

Case Report

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Case Report

Anaerobic Digestion Remediation in Three Full-Scale Biogas Plants through Supplements Addition

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Abstract: Additives can improve the efficiency of anaerobic digestion by increasing biogas production, reducing air pollution, and preventing total ammoniacal nitrogen (TAN) inhibition. Biological or chemical supplementation can also improve the economic efficiency of anaerobic digestion. However, the effects of specific additives on biogas production can vary depending on the type of supplement used. This research utilizes the additives on an industrial scale and monitors the optimization of the anaerobic digestion operating parameters after their addition. The various AD additives were examined in a sufficient cycle of operation for three biogas plants located in northern Greece. In this manner, the effectiveness was investigated in multiple initial feeds and unstable operating situations caused by the seasonality of specific feedstocks. The existing operation state in the three biogas plants was recorded before and after adding the supplements. In all three cases, lower concentration levels were observed in many of the examined trace elements. Introducing additives proved to be a stabilization factor in AD performance and inhibition mediator.

Keywords: additives; anaerobic digestion; digestate; trace elements; zeolites

1. Introduction

Additives can have a significant impact on the efficiency of anaerobic digestion (AD) [1–3]. The dosage and types of additives used can influence the efficiency of AD, which mainly depends on the substrate material [1]. Inhibitors such as volatile fatty acids accumulation, high levels of total ammoniacal nitrogen (TAN), sulfur, and heavy metals can slow down the AD process and reduce its efficiency. However, the use of additives can also have advantages, such as reducing greenhouse gas emissions and converting carbon dioxide energy to methane [2]. Enzyme additives have been shown to increase the efficiency of AD. Overall, using additives in AD can be an effective way to improve biogas production and increase the energetic efficiency of biogas plants [1,3]

The performance of a biogas production plant depends on the conditions prevailing inside the bioreactor during AD. Anaerobic digestion is the decomposition and stabilization of organic materials by microbial organisms under anaerobic conditions, which leads to the production of biogas (a mixture of carbon dioxide and methane, a renewable energy source) and microbial biomass [4]. Anaerobic digestion is a synergistic process that uses mainly anaerobic microbes and consists of four phases: 1) hydrolysis, 2) acidogenesis, 3) acetogenesis, and 4) methanogenesis. Figure 1 exhibits the progression and metabolic chemical compounds for each phase [5].

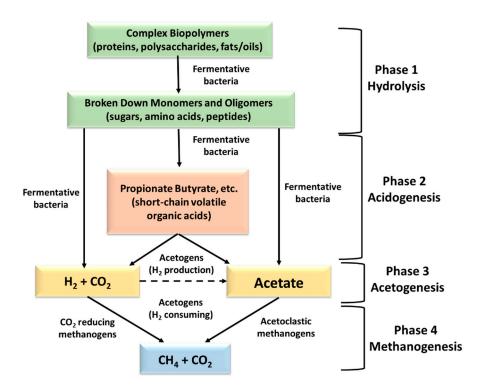


Figure 1. Schematic of four phases of biogas production [5].

Many variables can limit anaerobic digestion, including unstable feed, temperature and pH variations, a shortage of trace elements that are required for the "community" of bacteria to function, and the presence of interfering factors such as ammonia and other substances. One of the most critical parameters of anaerobic digestion is ammonia. Free ammonia creates dysfunctional blockages. Its non-polar chemical structure has the ability to easily pass through the cell membrane causing fluctuations in the chemical balance of protons and loss of potassium (K). Methanogenic microorganisms are considered to be the most sensitive to the increase in ammonia concentration. The concentration of free ammonia and ammonium are inextricably linked through chemical equilibrium. Through rising temperatures, the ratio of free ammonia to ammonium increases. The main destabilizing factors of ammonia are pH and temperature [6]. pH is a fundamental parameter that directly affects anaerobic digestion. The consistency of the pH value reveals the stability of the system and the lack of any interfering elements. Potential pH variations might be a sign of existing toxicity and a lack of buffering power. Free ammonia and ammonium are in equilibrium in aqueous solution, high pH values favor the formation of free ammonia, which is the most toxic form of ammonia for the methanogens, instead of ammonium, limiting methane production [7]. While low pH values inhibit the action of methanogenic bacteria and, by extension, methane production [8].

Determining the buffering capacity of digester contents is the most direct and reliable method for evaluating the smooth operation of the process. The total of the various volatile fatty acids produced during the acidogenesis phase is expressed through the FOS index (mg CH₃COOH/L). The total carbonate in the reactor is the TAC and consists of the fraction of carbonate derived from microbial metabolism plus carbonate derived from the reactor feed. The pH inside the reactor is controlled by the concentration of carbon dioxide in the gas phase and the concentration of carbonate ions in the liquid phase. In case of low buffering capacity (low TAC) of the digester material it is recommended to reduce the supply, add salts leading to carbonate production or directly add carbonate with the supply. Volatile fatty acid (VFA) concentrations and acetic acid equivalent are quite critical parameters for the anaerobic digestion process, as it gives an accurate picture of the prevailing situation inside the digesters. VFAs are a product of the metabolic acidogenesis stage of the anaerobic digestion process. It is necessary to check the profile of volatile fatty acids as there is a possibility of some acid accumulation. Accumulation of some acid is more often than not capable of

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causing a decrease in efficiency in the unit as supply accumulates, which cannot be degraded by the micro-organisms [9].

Products based on zeolite, trace elements, tri-valent iron, activated carbon, enzymes, buffer solutions (for pH adjustment) and bacteria cultures are additives or supplements that can improve the performance of anaerobic digestion. Zeolite has been shown to have a good adsorption effect on ammonia nitrogen in anaerobic digestion [10], and therefore has been proposed as additives to alleviate ammonia toxicity. Trace element supplements, such as iron, cobalt, nickel and selenium can improve the economic viability and conductivity of anaerobic digesters [2], especially under deficit conditions of these cations, while buffer solutions have been used to regulate the pH [11]. These additives can promote gas production and improve process stability, system recovery time from volatile fatty acids inhibition, and microbial community dynamics in anaerobic digestion [12]. Although there is extensive literature concerning the use of these supplements in laboratory scale reactors, reports about their use in full scale biogas plants are limited. In this study, the application of specialized supplements for the stabilization of the anaerobic digestion process in two cases of full-scale biogas plants operating under high ammonia concentrations and high pH, as well as a case where a deficiency of trace elements was observed.

2. Results

2.1. Operating Conditions of Biogas Plants and Additives Application

Data were collected from three different biogas plants (BG01, BG02, and BG03), in order to monitor the pre-additive state of phases. Each plant exhibited different operational issues, for which a plant-individual approach was used to provide solutions. Analyses were performed on digester material samples (digestate), and operational parameters such as pH, total ammonia nitrogen concentration, FOS/TAC, VFA profile, and trace elements concentration were verified. **Table 1** exhibits the operating conditions of the three examined biogas production plants.

Table 1. Technical specifications and operational parameters amongst the three biogas plants (BG01, BG02, and BG03).

Biogas Plant	BG01	BG02	BG03	
Electrical Power Capacity	1 MW	2 MW	1 MW	
Pre-tank	300 m ³	None	312 m³ 195 m³	
Deiler Grander	100 tn/d: cow slurry	45 tn/d: corn silage	1 tn/d: cow manure	
	20 tn/d: olive mill waste	8 tn/d: LD recirculation from storage tank	90 tn/d: cow slurry	
	20 tn/d: cheese whey	8 tn/d: glycerol	17 tn/d: chicken manure	
	15 tn/d: corn silage	21 tn/d: waste	3 tn/d: vegetable residue	
Daily Supply	First,	residues	30 tn/d: cheese whey	
	20 tn/d: chicken manure Then, 5 tn/d: chicken manure and 15tn: sheep	20 tn/d: pomace (olive, fruits)	1,5 tn/d: corn silage	
	manure			

Feeding Rate	7,3 tn/h 2,1 tn/ 30min		5,94 tn/h	
1st Digester (D1)	4000 m ³	4000 m ³	6200 m ³	
Temperature	37 °C	45 °C	40-42 °C	
HRT	30 days	50 days	60 days	
Stirring	45 min	Constantly	30 min	
2 nd Digester (D2)	4000 m ³	2.800 m ³	2300 m ³	
Temperature	40 °C	39,5 °C	54-56 °C	
HRT	HRT 60 days		20 days	
Recirculation of Digested Residue	No	Yes	No	

A customized monitoring plan was implemented to enhance each plant's performance and address any issues. The usage of the proper additive was advised for each plant, either on a daily or weekly basis. Zeolite was added in plants BG01 and BG03 to reduce total ammoniacal nitrogen levels, and an acidic buffer solution was added to adjust the pH. A trace element mixture was applied to plant BG02. The quantity and frequency of use for each plant are detailed in Table 2.

Table 2. Frequency and amount of additives supplement in plants BG01, BG02, and BG03.

Biogas Plant	Additive	Quantity	Frequency	Period
BG01	Zeolite	4 tn	500 kg/day for 6 days, and 41,6 kg/day for 24 days	
	Buffer solution	25 kg citric acid and 100 lt phosphoric acid 5% v/v	Every 5 days	60 days
BG02	Trace Elements mixture	5 kg	Weekly	60 days
BG03	Zeolite	3,5 tn	500 kg in the first day, and 103,4 kg/day for 29 days	
	Buffer Solution	25 kg citric acid and 100 lt phosphoric acid 5% v/v	Every 5 days	30 days

2.2. The Effect of Additives Zeolites and Buffer Solution in the Stabilization of the Biogas BG01 Plant

The pH and total ammoniacal nitrogen values were decreased by utilizing zeolite and the buffer solution in plants BG01 and BG03. Additionally, in the instance of plant BG03, digester D2 similarly showed a decrease in VFA accumulation. Zeolite was used as an additive in both situations, which enhanced the performance of the plant. The BG02 plant's requirements for crucial trace elements for the operation were similarly provided by the addition of trace elements. Both the number of additives and the frequency of their addition to the digesters were fundamental in combating plant malfunctions.

The BG01 biogas plant operated under unstable conditions as shown in **Figure 2**. Along with the increase in pH to 8.5, there was also a significant rise in ammonia exceeding 5000 ppm, which in combination affected the significant reduction in methane production by approximately 2000 m³ per day, just before the additives are introduced. The high value of ammonia as well as the increase in pH, since at increased pH ammonia transforms into free ammonia, which is the toxic form of ammonia for methanogenic populations, contributed to the significant reduction of methane. To address this situation, the biogas plant stopped feeding it with poultry manure, which due to its

protein composition is rich in ammonia, and at the same time, zeolite and buffer solution were introduced into the reactor as shown in **Table 2**. With the combination solution chosen, immediately within a few days, the biogas plant recovered, presenting an increase in the daily production of methane by >2500 m³, and on average >5906 m³ during the period when the additives were introduced day 11 to day 72 in relation to the production of methane before the introduction of additives. The introduction of additives combined with the discontinuation of poultry manure supplement helped to reduce the ammonia concentration in the biogas plant and to stabilize the pH resulting in the treatment of the ammonia toxicity that had occurred. The drastic reduction in ammonia is due in part to the addition of the zeolite which adsorbed some of the ammonium ions. It is noteworthy that the reactor maintained steady conditions long after the additives' inclusion.

Methane Production

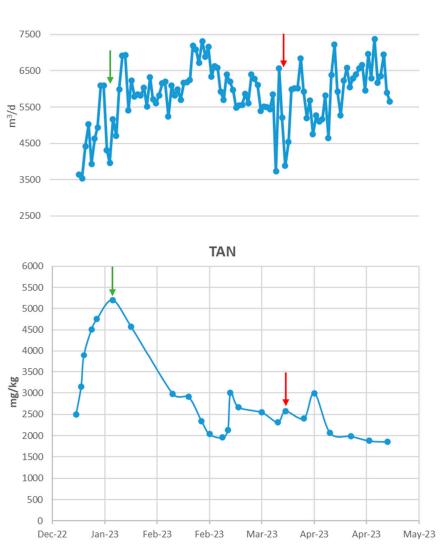


Figure 2. Variation diagrams of methane production and total ammonia nitrogen (TAN) in plant BG01 over a period of 6 months, marking the beginning (green arrow) and the end (red arrow) of the additives' application.

Figure 3 shows the VFAs of the plant which were elevated during the toxicity period and which decreased with the introduction of the additives, which results are consistent with the increased methane production that occurred during this period. It should be noted that increased volatile fatty

acid concentrations in a reactor, especially propionic acid, are an indicator of anaerobic degradation instability.

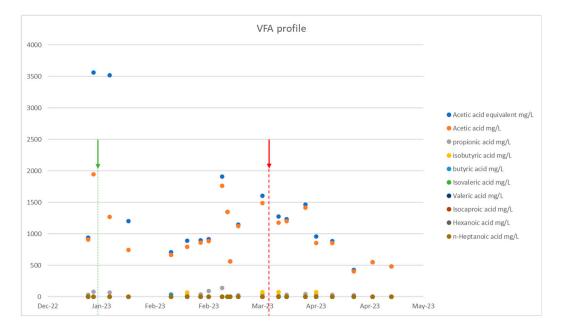


Figure 3. Variation diagram of Volatile Fatty Acids values in plant BG01 over a period of 6 months, marking the beginning (green line) and the end (red line) of the additives' application.

2.2. The Effect of Additives Zeolites and Buffer Solution in the Stabilization of the Biogas BG02 Plant

Due to nutritional deficits in the digesters, the plant had operational issues with reduced yields and unstable operation. Low quantities of copper (Cu), zinc (Zn), iron (Fe), manganese (Mn), calcium (Ca), and sodium (Na), six elements that are crucial to the process, were present in the biogas plant. In digester D1, elevated VFA values were additionally noted.

The variation diagrams of trace element values, before and after their addition to the plant's digester, are shown in Figures 4 and 5 (micro- and macro-elements). The use of the additive contributed to the increase of critical for the plant trace elements (Cu, Zn, Fe, Mn, Ca, and Na), which are responsible for combating the toxicity that may occur in the plant and expanding to ensure its steady operating state.

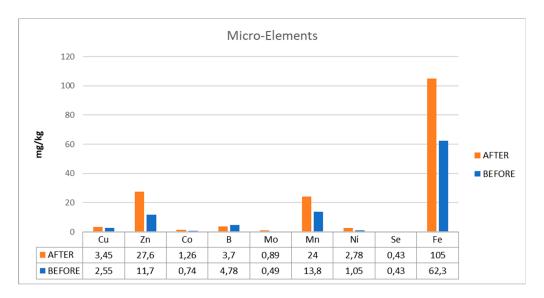


Figure 4. Micro-elements profile of digester D1 of plant BG02 over a period of 2 months.

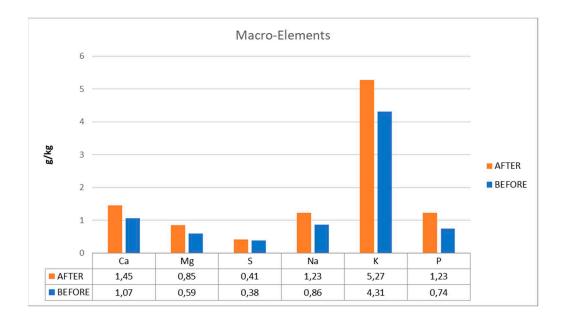


Figure 5. Macro-elements profile of digester D1 of plant BG02 over a period of 2 months.

2.3. The Effect of Additives Zeolites and Buffer Solution in the Stabilization of the Biogas BG03 Plant

It was considered reasonable to test the same recipe as the prior plant, in which the introduction showed positive results, in a plant that ran with reduced methane output, at relatively high ammonia concentrations, and at a high pH. While the reactor initially produced more methane after the addition of the supplements (during the first days after the addition of the supplements, Figure 6), this improvement was not maintained after the addition of the zeolite and the buffer solution. As shown in Figure 7, the FOS-TAC remained unaffected by the addition of the supplements, and while the increased production of methane during the initial period was seen, this was not maintained, meaning that this reactor was not operating under ammonia toxicity conditions, but another was the reason for the reduced methane production during the initial period (probably the phenols as high amounts of olive mill waste were employed, and therefore this mixture of additives was not able to address the real cause of the problem and therefore the increase in methane production was not maintained and the following days.

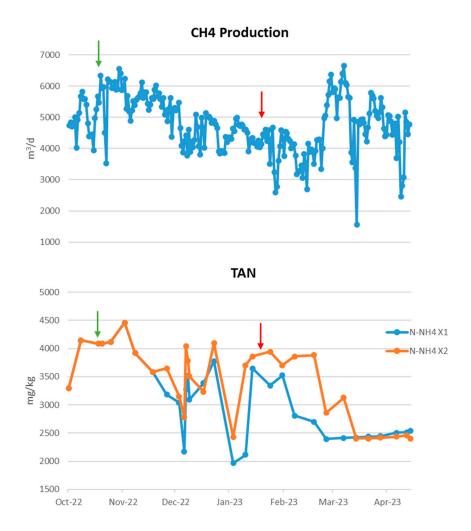
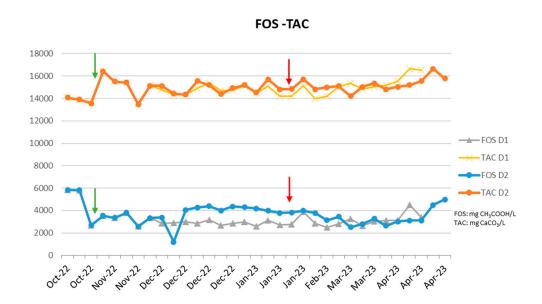


Figure 6. Variation diagrams of methane production and total ammonia nitrogen (TAN) in plant BG03 over a period of 7 months, marking the beginning (green line) and the end (red line) of the additives' application.



These two cases showed that the use of zeolite that adsorbs ammonia and buffers to stabilize the pH contributed to the immediate treatment of ammonia toxicity. Before the use of additives, the problem of the instability of anaerobic degradation should be correctly diagnosed. It's important that the problem to be addressed should first be correctly diagnosed and then the appropriate additives should be used, as the supplements are customized for specific problems and on the individual technical specifications of each biogas plant.

3. Discussion

The performance of a biogas production plant depends on the conditions prevailing inside the bioreactor during anaerobic digestion (AD). The use of additives contributes to the better performance and operation of bioreactors. In this research, issues encountered by three biogas plants (BG01, BG02 and BG03) have been identified and AD supplements were offered to address them. The malfunctions displayed by the plants are mainly due to their seasonal feedstock variation, the temperature prevailing inside the digesters and various operational parameters, such as the frequency of mixing the substrate material. In particular, in plant BG01, high pH and total ammoniacal nitrogen values were observed at the beginning of the recording of the plant's digester conditions. The use of the buffer solution to reduce the pH value and the addition of zeolite to maintain the values at a constant level resulted in the smooth operation of the digester. Accordingly, the combination of the two additives resulted in the reduction of total ammoniacal nitrogen recorded in the digester.

The phenomenon of high pH values also appeared in plant BG03, where the pH value in both digesters was above 8,2. Additionally, high ammoniacal nitrogen values and accumulation of volatile fatty acids were observed in digester D2. To improve the operation system of the plant's digesters, a buffer solution and zeolite were used in a quantity and frequency that corresponded to the size and needs of the digesters.

BG02 biogas plant, however, showed deficiencies in trace elements that contribute to its improper functioning. The use of trace elements in the D2 digester, which due to the recirculation of the digested substrate material also affected the microbiome of the D1 digester, helped to restore the trace element concentrations to optimal values. This had a positive impact on AD process instability, which was observed during the period of their shortage, reducing the efficiency rate of the plant.

4. Materials and Methods

Additives used for the treatment of anaerobic digestion destabilization in a biogas plant were zeolite (Quartz Sand, Industrial Minerals, Olympus SA, Thessaloniki, citric acid, phosphoric acid (food grade) and trace elements (Methodo Chemicals, Via A.M. Ampère, 19/21/33, 42017 Novellara (RE) - Italy).

4.1. Determination of Trace Elements

An Agilent 7850 ICP-MS (Agilent Technologies, Santa Clara, CA, USA) equipped with the ORS⁴ collision cell was used for the analysis of macro-elements and trace metals. Sampling was performed using an Agilent SPS 4 autosampler. The 7850 ICP-MS was configured with the standard ISIS 3 injection system. The IntelliQuant function in the ICP-MS MassHunter 5.1 software provides the capability of a full mass-spectrum scan with only two seconds additional measurement time, though the samples were quantitated by internal standard seven-point calibration. The samples were prepared for analysis according to the digestion procedure outlined in ISO 17294 Part I & II and APHA 3125 [14–16].

The sample is decomposed in acid at a high digestion vessel pressure with the help of a Milestone Ethos Up microwave oven and the resulting solution is analyzed. First, an amount of sample (0.5-1.0 g) was weighed and HNO3 and H2O2 were added to the sample followed by digestion

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4.2. Determination of Moisture

For moisture determination, an amount of sample (1 g) was weighed in a pre-weighed crucible and placed in an oven at 105 °C for 18 hours. The sample was then re-moved from the oven and placed in a desiccator until it returned to ambient temperature and reweighed. The moisture content as a percentage of the sample is calculated as follows:

Moisture =
$$100 - \left[\frac{(W_F - W_I)}{W_S} \times 100 \right]$$

W_I: initial container weight (dry), in grams, WS: weight of the sample amount, in grams and W_F: final weight of the container with the dry sample, in grams.

4.3. Determination of Ash

For the determination of ash, an amount of sample (2 g) was weighed in a pre-weighed crucible and placed in a furnace at 550 °C for 3 hours. The sample was then removed from the furnace and placed in a desiccator until it returned to ambient temperature and reweighed. The crude ash content as a percentage of the sample is calculated as follows:

Crude Ash
$$= \frac{(W_F - W_A)}{W_S} \times 100$$

W_I: initial container weight (dry), in grams, WS: weight of the sample amount, in grams and W_F: final weight of the container with ash, in grams.

4.4. Determination of Total Ammoniacal Nitrogen (TAN) Concentration by Nessler Method

The determination of total ammoniacal nitrogen (TAN) concentration was held using a Vapodest (Vapodest 40s Gerhardt, S.N. 7340130001) for steam distillation of and receival of ammonia in aqueous solution, based on a modified method according to A.P.H.A. The digester sample bottle was sufficiently stirred on a magnetic stirrer. A sample weighing 5 g (with an accuracy of \pm 0.05 g) was taken and weighed in a 50 mL falcon tube and 45 mL of deionized water was added. Another identical falcon tube was prepared to balance the centrifuge. Centrifugation was applied at 6000 rpm for 20 mins.

The samples were removed from the centrifuge, and a volume of 5 mL of the supernatant was extracted from them (without shaking) and brought up to the required volume in a 250 mL volumetric flask with deionized water. The flask was then vigorously shaken and a volume of 5 mL was transferred to a 25 mL volumetric flask with deionized water. Then, 3 drops of Mineral Stabilizer were added, 3 drops of Polyvinyl Alcohol Dispersing Agent followed by agitation, and finally 1 mL of Nessler Reagent. The sample was left to rest for 15 min.

Using 10 mm optical path cells, the concentration of NH_4^+ was determined photometrically in the JASCO V-630 Spectrophotometer after 15 minutes. The range of the measurement is 0.1 mg/L to 2 mg/L. The Nitrogen (Ammoniacal) APHA 4500-NH3 B & C method was used to base the measurement (APHA, 2017).

$$C_{N-NH_4^+} = \frac{C_{NH_4^+}}{1,2871} = \frac{D_f \cdot C_{420nm}}{1,2871}$$

 $C_{N-NH_4}^+$: Concentration of ammonium nitrogen (ppm), $C_{NH_4}^+$: Concentration of ammonia (ppm), D_f : Dilution factor (sample weight corrected), and C_{420nm} : Absorbance concentration at 420nm (nm).

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4.5. Determination of FOS/TAC Ratio

The FOS/TAC ratio is an indicator for assessing fermentation processes. The TAC value is an estimation of the total inorganic carbon while the ratio corresponds to the alkalinity buffer capacity of the sample and the FOS value corresponds to the volatile fatty acids content. It is calculated empirically according to the Nordmann method. A sample of 5 mL of fermentation substrate is titrated by 0.1 N of sulfuric acid solution (H₂SO₄) up to pH 5.0 to calculate the TAC value, expressed in mg/L of calcium carbonate (CaCO₃). Then the FOS value is obtained after a second titration step between pH 5.0 and pH 4.4. It is expressed in mg/L of acetic acid (CH₃COOH) [13].

4.6. Determination of Volatile Fatty Acids (VFAs)

The Eppendorf minispin table centrifuge is used to centrifuge a 1.5 ml sample in a 2 ml Eppendorf tube for 10 minutes at 12.000 rpm. In order to have the VFAs (acetate, propionate, butyrate, iso-butyrate, valerate, and iso-valerate) in their acidic form and saturate the basic sites on the analytical column, the sample is acidified with 100 μL ortho-phosphoric acid to pH 2 prior to centrifugation. 100 μL of the injection standard and 1 mL are added to the GC vial. A flame-ionization-detector (FID)-equipped GC Shimadzu GC - 2010 Plus High-End gas chromatography system is used to inject the liquid phase. The column used was an Altmann Anaytik AS-FFAP EXT, $30m\times0.25mm\times0.25\mu m$. Helium (grade 99.999%) was used as a carrier gas at a flow rate of 1.9 mL/min. The injection volume was 1 μL with a split ratio of 1:10 and the injector temperature at 250 °C. The detector temperature was set at 250 °C. The temperature program employed was: initial oven temperature at 100 °C (hold time: 2 min), increasing at 10 °C/min to 220 °C (hold time: 0 min), then in the last step at 30 °C/min to 240 °C (hold time: 12 min). The total run time was: 27 min. The VFA concentration is determined by a linear calibration curve obtained by calibration standards and adjusted by the injection standard.

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Data Availability Statement: The data presented in this study are available upon request from the corresponding author.

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Conflicts of Interest: The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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