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Syngas Fermentation: Cleaning of Syngas as a Critical Stage in Fermentation Performance

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Abstract: The fermentation of syngas is an attractive technology that can be integrated with gasification of lignocellulosic biomass. The coupling of these two technologies allows for treating a great variety of raw materials. Lignin usually hinders microbial fermentations; thus, the thermal decomposition of the whole material into small molecules allows for the production of fuels and other types of molecules using syngas as substrate, a process performed at mild conditions. Syngas contains mainly hydrogen, carbon monoxide and carbon dioxide in varying proportions. These gases have a low volumetric energy density, resulting more interesting its conversion into higher energy density molecules. Syngas can be transformed by microorganisms, thus avoiding the use of expensive catalysts, which may be subject to poisoning. However, the fermentation is not free of suffering from inhibitory problems. The presence of trace components in syngas may cause a decrease in fermentation yields or cause a complete cessation of bacteria growth. The presence of tar and hydrogen cyanide are just examples of this fermentation's challenges. Syngas cleaning impairs significant restrictions in technology deployment. The technology may seem promising, but it is still far from large-scale application due to several aspects that still need to find a practical solution.

Keywords: biomass gasification; lignocellulosic material; biofuels; ethanol; short chain alcohols

1. Introduction

Syngas fermentation is a technology that uses specific biomass to transform small gaseous molecules into other gaseous compounds such as methane, but also other compounds such as ethanol, butanol and hexanol may be obtained. Alcohols are released into the liquid phase, thus requiring additional separation stages. The main advantages of the process are the mild conditions applied to the fermentation (low temperature and pressure) [1] to achieve the conversion of hydrogen and carbon monoxide (CO)/carbon dioxide (CO₂), just in an equivalent way as in the Fischer-Tropsch synthesis. Current interest in reducing the use of fossil sources for energy production and attaining a circular economy model in Europe to decouple economic growth and resource use [2] have led to the search for technologies capable of reusing materials and reducing the demand for virgin raw materials.

The circular economy concept attempts to reduce waste generation by keeping materials active in the economic cycle for longer periods, thus reducing mass and energy losses in production balances [3]. This concept is a promising approach to attaining sustainability in economic activity [4]. A circular economy strategy can aid in mitigating global climate change by increasing the reuse of materials, valorizing waste streams, and increasing the share of energy production from renewable sources and wastes [5]. However, not all aspects of this circular conceptualization result in advantages. Integrating wastes into the production chain needs to consider material quality, dispersion, transportation costs, and pre-treatments required to recover valuable components [6,7], which, as an intrinsic disadvantage, has an increase in energy demand. Other aspects involve market behavior and consumer perception, which may favor or hinder the introduction of recycling materials

into the production chain. Although the public accepts recycled plastics and paper, organic materials do not benefit from a good public perception. In addition, concerns regarding contaminants and health risks limit the reintroduction of organic wastes into the production chain. Energy and mass balances must also be carefully evaluated; thus, the conversion of biomass and the development of circular cycles should consider energetic constraints [8]. Absolute circularity is not achievable due to restrictions dictated by the second thermodynamic law since some energy is unavoidably lost [9].

The thermal treatment of biomass involves different processes, such as direct energy production from combustion, transformation to produce energy-containing molecules by pyrolysis/gasification [10–12], or processing in the presence of water under high temperature and pressure to generate a stable carbonaceous product [13,14]. This latter process is called hydrothermal carbonization and has been demonstrated to be a solution (currently at the experimental level) to treat biomass material with high moisture content. Thermal hydrolysis and decarboxylation of biomass occur, forming a char solid product and water-soluble compounds [15,16].

In the case of pyrolysis and gasification, the increase in temperature produces the thermal cracking of complex molecules. Pyrolysis, on the one hand, is carried out in the absence of air, resulting in a solid carbonaceous product (char), liquid and gaseous compounds with varying yields depending upon pyrolysis temperature and heating rate [17,18]. Common pyrolysis processes are classified as slow, fast, and flash pyrolysis. The first one takes place at temperatures around 300–500 °C and low heating rates. Usually, the increase in process temperature and heating ramp marks the difference between fast and flash pyrolysis, with the latter having heating rates greater than 1000 k/s [19,20]. A particularly slow pyrolysis process is torrefaction. This slow thermal treatment is intended as a biomass pre-treatment method to increase energy density characteristics, facilitating the storage and transport of biomass to be later used as a primary fuel [21]. Gasification, on the other hand, is a process that involves a first pyrolysis stage. However, in this case, a gaseous agent, which can be air, steam, oxygen or carbon dioxide, is introduced into the thermal reactor, mediating the conversion of heavy hydrocarbons into light molecules (CO and H₂) [22].

Syngas is produced from pyrolysis/gasification using different materials as inputs. The great advantage of thermal processing is its versatility, being capable of treating fossil sources such as oil sludge, a viscous residue derived from crude extraction and processing, heavy oil, coal, plastics and also renewable sources such as biomass, manures and organic wastes in general [23–28]. The gas produced has a low volumetric energy density mainly due to H₂ and CO. When air is used in gasification, nitrogen reduces the calorific value even more due to its high content in the incoming air.

The fermentation of gaseous components conforming syngas has awakened great interest. The concerns regarding the use of fossil fuels, future availability, and climatic impacts have caused the revival of several forgotten technologies previously considered unfeasible. These technologies are now considered suitable and capable of aiding in decarbonizing the energy and transport sector and increasing the recycling rate of raw materials by valorizing waste streams. Thus, concepts such as power to liquid (PtL) and waste to energy (WtE) have become common in the scientific and technical literature. In the first case, energy is used for producing small molecules to be later transformed into liquid components, mainly using the Fischer-Tropsch synthesis to obtain saturated hydrocarbons or synthetic liquid fuels from other catalyzed processes [29–31]. In the WtE case, waste streams, having low quality and high production volume, are used as raw materials. In this sense, municipal solid wastes, sewage sludge and manures have been considered suitable inputs for energy production either under thermal processes or biological ones such as anaerobic digestion [32–34].

The biological conversion of hydrogen and CO/CO₂ is possible by the use of specific microflora, which can be obtained from mixed cultures or using specific strains under anaerobic conditions. Anaerobic microorganisms can use C1 substrates as carbon sources, producing short-chain acids, alcohols, or methane. However, the use of syngas requires special cleaning procedures since this gas carries ash particles, nitrogen/sulfur gaseous compounds (H₂S, SO₂, COS, NH₃, HCN, NOx), oxygen, condensable organics and tar, which can inhibit microorganisms' activity [35–37]. Since the fermentation needs to be coupled to a syngas-producing process, the integration of biomass

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gasification and subsequent biological syngas conversion seems the logical sequence. However, pyrolysis and gasification processes are full of challenges due to their technical complexity and low profitability associated with high installation costs [38]. Therefore, the coupling with a fermentation stage intended to assimilate gaseous substrates will have to overcome their own constraints associated with mass transfer limitations, inhibitory conditions, and reactor conversion efficiency [39] and those associated with the thermal treatment of raw materials.

The present review aims to analyze the current state of gasification technology and syngas fermentation in an attempt to identify the feasibility of implementing this technology as one of the pathways to increase the share of renewables in the energy sector and aid in attaining full decarbonization of the economy.

2. Gasification/Pyrolysis Technologies

The gasification process is a proven technology used to produce syngas from coal for electricity generation in gas turbines. Synthesis of syngas molecules can be attained by catalytic processes like Fischer-Tropsch, producing liquid hydrocarbons, generating methanol from the Basf process, or methane from the Sabatier reaction [40–42]. The use of syngas dates back to 1812 when the Westminster and London Gas Light and Coke Co. was provided with a royal grant to light London streets in 1812 [43]. Although the gasification process has been widely studied, the technology deployment has suffered several drawbacks, still being at a demonstration scale or needing government subsidies to make plant installation feasible.

The integrated gasification combined cycle (IGCC) concept counted with four demonstration plants. Two located in the United States (Wabash River Coal Gasification Repowering Project and the Tampa Electric Integrated Gasification Combined-Cycle Project), and other two located in Europe (Willem Alexander IGCC Plant in Buggenum, Netherlands and ELCOGAS IGCC Plant in Puertollano, Spain) [44]. These plants were either shut down due to air pollutant constraints or retired due to finalizing project activities [45,46]. These large-scale demonstration projects allowed the development of the technology to reach a status close to commercial scale, although high installation costs are still a significant burden. However, experience has been gained regarding syngas composition and direct valorization in turbines for energy production, which is a valuable feature for the deployment of the technology when using other fuels.

Gasification technologies currently available are based on fixed-bed downdraft systems, updraft, bubbling bed, circulating fluidized bed or dual configurations to increase process efficiency (see Figure 1). It is worth mentioning that any technology should comply with current environmental legislation. Therefore, gasification/pyrolysis is not an exception. The technology must meet restrictions regarding volatile compounds production, NOx, sulfur compounds and particulate matter (PM2.5). Configurations exploring the feasibility of treating mixtures of coal and biomass capable of complying with emission standards were studied by Ward et al. [47] as part of the Alaska Syngas Project using a gasifier designed by Hamilton Maurer International, Inc. Large-scale configurations capable of producing a significant amount of energy require as well a high input rates, for this reason the combined use of coal and biomass allows adapting scale and materials availability in addition to reducing costs of gas cleaning technologies.

Researchers have studied the gasification of lignocellulosic biomass and wastes as a solution for transforming different materials. Gasification is an interesting option for materials with either a low value or that require high pretreatment costs when attempting other valorization pathways, such as fermentation for producing ethanol, butanol, methane, among others [48–50]. Applying pretreatments for releasing cellulose and subsequent transformation into sugars impairs high energy demand and operating costs, translating into difficulties when reaching profitability [51–53]. To this, it should also be added the production of inhibitory compounds released during pretreatments, adversely affecting the subsequent fermentation stages [54,55].

Most of the research on gasification and pyrolysis has been carried out at an experimental scale, although a wide variety of substrates has been evaluated [56–60]. The translation of these abundant results into an increase in scale and technology deployment has not been attempted at the same pace.

Most of these works evaluate product yields and composition. However, several aspects regarding the practical implementation of a technology are usually missed when performing small pilot-scale studies. Ash melting behavior, energy recovery, gas cleaning to remove acids, toxic compounds and trace contaminants, wastewater production and the presence of aromatic compounds in char are just a few factors that can endanger plant operability.

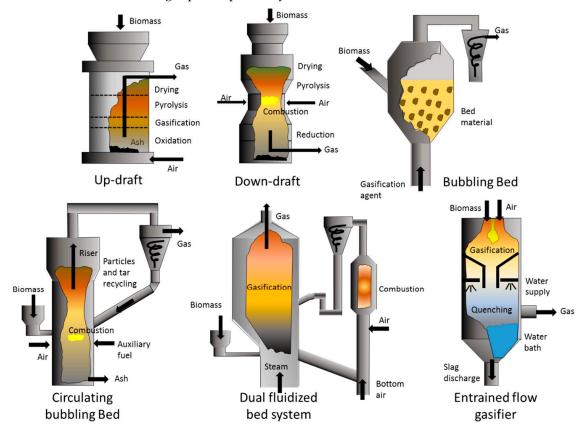


Figure 1. Schematization of different gasification technologies.

Table 1 lists different studies performed under laboratory and pilot-scale reactors. Other thermal processes, such as hydrothermal carbonization, were not considered in this table to set the focus on those technologies producing syngas. Thermal processes have the advantage of cracking complex molecules; thus, organic pollutants initially present in sludge may be eliminated. In the case of pyrolysis, the char produced is almost free from the presence of compounds that may cause concerns, such as hormones, antibiotics, microplastics, per- and polyfluoroalkyl substances (PFAS) [61]. Although metals may be concentrated in the char, the stability of these species increases with the increase in pyrolysis temperature, reducing its propensity to produce metal lixiviates [62,63]. Even though scientific literature considers the process feasible when using low-grade materials with high ash content, small commercial plants currently treat high-quality wood chip material, and only large-scale plants incorporating complex post-treatment equipment are able to treat a wide quality range of input materials.

Table 1. Gasification and pyrolysis assays carried out at pilot and semi-pilot scale available in the scientific literature using as substrate sewage sludge, manures and lignocellulosic biomass.

| Material | Gasification | Pyrolysis |
|----------------|--|--|
| | Steam gasification, laboratory scale reactor. 35 g | Fixed bed reactor. Slow pyrolysis |
| Courago cludgo | of sample. Increasing temperature from 700 to | Temperature: 400 – 800 °C |
| Sewage studge | 1000 °C increases hydrogen content in syngas | Pyrolysis gas was strongly temperature |
| | [64]. | dependent [65] |

Air as gasification agent. Analysis of tar and heavy metal content in tar. Concerns regarding final ash disposal after gasification [66].

Use of rotary kiln reactor with long residence time (30-50 min)

Temperature: 700-850 °C.

Gas yields of 1 m 3 /kg sludge with HHV 1 of 6 – 9 MJ/m 3 [68].

Fixed bed gasifier with varied ER (0.12 – 0.27). Applying air preheating improved H₂ and CO yields [70]

Manure

Fluidized bed gasifier. Steam gasification. Evaluated the effect of temperature. Syngas LHV: 2 – 4.7 MJ/m³ [71].

Fluidized bed gasifier. Air – oxygen used as gasification agent.

Feeding rate: 8 kg/min Temperature: 600 – 800 °C Syngas LHV: 1.78-8 MJ/m³ [73]

Tubular furnace chamber

ER: 0.21-0.3

Syngas HHV: 4.89 MJ/m³

Use of electrical furnace. Electricity obtained

from photovoltaic panels [75].

Quartz tube reactor.

Temperature: 300 – 700 °C

The presence of heavy metals in biochar was studied, reporting accumulation in char [67]

Horizontal tube reactor. Temperature: 550 – 850 °C

Increase in temperature reduces bio-oil and char yield [69]

Horizontal auger reactor. Pilot-plant. Electrically heated, temperature between 500 - 600 °C.

Mixture of sewage sludge and manure. Feeding rate: Charges of 12 kg every 2 min [23]

Sequential pyrolysis-gasification: Pyrolysis $(400 - 550 \, ^{\circ}\text{C})$ to produce char. Gasification of char. LHV 3 syngas: $5.31 - 5.65 \, \text{MJ/m}^{3}$ [57].

Kinetic evaluation by use of thermal analysis. Use of tubular pyrolyzer.

Fast pyrolysis maximized oil yields (550 °C) [72].

Solid fraction of pig manure Vertical auger pyrolysis reactor Temperature: 500 - 650 °C Flow rate: 0.4 - 0.8 kg/h [74].

Poultry litter

Laboratory-scale bubbling fluidized bed reactor using AL₂O₃ as bed material.

Temperature: 460 and 530 °C Residence time: 0.9 and 0.7 s

Feeding rates: 0.96 and 0.88 kg/h [76].

Chicken manure

Pilot-scale screw pyrolysis reactor STYX. Char was produced and heavy metal toxicity was evaluated when applying the material to soils [77].

Cattle manure Rotary kiln reactor

Temperatures: 400, 500 and 600 °C. Best oil yield obtained at 500 °C [78].

Pig and chicken manure Temperature: 600 °C Capacity: 6 t/d Retention time: 45 min

Gas and oil phase was recycled into the chamber and burned to supply energy to

the process [79].

Sequential pyrolysis-gasification

Pyrolysis: 700 – 800 °C Gasification agent: Steam/CO₂

Lower char yields were obtained gasification with steam. Increase process temperature reduces production [80].

Wood pellet

Gasification agent: steam

Temperature: 750 - 850 °C

Biomass

Pilot plant. Syngas composition was analyzed, attaining 43.3% of H₂ when optimizing temperature and steam injection. Energy content in syngas was higher for tests where methane concentration was higher [81].

Fluidized bed gasifier. Gasification agent: steam Steam biomass ratio (0.75/2) Temperature: 650 - 850 °C

The increase in temperature increases H₂, CO content in syngas. Increase in steam ratio increases H2 and methane content as fuel interest gases [82].

Sawdust

Bubbling fluidized bed gasifier

Gasification agent: air, oxygen enriched air,

H₂ production was higher when using steam LHV syngas: 5.95 - 7.16 MJ/m³ with air, 6.68 -11.4 with oxygen enriched air and pure oxygen [83]

Wood pellets (Picea mariana and Pinus banksiana mixture)

Vertical auger pyrolysis reactor Temperature: 500 – 650 °C Flow rate: 0.61 – 1.08 kg/h [74].

Switchgrass (Panicum Virgatum L.) Vertical auger pyrolysis reactor Temperature: 450 - 600 °C Flow rate: 0.57 kg/h [74].

Beech wood (Lignocel HBS 150-500 by J. Rettenmaier & Söhne GmbH + Co KG, Germany)

Bench-scale fixed bed reactor

Use of H-ZSM-5 and Al-MCM-41 pellet catalyst to reduce oxygen content in biooil [84]

Bagasse

Fluidized bed reactor - Pilot plant Flow

rate: 3 kg/h Retention time: 1 h Temperature: 500 °C Catalyst: CaO

Oxygen content if bio-oil is reduced but a lower oil yield is obtained [85]

¹ HHV: Higher heating value. ² ER: Equivalence ratio. ³ LHV: Lower heating value.

The experience and knowledge obtained with the gasification process in the petroleum industry have been adapted to treat waste and lignocellulosic biomass. Table 2 shows a list of companies with experience in this technology. The complexity of the process regarding emissions and the presence of tar and other contaminants in gas are aspects that can be better controlled with an increase in scale. However, when considering sole biomass as input, the amount of material locally available may not be sufficient for producing enough syngas to be efficiently coupled to an electricity production system, as would be the case of combined heat and power (CHP) engines or gas turbines. A solution is to deal with a flexible input; thus, mixtures of municipal solid wastes (MSW), plastics and biomass can serve as raw materials in this type of facility. Other options may be partial decentralization of gasification stages; therefore, biomass can be transformed close to its location, generating a condensed product that is easy to transport. A centralized large-scale unit capable of cleaning and processing syngas would receive then the condensed material. This is the idea behind the bioliq® process, where fast pyrolysis was selected as the pretreatment technology of biomass in a decentralized configuration. The oil obtained can be transported and transformed in a large-scale plant where syngas cleaning is effective and poisoning components can be removed prior to catalytic conversion to dimethyl ether (DME) and then to biogasoline [86,87] which is compatible with current engine fuels [88]. The increase in scale allows for a decrease in Levelized unitary costs. Therefore, it becomes feasible to use pure oxygen or oxygen-enriched air to obtain syngas with higher calorific value.

Table 2. This is a table. Tables should be placed in the main text near to the first time they are cited.

| Process | Company | Technology description | References |
|--|---|--|------------|
| Shell gasification technology | Shell global | Large scale commercial technology. The technology is capable of upgrading the bottom-of-the-barrel fraction and low-value streams into synthesis gas. | [89] |
| Valmet gasifier: Circulating fluidized bed gasification | Valmet | Large scale plant with several units operating in Finland. Partial combustion of biomass/waste at high temperatures with controlled air addition. | [90] |
| Bubbling fluidized bed gasification | EQTEC | Demonstration plant at Movialsa (Spain) fueled with olive mill solid waste. Several projects under construction | [91] |
| Co-current fixed bed downdraft gasification (GASCLEAN®) | Co-designed by PROVADEMSE (technological platform) and Cogebio is the manufacturer. | TRL7, demonstration plant. The reactor contains different zones: drying, pyrolysis, oxidation and reduction | [92] |
| Uhde® entrained-flow gasification | Thyssenkrupp | Demonstration plant in Puerto Llano Spain. Now shut down. Maximization of feedstock flexibility. Co- gasification of biomass and coal | [93,94] |
| Mitsubishi Municipal Solid Waste (MSW) Gasification & Ash Melting System | | Commercial plant. Gasification plant with ash melting process to reduce the volume of fly ash produced. Metals can be recovered from the process. | [95] |
| Biomass gasification and chemicals from syngas | Mitsubishi Heavy Industries, Chubu Electric Power Co., Inc., National Institute of Advanced Industrial Science and Technology | Commercial plant. Entrained-flow gasifier developed by MHI. The system gasifies pulverized biomass. No bed material is necessary thus temperature can be as high as $1000\ ^{\circ}\text{C}$ | [96] |
| Bubbling fluidized bed gasifier and methanol production | Enerkem | Gasification of wastes using a specialized product purification to obtain ultraclean syngas for catalytic conversion into methanol/ethanol. | [97] |
| Bioliq [®] process | KIT, Karlshruhe Institute of Technology | Decentralized fast pyrolysis of biomass to produce bioSyncrude. Transport of pyrolysis-oil to a centralized unit for gasification and synthesis of fuels. | [98] |

| Aitos Gasification Technology | GTH, Green transition holding | Large scale plant. Waste gasification. Modular process. Low NOx emission process. | [99] |
|--|--|---|-------|
| Wood gas CHP | URBAS energietechnik | Downdraft fixed bed gasifier. Feasible system for electricity production of less than 1000 kWel. | [100] |
| Syncraft®: Floating fixed bed gasification process | Syncraft Engineering GmbH | The floating bed concept allows keeping char loose inside the reactor preventing compaction and obtaining a permeable material. | [101] |
| Wood gasifier with CHP | Burkhardt Energy and Building Technology | Ascending downdraft gasification. Fuel and air are fed to the gas reactor from the bottom allowing pellets to swirl in certain zone but avoiding being carried out. Wood pellets should be high quality and uniform to attain bed stabilization. | [102] |
| Biomass steam gasification | Repotec | Medium-sized power plants. The technology is based on steam-blown fluidized-bed gasifier. A nitrogen-free atmosphere is created producing a low-tar content gas with high calorific value. Syngas is suited for power and heat generation and catalytic transformations | [103] |
| Wood gasifier with CHP | Pyrox | Medium scale. Combined updraft - downdraft fixed bed gasifier system. Four stages: drying – pyrolysis – oxidation-reduction. Oxidation takes place at high temperature (1000 °C). No waste water is produced. Ash production is about 1% of the wood chip input. | [104] |
| ECO20x CHP System | ECO20x Energia rinnovabile | Downdraft gasifier capable of using high quality biomass and low grade biomass such as crop waste with water content up to 20%, olive mill waste and textiles. | [105] |

| CHiP50 | ESPE energy expertise | Downdraft gasifier treating high quality wood chips maximum 10% humidity [106] content. Low ash production. |
|--------|--------------------------|---|

¹ Tables may have a footer.

Small-scale gasification technologies are currently available in the market for producing electricity or thermal energy. In this case, syngas cleaning is simplified since burning syngas will focus on reducing NOx and sulfur emissions. When internal combustion engines are used, then a cooling stage is necessary, requiring a careful control of tar formation to avoid precipitation on valves and engine components [107]. Patuzzi et al. [108] reviewed the performance of small gasification units that were installed in South Tyrol (Northern Italy) thanks to the availability of a very favorable feedin tariff. Small gasification units resulted in profitability with the increase in electricity tariff, but all these units had as a requirement the use of very high-quality biomass with low ash content. Therefore, the feasibility of applying decentralized gasification for valorizing crop or livestock wastes is currently null, although researchers have set the focus on valorizing low-grade lignocellulosic materials and wastes. Another fact that deserves special attention from their study is that technologies available showed high efficiency in producing gaseous products with low char yields. However, char generated presented high metal and PAH (polycyclic aromatic hydrocarbons) content; therefore, its direct use as a soil amendment is not recommended.

Thermal analysis is a widely used technique for establishing reaction kinetics and understanding sample behavior under different atmospheres. Pyrolysis, combustion and gasification of biomass have been studied by different authors, determining best fits to different degradation models and kinetics parameters based on curves profiles derived from thermal analysis using isothermal and non-isothermal methods [109–112]. However, there is a lack of correlation between kinetic parameters and gasifier/pyrolyzer performance.

Fernandez-López et al. [113] studied the gasification of manure samples by the use of thermal analysis. In this study, samples were initially pyrolyzed and then submitted to gasification under CO₂ at 800–900 °C. Temperature affected the rate of conversion and the amount of residual ash obtained. Lower temperatures caused a significant decrease in reaction rates but enhanced the final conversion, resulting in a greater mass loss. Similar studies can be cited regarding this subject; however, the major drawbacks of the gasification technology are associated with gas cleaning and tar removal. No matter what the final use of syngas is, the removal of poisoning compounds is needed if a chemical synthesis is the valorization choice for syngas or if fermentation would be the technology selected. Given the wide experimental work regarding gasification and experience gained in biomass gasification under laboratory and industrial scale, the technology can be considered mature, but syngas cleaning is the next challenging step. Tar seems unavoidable unless excessive high-temperature conditions are applied or catalysts are added to the gasification unit to favor tar cracking [114].

Co-gasification with fossil sources has been an option widely studied, starting with the use of coal and mixtures with organic wastes [115–117], and following with heavy hydrocarbons finding difficult treatment [118–120]. Bottom sludge from the petrochemical industry was gasified by Ongen et al. [121] in an updraft fixed bed gasifier with a recirculation zone to reduce tar formation. These authors added chicken manure in different proportions as a complementary organic input material. The final gas output was affected by the proportion of the mixture, and the best operation was found to be with 25% manure content.

The high input rate of thermal processes makes the volume of residues to be locally treated unable to satisfy the demand for raw materials unless a flexible feeding strategy is assumed. However, this option may not be perceived as environmentally friendly for the public as it would be the use of lignocellulosic biomass as a single feeding material. Treating mixtures of different wastes is a suitable option for attaining a desired power output but brings as a disadvantage a complexity in gas cleaning procedures and by-product disposal. Just as in any other process, the scale of the plant

highly affects profitability. Thus, Levelized unit costs decrease with the increase in plant size, and although co-gasification units may require a more complex cleaning system, the larger scale allows for affording this complexity.

Pattanayak et al. [122] studied the profitability of gasification in India by considering a downdraft gasifier in conjunction with electricity production by a combined heat and power engine (500 – 1000 kW). The proposal was reported as feasible, with electricity cost production prices much lower than the current tariff from conventional technologies. A similar study was previously performed by Porcu et al. [123], also intended for electricity production and indicating the economic feasibility of the approach. However, this study did not consider any adverse effect on plant performance when changing biomass from high-quality material to low-grade waste biomass with high ash content, thus skipping difficulties that may arise with tar condensation.

The gasification process may seem feasible if only considering product yields, but the technology necessary to comply with environmental regulations or to avoid problems in subsequent valorization stages, such as the presence of filters to remove ash and tar components, catalysts to reduce tar formation and adsorbents to eliminate inhibitory compounds increases capital investments and maintenance costs thus requiring of substantial subsidies to become feasible [107]. The experience gained with small-scale biomass gasification and energy production by CHP units may serve as a first step to moving forward to syngas fermentation since common requirements are established, such as syngas cooling and tar/particle removal.

3. Syngas Fermentation

Fermentation is an environmentally friendly technology due to its low energy demand compared to other technologies that operate under high pressure and temperature conditions. Several microorganisms have been studied for their capability of transforming small carbon molecules into organic acids and alcohols. Among common species studied are *Clostridium ljungdahlii*, *C. autoethanogenum*, *Acetobacterium woodii*, *C. carboxidivorans* and *Butyribacterium methylotrophicum* [124–128]). However, the fermentation process must deal with mass transfer limitations and culture contamination by undesired microflora or the presence of phage. Thus, the feasibility of the process may be compromised due to low titter production and high operating costs.

Demonstration plants have been built in different projects with the technology developed by companies such as INEOS Bio, Coskata Inc. and LanzaTech. Fermentation of syngas derived from biomass gasification was attempted in the bioenergy demonstration plant in Vero Beach, Florida [129]. However, inhibitory conditions experienced in the fermentation stage due to the presence of hydrogen cyanide led to unsuccessful performance after spending several millions of governmental subsidies [130]. Removing trace contaminants was not an easy task; thus, the approach of Coskata Inc. by coupling the fermentation process with the technology of Westinghouse Plasma (a subsidiary of Alter NRG), which allows plasma gasification obtaining a free-tar syngas, seemed to facilitate fermentation operation by eliminating the tar production [131]. Although, the approach could not be demonstrated, the Mihama-Mikata plasma gasification plant is clear proof of the significant advantages plasma technology offers [132,133].

Coskata Inc. was out of business and its technology was acquired by Synata Bio [134] and then by True North Venture Partners (TNVP) [135] with no further demonstrations plants being constructed. LanzaTech, on the other hand, has been able to keep working in demonstration plants thanks to the Steelanol project (financed under Horizon 2020), in conjunction with ArcelorMittal [136]. Process gases derived from the blast furnace located in Ghent, Belgium, will be transformed by biological means into ethanol [136]. Commercial facilities of LanzaTech are located in China (Shougang LanzaTech, Shougnag JiYuan and NingXia Binze) [137], with the plant of Shougang LanzaTech receiving a carbon label certification from the China Electronic Energy Saving Technology Association for its bioethanol products in 2023 [138]. However, information regarding ethanol yields, product concentration and energy demand associated with the distillation process is not easily available.

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3.1. Fundamentals of Syngas Fermentation

Alcohols and organic acids can be produced by acetogens using the acetyl-CoA reductive pathway, which is their main unifying feature given their wide genetic diversity. Ethanol and acetate production has been extensively studied, but C4 to C8 chemicals can also be produced from this pathway using different types of clostridium organisms [139]. This pathway is known as Wood-Ljungdahl and allows for reducing CO/CO2 using H2, obtaining energy, and assimilating carbon dioxide to produce cell carbon [140]. The pathway contains two branches, the methyl and carbonyl branch. In the methyl branch, the methyl group obtained from the reduction of CO/CO2 is transformed into formate by formate dehydrogenase and by a sequence of multiple steps forms methyl radicles that are further assimilated along with CO, forming acetyl-CoA [37]. CO can also be oxidized by biological water gas shift reaction into CO2, and the reducing equivalents derived from the reaction are conserved as reduced ferredoxin [141,142]. The production of acetyl-CoA is mediated by acetyl-CoA synthase (ACS) and carbon monoxide dehydrogenase complex (CODH) [1]. The bifunctional CO dehydrogenase enzyme reduces CO2 into CO, thus serving as the carbonyl group. In contrast, the methyl group is derived by a multistep reduction of CO2 where formyl, methenyl, methylene and methyl intermediates are bound to a pterin cofactor [143]. The carbonyl branch is exclusive of anaerobic microorganisms.

Acetate is formed from acetyl-CoA to recover energy, and ethanol is produced from further reduction of acetate [143]. Hydrogenases are inhibited by the presence of CO, causing a decrease in hydrogen uptake, but as CO levels decrease, hydrogen uptake increases again [144]. Some acetyl-CoA is used to produce complex organic cell components, carbohydrates, proteins, and lipids [145]. Figure 2 shows a schematized simplification of the Wood-Ljungdahl pathway. Detailed descriptions of this pathway are available at Bengelsdorf et al. [146]; Sahoo et al. [147] and Gencic et al., [148].

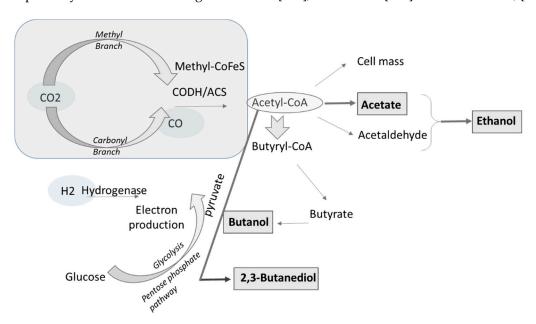


Figure 1. Simplified schematization of the Wood-Ljungdahl pathway. Figure adapted from Ahuja et al. [37], Daniell et al. [144] and Phillips et al. [145].

Ethanol and acetic acid are produced from syngas by the following equations [149].

$$6 \text{ CO} + 3 \text{ H}_2\text{O}$$
 → $\text{C}_2\text{H}_5\text{OH} + 4 \text{ CO}_2$ (1)

$$6 H_2 + 2 CO_2 \rightarrow C_2H_5OH + 3 H_2O$$
 (2)

$$4 \text{ CO} + 2 \text{ H}_2\text{O} \rightarrow \text{CH}_3\text{COOH} + 2 \text{ CO}_2$$
 (3)

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Ethanol production from syngas is usually carried out by the use of *Clostridium ljungdahlii* strains. The fermentation requires a change in conditions to promote solventogenesis, transforming organic acids into alcohol. Thus, ethanol production should be initially favored by biomass growth along with organic acid production (acetate) and, by shifting conditions, the formation of ethanol is attained in a subsequent stage [150]. Martin et al. [151] compared the performance of three different clostridium strains under batch conditions, reporting that *Clostridium ljungdahlii* showed a higher ethanol production rate (0.301 g/L h), whereas *Clostridium autoethanogenum* showed a poor performance when solventogenesis phase was induced. However, ethanol yields only reach a concentration of 1.9%. Klasson et al. [152] reported the highest ethanol concentration ever recorded (48 g/L) using *C. ljungdahlii* at a pH of 4.0–4.5 in a continuously stirred tank reactor (CSTR) under nutrient-limited conditions during 560 h of fermentation.

Keeping high ethanol productivity under continuous conditions is still a challenge due to the loss of culture viability and low levels of metabolic activity, as demonstrated by Mohammadi et al. [153], who reported that recovery stages and pH adjustments are needed to keep active microflora. These authors obtained an ethanol concentration of 6.5 g/L, but this value was just a peak concentration attained during a short period. The fermentation showed irregular performance for the 30-day operation period due to changes in biomass activity and pH, with ethanol evolution initially increasing until reaching peak values, suffering a decrease and posterior recovery afterward.

Liu et al. [154] also evaluated fermentation performance under continuous conditions, retaining biomass by cell recycling and using corn-steep liquor to reduce fermenting medium costs. These authors used as a fermenting organism a pure culture of *Alkalibaculum bacchi* strain CP15, although contamination was reported during continuous operation of the system. The ethanol concentration achieved was 6 g/L, whereas the contamination experienced caused a positive effect, allowing the coupled production of propanol and butanol. The acid production phase and subsequent transformation into alcohols must be clearly understood to control fermentation performance, either under continuous or batch-sequential conditions. Low availability of CO due to mass transfer limitations, pH values, and acetate concentration seem to be determinants in promoting metabolic changes in the microflora to activate the solventogenesis phase to counteract the inhibitory effect of undissociated acetic acid [155].

The number of scientific publications regarding syngas fermentation has increased exponentially in recent years [156]. Alcohols with longer chains than ethanol can also be obtained from syngas fermentation. *Clostridium carboxidivorans* and *C. kluyveri* have been proposed as organisms suitable for producing elongated alcohols and fatty acids in co-cultures or mixed microbial cultures [157–159]. Hexanol is produced along with butanol and ethanol, with the latter being the predominant product [160]. In this type of syngas fermentation, butanol and hexanol concentrations hardly surpass the threshold of 1 g/L, thus setting great difficulties in subsequent alcohol recovery stages. Fernández-Naveira et al. [161] reported higher hexanol values, but the concentration of this alcohol just reached 2.66 g/L. The decrease in fermentation temperature from 37 to 25 °C allows for the reduction of acid crash. It results beneficial to hexanol and butanol production, but although a significant improvement is attained, the hexanol concentration reported by Ramió-Pujol et al. [162] using this strategy was just 8.21 mM (0.84 g/L).

Reported titters in the scientific literature seem extremely low compared to conventional ethanol fermentation and even with fermentation of pre-treated lignocellulosic biomass, which can reach values around 100 - 140 g/L [163,164]. Table 3 shows a list of experimental studies regarding syngas fermentation and media optimization. Most experimental studies deal with laboratory conditions using reactors with a volume in the range of a few liters, showing low productivity and low product concentration. This fact is striking if compared with the aim of the Steelanol project, where a plant of 64,000 t ethanol/year will be built using a similar fermentation system [165].

Table 3. Experimental studies available in the scientific literature reporting on syngas fermentation.

| Microorganism | Product concentration (g/L) | Main characteristic of the study | Reference |
|---|---|--|---------------------------|
| C. autoethanogenum Ethanol: 2.24 – 3.76 | | Addition of malt and vegetable extracts | Thi et al. [125] |
| Ci iiiiiceiiiiiiicgeiiiiii | Ethanol | as replacement of yeast extract Inactivation of adhE results in 180% | Liew et al. [166] |
| | Ethanol: 4.23 – 4.57 | increase in ethanol production Tryptone and peptone supplementation | Im et al. [167] |
| | Ethanol. 4.23 – 4.37 | Yeast extract optimization | mi et al. [107] |
| | Ethanol: 3.45 | Acetate supplementation increased ethanol yield | Xu et al. [168] |
| | | Unable to achieve cell resting conditions | |
| | Ethanol < 1.5 mM (0.069) | when nitrogen limited environment was stablished | Cotter et al. [169] |
| | Ethanol | Simultaneous feeding of xylose and CO Metabolic engineering: expression of the | Mann et al. [170] |
| | Ethyl acetate | Sce Atf1 resulted in ethyl acetate formation | Dykstra et al. [171] |
| | Values reported as | | |
| | • | Co-culture with Clostridium kluyveri. | |
| | day) | Acetate and ethanol initially produced | D: 1 . 1.14701 |
| | Butyrate: 8.5 | were converted into elongated products. | Diender et al. [172] |
| | Caproate: 0.63 Butanol: 3.5 | Different pH conditions are necessary for the two species. | |
| | Hexanol: 2.0 | the two species. | |
| C. ljungdahlii | Ethanol: 0.3 | Nano particle addition to enhance syngas solubility | Kim et al. [173] |
| | Ethanol | Nutrient availability and pH can be manipulated to achieve solventogenesis | Richter et al. [127] |
| | Ethanol: 2.0 | pH and gas flow regulation | Infantes et al. [174] |
| | Ethanol: 1.09 | Improving bioreactor productivity by the use of hollow fiber system | Anggraini et al. [175] |
| | Ethanol: 0.34 2,3-Butanediol: 0.47 | Optimizing H2/CO ratio. Acetate productionwas favored by higher concentrations of hydrogen in the headspace. Alcohol production was favored by greater carbon monoxide concentrations in the headspace | Jack et al. [176] |
| | Ethanol: 0.85 – 3.75 | Evaluating gas flow rate, media and effluent flow rate, pH level, and stirrer speed. Pure CO and syngas mimic streams were fermented. Better results were obtained with synthetic syngas. | Acharya et al. [177] |
| | Ethanol: 0.24 – 0.53 | Trace element medium optimization | Sertkaya et al. [178] |
| C. carboxidivorans | Ethanol: 2.0 Butanol: 1.0 | Trace element medium optimization | Han et al. [179] |
| | Ethanol: 1.7 – 3.23 Butanol: 0.09 – 1.02 | Effect of NH ₃ , H ₂ S and NOx | Rückel et al. [180] |
| | Ethanol: 3.64 Butanol: 1.35 Hexanol: 0.66 | Temperature optimization (two-steps: 37 – 25 °C) | Shen et al. [181] |
| | Ethanol: 23.93 | Improving bioreactor productivity by the use of hollow fiber system | Shen et al. [182] |
| | Ethanol: 1.20 Butanol: 1.20 | Hexanol production was enhanced to 2.34 g/L when ethanol was | Oh et al. [183] |
| | Hexanol: 1.90 Ethanol: 1.40 – 1.50 Butanol: 0.40 – 0.50 | supplemented Evaluating the effect of oxygen presence in syngas | Rückel et al. [184] |

| | Hexanol: 0.10 – 0.20 ¹ | | |
|--------------|---|---|---------------------------|
| | Ethanol: 2.28 | Optimizing medium and reducing costs | Benevenuti et al. |
| | Butanol: 0.74 | | [185] |
| | Ethanol concentration not reported | Evaluating gas - liquid volume (V_L/V_G) ratio. Optimum growth rate takes place at CO partial pressure of 1.1 atm (equivalent to 25 mg/L) | Lanzillo et al. [128] |
| | C6 acids/alcohols Clostridium sp. JS66 | Characterization of a new acetogen for producing hexanoic acid. Increase in gas feeding pressure reduces product yield | Kim et al. [186] |
| | Total alcohols (ethanol + butanol): 2.43 – 4.58 | Addition of char increased product yield | Sun et al. [187] |
| C. ragsdalei | Ethanol: 2.01 | Key nutrients modulation: calcium pantothenate, vitamin B12, cobalt chloride (CoCl ₂) | Kundiyana et al. [188] |
| | Ethanol: 11 – 13.2 | Addition of poultry litter biochar as substitute of costly buffer components | Sun et al. [189] |
| | Ethanol: 14.92 | Random mutagenesis was performed using ethyl-methyl-sulfonate and UV followed by protoplast fusion | Patankar et al. [190] |
| | Ethanol: 2.86 – 5.14 | Addition of char increased product yield | Sun et al. [187] |
| | Ethanol: 0.5 – 1.5 | Optimization of fermenting media and reducing medium costs | Gao et al. [191] |

¹ Values were reported in graph, data here listed were obtained from reported data digitalization.

3.2. Experimental Work and Integration with Biomass Gasification

The experimental work available in the scientific literature deals mainly with small-batch scale reactors using synthetic syngas free of inhibitory components. Data obtained from large-scale experiences are scarce and even more if the use of syngas derived from biomass gasifiers is considered. Kundiyana et al. [192] evaluated a *Clostridium* strain P11T in a semi-pilot scale system. These authors tested a biomass gasifier and a 100 L reactor to ferment the resulting syngas. The main fermentation products were ethanol, acetic acid and 2-propanol. Ethanol concentration reached a value of 25.3 g/L. The fermentation was tested under batch conditions, and cell concentration in the reactor was kept low, about 0.84 g/L. Ethanol showed an increasing trend during the whole operation period (about two months), indicating promising future performance on a larger scale. However, the presence of trace contaminants resulted in severe fermentation failure. Rückel et al. [180] tested a culture of *Clostridium carboxidivorans* to produce short and medium-chain alcohols. These authors reported a beneficial effect under the presence of ammonia and hydrogen sulfide, but strong inhibition was caused by nitrogen oxides (added in the form of sodium nitrate or nitrite).

Gasification of low-quality biomass tends to produce more tars and inhibitors, thus demanding specific cleaning operations to remove contaminants, increasing cleaning-associated costs and adversely affecting process feasibility. Ramachandriya et al. [193] reviewed the effect of contaminants such as HCN, NOx, sulfide compounds, oxygen, and tars, among others, highlighting the relevance of producing clean syngas to integrate the two processes safely. Given the difficulties found in attaining stable performance when coupling small-scale biomass gasification and CHP energy production, then it is expected that syngas fermentation be linked to large-scale gasification units, which can stand a costly syngas upgrading process and afford additional equipment needed for controlling and removing contaminants.

Liakakou et al. [194] tested *Clostridium ljungdahlii* in a fermenting system coupled to a biomass gasifier. These authors studied the inhibitory effect of trace substances and tar components, evaluating the efficiency of the syngas cleaning processes developed to remove benzene, toluene, and xylene (BTX) mixtures using a specific oil absorber. The cleaning system also included a

hydrodesulfurization and a bed adsorption unit for removing H₂S and COS. The high efficiency of the cleaning process allowed for running a fermentation free of inhibitory conditions. The final ethanol concentration attained when feeding the clean gas was 2.2 g/L, using a 1.5 L CSTR.

Sharma et al. [195] alerted on the difficulties of producing a clean syngas stream. Cleaning technologies usually involve a wet scrubber to remove contaminants, causing syngas to cool down, affecting process efficiency and creating a wastewater disposal problem. On the contrary, removing contaminants at high temperatures seems more efficient, although extreme environments create other technical challenges when eliminating tars and particulate contaminants [196]. The use of oil instead of water is a concept tested by the OLGA technology, where heavy and light tar components are efficiently recovered using a two-stage absorber. Tar removed is then recycled back into the gasifier, reducing waste disposal costs and recovering energy from these undesirable by-products [197].

Other cleaning technologies developed include catalytic decomposition, BTX absorbers, removal of acid gases using adsorbents, and removal of nitrogen species [86,198]. A recent cleaning process was tested by Frilund et al. [199] using low-cost adsorption systems and organic solvent-free removal concepts to reduce costs and complexity of operation. On the contrary, Calì et al. [200] tested a water scrubber along with a chemical and physical wastewater management unit containing an oil skimmer and an activated carbon adsorption filter, attaining a significant reduction in the amount of water demanded by the cleaning stage. The use of an innovative cleaning system was tested by Hai et al. [201], proposing a mop fan with water spry, obtaining a tar removal efficiency of 89.6%.

Not all components act as toxic inhibitors; some others may even have a beneficial effect at specific concentrations. Oliveira et al. [202] studied the addition of sodium sulfide in a culture of *Clostridium ragsdalei*, observing an increase in ethanol concentration to 7.67 g/L. In a recent study, Oliveira and co-workers [203] tested different cultures of *C. autoethanogenum*, *C. ljungdahlii*, and *C. ragsdalei*, with *C. ljungdahlii* showing the highest tolerance to the presence of ammonium and nitrate whereas *C. ragsdalei* showed a positive effect under the presence of 0.1 g/L of H₂S. Table 4 lists studies that evaluate the effect of contaminants in syngas fermentation.

Table 4. This is a table. Tables should be placed in the main text near to the first time they are cited.

| | C 11 | ECC. | D (|
|---|--------------------|--|-----------------------|
| Contaminant | Culture | Effect | Reference |
| Ammonia | C. ragsdalei | Ammonia transforms into NH4+ ion accumulating in the system thus inhibiting hydrogenase activity. | Xu et al. [204] |
| Hydrogen cyanide | C. ljungdahlii | Product distribution was affected by the presence of cyanide, showing changes in ethanol-acetic acid ratio. Growth on fructose showed better tolerance, but growth on syngas was highly affected at a 0.1 mM concentration of cyanide in syngas. | Oswald et al. [205] |
| Oxygen | C. carboxidivorans | The presence of oxygen led to drastically reduced growth and product formation without alcohol production. | Rückel et al. [184] |
| Mixture of impurities. Testing commercially cleaned biomass syngas | C. ljungdahlii | Commercial syngas gas resulted in lower productivity when compared to clean syngas. Biomass derived syngas adversely affected carbon fixation. | Infantes et al. [206] |
| Mixture of impurities. Testing tar free syngas obtained from absorbers and particle removal filters | C. butyricum | Impurities caused complete inhibition. Clean syngas produced 29.24 mmol of butanol from 1 L of syngas. | Monir et al. [207] |

| Condensables | Butyribacterium methylotrophicum | complex mixtures of syngas impurities hinder growth and alter the profile carboxylic acid production. | Pacheco et al. [208] |
|--------------|-------------------------------------|---|----------------------|
| Tar | Saccharomyces cerevisiae | Total inhibition of cell growth. | Monir et al. [209] |

It should be noted that CO can also exert a toxic effect on hydrogenase enzymes, thus making the CO route the favorable one for producing reducing power and reducing ethanol production efficiency [193]. This effect explains results obtained by Lanzillo et al. [128] and Kim et al. [186]. However, results reported by Hurst & Lewis [149] indicated a better performance when increasing gas reactor pressure from 0.35 to 2.0 atm, reporting almost nil ethanol production at the lowest pressure tested and reaching an ethanol concentration up to 2.5 g/L *using Clostridium carboxidivorans* P7^T. Experiments performed at an even higher pressure, on the contrary, confirm the decrease experienced in product yield.

Stoll et al. [210] reported an initial increase in acetic acid production with pressure increase when assessing the performance of *Clostridium ljungdahlii* DSM13528 in a CSTR with a continuous supply of gas and operating under batch culture mode. The increase in pressure led to disappointing results. At 7 bar, the culture was unstable, showing significantly lower gas consumption and cell growth. There should be an equilibrium between enhancing gaseous substrate mass transfer to the liquid media and avoiding excessive CO levels to prevent inhibitory conditions.

CSTR are the most widely used laboratory reactors tested due to the simplified operation of the system at a small scale. However, other configurations offer outstanding performance when attempting an increase in mass transfer. Factors that affect the mass transfer phenomenon of gaseous species into the liquid phase include impeller configuration, agitation speed, partial pressure, temperature, the surface area available for mass transfer, mean bubble size, bubble size distribution, and bubble residence time [211–213]. In the present case, the inhibitory effect caused by CO sets limits to the amount of substrate safely transferred from the gas phase.

Munasinghe & Khanal [214] tested different reactors and diffuser types, indicating that gas lift reactors with bulb diffusers showed better performance regarding mass transfer, surpassing the performance of hollow fiber membrane modules. Impeller configuration also has a great effect on mass transfer. The propensity to gas flooding is greatly reduced if impellers are changed from standard Rushton turbines to concave-shaped turbines. However, impellers are not convenient when large-volume reactors are considered due to the high increase in the energy demand experimented when scale increases [215]. Figure 4 shows different reactor configurations suitable for fermenting gaseous substrates.

It must be borne in mind that the fermentation is not a final stage of a global process. Separation units are necessary to obtain the desired product, and energy demand is highly dependent on the fermentation yield attained. In addition, sterilization requirements to keep a pure culture free of external microbial contamination increase the process energy demand. Syngas fermentation has similarities with acetone-butanol-ethanol (ABE) fermentation, a process that, after experiencing an industrial boom, suffered from high energy prices, bacteriophage infection and more efficient process competitors [223–225], being relegated to experimental studies and waiting for a new opportunity. Configurations capable of overcoming inhibitory conditions and achieving higher titer and separation efficiency may make this fermentation a viable alternative to petroleum-based processes.

The capabilities of clostridium species to be integrated into a biorefinery context have been reviewed by Liberato et al. [226], considering these species ideal candidates due to their versatility in using different types of substrates and operating under anaerobic conditions. Although the variety of species and products generated by different strains include alcohols and organic acids, the process either using the conversion of simple sugars, lignocellulosic biomass or gaseous streams has not been able to become feasible at an industrial scale. Efforts to reduce fermentation costs have been attempted using low-cost fermenting media and supplements [185,187,227]. However, a simple solution is yet to be found due to the several complexities associated with fermentation stability and those added when coupling with biomass gasification.

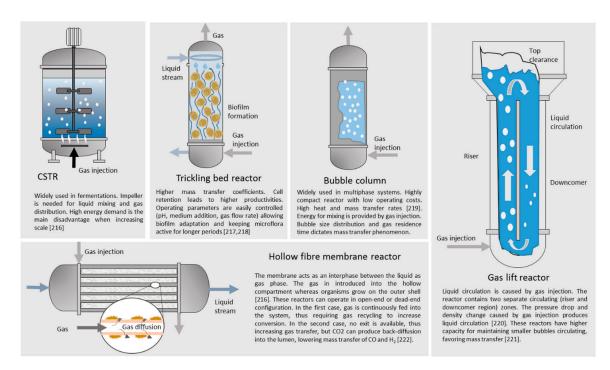


Figure 4. Schematization of different reactor configurations suitable for the fermentation of gaseous substrates.

The discovery of new strains capable of producing higher product concentrations opens a promising route. However, several deficiencies need to be solved to allow a real profitable process scaling. Lee et al. [228] reported on a novel strain (*Clostridium* sp. AWRP), which was isolated and studied using small batch serum bottles. The ethanol concentration attained was 119 mM (5.47 g/L), an interesting value compared with the previous ones reported in Table 3, but is yet extremely far from those obtained by the conventional fermentation processes.

Cleaning syngas is essential for avoiding the cessation of microbial growth during fermentation. The type of gasifier employed, gasification conditions and biomass quality also greatly influence the type of impurities and syngas cleaning requirements. Therefore, a global optimization of the process is needed [229] to attain low levels of contaminants without the requirement of costly cleaning processes. Although efforts are being made with successful performance, as demonstrated by Hai et al. [201], Frilund et al. [199], and Straczewski et al. [230]. Industrial application of the whole integrated approach still seems far due to other alternatives having better performance or demonstrating to be much closer to a commercial scale, as it would be integrating gasification and energy production by the use of solid oxide fuel cells [231,232], gas turbines [233,234], CHP engines and even its fermentation homologous for the production of methane since this small molecule can be used as fuel, having greater energetic density than carbon monoxide and hydrogen and does not need a phase separation as it is the case of producing acids of alcohols.

H₂ and CO/CO₂ can be converted into methane by a sequence or reactions involving water-gas shift reaction, acetogenesis, hydrogenotrophic methanation, carboxydotrophic methanation, and acetoclastic methanation [235]. Multiple reviews on this subject highlight the various benefits of this fermentation [213,236,237], and several studies report on high conversion rates when using membrane reactors, tricking beds, and high-pressure systems capable of attaining high cell concentration and productivity [238–240].

A final remark worth mentioning is the scarce information regarding ethanol recovery from low-concentrated streams. This stage is fundamental to attaining process feasibility since the ethanol concentration greatly affects the performance of recovery stages and energy demand [241]. However, this fermentation suffers from product inhibition. Thus, simultaneous removal of products during the fermenting stage may become an option for increasing reactor productivity, just as it has already been proposed for ABE fermentation [242–244]. Technical feasibility evaluated by Michailos et al.

[245] clearly summarized the disadvantages of this technology, indicating that conventional ethanol biorefineries have a better performance in terms of sustainability. The challenges to be overcome have been widely exposed: an increase in ethanol yields and mass transfer improvement of the gaseous substrate without causing metabolic shifts would benefit the mass and energy balance of the fermentation system. The integration with a biomass gasification stage requires solving the well-known tar formation problem along with removing specific toxic trace contaminants at a low cost.

4. Conclusions

The present manuscript reviewed the main parameters affecting the integration of biomass gasification and the subsequent transformation of syngas into alcohols. The fermentation process is an exciting technology, but unfortunately, the process suffers from several inhibitory effects when syngas derived from biomass gasification is used as substrate. Several studies in the scientific literature report on fermentation yields and the effect of contaminants. There is a lack of fermentation data obtained from pilot scale systems that consider the whole integration of the process. Significant technical advances have been made in the development of efficient gasifiers. However, research must continue to allow the development of high-rate fermenters capable of converting syngas without suffering from substrate or product inhibition. A global optimization is necessary, considering also the alcohol recovery stage to allow comparison with other types of fermentations and energy-producing processes.

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