q$ . The predicted result is shown in Figure 3. With increase in quenching temperature, the volume fraction of RA first increased when the temperature was lower than 220 °C, followed by a decrease when the temperature was higher than 220 °C, i.e., highest volume fraction (26.7%) of RA was present at the quenching temperature of 220 °C. Besides, no secondary martensite was formed when the quenching temperature was less than or equal to 220 °C, while secondary martensite started to appear when the quenching temperature was higher than 220 °C and its volume fraction increased with increasing temperature. This is related to the fact that the initial austenite fraction increased with increasing quenching temperature. The amount of carbon partitioned into per unit volume of austenite was lower for higher volume fraction of initial austenite, such that a lower thermal stability of partitioned austenite (initial austenite after partitioning and prior to final quenching) was obtained at higher quenching temperature, leading to a higher fraction of partitioned austenite transformed to secondary martensite during final quenching.



**Figure 3.** Predicted phase fractions after QP process basing on CCE model.  $M_1$  is primary martensite,  $M_2$  is secondary martensite and  $\gamma_1$  is initial austenite.

### 3.3. Dilatometric Curves and Microstructure of QP-Processed Samples

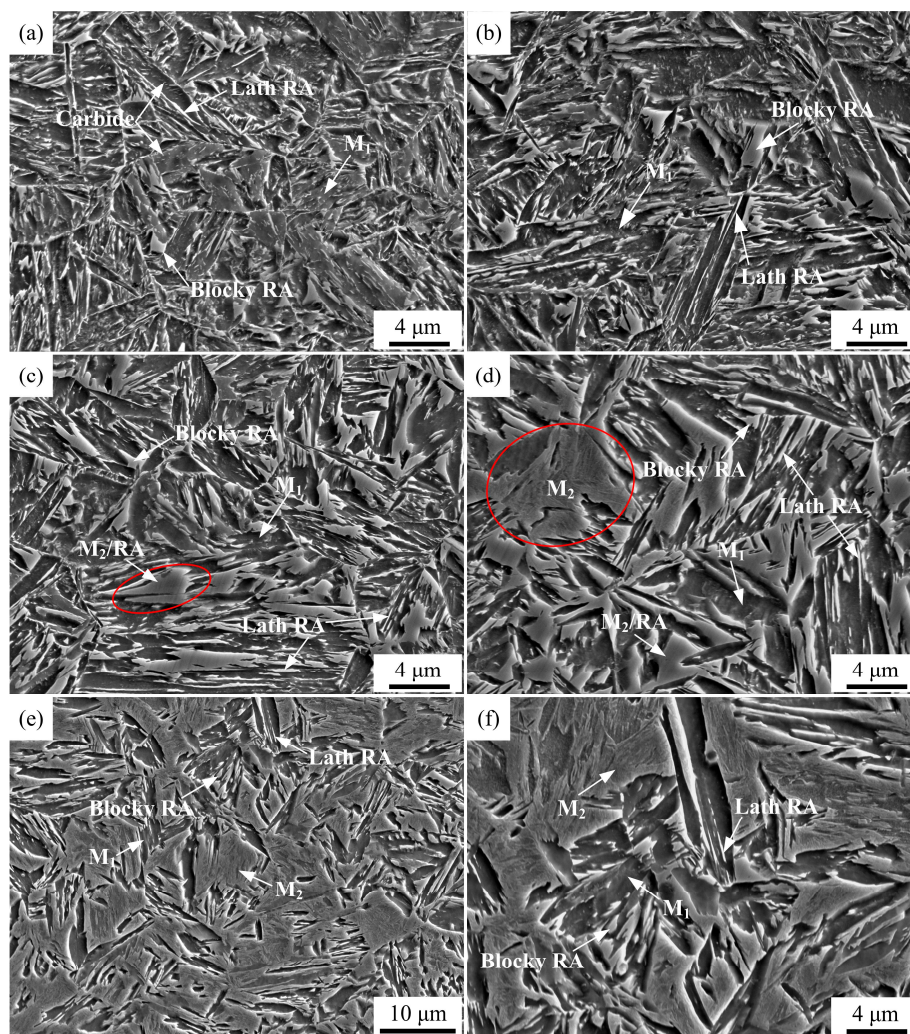
Figure 4 shows dilatometric curves of QP-processed samples subjected to different quenching temperatures. When the quenching temperatures were 140 and 180 °C, no volume expansion was present during the final quenching, i.e., no secondary martensite transformation occurred. This indicated adequate carbon diffused into initial austenite during the partitioning process, such that the carbon enriched partitioned austenite remained stable during the final quenching. When the quenching temperature was in the range of 220 to 300 °C, an obvious volume expansion was observed during the final quenching because of the transformation of partitioned austenite to secondary martensite. Besides, the secondary martensite start temperature and the volume expansion were increased with increasing quenching temperature. This indicated the thermal stability of partitioned austenite decreased with increasing quenching temperature, leading to more secondary martensite formed in the sample subjected to higher quenching temperature, corresponding to the predicted result basing on CCE model (Figure 3).



**Figure 4.** Dilatometric curves of QP-processed samples subjected to quenching temperature of (a) 140 °C, (b) 180 °C, (c) 220 °C, (d) 260 °C and (e) 300 °C.  $T_0$  is quenching temperature,  $T_p$  is partitioning temperature and  $M'_s$  is secondary martensite start temperature.

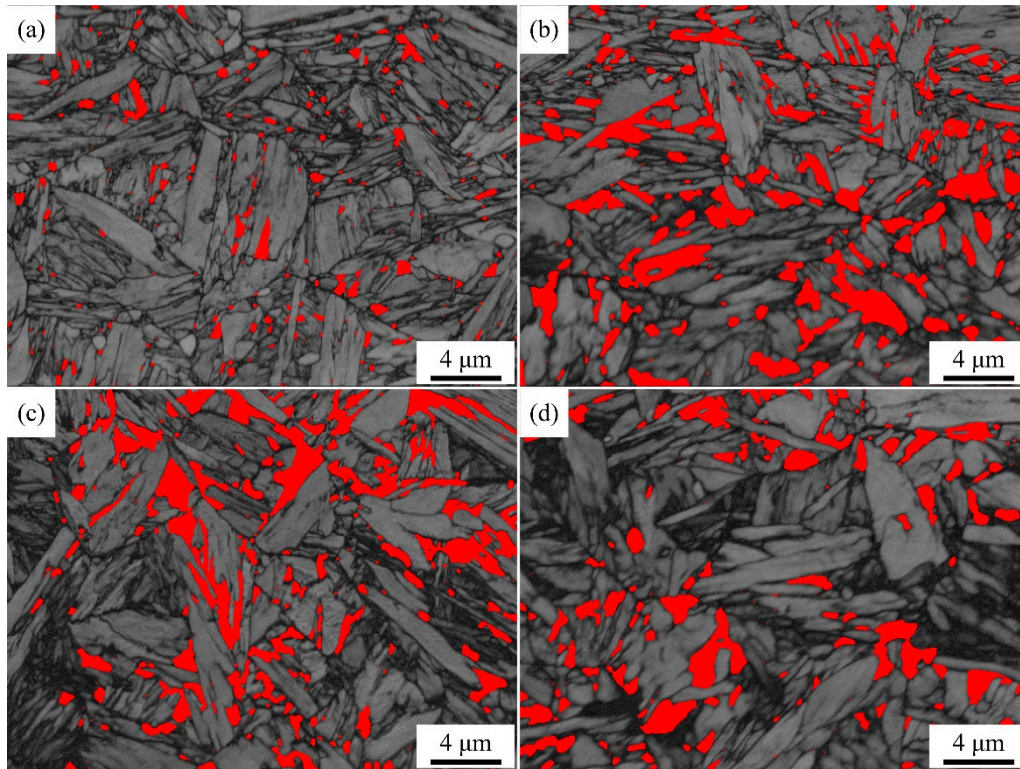
Figure 5 shows secondary electron images and Figure 6 shows EBSD phase maps of QP-processed samples subjected to different quenching temperatures. In Q140 steel, the microstructure consisted of primary martensite, blocky RA and lath RA. Carbides were also observed in the primary martensite. Q180 steel had similar microstructure with Q140 steel, while the amount of blocky RA

was higher than Q140 steel. When the quenching temperature was increased to 220 °C, blocky RA and lath RA were also observed in the primary martensite matrix. The blocky RA and lath RA in Q220 steel were also observed using TEM, as shown in Figure 7. Besides, the size of some blocky structure was  $\sim 3.5 \mu\text{m}$ , as shown in the red circle in Figure 5c. Based on the dilatometric curve (Figure 4c), it can be inferred that this blocky structure was island of secondary martensite and RA ( $M_2$ /RA island). Similarly, blocky RA, lath RA and  $M_2$ /RA island were observed in the primary martensite matrix in Q260 steel. Besides, the secondary martensite with a large size of  $\sim 6 \mu\text{m}$  was observed in Q260 steel, as shown in the red circle in Figure 5d. This is because the quenching temperature was relatively high, leading to the presence of the partitioned austenite with a large size. The large size partitioned austenite had low thermal stability because of its large grain size and insufficient carbon content obtained from adjacent primary martensite, such that it was transformed to secondary martensite during final quenching. In Q300 steel, the fraction of secondary martensite was higher than that in Q260 steel, corresponding to the predicted result basing on CCE model (Figure 3) and the dilatometric curves (Figure 4).

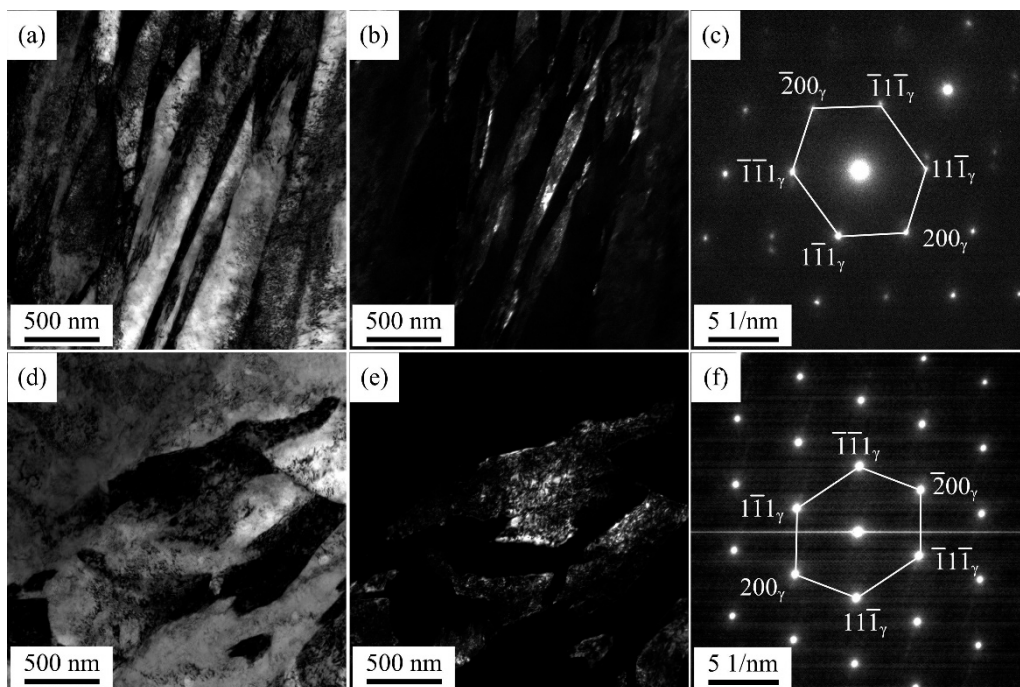


**Figure 5.** Secondary electron images of (a) Q140, (b) Q180, (c) Q220, (d) Q260 and (e, f) Q300 steels.





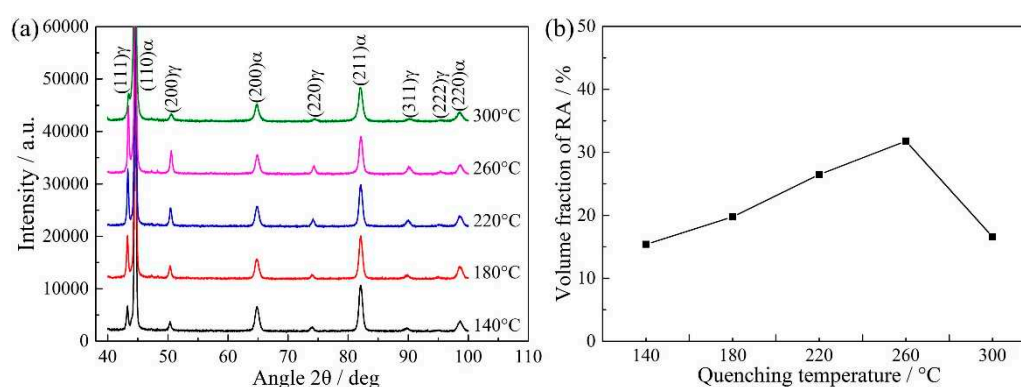
**Figure 6.** EBSD phase maps of (a) Q140, (b) Q220, (c) Q260 and (d) Q300 steels. Phases in red correspond to RA.



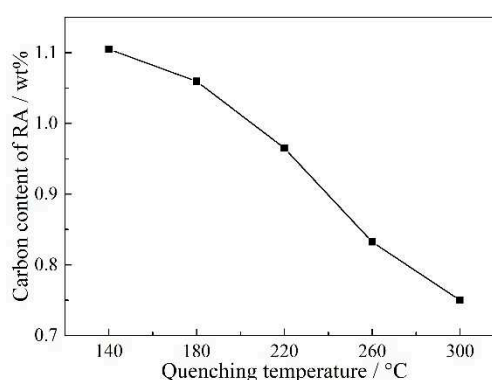
**Figure 7.** TEM micrographs of Q220 steel: (a) lath RA bright field, (b) lath RA dark field, (c) SAED pattern of RA in (a), (d) blocky RA bright field, (e) blocky RA dark field and (f) SAED pattern of RA in (d). SAED is selected area electron diffraction.

Figure 8a shows XRD patterns of QP-processed samples subjected to different quenching temperatures. Both austenite and ferrite peaks were observed in the XRD patterns. Basing on the XRD results, the volume fractions of RA in Q140, Q180, Q220, Q260 and Q300 steels were 15.4%, 19.8%, 26.5%, 31.8% and 16.6%, respectively, i.e., the RA fraction first increased when the quenching temperature

increased from 140 to 260 °C, followed by a decrease on further increasing the quenching temperature to 300 °C, as shown in Figure 8b. It was noted that the variation of RA fraction calculated by XRD result was same to the predicted result basing on CCE model, i.e., first increase followed by a decrease. However, the highest volume fractions of RA were present at different quenching temperatures, which were 220 °C under CCE model and 260 °C by XRD, respectively. Besides, under CCE model, secondary martensite started to disappear when the quenching temperature was less than or equal to 220 °C. This was different from the result of dilatometric curves (Figure 4) and secondary electron images (Figure 5) that secondary martensite was present when the quenching temperature was 220 °C. Thus, there was some deviation between the predicted result under CCE model and the actual experimental result. Figure 9 shows carbon content of RA in QP-processed samples subjected to different quenching temperatures. It was seen that the carbon content of RA decreased with increasing quenching temperature. This variation corresponded to the previous discussion basing on CCE model, i.e., the carbon content of partitioned austenite decreased with increasing quenching temperature because of higher fraction of initial austenite. The lower carbon content of partitioned austenite led to lower carbon content of RA in the final microstructure.



**Figure 8.** (a) XRD patterns of QP-processed samples subjected to different quenching temperatures and (b) the volume fraction of RA calculated by XRD result.



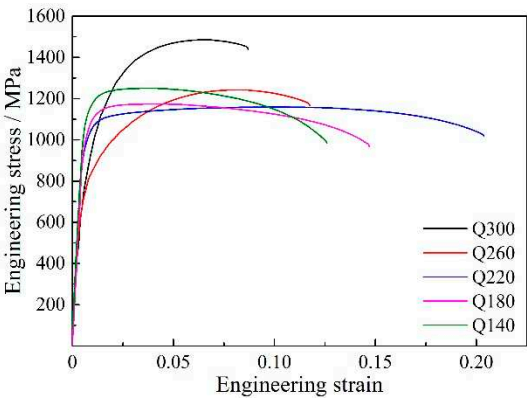
**Figure 9.** Carbon content of RA in QP-processed samples subjected to different quenching temperatures.

### 3.4. Mechanical Properties and Transformation of RA

The engineering stress-strain plots and the detailed properties of QP-processed samples are shown in Figure 10 and Table 1, respectively. With an increase in quenching temperature, the TS first decreased when the quenching temperature increased from 140 to 220 °C, followed by an increase on further increasing the quenching temperature to 300 °C, while the variation of TE was opposite to the variation of TS. Besides, the variation of yield strength (YS) first increased in the quenching temperature range of 140 to 260 °C, followed by a decrease in the range of 260 to 300 °C. Moreover, it should be noted that Q220 steel had optimum mechanical properties with YS of 992 MPa, TS of



1159 MPa, TE of 20.4% and PSE of 23.64 GPa%. Compared with the strip-cast medium-Mn steel processed by IA process in our previous study [20], the strip-cast medium-Mn steel processed by QP process had higher YS together with lower TE and lower PSE than IA process when they had similar TS (Table 1). This is related to the different microstructure obtained by QP and IA process. The matrix structure of QP-processed sample was martensite, which was beneficial to improve YS and was bad for TE. However, the matrix structure of IA-processed sample was ferrite, leading to lower YS, but the ferrite matrix was good for TE. Besides, the IA-processed sample had higher volume fraction of RA than QP-processed sample [20]. Thus, the higher volume fraction of RA resulted in more deformation induced transformation in the IA-processed sample than QP-processed sample, which was good for improving TE through TRIP effect [27-29].

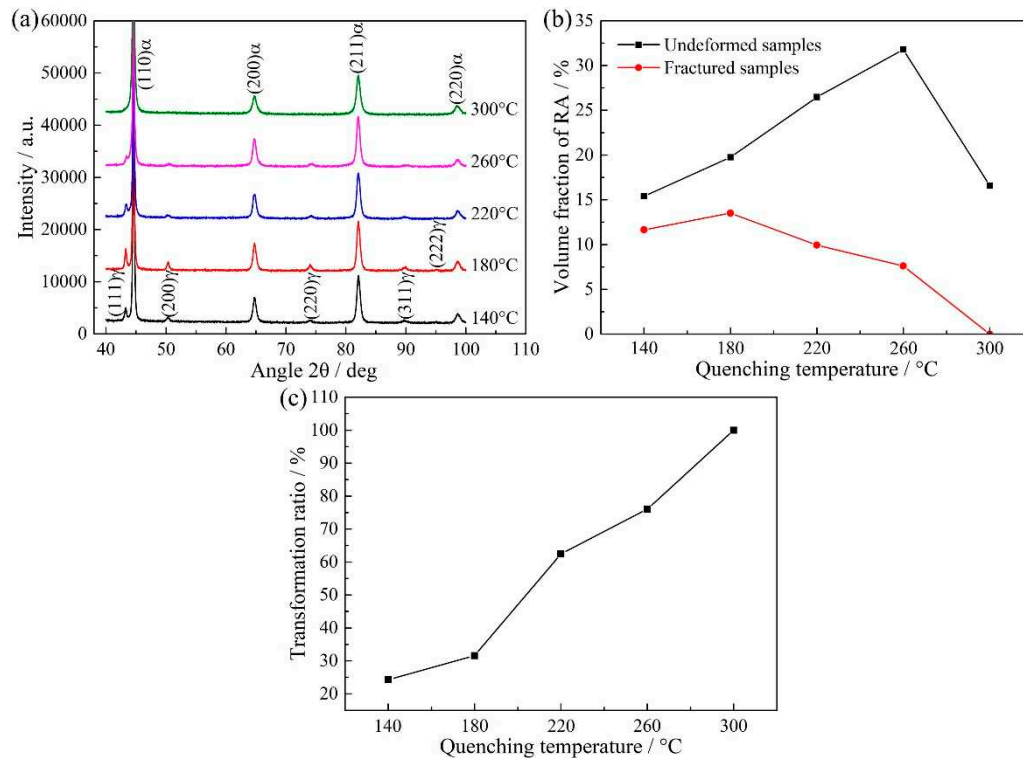


**Figure 10.** Engineering stress-strain plots of QP-processed samples.

**Table 1.** Mechanical properties of QP-processed samples and IA-processed samples.

Sample	YS / MPa	TS / MPa	TE / %	PSE / GPa%
Q140	1133	1250	12.6	15.75
Q180	1048	1173	14.7	17.24
Q220	992	1159	20.4	23.64
Q260	739	1242	11.7	14.53
Q300	781	1485	8.7	12.92
IA at 725 °C for 30 min [20]	609	1126	33	37.16
IA at 740 °C for 30 min [20]	361	1231	23.2	28.56

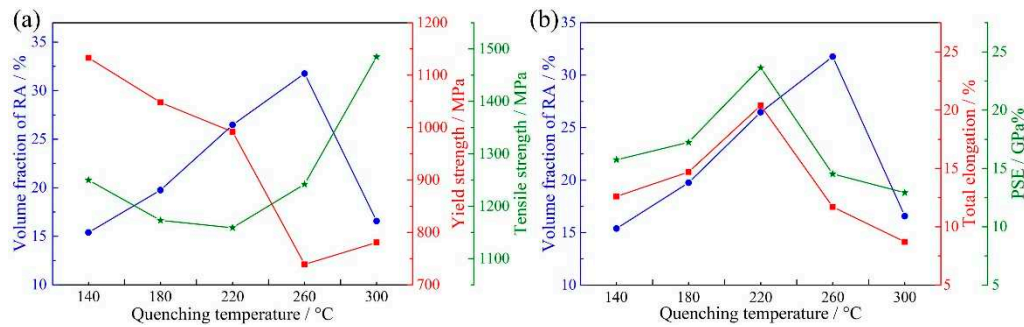
Figure 11a shows XRD patterns of fractured samples. The austenite peak of fractured sample was of lower intensity than the undeformed samples (Figure 8a). Especially, almost no austenite peak was observed in the fractured sample at quenching temperature of 300 °C. Figure 11b shows the comparison of the volume fraction of RA in undeformed and fractured samples and the corresponding transformation ratio of RA is shown in Figure 11c. It was observed the transformation ratio of RA increased with increasing quenching temperature. This is because the carbon content of RA in undeformed samples was decreased with increasing quenching temperature (Figure 9), leading to lower mechanical stability of RA in the sample subjected to higher quenching temperature. Besides, it should be noted that almost all RA transformed to martensite when the quenching temperature was 300 °C. This is related to the fact that the carbon content of RA in this sample was only 0.75 wt% that was relatively lower than the other samples, leading to an extremely lower mechanical stability of RA.



**Figure 11.** (a) XRD patterns of fractured samples, (b) comparison of volume fraction of RA and (c) transformation ratio of RA.

### 3.5. Relationship between Microstructure and Mechanical Properties

In the present study, the quenching temperature had influence on the mechanical properties of QP-processed samples (Figure 10). This is related to the different microstructure and TRIP effect occurred in Q140, Q180, Q220, Q260 and Q300 steels. Figure 12a shows the variation of RA fraction, YS and TS. The variation of YS was opposite to the variation of RA fraction and the YS had a minimum value in Q260 steel. When the quenching temperature was 140–260 °C, the YS may be mainly related to the volume fraction of RA, resulting in lower YS for the sample containing higher volume fraction of RA. However, when the quenching temperature was 300 °C, a considerable amount of secondary martensite formed during final quenching (Figure 4e and Figure 5e). The presence of a high fraction of secondary martensite in Q300 steel contributed to the rebound in the YS. In terms of TS, it was decreased from 1250 to 1159 MPa when the quenching temperature increased from 140 to 220 °C. This is also because the volume fraction of RA increased with increasing quenching temperature, leading to lower volume fraction of hard phase (martensite) at higher quenching temperature. Besides, it should be noted that the TS of Q220 steel was only 14 MPa lower than Q180 steel. On the one hand, this is due to the presence of secondary martensite in Q220 steel. The hardness of secondary martensite is higher than primary martensite because the former has higher carbon content and dislocation density than the latter. Thus, secondary martensite can effectively enhance the TS of Q220 steel. On the other hand, the transformation ratio of RA in Q220 steel was obviously higher than Q180 steel, which also enhanced the TS of Q220 steel through TRIP effect. When the quenching temperature was 260 °C, the highest volume fraction of RA was obtained and the secondary martensite fraction was also increased (Figure 5). The higher fraction of secondary martensite and higher transformation ratio of RA in Q260 steel contributed to the higher TS than Q220 steel. Furthermore, when the quenching temperature was 300 °C, the highest fraction of secondary martensite was present, leading to the highest TS of Q300 steel.



**Figure 12.** (a) Variation of RA fraction, YS and TS and (b) variation of RA fraction, TE and PSE.

Figure 12b shows the variation of RA fraction, TE and PSE. The variations of TE and PSE were first increased when the quenching temperature increased from 140 to 220 °C, followed by a decrease on further increasing the quenching temperature to 300 °C, i.e., the highest TE and highest PSE were present at the quenching temperature of 220 °C. However, the highest volume fraction of RA was obtained at the quenching temperature of 260 °C. This is because the mechanical property of QP-processed samples not only was related to the volume fraction of RA, but also was related to the mechanical stability of RA and the presence of secondary martensite. When the quenching temperature increased from 140 to 220 °C, the volume fraction and transformation ratio of RA were increased, improving TE through the enhanced TRIP effect. For Q260 steel, the carbon content of RA decreased to 0.83 wt%, which was lower than Q220 steel (0.97 wt%). Thus, the mechanical stability of RA in Q260 steel was relatively lower than Q220 steel. In this condition, although the fraction and transformation ratio of RA in Q260 steel were higher than Q220 steel, the TRIP effect occurred in Q260 steel may finish at lower strain than Q220 steel, leading to lower TE and PSE than Q220 steel. Besides, the presence of large size secondary martensite was also harmful for the TE and PSE of Q260 steel. When the quenching temperature increased to 300 °C, the carbon content of RA further decreased to 0.75 wt%. In this condition, the volume fraction and mechanical stability of RA in Q300 steel were decreased, contributing to the lower TE and PSE than Q260 steel. Similarly, the relatively high fraction of secondary martensite also led to the low TE of Q300 steel.

#### 4. Conclusions

A medium-Mn steel (Fe-0.3C-4Mn-1.82Al-0.6Si wt%) was processed by TRSC, hot rolling and QP process. The microstructure evolution and the structure–property relationship were studied. The main conclusions are as follows:

- (1) When the quenching temperature was less than or equal to 180 °C, the microstructure of QP-processed samples consisted of primary martensite and RA. However, when the quenching temperature was in the range of 220 to 300 °C, secondary martensite was also obtained in the QP-processed samples besides primary martensite and RA. This is related to the lower carbon content of partitioned austenite at higher quenching temperature, decreasing the thermal stability of partitioned austenite.
- (2) Because of the carbon partitioning during QP process, the RA with volume fraction of ~ 15.4%–31.8% was obtained in the QP-processed samples. The volume fraction of RA first increased from 15.4% to 31.8% when the quenching temperature increased from 140 to 260 °C, followed by a decrease to 16.6% on further increasing the quenching temperature to 300 °C.
- (3) The mechanical property with YS of 992 MPa, TS of 1159 MPa, TE of 20.4% and PSE of 23.64 GPa% was obtained in the QP-processed sample at quenching temperature of 220 °C. Compared with the strip-cast medium-Mn steel processed by IA process, the QP-processed sample had higher YS but lower TE than IA-processed sample under the condition of similar TS.
- (4) The mechanical properties of QP-processed samples were related to the RA fraction, mechanical stability of RA and the presence of secondary martensite. The superior mechanical properties of Q220 steel were achieved by an optimum combination of high RA fraction (26.5 vol%), appropriate mechanical stability of RA and a small amount of secondary martensite.

**Author Contributions:** C.Y. participated the research and analyzed the data. H.W. conceived of the study, designed the study, performed the research and wrote the paper. Y.Z. performed the TRSC experiment. Y.L. analyzed the data. J.K. developed the idea for the study and collected the data. Z.C. reviewed the paper. All authors have read and agreed to the published version of the manuscript.

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**Data Availability Statement:** Data presented in this article are available at request from the corresponding author.

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**Conflicts of Interest:** The authors declare no conflict of interest.

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