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Article

Finite-Time Synchronization of Chaotic Systems Using Fractional Order Nonlinear PID Adaptive Sliding Controller

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Abstract: This study presents finite-time synchronization of chaotic fractional order systems with disturbance uncertainty and unknown time delay. First, a PID sliding surface is presented. Then, for the finite-time synchronization of the master and slave systems, a robust sliding-adaptive control method is provided. Update rules have been retrieved to estimate the system parameters by using the Lyapunov function while establishing the stability of the suggested mechanism and assuring the convergence of errors to zero. The proposed approach was used to solve the fractional order system of Gensou-Tsei with time-varying parameters, and the simulation results show that the presented approach performs well.

Keywords: fractional order chaotic system; finite-time synchronization; sliding controller; robust adaptive

1. Introduction

One of the areas that has recently piqued the interest of many scientists is fractional calculus. More degrees of freedom are added in the model with fractional order systems. Furthermore, it has been demonstrated that fractional calculus can be a significant mathematical tool for precise modeling of practical systems. Medical sciences [1], zoological sciences [2], biological systems [3], viscoelastic materials [4], energy supply and demand system [5], nuclear cycle generating system [6], dynamo theory [7], multi-agent system [8], industrial automation system [9], and HIV immunity model [10] are some of the systems described using fractional differential equations. Because of its applications in secure communication, signal processing, encoding-decoding, and electronic circuits, the study of chaos, chaos synchronization, and control of fractional order systems has recently gained traction [7,11,12]. Researchers have proposed a variety of approaches to control and synchronize fractional order systems, including feedback control [13,14], nonlinear control technique [15], observation-based control [16], phase synchronization [17], impulse synchronization [18], multi-scale synchronization [19,20], sliding mode control technique [21–23], fault-tolerant control [24], and so on. Synchronization of chaotic systems has piqued the interest of scientists, with over 350,000 research papers listed in Google Scholar. Many studies have been conducted in this subject for the integer [25], fractional [26], and [(new article)] systems. Several control mechanisms have been presented thus far for this purpose. There are numerous synchronization strategies for the fractional order deterministic dynamic system. The time required for synchronization is not always restricted in all synchronization methods. However, in the actual world, synchronization must be completed in a timely manner. In finite-time stability, the system's state variables converge to their equilibrium point more quickly and in a finite time. Because convergence time is critical, the time horizon is constrained, providing an effective foundation for faster synchronization in control systems and reducing convergence time.

Analyzing preset time synchronization for two chaotic systems of different dimensions, which can achieve the simultaneity of two chaotic systems of different dimensions in a predetermined time, employing adaptive control [27]. For synchronization between two separate chaotic systems with unknown parameters and disturbances, the fast non-singular terminal sliding mode adaptive control strategy has been examined [28]. For complex fractional-order laser synchronization in the presence of system uncertainties and external disturbances, a chatter-free finite-time SMC sliding surface approach has been suggested [29]. For a class of complex networks with fractional-order delays, delay-dependent finite-time synchronization has been investigated [30]. The finite-time synchronization problem for fractional order complex dynamical networks with intermittent control has been described in [31].

The finite-time synchronization problem of various systems with entirely unknown parameters has been investigated in this article. The synchronization error between the master and slave systems is defined first, and its finite time convergence to zero is demonstrated. The required adaptive rules are then derived to deal with the unknown characteristics of the systems, and the control law and update rules are built in such a way that the achievement condition is met. The next section introduces a mechanism for synchronizing fractional order systems with uncertainty, disturbance, and unknown time delay. The confirmation of its stability is examined in the following section. The proposed method was then applied to a system with time-varying characteristics, and a numerical simulation was provided at the end.

2. Definitions, Theorems, and Lemmas in Fractional Calculus

Definitions and lemmas for finite-time synchronization of fractional order chaotic systems with unknown uncertainty, disturbance, and time delay are given in this section.

Assume that the fractional order nonlinear system is defined as [32]:

$$D_t^q x(t) = f(x(t - \tau), t) \quad (1)$$

In which $q \in (0,1)$, $f = (f_1, f_2, \dots, f_n)^T$, and the synchronization error is defined as follows:

$$\lim_{t \rightarrow T} |e_{i-1}(t)| \rightarrow 0 \quad i = 2, 3, \dots, N \quad (2)$$

If for $t \geq T$, we have $|e(t)| \equiv 0$, system (1) is finite-time synchronized.

Lemma 1: for each constant value, $\alpha_i (i = 0,1,2,3)$ and $\sigma \in (0,1)$, the following relationships are established [33]:

$$\begin{aligned} (|a_1| + |a_2| + \dots + |a_n|)^\sigma &\leq |a_1|^\sigma + |a_2|^\sigma + \dots + |a_n|^\sigma \\ (|a_1| + |a_2| + \dots + |a_n|)^2 &\geq |a_1|^2 + |a_2|^2 + \dots + |a_n|^2 \end{aligned} \quad (3)$$

Theorem 1: Assume that $x = 0$ is the equilibrium point of the fractional order system (1), and that $f(x, t)$ meets the Lipschitz condition with constant $l > 0$ and $q \in (0,1)$. If the following equations are true for the Lyapunov function $v(t, x(t))$ and the class δ_i functions, then the Lyapunov function $v(t, x(t))$ achieves zero in finite time T [34,35]:

$$\delta_1(\|x\|) \leq v(t, x(t)) \leq \delta_2(\|x\|) \quad (4)$$

$$D^q v(t, x(t)) \leq -\delta_3(\|x\|) \quad (5)$$

$$D^q v(t, x(t)) \leq -\alpha v(t, x(t)) + b v(t - \tau_i(t), x(t - \tau_i(t))) - c v^\beta(t, x(t)) \quad (6)$$

$$\varphi = \sup_{t_0 - \tau \leq s \leq t_0} v(t, x(t)) \in (0,1) \quad , \quad \beta \in (0,1] \quad , \quad \tau_i(t) \leq \tau \quad (7)$$

Such that $a > b > 0$ and $c > 0$.

Thus, $v(t, x(t))$ converges to zero in finite time T.

$$T \leq \left[v(0, x)^{q-\frac{1}{\beta}} \frac{\Gamma\left(1 + \frac{1}{1-\beta}\right) \Gamma(2-\alpha) \Gamma(1+\alpha)}{\Gamma\left(1 + \frac{1}{1-\beta} - \alpha\right) (a-b)} \ln \frac{(a-b)\varphi^{1-\beta} + c}{c} \right]^{\frac{1}{q}} \quad (8)$$

Where Γ is the gamma function.

Lemma 2: Assuming that $x(t) \in R^n$ has continuous first order derivative, then [36]:

$$D_t^q \left(\frac{1}{2} x^T(t) Q x(t) \right) \leq x^T Q D_t^q x(t) \quad (9)$$

Where $q \in (0,1)$ and the matrix is positive definite.

3. Dynamic of the Fractional Order System

The synchronization of a fractional order chaotic system in the face of disturbance, uncertainty, and unknown time delay is presented in this section. The saturation operator on the control signal is incorporated in the design process of this subject to facilitate implementation. The simulation findings indicate that the performance will be good and acceptable.

The sliding mode control strategy for the fractional order chaotic system is described, and the synchronization of the fractional order system is examined as a result.

Consider the fractional master and slave system shown below:

$$\begin{cases} D^q x_i = x_{i+1}, & 1 \leq i \leq n-1 \\ D^q x_n = \sigma_0^T x + f(x(t-\tau_1), t) + \Delta f(x(t), t) + d_1(t) \end{cases}, \quad (10)$$

The fractional order slave system is as follows:

$$\begin{cases} D^q y_i = y_{i+1}, & 1 \leq i \leq n-1 \\ D^q y_n = \sigma_0^T y + g(y(t-\tau_2), t) + \Delta g(y(t), t) + d_2(t) + \varphi(u(t)) \end{cases} \quad (11)$$

In which $0 < q < 1$.

The fractional order error dynamic between the master (10) and slave (11) systems is given in (12).

$$\begin{cases} D^q e_i = e_{i+1}, & 1 \leq i \leq n-1 \\ D^q e_n = \sigma_0^T E + g(y(t-\tau_2)) - f(x(t-\tau_1)) \\ \quad + \Delta g(y(t), t) - \Delta f(x(t), t) + d_2(t) - d_1(t) + \varphi(u(t)) \end{cases}, \quad (12)$$

For system (11), Mittag-Leffler stability lemmas of fractional order type and asymptotic stability lemmas will be developed and proved, providing a theoretical foundation for demonstrating the performance of the suggested controllers.

Assumption 1: In master and slave systems, uncertain external distortions $d_1(t), d_2(t)$ as well as unknown bounded nonlinear uncertainties $\Delta f(x(t), t)$ and $\Delta g(x(t), t)$ satisfy the following conditions:

$$\begin{aligned} \|\Delta f(x(t), t)\| &\leq \beta_1 \omega_1(x), \\ \|\Delta g(y(t), t)\| &\leq \beta_2 \omega_2(y), \\ \|d_1(t)\| &\leq \rho_1 \\ \|d_2(t)\| &\leq \rho_2 \\ \underline{\tau}_1 &\leq \tau_1 \leq \bar{\tau}_1 \\ \underline{\tau}_2 &\leq \tau_2 \leq \bar{\tau}_2 \end{aligned} \quad (13)$$

So that $\|\cdot\|$ indicates norm of l_1 , and $\beta_2, \beta_1, \gamma_2, \gamma_1$ are definite positive real values and $\omega_2(\cdot), \omega_1(\cdot)$ are definite functions in general.

Definition 1: If $f(x, t)$ is piecewise continuous at t and meets the Lipschitz condition, then [36]:

$$\|f(t, x) - f(t, z)\| \leq \gamma_f \|x - z\|, \quad \forall x, z \in R^n \quad (14)$$

Then, $f(x, t)$ is Lipschitz at x and the positive constant, γ_f , is called the Lipschitz constant.

Assumption 2: The unknown time delays presented by nonlinear functions $f(x(t - \tau_1), t)$, $g(y(t - \tau_2), t) \in R$ and represented in general forms of (10) and (11) in the chaotic master and slave systems satisfy the Lipschitz conditions for each $x(t), y(t) \in R$ and considering (14):

$$\begin{aligned} |f(x(t - \tau_1)) - f(x(t - \hat{\tau}_1))| &\leq m_1 \|x(t - \tau_1) - x(t - \hat{\tau}_1)\| \\ &\leq l_1 |(t - \tau_1) - (t - \hat{\tau}_1)| = l_1 |\tau_1 - \hat{\tau}_1| = l_1 |\tilde{\tau}_1|. \\ |g(y(t - \tau_2)) - g(y(t - \hat{\tau}_2))| &\leq m_2 \|y(t - \tau_2) - y(t - \hat{\tau}_2)\| \\ &\leq l_2 |(t - \tau_2) - (t - \hat{\tau}_2)| = l_2 |\tau_2 - \hat{\tau}_2| = l_2 |\tilde{\tau}_2|. \end{aligned} \quad (15)$$

Such that $\tau_1, \tau_2 \in R$ represents unknown time delays, $\hat{\tau}_1, \hat{\tau}_2 \in R$ represents estimate of unknown time delays, and l_1, m_1 and l_2, m_2 are unknown positive constants.

4. Calculating the Control Signal

If the system is in sliding mode, the following conditions should be met:

$$\begin{aligned} s(t) &= 0, \quad D^q s(t) = 0 \\ s(t) &= h(e) \cdot [k_p e_n(t) + T_l D^{-\lambda} \sum_{i=1}^n k_{1i} e_i + T_d D^\delta \sum_{i=1}^n k_{2i} e_i(t)] = 0 \end{aligned} \quad (16)$$

Therefore, the sliding surface fractional order derivative in (16) is as follows.

$$\begin{aligned} D^q s(t) &= k_0 k_p D^q e_n(t) + k_0 T_l D^{q-\lambda} \sum_{i=1}^n k_{1i} e_i(t) \\ &+ k_0 T_d D^{q+\delta} \sum_{i=1}^n k_{2i} e_i(t) + (1 - k_0) k_p D^q (\|E(t)\| e_n(t)) \\ &+ (1 - k_0) T_l D^q (\|E(t)\| D^{-\lambda} \sum_{i=1}^n k_{1i} e_i(t)) \\ &+ (1 - k_0) T_d D^q (\|E(t)\| D^\delta \sum_{i=1}^n k_{2i} e_i(t)) = 0 \end{aligned} \quad (17)$$

In this case, the last dynamic of the fractional order system error, defined in (12) is substituted in (17):

$$\begin{aligned} D^q s(t) &= k_0 k_p (g(y(t - \tau_2), t) + \Delta g(x(t), t) + d_2(t) \\ &- (f(x(t - \tau_1), t) + \Delta f(x(t), t) + d_1(t)) + \sigma_0^T \cdot E(t) + u(t)) \\ &+ k_0 T_l D^{1-\lambda} \sum_{i=1}^n k_{1i} e_i(t) + k_0 T_d D^{1+\delta} \sum_{i=1}^n k_{2i} e_i(t) \\ &+ (1 - k_0) k_p D^q (\|E(t)\| e_n(t)) \\ &+ (1 - k_0) T_l D^q (\|E(t)\| D^{-\lambda} \sum_{i=1}^n k_{1i} e_i(t)) \\ &+ (1 - k_0) T_d D^q (\|E(t)\| D^\delta \sum_{i=1}^n k_{2i} e_i(t)) = 0 \end{aligned} \quad (18)$$

Such that is defined as in (18):

$$\begin{aligned} u(t) &= \frac{-1}{k_0 k_p} \left(k_0 T_l D^{q-\lambda} \sum_{i=1}^n k_{1i} e_i(t) + k_0 T_d D^{q+\delta} \sum_{i=1}^n k_{2i} e_i(t) \right. \\ &+ (1 - k_0) k_p D^q (\|E(t)\| e_n(t)) \\ &+ (1 - k_0) T_l D^q (\|E(t)\| D^{-\lambda} \sum_{i=1}^n k_{1i} e_i(t)) \\ &+ (1 - k_0) T_d D^q (\|E(t)\| D^\delta \sum_{i=1}^n k_{2i} e_i(t)) \Big) \\ &+ f(x(t - \hat{\tau}_1), t) - g(y(t - \hat{\tau}_2), t) - \sigma_0^T \cdot E(t) \\ &- b(s + \text{sgn}(s)|s|^\mu) + \bar{u}(t), \quad \mu \in (0, 1) \end{aligned} \quad (19)$$

$\bar{u}(t)$ is defined as follows:

$$\bar{u}(t) = -\text{sgn}(s) [\hat{\beta}_2 \omega_2(y) + \hat{\beta}_1 \omega_1(x) + \hat{\rho}_2 + \hat{\rho}_1] + u_{00}(t) \quad (20)$$

$$u_{00}(t) = -\frac{b}{k_0 k_p s} \sum_{i=1}^2 \left[(|\hat{\rho}_i| + \bar{\rho}_i)^2 + (|\hat{\tau}_i| + \bar{\tau}_i)^2 + (|\hat{\beta}_i| + \bar{\beta}_i)^2 + (|\hat{\rho}_i| + \bar{\rho}_i)^\mu + (|\hat{\tau}_i| + \bar{\tau}_i)^\mu + (|\hat{\beta}_i| + \bar{\beta}_i)^\mu \right],$$

(20) includes terms resulting from estimation of system uncertainties that are updated using the adaptive controller described in the next section. Thus, according to (13) in which the uncertainty bound is defined, $\bar{\beta}_i$, $\bar{\rho}_i$ and $\bar{\tau}_i$ are the upper bound of uncertainty, disturbance, and time delay in master and slave systems.

5. Proof of Stability and Update Rules

In this section, we will develop a robust adaptive controller employing a non-linear fractional order PID-based sliding surface in such a way that the suggested control strategy ensures the stability of the synchronization process of the aforementioned chaotic systems.

Theorem 2-5: Synchronization of the systems (10) and (11) is assured despite the disturbances d_1 and d_2 and the unknown uncertainties Δf and Δg , as well as the unknown time delay τ_1 and τ_2 with the controller definition $u(t)$ as follows:

$$\begin{aligned} u(t) = & -g(y(t - \hat{\tau}_1)) + f(x(t - \hat{\tau}_2)) \\ & - \frac{1}{k_0 k_p} \left(k_0 T_l D^{q-\lambda} \sum_{i=1}^n k_{1i} e_i(t) + k_0 T_d D^{q+\delta} \sum_{i=1}^n k_{2i} e_i(t) \right. \\ & + (1 - k_0) k_p D^q (\|E(t)\| e_n(t)) \\ & + (1 - k_0) T_l D^q (\|E(t)\| D^{-\lambda} \sum_{i=1}^n k_{1i} e_i(t)) \\ & + (1 - k_0) T_d D^q (\|E(t)\| D^\delta \sum_{i=1}^n k_{2i} e_i(t)) \Big) - \sigma_0^T \cdot E(t) \\ & - b(s + \text{sgn}(s)|s|^\mu) \\ & - \text{sgn}(s) (\hat{\beta}_2 \omega_2(y) + \hat{\beta}_1 \omega_1(x) + \hat{\rho}_2 + \hat{\rho}_1) + u_{00}(t) \end{aligned} \quad (21)$$

where $\hat{\rho}_1$ and $\hat{\rho}_2$ are estimates of the input disturbance bounds, $\hat{\tau}_1$ and $\hat{\tau}_2$ are estimates of time delays, and $\hat{\beta}_1$ and $\hat{\beta}_2$ are estimates of the uncertainty bounds in the master and slave systems. Furthermore, $\bar{\rho}_i$, $\bar{\tau}_i$, and $\bar{\beta}_i$ represent the upper bounds of disturbance, time delay, and uncertainty, respectively. As a result, in order to ensure the system's stability, we apply the update rules to estimate the mentioned parameters:

$$\begin{aligned} D^q \hat{\tau}_i &= -D^q \tilde{\tau}_i = l_i |s| \text{sgn}(\tilde{\tau}_i), \quad \hat{\tau}_i(0) = \bar{\tau}_i \\ D^q \hat{\rho}_i &= -D^q \tilde{\rho}_i = k_0 k_p |s| \\ D^q \hat{\beta}_1 &= -D^q \tilde{\beta}_1 = -k_0 k_p |s| \omega_1(x) \\ D^q \hat{\beta}_2 &= -D^q \tilde{\beta}_2 = -k_0 k_p |s| \omega_2(y) \end{aligned} \quad (22)$$

l_i is a positive constant number in the above relationship. Furthermore, $\tilde{\tau}_i$, $\tilde{\rho}_i$, and $\tilde{\beta}_i$ represent the estimation error of time delay, disturbance, and uncertainty, respectively. The update rules for delays are based on estimation errors, which are not available. You can overcome this problem by doing the following:

Given that: $0 < \underline{\tau}_i < \tau_i < \bar{\tau}_i$ such that $\bar{\tau}_i$ is the upper bound and $\underline{\tau}_i$ is the lower bound of the time delay. As a result of selecting $\hat{\tau}_i(0) = \bar{\tau}_i$, we have:

$$\tilde{\tau}_i(0) = \tau_i - \hat{\tau}_i(0) = \tau_i - \bar{\tau}_i < 0 \Rightarrow \text{sgn}(\tilde{\tau}_i) = -1$$

By defining $v_{\tilde{\tau}_i} = \frac{1}{2} \tilde{\tau}_i^2$ and calculating its derivative:

$$D^q v_{\tilde{\tau}_i} \leq \tilde{\tau}_i D^q \tilde{\tau}_i = \tilde{\tau}_i l_i |s| \text{sgn}(\tilde{\tau}_i) = -l_i |\tilde{\tau}_i| |s| < 0 \quad (23)$$

Therefore, $v_{\tilde{\tau}_i}$ is a descending function that tends to zero, thus: $\forall t \geq 0 : \tilde{\tau}_i < 0 \Rightarrow \text{sgn}(\tilde{\tau}_i) = -1$

Thus, the update rules for time delays would be as follows:

$$D^q \hat{\tau}_i = l_i |s| \operatorname{sgn}(\tilde{\tau}_i) = -l_i |s|, \quad \hat{\tau}_i(0) = \bar{\tau}_i, \quad i = 1, 2 \quad (24)$$

We will now investigate the stability of the controlled fractional order system by taking into account the sliding surface using nonlinear fractional order PID controllers. The following Lyapunov function is introduced for the sliding surface given in relation (5-9).

$$v(t) = \frac{1}{2} [s^2(t) + \tilde{\beta}_1^2 + \tilde{\beta}_2^2 + \tilde{\tau}_1^2 + \tilde{\tau}_2^2 + \tilde{\rho}_1^2 + \tilde{\rho}_2^2] \quad (25)$$

According to (21), derivative of the Lyapunov function would be as follows:

$$\begin{aligned} \rightarrow D^q v(t) &= \frac{1}{2} D^q (s^2 + \tilde{\beta}_1^2 + \tilde{\beta}_2^2 + \tilde{\tau}_1^2 + \tilde{\tau}_2^2 + \tilde{\rho}_1^2 + \tilde{\rho}_2^2) \\ &\leq s \cdot D^q s + \sum_{i=1}^2 (\tilde{\beta}_i D^q \tilde{\beta}_i + \tilde{\tau}_i D^q \tilde{\tau}_i + \tilde{\rho}_i D^q \tilde{\rho}_i) \end{aligned} \quad (26)$$

By applying (22) in (26), the above derivative is extended as follows:

$$\begin{aligned} D^q v(t) &\leq s \cdot \left[k_0 k_p \left(g(y(t - \tau_2), t) + \Delta g(x(t), t) + d_2(t) \right. \right. \\ &\quad \left. \left. - (f(x(t - \tau_1), t) + \Delta f(x(t), t) + d_1(t)) + \sigma_0^T \cdot E(t) + u(t) \right) \right. \\ &\quad \left. + k_0 T_i D^{q-\lambda} \sum_{i=1}^n k_{1i} e_i(t) + k_0 T_d D^{q+\delta} \sum_{i=1}^n k_{2i} e_i(t) \right. \\ &\quad \left. + (1 - k_0) k_p D^q (\|E(t)\| e_n(t)) \right. \\ &\quad \left. + (1 - k_0) T_i D^q (\|E(t)\| D^{-\lambda} \sum_{i=1}^n k_{1i} e_i(t)) \right. \\ &\quad \left. + (1 - k_0) T_d D^q (\|E(t)\| D^{\delta} \sum_{i=1}^n k_{2i} e_i(t)) + u_{00}(t) \right] \\ &\quad + \sum_{i=1}^2 (\tilde{\beta}_i D^q \tilde{\beta}_i + \tilde{\tau}_i D^q \tilde{\tau}_i + \tilde{\rho}_i D^q \tilde{\rho}_i) \end{aligned} \quad (27)$$

In this case, the Lyapunov function derivative is as follows:

$$\begin{aligned} D^q v(t) &\leq s \cdot \left[k_0 k_p \left(g(y(t - \tau_2), t) - g(y(t - \hat{\tau}_2), t) + \Delta g(x(t), t) + d_2(t) \right. \right. \\ &\quad \left. \left. + f(x(t - \hat{\tau}_1), t) - f(x(t - \tau_1), t) - \Delta f(x(t), t) - d_1(t) \right. \right. \\ &\quad \left. \left. - \frac{b}{k_0 k_p} (s + \operatorname{sgn}(s) |s|^\mu) \right. \right. \\ &\quad \left. \left. - \operatorname{sgn}(s) [\hat{\beta}_2 \omega_2(y) + \hat{\beta}_1 \omega_1(x) + \hat{\rho}_2 + \hat{\rho}_1] \right) \right] + s k_0 k_p u_{00}(t) \\ &\quad + \sum_{i=1}^2 (\tilde{\beta}_i D^q \tilde{\beta}_i + \tilde{\tau}_i D^q \tilde{\tau}_i + \tilde{\rho}_i D^q \tilde{\rho}_i) \end{aligned} \quad (28)$$

Thus, we have:

$$\begin{aligned} D^q v(t) &\leq |s| \cdot \left[k_0 k_p (|g(y(t - \tau_2), t) - g(y(t - \hat{\tau}_2), t)| + |\Delta g(x(t), t)| \right. \\ &\quad \left. + |f(x(t - \hat{\tau}_1), t) - f(x(t - \tau_1), t)| + |\Delta f(x(t), t)| \right. \\ &\quad \left. + |d_2(t) - d_1(t)|) - b(s^2 + |s|^{\mu+1}) \right. \\ &\quad \left. + k_0 k_p s (-\operatorname{sgn}(s) [\hat{\beta}_2 \omega_2(y) + \hat{\beta}_1 \omega_1(x) + \hat{\rho}_2 + \hat{\rho}_1]) \right. \\ &\quad \left. - b \left(\sum_{i=1}^2 [(|\hat{\rho}_i| + \bar{\rho}_i)^2 + (|\hat{\tau}_i| + \bar{\tau}_i)^2 + (|\hat{\beta}_i| + \bar{\beta}_i)^2 \right. \right. \\ &\quad \left. \left. + (|\hat{\rho}_i| + \bar{\rho}_i)^\mu + (|\hat{\tau}_i| + \bar{\tau}_i)^\mu + (|\hat{\beta}_i| + \bar{\beta}_i)^\mu \right] \right) \\ &\quad + \sum_{i=1}^2 (\tilde{\beta}_i D^q \tilde{\beta}_i + \tilde{\tau}_i D^q \tilde{\tau}_i + \tilde{\rho}_i D^q \tilde{\rho}_i) \end{aligned} \quad (29)$$

Relationship (29) will be recast as follows, based on assumptions 1 and 2 stated in relations (14) and (15):

$$\begin{aligned}
 D^q v(t) \leq & |s| \cdot [k_0 k_p (l_2 |\tau_2 - \hat{\tau}_2| + \beta_2 \omega_2(y) + l_1 |\tau_1 - \hat{\tau}_1| - \beta_1 \omega_1(x) + \rho_1 \\
 & + \rho_2)] - b(s^2 + |s|^{\mu+1}) \\
 & + k_0 k_p s \left((-\operatorname{sgn}(s) [\hat{\beta}_2 \omega_2(y) + \hat{\beta}_1 \omega_1(x) + \hat{\rho}_2 + \hat{\rho}_1]) \right) \\
 & - b \left(\sum_{i=1}^2 [(|\hat{\rho}_i| + \bar{\rho}_i)^2 + (|\hat{\tau}_i| + \bar{\tau}_i)^2 + (|\hat{\beta}_i| + \bar{\beta}_i)^2 \right. \\
 & \left. + (|\hat{\rho}_i| + \bar{\rho}_i)^\mu + (|\hat{\tau}_i| + \bar{\tau}_i)^\mu + (|\hat{\beta}_i| + \bar{\beta}_i)^\mu] \right) \\
 & + \sum_{i=1}^2 (\tilde{\beta}_i D^q \tilde{\beta}_i + l_i \tilde{\tau}_i D^q \tilde{\tau}_i + \tilde{\rho}_i D^q \tilde{\rho}_i)
 \end{aligned} \tag{30}$$

The derivative of the Lyapunov function would be as follows:

$$\begin{aligned}
 D^q v(t) \leq & |s| [k_0 k_p (l_1 |\tilde{\tau}_1| + \tilde{\beta}_2 \omega_2(y) + l_2 |\tilde{\tau}_2| + \tilde{\beta}_1 \omega_1(x) + \hat{\rho}_2 + \hat{\rho}_1)] \\
 & - b(s^2 + |s|^{\mu+1}) \\
 & - b \left(\sum_{i=1}^2 [(|\hat{\rho}_i| + \bar{\rho}_i)^2 + (|\hat{\tau}_i| + \bar{\tau}_i)^2 + (|\hat{\beta}_i| + \bar{\beta}_i)^2 + (|\hat{\rho}_i| + \bar{\rho}_i)^\mu \right. \\
 & \left. + (|\hat{\tau}_i| + \bar{\tau}_i)^\mu + (|\hat{\beta}_i| + \bar{\beta}_i)^\mu] \right) + \sum_{i=1}^2 (\tilde{\beta}_i D^q \tilde{\beta}_i + \tilde{\tau}_i D^q \tilde{\tau}_i + \tilde{\rho}_i D^q \tilde{\rho}_i)
 \end{aligned} \tag{31}$$

At this point, the update rules described in (22) are used to estimate the system parameters in relation (29). On the other hand:

$$|\tilde{\tau}_i| = |\tau_i - \hat{\tau}_i| \leq |\tau_i| + |\hat{\tau}_i| \leq |\hat{\tau}_i| + \bar{\tau}_i \Rightarrow -(|\hat{\tau}_i| + \bar{\tau}_i)^2 \leq -|\tilde{\tau}_i|^2 \tag{32}$$

That relationship (32) can also be extended for $\tilde{\rho}_i$ and $\tilde{\beta}_i$. In this case, the Lyapunov function derivative will be simplified as follows:

$$\begin{aligned}
 \Rightarrow D^q v(t) \leq & -b \left(|s|^2 + \sum_{i=1}^2 [|\tilde{\beta}_i|^2 + |\tilde{\tau}_i|^2 + |\tilde{\rho}_i|^2] \right) \\
 & - b \left(|s|^{1+\mu} + \sum_{i=1}^2 [|\tilde{\beta}_i|^{1+\mu} + |\tilde{\tau}_i|^{1+\mu} + |\tilde{\rho}_i|^{1+\mu}] \right)
 \end{aligned} \tag{33}$$

$$\begin{aligned}
 \Rightarrow D^q v(t) \leq & -b \left(|s|^2 + \sum_{i=1}^2 [|\tilde{\beta}_i|^2 + |\tilde{\tau}_i|^2 + |\tilde{\rho}_i|^2] \right) \\
 & - b 2^{\frac{1+\mu}{2}} \left(\frac{|s|^2 + \sum_{i=1}^2 [|\tilde{\beta}_i|^2 + |\tilde{\tau}_i|^2 + |\tilde{\rho}_i|^2]}{2} \right)^{\frac{1+\mu}{2}} \\
 & \leq -bv - b 2^{\frac{1+\mu}{2}} v^{\frac{1+\mu}{2}}
 \end{aligned} \tag{34}$$

Its finite-time stability is demonstrated for a chaotic considering the PID sliding surface and nonlinear fractional order derivative.

For boundedness, the control signal is modified as follows:

$$\begin{aligned}
u(t) = & -g(y(t - \hat{\tau}_1)) + f(x(t - \hat{\tau}_2)) \\
& - \frac{1}{k_0 k_p} \left(k_0 T_l D^{q-\lambda} \sum_{i=1}^n k_{1i} e_i(t) + k_0 T_d D^{q+\delta} \sum_{i=1}^n k_{2i} e_i(t) \right. \\
& \quad + (1 - k_0) k_p D^q (\|E(t)\| e_n(t)) \\
& \quad + (1 - k_0) T_l D^q (\|E(t)\| D^{-\lambda} \sum_{i=1}^n k_{1i} e_i(t)) \\
& \quad \left. + (1 - k_0) T_d D^q (\|E(t)\| D^{\delta} \sum_{i=1}^n k_{2i} e_i(t)) \right) - \sigma_0^T \cdot E(t) \\
& - b(s + \operatorname{sgn}(s)|s|^\mu) - \operatorname{sgn}(s)(\hat{\beta}_2 \omega_2(y) + \hat{\beta}_1 \omega_1(x) + \hat{\rho}_2 + \hat{\rho}_1) \\
& - \frac{bs}{k_0 k_p (s^2 + \epsilon)} \left(\sum_{i=1}^2 \left[(|\hat{\rho}_i| + \bar{\rho}_i)^2 + (|\hat{\tau}_i| + \bar{\tau}_i)^2 + (|\hat{\beta}_i| + \bar{\beta}_i)^2 \right. \right. \\
& \quad \left. \left. + (|\hat{\rho}_i| + \bar{\rho}_i)^\mu + (|\hat{\tau}_i| + \bar{\tau}_i)^\mu + (|\hat{\beta}_i| + \bar{\beta}_i)^\mu \right] \right)
\end{aligned} \tag{35}$$

In which, ϵ is a small positive number.

Adaptive rules should be updated to increase their robustness to uncertainty and disturbance. These changes are possible in a variety of ways. The law of sigma correction is one of these ways.

The Sigma function represented in Figure 1 is defined as follows:

$$\sigma(t) = \begin{cases} 0 & \text{if } |\hat{\theta}(t)| \leq M_0 \\ (|\hat{\theta}(t)|/M_0 - 1)^n \sigma_0 & \text{if } M_0 < |\hat{\theta}(t)| \leq 2M_0 \\ \sigma_0 & \text{if } |\hat{\theta}(t)| \geq 2M_0 \end{cases} \tag{36}$$

The presence of uncertainty and disturbance in the system causes a mild increase in estimations in the controller under investigation, which can be dealt with utilizing the sigma correction approach. As a result, the following are the update rules of the estimation of delays and the disturbance and uncertainty bounds:

$$\begin{aligned}
D^q \hat{\tau}_i &= -l_i |s| - \sigma_0 (|\hat{\tau}_i|) \hat{\tau}_i, \quad \hat{\tau}_i(0) = \bar{\tau}_i, \quad i = 1, 2 \\
D^q \hat{\rho}_i &= k_0 k_p |s| - \sigma_0 (|\hat{\rho}_i|) \hat{\rho}_i, \quad i = 1, 2 \\
D^q \hat{\beta}_1 &= -k_0 k_p |s| \omega_1(x) - \sigma_0 (|\hat{\beta}_1|) \hat{\beta}_1, \\
D^q \hat{\beta}_2 &= -k_0 k_p |s| \omega_2(y) - \sigma_0 (|\hat{\beta}_2|) \hat{\beta}_2,
\end{aligned} \tag{37}$$

[] (new article going to be released) describes in full the proof of error convergence to zero in the condition that the sliding surface tends to zero.

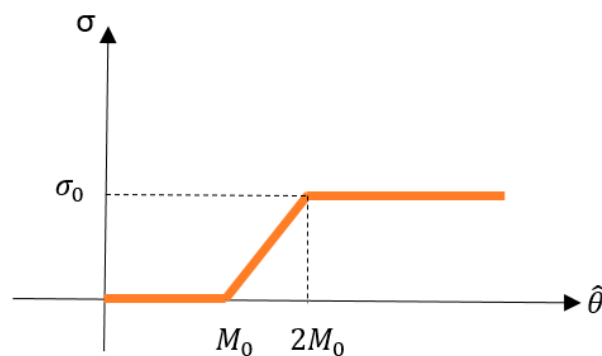


Figure 1. Sigma Function Graph.

6. Simulation Results

Consider the master and slave system with disturbance, uncertainty, unknown parameter and time delay for a fractional order Gensou-Tsei system as follows:

$$\begin{aligned} {}_0D_t^{q(t)}x_1(t) &= x_2(t), \\ {}_0D_t^{q(t)}x_2(t) &= x_3(t), \\ {}_0D_t^{q(t)}x_3(t) &= -\beta_1x_1(t) - \beta_2(t) - \beta_3x_3(t) + f(x(t)), \end{aligned} \quad (38)$$

Such that $\beta_1, \beta_2, \beta_3, \beta_4$ are system parameters, and $f(x(t)) = \beta_4x_1^2(t)$. In the presence of external disturbances, nonlinear uncertainties, parametric uncertainties, and unknown time delays, the above equations take the following form:

$$\begin{aligned} {}_0D_t^{q(t)}x_1(t) &= x_2(t), \\ {}_0D_t^{q(t)}x_2(t) &= x_3(t), \\ {}_0D_t^{q(t)}x_3(t) &= -\beta_1(t)x_1(t) - \beta_2(t)x_2(t) - \beta_3(t)x_3(t) \\ &\quad + f(x(t - \tau_1)) + \Delta f(x(t), t) + d_1(t), \end{aligned} \quad (39)$$

And $f(x(t - \tau_1)) = \beta_4x_1^2(t - \tau_1)$. Also, the slave system is presented as follows.

$$\begin{aligned} {}_0D_t^{q(t)}y_1(t) &= y_2(t), \\ {}_0D_t^{q(t)}y_2(t) &= y_3(t), \\ {}_0D_t^{q(t)}y_3(t) &= -\beta_1(t)y_1(t) - \beta_2(t)y_2(t) - \beta_3(t)y_3(t) \\ &\quad + g(y(t - \tau_2)) + \Delta g(y(t), t) + d_2(t) + u(t), \end{aligned} \quad (40)$$

$\beta_1(t), \beta_2(t), \beta_3(t)$ are parametric uncertainties, and $g(y(t - \tau_2)) = \beta_4y_1^2(t - \tau_2)$ in the simulation process are considered as follows:

$$\beta_i(t) = \beta_{0i} + \Delta\beta_i(t)$$

$$\beta_1(t) = \beta_1 + 0.3 \sin(t) \rightarrow \beta_1(t) \in [0.7 \ 1.3],$$

$$\beta_2(t) = \beta_2 + 0.2 \cos(t) \rightarrow \beta_2(t) \in [0.9 \ 1.3], \quad (41)$$

$$\beta_3(t) = \beta_3 + 0.6 \cos(t) \rightarrow \beta_3(t) \in [-0.16 \ 1.04].$$

$$\beta_4 = 1.$$

The following system disturbances and nonlinear uncertainties are considered during the simulation process:

$$d_1(t) = 0.6 \sin(t) \cos(\pi t), \quad d_2(t) = \sin(\pi t) \cos(t)$$

$$\Delta f(x(t), t) = 0.65 \sin(\pi x_1(t)) + 0.8 \sin(2\pi x_1(t)x_2(t)) + 0.9 \sin(3\pi x_3(t)), \quad (42)$$

$$\Delta g(y(t), t) = 0.1 \cos(y_1(t) + y_2(t)) + 0.8 \sin(\pi y_3(t)),$$

The dynamic equations of the synchronization error of the fractional order chaotic system with uncertainty, unknown disturbance, and unknown time delay are defined using equations (10) and (11).

$$\begin{aligned} {}_0D_t^q e_1(t) &= e_2(t), \\ {}_0D_t^q e_2(t) &= e_3(t), \\ {}_0D_t^q e_3(t) &= -\beta_{10}e_1(t) - \beta_{20}e_2(t) - \beta_{30}e_3(t) + g(y(t - \tau_2)) - f(x(t - \tau_1)) \\ &\quad + \Delta g^{new}(y(t), t) - \Delta f^{new}(x(t), t) + d_2(t) - d_1(t) + u(t). \end{aligned} \quad (43)$$

Such that $\beta_{10} = 1, \beta_{20} = 1.1, \beta_{30} = 0.44$. Also:

$$\Delta f^{new}(x(t), t) = \Delta f(x(t), t) - \Delta\beta_1(t)e_1(t) - \Delta\beta_2(t)e_2(t) - \Delta\beta_3(t)e_3(t)$$

$$\Delta g^{new}(x(t), t) = \Delta g(x(t), t) - \Delta\beta_1(t)e_1(t) - \Delta\beta_2(t)e_2(t) - \Delta\beta_3(t)e_3(t)$$

Figures 2 and 3 depict the chaotic behavior of a fractional order master and slave system with time-varying parameters in the absence of controller operations.

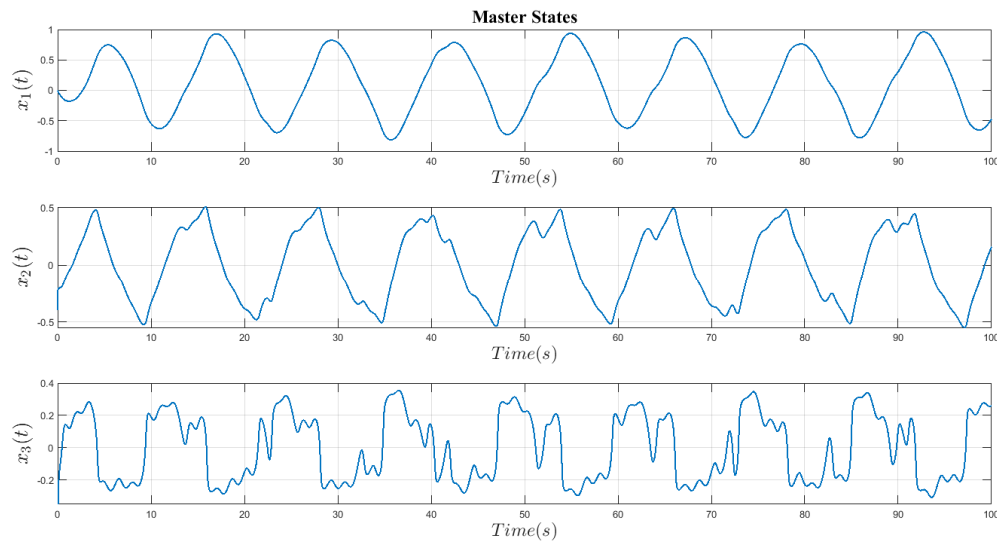


Figure 2. Chaotic behavior of the master Gensou-Tsei system.

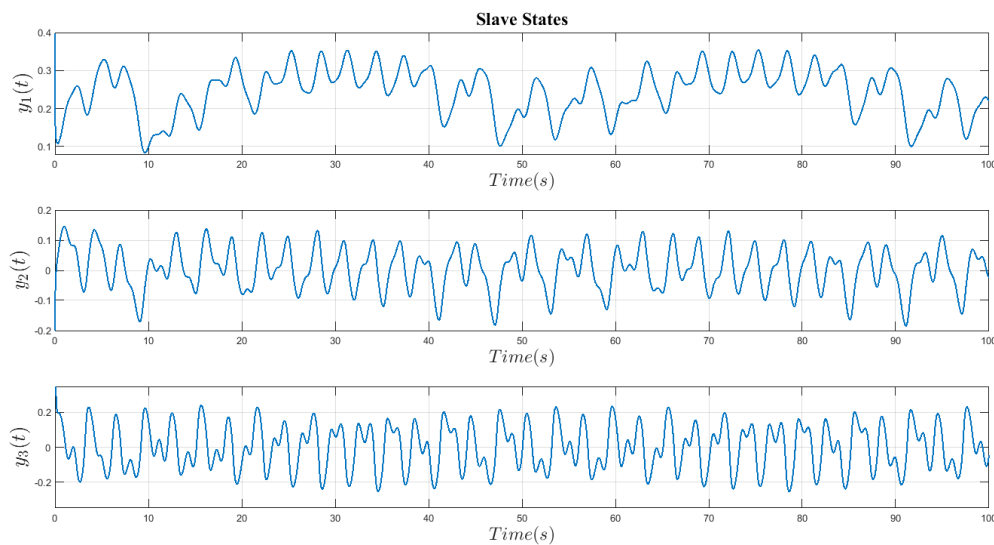


Figure 3. Chaotic behavior of the slave Gensou-Tsei system.

Figure 4 depicts the phase diagram of the fractional-order Gensou-Tsei system, and Figure 5 depicts the behavior of the master and slave system states separately and without controller actions. The behavior of both the master and slave systems is utterly chaotic, as demonstrated in the figures above.

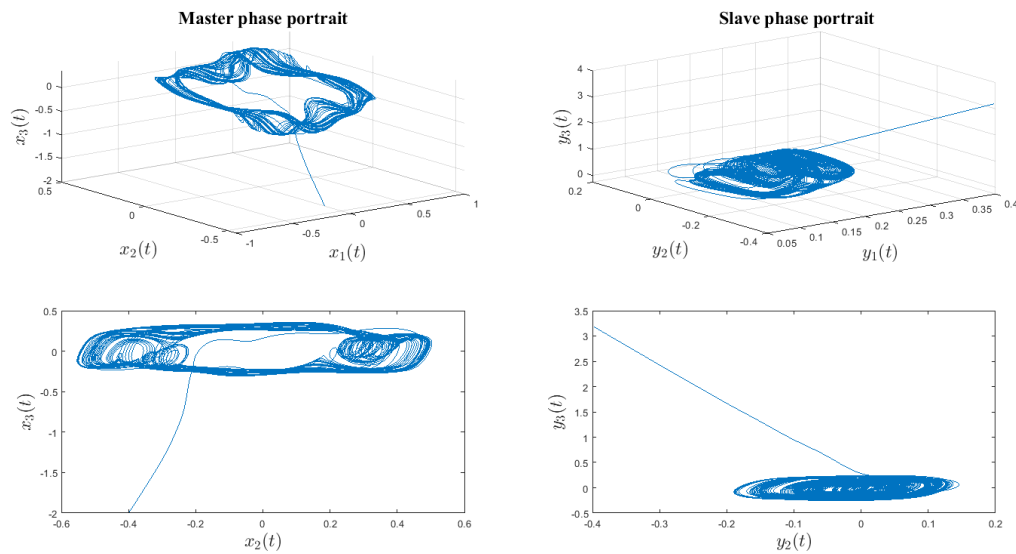


Figure 4. The chaotic behavior of fractional order master and slave Gensou-Tsei in the absence of controller operations.

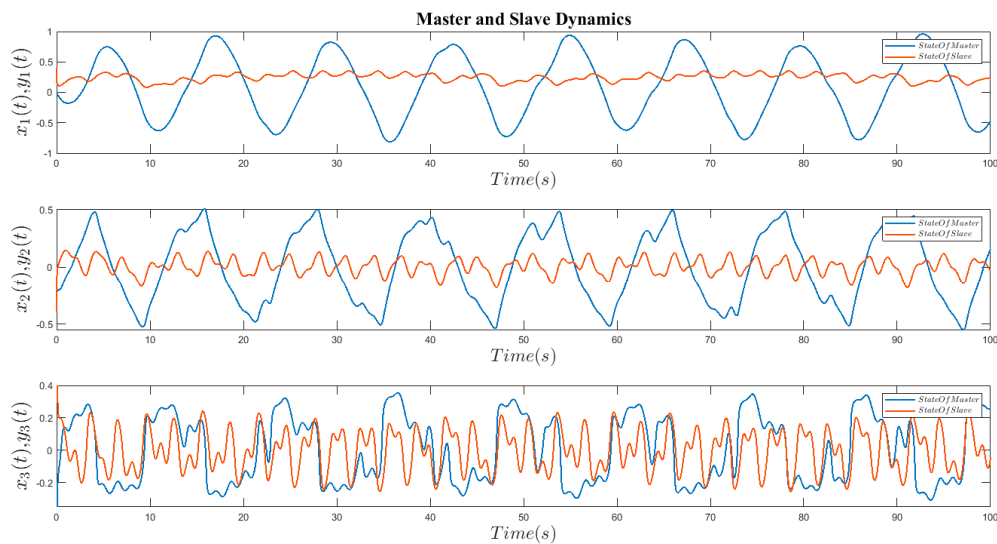


Figure 5. The behavior of the master and slave Gensou-Tsei system modes in the absence of a control signal.

Figure 6 depicts the synchronization of the Gensou-Tsei chaotic system before and after the finite-time controller is applied. The suggested mechanism is based on adaptive sliding mode control, and its performance is such that after applying the controller, the synchronization error achieves zero at an acceptable speed, as illustrated in Figure 7.

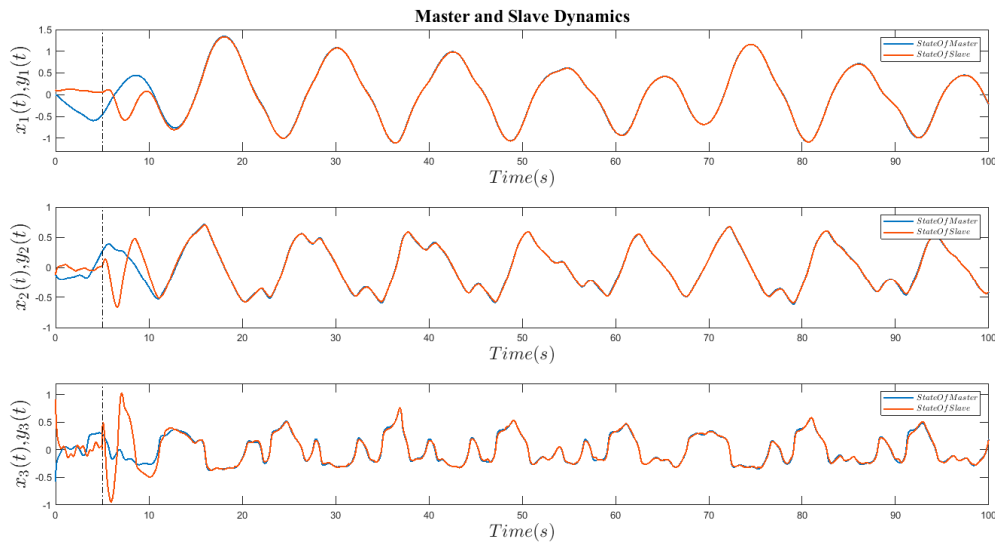


Figure 6. Synchronization of chaotic Gensou-Tsei systems using the proposed adaptive sliding mode control and applying the control signal at $t=5s$.

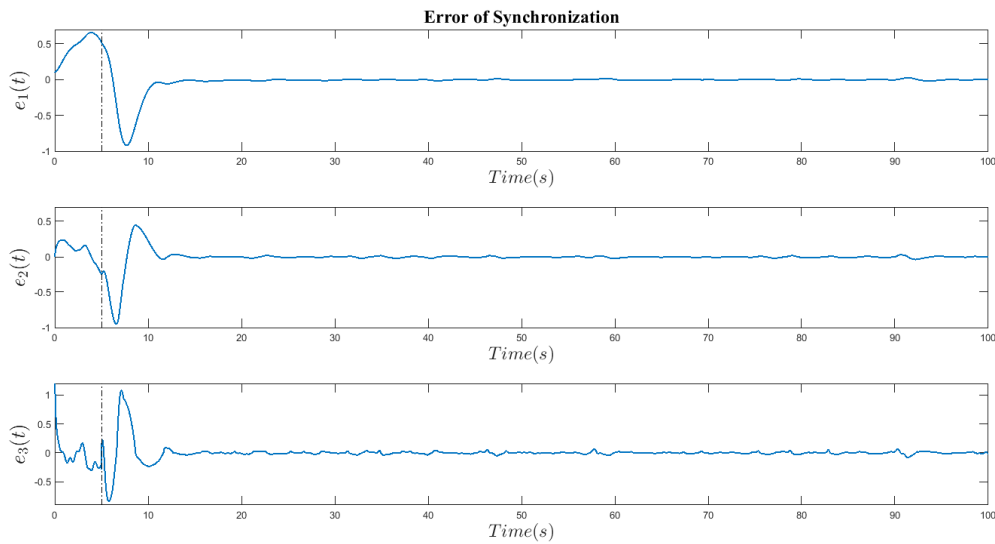


Figure 7. Synchronization error of the master and slave system using the proposed adaptive sliding mode control mechanism.

Figure 8 depicts the control signal obtained by employing the finite time scenario during the controller design process. Figure 9 depicts the estimation error of the system parameters, which has converged to zero well and rapidly, incorporating unknown uncertainties, time delays, and disturbances.

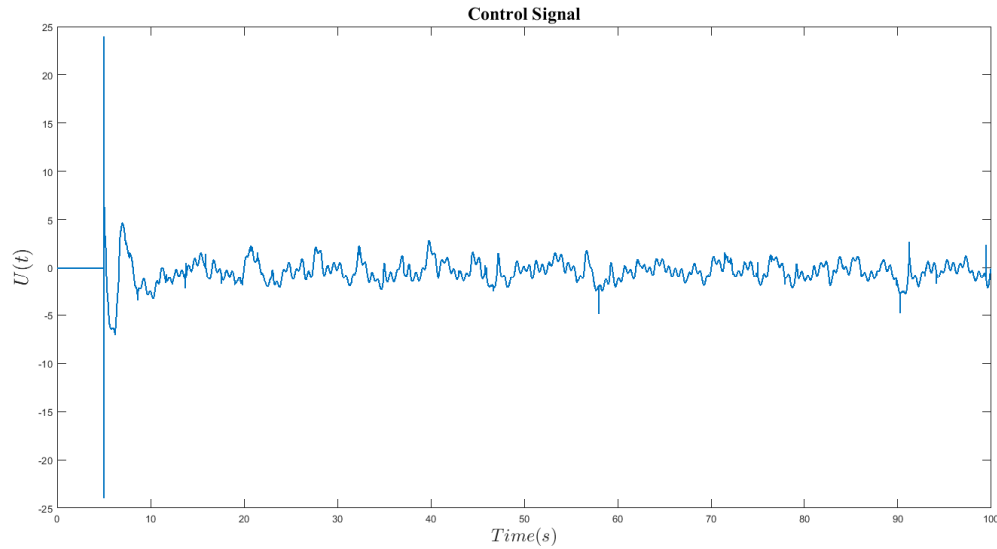


Figure 8. The control signal based on the proposed adaptive sliding mode control mechanism.

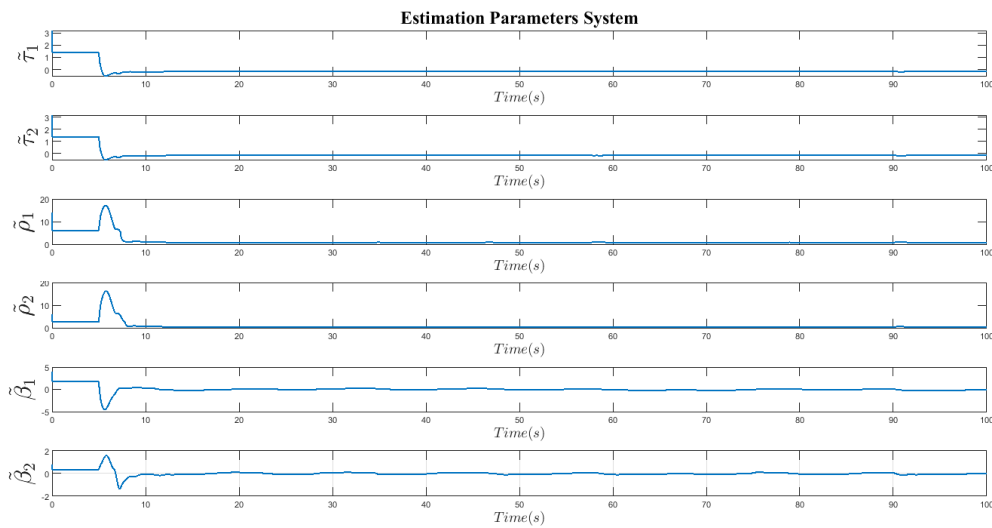


Figure 9. Estimation error of the system parameters, including unknown uncertainties, time delays, and disturbances.

The uncertainties and disturbances in the master and slave systems are depicted in Figure 10. Despite the presence of undesired signals in Figure 10 and their imposition on the above system, the design mechanism of the above controller guarantees an effective synchronization process of the master and slave systems.

To evaluate the performance of the proposed adaptive control strategy for the robust synchronization of the systems (39) and (40), the initial conditions of the master and slave systems are set to $[0, -0.1, -0.5]$ and $[0.1, -0.1, 0.8]$, respectively, with time delays of $\tau_1 = 0.45s$ and $\tau_2 = 0.1s$. At $t = 50s$, the time delay of the master system changes to $\tau_1 = 0.3s$, and the time delay of the slave system changes to $\tau_2 = 0.075s$ at $t = 60s$. In addition, parameters k_3, k_2, k_1 , and k_0 are treated similarly to the preceding case. Furthermore, the upper bound of disturbance is $\bar{\rho}_1 = \bar{\rho}_2 = 1$, the time delay is $\bar{\tau}_1 = 0.7$, $\bar{\tau}_2 = 0.5$, and the uncertainty bound of the slave system is $\bar{\beta}_1 = 2$, $\bar{\beta}_2 = 0.5$. Different simulation results are shown in (2) through (10).

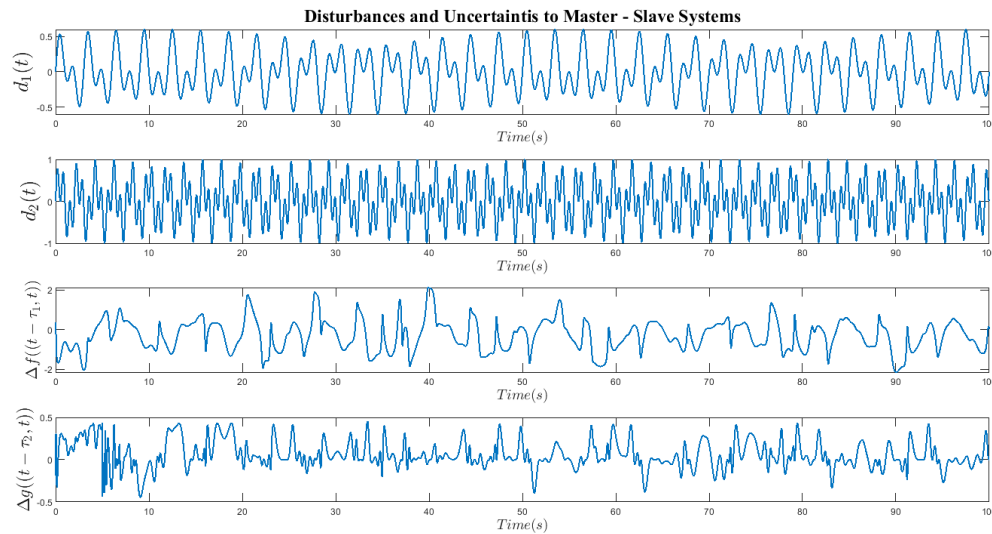


Figure 10. Representation of uncertainties and disturbances of the master and slave systems.

Based on the simulation results in Figures 2 to 10, it is clear that using the proposed adaptive control strategy to synchronize uncertain chaotic systems with unknown time delays, disturbances, and parametric uncertainties leads to convergence of all synchronization errors. And this synchronization is of acceptable robustness. The quantity of chattering in the suggested control signal is low, indicating the optimal performance of the proposed controller. Furthermore, the error in predicting the unknown parameters of the systems depicted in Figure 9 demonstrates the efficacy of the proposed control mechanism in parameter estimation utilizing the proposed updating rules using equations (37).

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