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Article

Catalytic Pyrolysis of Waste Low-Density Polyethylene (LDPE) Carry Bags to Fuels: Experimental and Exergy Analyses

Krishna Prasad Rajan *, Ibrahim Mustafa, Aravinthan Gopanna and Selvin P. Thomas *

Abstract: Plastics are highly beneficial for the day-to-day activities of human beings; however, their decomposition is limited due to their strong covalent bonding. The concept of degradation of these big molecules into smaller ones or monomers was attempted by several researchers in the preceding decades with limited success. Pyrolysis is one of the ideas used to convert plastics into fuel, rather than small molecules, compared to the crowded structure of polymers. Among these plastics, low-density polyethylene (LDPE) is largely used as carry bags throughout the world, and, herein, the results of catalytic pyrolysis of the conversion of LDPE into fuel are reported. Different dosages of zinc oxide (ZnO) were used as a catalyst to do the pyrolysis at a specific temperature in a batch reactor specially designed at our laboratory. 0.6 g of ZnO was found to be the optimal dosage for a 50 g waste LDPE batch to get the maximum oil yield. The yielded oil was analyzed chemically through Fourier transform infrared spectroscopy (FTIR) and Reformulyzer M4 Hydrocarbon Group Type Analyzer. Evaluation of physical and chemical exergy along with exergetic efficiency of the process was done.

Keywords: plastic conversion; catalytic pyrolysis; low-density polyethylene (LDPE); zinc oxide (ZnO); exergy

1. Introduction

Plastics have an important role in everybody's life these days. Many of the household items that we come across in our daily life are made up of plastics. They are mainly packaging materials for foods and beverages, various types of containers, toys, decorating materials, household items, automobile components, construction materials, and, so on. Most of these items are disposable in nature, which means we discard these items after their intended use and these materials pile up as a major component in the municipal solid waste (MSW) stream. Annually 2.01 billion tons of municipal solid wastes are generated of which 33% are not managed in an environmentally safe manner [1]. Nearly 70% of MSW ends up in landfills and dump sites, 19% is recycled and 11% is used for energy recovery [2]

Responsible use of these materials will help to preserve our environment because it takes hundreds of years for the natural degradation of plastics. All the commodity plastics are recyclable and safe disposal at designated collection bins is essential. The littering of plastic packaging items, especially carry bags, creates a big menace to the environment. Around 300 million plastic bags are found in the Atlantic Ocean alone [3]. These bags are very dangerous for marine life and aquatic species, especially for those of the mammalian variety. The most common victim is the sea turtles because they eat debris and jellyfish. Even if they survive after swallowing the waste plastics, their digestion system will be affected, and eventually die a slow death because of toxicity or intestinal blockage [4]. As a result, one species will die at an abnormal rate; every other living organism in the waterway will be impacted.

Another problem with the littering of waste plastic carry bags is the effect on animals in the forest. Improper digestion of plastic waste has the potential to kill an animal in the forest every three months [5]. The plastic waste accumulates in the municipal sewage systems and leads to blockages

the drainage and in turn, can act as a breeding ground for the insects that cause infectious diseases [6].

In the Kingdom of Saudi Arabia (KSA), it was reported that 64–72 M tons of solid waste was produced annually and it is predicted to reach 125 M by 2031 [7]. The majority of this MSW is disposed of in landfills or offsites after generous recycling by the informal sector. They recycle only paper cardboard included in MSW. Two of the key performance indicators (KPIs) of Vision 2030 of KSA specifically address the need for increased recycling of MSW in the country [8].

The various strategies adopted for properly disposing of plastics in MSW are mechanical recycling, incineration, pyrolysis, gasification, and anaerobic conversion [9]. Pyrolysis is considered an economically favorable process for converting MSW into fuels with many operational and environmental benefits. The plastic components in the MSW stream have a rich combustible composition, which can be easily converted to carbonaceous fuels by the process of pyrolysis [10]. Pyrolysis is defined as a thermal process in which controlled thermal degradation of long-chain polymeric materials takes place in an inert atmosphere in the presence or absence of a suitable catalyst. The former process is known as thermal pyrolysis, whereas, the latter is known as catalytic pyrolysis. Various catalysts were employed for the pyrolysis of waste plastics such as zeolites, red mud, silica-alumina mixture, Fe₂O₃, Al₂O₃, etc [11–14]. The reduction in the overall process energy requirements and improvements in the quality of the product fuels are the major advantages of catalytic pyrolysis [15] The oil produced from pyrolysis of waste plastics can be used in combustion engines, burners, and in less to produce thermal energy due to its high calorific values [10,16–18]. As an alternative to the landfilling process, the pyrolysis process contributes to the reduction of carbon monoxide (CO) and carbon dioxide (CO2) emissions. As pyrolysis takes place in the presence of inert gases, it eliminates the formation of dioxins, which are produced at high temperatures in an oxygen atmosphere [19].

In the case of energy-intensive processes such as pyrolysis of LDPE at high temperatures, it is always necessary to develop the process that is the most energy efficient [20]. This can be achieved by performing the exergy analysis of the process at different operating conditions. In the past, only a few attempts have been made to look at the thermodynamic or exergetic efficiency of the pyrolysis processes. Chaudhary et. al. investigated the effect of pyrolysis process temperature on the exergy efficiency and concluded that the exergy of pyro-gas increased with the increase in temperature [21]. They found out that higher temperatures have a beneficial effect on pyro-gas exergy. Their calculations revealed exergy efficiency in the 59.2% - 91.1% range. They used the temperature range of 300°C – 600°C. They considered the effect of temperature only and did not consider the effect of the amount of catalyst. Wang et. al. investigated the energy and exergy efficiency of rice husk pyrolysis at the temperature range of 800 – 1000°C [22]. They estimated energy and exergy efficiencies in the range of 64.57 – 72.68% and 52.93 – 60.64% respectively. Zhang et al. analyzed the pyrolysis of plastic waste in a rotary kiln with a heat carrier [23]. They considered the heat carrier loading impact on the heat and mass transfer in the process as well as on the energy and exergy efficiencies. They calculated the exergy and energy efficiencies in the range of 60.9 - 67.3% and 59.4 - 66.0% respectively. Rajkumar and Somsundaram reported kinetics and pyrolysis of residual tyres They reported kinetics parameters at 450-500°C without the use of any catalyst [24]. They also estimated the amount of exergy and energy but did not elaborate on the process efficiency. Huang et. al., focused on estimating the chemical exergy of six types of plastic wastes [25]. They developed a model to predict the chemical exergy of multi-component plastic wastes with an error of less than 5%. The model input was the high heating value for the plastic wastes.

Overall, the research literature to improve LDPE catalytic pyrolysis is still evolving. Further work such as the use of different types of catalysts, to reduce pyrolysis temperature, and estimation of related energy efficiency is highly desirable. In the present investigation, pyrolysis of waste plastic carry bags was carried out in the presence of a zinc oxide (ZnO) catalyst to study its effect on the overall process. In addition to thermal pyrolysis, three experimental runs were made with varying amounts of ZnO catalysts that is, 0.5g, 0.6g, and 0.7g. Moreover, exergy analyses for each pyrolysis case (with or without a catalyst) were conducted to determine the thermodynamic efficiency of the

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process. Process Simulation Software ASPEN Plus v.11.0 was used to extract and simulate thermodynamic properties of pyrolysis raw material and products.

2. Experimental

Waste plastic carry bags was collected and cut into square pieces approximately 3 cm in size and washed well in water to remove any dirt and other impurities. The washed samples were dried in a hot air oven at 60°C for 24 hours before the pyrolysis experiments. The amount of waste carry bag material used for the pyrolysis process (batch size) was fixed as 50 g. A block flow diagram for the pyrolysis process starting with the collection stage is shown in Figure 1. Shredded plastic waste material was fed into a round bottom flask. Nitrogen gas was supplied to the flask at a rate of 30 ml/minute to create an inert atmosphere. The temperature chosen for the experiment was 300°C, which was supplied with the help of an electric heater (Electrothermal UK, power 170W, 230V). After melting the feed, the vapor was allowed to pass through a condenser. The condensate was collected in the oil flask. A schematic of the experimental setup is given in Figure 2.

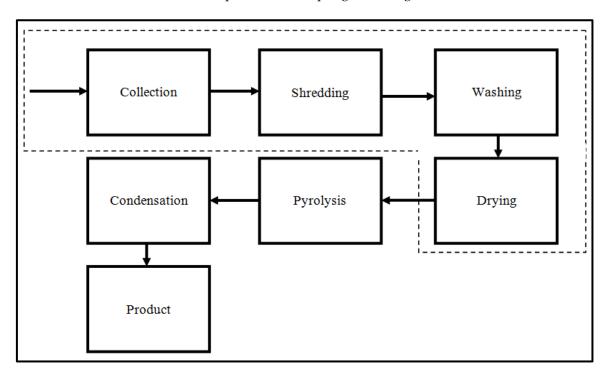


Figure 1. Block Flow Diagram of Pyrolysis Process.

The first trial of the experiment was carried out as thermal pyrolysis (without using a catalyst). ZnO (Analytical grade, Merck) was used as the catalyst for catalytic pyrolysis. The various catalyst dosages used for catalytic pyrolysis were 0.5 g, 0.6 g, and 0.7g for a batch size of 50g waste carry bags. The pyrolysis time was fixed as 2 hours for all sets of experiments.

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Figure 2. Schematic of the experimental set-up.

2.1. Characterization

A Fourier Transform Infrared spectrometer (FTIR, Nicolet iS5, Thermo Scientific, USA) was used to characterize the waste carry bags and the oil obtained after pyrolysis. 32 scans were done with a resolution of 4 cm⁻¹. The oil obtained after pyrolysis was analyzed using Reformulyzer M4 Hydrocarbon Group Type Analyser (PAC, USA). This analysis is useful to measure the n-/iso-Paraffin content and detection of possible aromatic or naphthenic components in the liquid product according to ASTM D6839.

2.2. Exergy analysis

Exergy analysis is a tool that can be used to isolate and improve process conditions that contribute to lower efficiency. In this method, together with energy and mass balances the exergy destruction or loss of work potential is determined across a system [26–28]. The higher the exergy destruction the lower is the thermodynamic efficiency of the system or process. Thus, if the system's actual exergy decrease is much higher than the thermodynamic exergy decrease then there is room for improvement.

Exergy can be evaluated by doing exergy balance on a given process which may be continuous, semi-continuous, or batch. In our case the pyrolysis of LDPE was semi-continuous. Hence the exergy balance, around the flask as a control volume, can be written as:

$$\frac{\Delta \xi}{\Delta t} = -\xi_{out} - \xi_{destroyed} \tag{1}$$

Where ξ is the exergy in Joules. The extra destruction term is because conversely to entropy the exergy is always destroyed during the process.

The term on the left-hand side indicates the change in the exergy of the system with time. In our case, the time of exergy change lasted for 30 minutes when the LDPE was put in the flask and heated for 30 minutes

It should be noted that the exergy change of the system, is due to heat transfer from the electric heater (130W) and the exergy of the LDPE. The exergy due to heat transfer is determined by the following formula:

$$\xi_{heat_transfer} = \left(1 - \frac{T_o}{T}\right)Q\tag{2}$$

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Where To is the environment temperature and T is the temperature of the heating source.

Now the first term on the right-hand side is the exergy of the pyrolysis products leaving the flask and the second term on the right-hand side is the exergy destroyed during the process.

In the pyrolysis process where nuclear, magnetic, and surface tension effects are unavailable, the exergy associated with mass ' ξ ' is usually taken as the sum of kinetic, potential, physical, mixing, and chemical exergies [29].

$$\xi = \xi^{ke} + \xi^{pe} + \xi^{ph} + \xi^{ch} + \xi^{M} \tag{3}$$

In LDPE pyrolysis the changes in kinetic, potential, and mixing exergies can also be ignored [30]. The contributions of physical and chemical exergies are important because of significant temperature and decomposition reactions effects and are discussed next.

2.2.1. Physical exergy (ξ^{ph})

The physical exergy is written as the exergy due to temperature and pressure effects and is determined as follows:

$$\xi_{TP}^{ph} = (h - h_d) - (s - s_d)T_d \tag{4}$$

Where h is the enthalpy, s is the entropy and d represents the dead state of 25°C and 1 atm.

2.2.2. Chemical exergy (ξ^{ch})

The exergy of chemical compounds according to their standard states or the most stable states available is defined as the chemical exergy. Here the stable states are referred to as species available at normal temperature and pressure in air, seawater, or lithospheric solids [31]. In a reaction, if the affinity of reactants and products are known and it is done under standard conditions the calculation of chemical exergy is easy. If the chemical exergy of a chemical species is calculated under standard conditions, it can be utilized to calculate the chemical exergy at other temperatures and pressures.

The chemical exergy of organic molecules, as is the case of LDPE pyrolysis, can be estimated by using the correlations available in the literature [32]. We used the correlation developed by Rant [33].

2.2.3. Process exergetic/thermodynamic efficiency

Exergetic efficiency can be defined in several ways. It is dependent on raw materials, fuel, and product exergies as envisaged in the current work [34]. The fuel exergy is important and it is the measure of product exergy. It includes heat transfer thereby helping to increase the temperature of the system studied. On the other hand, product exergy comprises exergies associated with all the streams leaving the system such as gas, oil, wax, and carbon residue. Thus we write exergy efficiency or second law efficiency as follows [35]:

$$\lambda_{II} = \frac{Exergy \ Recovered}{Exergy \ Expended} = \frac{Exergy \ of \ Products}{Exergy \ (Raw \ Material + Heat)} = 1 - \frac{Exergy \ Destroyed}{Exergy \ Expended}$$

3. Results and discussion

The pyrolysis process was carried out with and without a catalyst. Initially, the thermal pyrolysis of 50g of the waste plastic yielded about 20 g of pyrolysis oil, 9.053 g of wax, and about 6.984 g of residue remained inside the round bottom flask. This shows that about 13.963 g were the losses, which was the gaseous product (not collected) of the pyrolysis. The mass balance for the process is shown in Figure 3.



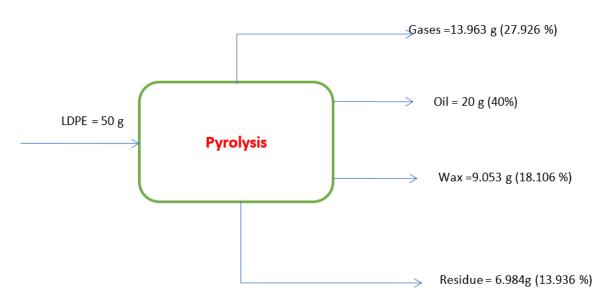


Figure 3. Mass balance for the thermal pyrolysis.

To understand the effect of ZnO as a catalyst for the pyrolysis process, experiments were carried out under similar conditions of thermal pyrolysis, with three different catalyst dosages (0.5g 0.6g, and 0.7g). The thermal process was compared with the catalytic process and the products obtained as a percentage are given in Table 1. It can be seen that the highest yield of pyrolysis oil (67.31%) was obtained with a catalyst dosage of 0.6 g with little wax formation. Similar results of little wax formation are reported by others also. Uthpalani et al used recycled LDPE and PP and converted them into oil through a batch reactor [36]. They reported that LDPE produced a small amount of wax while PP resulted in no wax formation. Another recent report also showed the elimination of wax formation while using a catalyst for the conversion of waste plastics to oil through pyrolysis [37].

Weight of Catalyst(g)	Gas (%)	Oil (%)	Wax (%)	Residue (%)
0	27.926	40	18.106	13.936
0.5	20.008	54.434	0.858	24.7
0.6	9.546	67.31	0	23.144
0.7	9.322	65	0	25 678

Table 1. Effect of catalyst on the pyrolysis product.

3.1. FTIR spectroscopy

FTIR is a powerful characteristic tool to understand the functional groups present in plastics as well as the oil produced from them. The IR spectra for the waste plastic carry bares are shown in Figure 4. The spectra show the characteristic peaks for polyethylene such as asymmetric C-H stretch of methylene groups at 2910 cm⁻¹ and symmetric stretch of methylene groups at 2850 cm⁻¹. The peak corresponding to CH₂ rocking can be seen at 710 cm⁻¹, whereas the peak at 1471 cm⁻¹ can be attributed to the bending vibrations of the methylene group in polyethylene.

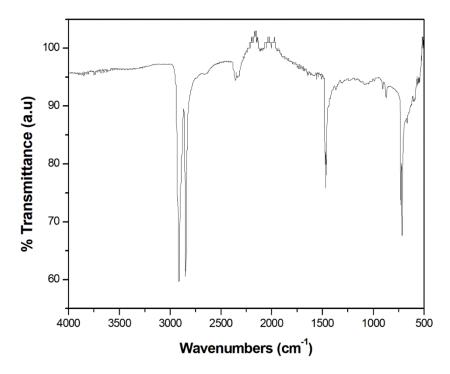


Figure 4. FTIR spectra of waste carry bags.

The IR spectra of the pyrolysis oil obtained with 0.6g of catalyst for the pyrolysis process are shown in Figure 5. The different peaks and functional groups assigned are given in Table 2. The results showed strong peaks at wavelengths around 2956, 2852, 2922, and 2954 cm⁻¹ due to C–H stretching belonging to alkanes. The bands around 1465 cm⁻¹ correspond to the C-H bending vibration of the methyl groups present in alkanes. The presence of aromatic compounds is confirmed by the presence of the absorption bands at 630 cm⁻¹, 721 cm⁻¹, and 887 cm⁻¹ which can be attributed to C-H out-of-plane bending vibrations [37]. –C-H out-of-plane bending vibration of vinyl groups or alkenes is shown at 908 cm⁻¹ [38]. From the peaks assignment, it is clear that the product obtained by the pyrolysis consists of low molecular weight alkanes most probably in the diesel and gasoline range with some alkenes and aromatic compounds.

Table 2. IR Peaks Assignment.

Wave number (cm ⁻¹)	Type of vibration	Nature of functional group				
3076	=C-H stretching	Aromatics				
2956, 2954	-C-H stretching	Alkane				
2922	-C-H stretching	Alkane				
2852	-C-H stretching	Alkane				
1641	-C=C stretching	Alkene/ fingerprint region for phenyl ring substitution overtone				
1465	-C=C stretching	Alkanes with methyl groups with C-H bending vibration				
1377	-C-H scissoring and bending	Alkane				
1236	-CH ₂ group bending	Alkane				
1088	In-plane deformation	Aromatics				
991	-C-H out-of-plane vibration	Alkane				
908	=C-H bending	Alkene				
887	-C-H out of plane bending	Alkene				
721	-C-H rock	Alkene				
630	-CH=CH2 twisting vibration	Alkene				

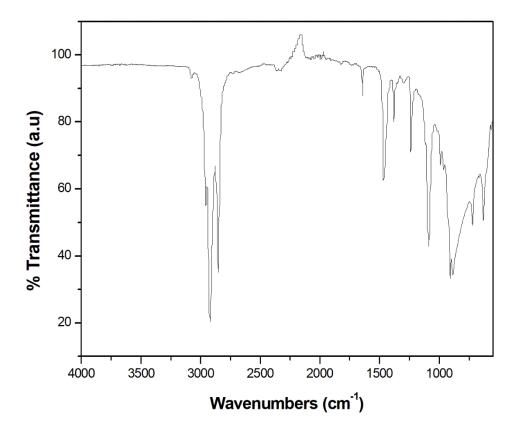


Figure 5. FTIR spectra of oil from waste carry bags with 0.6g catalyst.

3.2. Oil parameters

The key findings from hydrocarbon group type analysis (as per Test Methods ASTM D5443, ASTM D6839) are;

Calorific Value: 43150 J/kg
Carbon Ratio: 86.75 %
Hydrogen Ratio: 13.25 %
Research Octane No.: 80.41
Motor Octane No.: 66.84

The calorific value (43150 J/kg of the pyrolysis oil obtained in the present investigation is closely matching with the value reported by other research groups [39,40]. The carbon and hydrogen ratios of the oil are 86.75 and 13.25% respectively. Al-Salem et al reported recently that the pyrolysis of LDPE around 600°C yields similar results [41]. In the present investigation, the experiments were done at a relatively lower temperature. The research octane number (RON) and motor octane number (MON) of the pyrolysis oil were 80.41 and 66.84 respectively. From the FTIR studies it is concluded that the majority of the compounds obtained were of linear saturated materials. Therefore, the reported values of RON and MON are matching. Moreover, the composition summary of various hydrocarbons present in the oil is given in Table 3.

Table 3. Composition of the liquid product from pyrolysis.

Component	% (w/w)	% (v/v)		
Benzene	0.06	0.06		
Saturates	41.36	43.54		
Olefins	18.66	20.30		
Aromatics	39.98	36.16		

The analysis shows that saturates and aromatics are the major components present in the oil product obtained from pyrolysis.

3.3. Exergy analysis

We used ASPEN Plus v.11 to calculate the physical exergy of the raw material LDPE and the products LPG, OIL, Wax, and Carbon Residue. The thermodynamic method used was Peng-Robinson. In ASPEN Plus stand-alone streams cannot be processed without linking them to an equipment. To circumvent this issue we connected the streams to a splitter with 0 split fraction so that the input and one of the output streams remained the same (Figure 6).

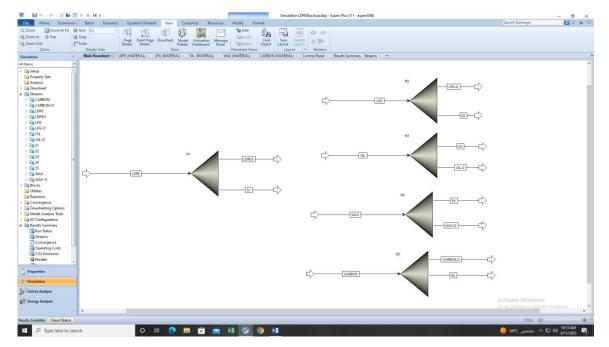


Figure 6. Aspen One Plus v.11 flowsheet simulations to extract physical exergies of components.

The calculated physical and chemical exergies for each component at different catalysts amounts are given in Table 4. As far as chemical exergy is concerned we used the correlations developed by Rant [33]. He correlated chemical exergy to the lower heating value (LHV) of the compound. It should be noted that the physical exergy and the chemical exergy values of LDPE and the electric heater remained fixed and were estimated to be 1.65 J, 2.23x10⁶, and 0.15x10⁶ J respectively. The exergy values for the catalyst have been ignored.

The product distribution concerning catalyst amount at 300°C is shown in Figure 7. As it can be seen that higher amount of catalyst ZnO favors the formation of oil and residue whereas the production of wax and gas decreases. Figure 8 shows exergy destruction as a function of catalyst weight. A slight increase in the exergy efficiency as catalyst weight is increased should be noted. It may be because, at higher catalyst amounts, products with higher exergy values are formed. Our calculations show exergy efficiency to be around 82% compared to 60% reported by Chaudhary et

al., [13] at 300°C (see Figure 9). This might be due to the different catalysts used. This indicates that ZnO is more energy efficient than MgO, ZSM-5, and activated charcoal. However, further experiments at different temperatures are needed to validate our argument.

Table 4. Exergy analysis of the conversion of LDPE to oil with varying amounts of ZnO catalyst.

	Physical exergy (kJ)				Chemical exergy (kJ)			Total exergy (kJ)				
	Catalyst loading (g)				Catalyst loading (g)			Catalyst loading (g)				
	0	0.5	0.6	0.7	0	0.5	0.6	0.7	0	0.5	0.6	0.7
gas	2.744	1.960	0.931	0.912	605.150	432.25	205.319	200.996	607.894	434.210	206.25	201.908
oil	6.098	8.309	10.260	10.016	846.300	1153.084	1423.9	1390.048	852.398	1161.0	1434.16	1400.064
wax	1.952	0.093	0	0	302.922	14.393	0	0	304.874	14.486	0	0
carbon	5.310	9.414	8.864	9.819	197.380	349.888	329.44	364.94	202.690	359.302	338.304	374.759

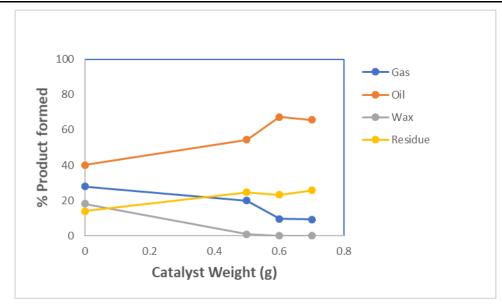


Figure 7. Production distribution as a function of catalyst weight.

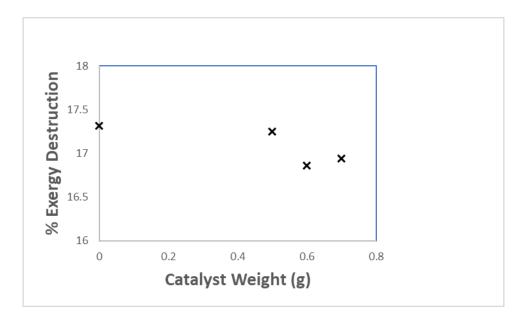


Figure 8. Exergy destruction as a function of catalyst weight.

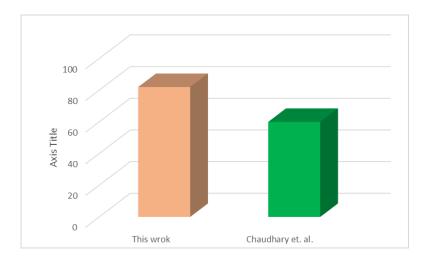


Figure 9. Exergetic efficiency of ZnO (this work) with other catalysts [13].

4. Conclusion

The described experiments and the results is a small and significant step to curb the menace of plastic solid wastes which are degrading the environment and human life worryingly and to utilize them for generating low-cost fuel for transportation and other applications. The reverse of polymerization is a challenging area of research and so far no noteworthy results were reported by the scientific community. This work adopted a catalytic pyrolysis technique with zinc oxide for the decomposition of low-density polyethylene into small fractions. The obtained products were characterized by various techniques like spectroscopy and composition analysis. The technique achieved the conversion of plastic into 67% of oil. The process has to be streamlined to limit the production of wax and gas so that the efficiency could be increased to 90% or so. The exergy analysis revealed that compared to other catalysts ZnO shows improved process efficiency. However, further experiments at different temperatures are required to validate our claim.

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Declaration of competing interest: The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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