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[Kyle G. Scheuer](#) \* and [Ray G. DeCorby](#) \*

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Article

# All-Optical, Air-Coupled Ultrasonic Detection of Low-Pressure Gas Leaks and Observation of Jet Tones in the MHz Range

Kyle G. Scheuer <sup>1,\*</sup> and Ray G. DeCorby <sup>2,\*</sup>

<sup>1</sup> Ultracoustics Technologies Inc, Sherwood Park, AB, Canada

<sup>2</sup> ECE Department, University of Alberta, 9211-116 St. NW, Edmonton, AB, Canada, T6G 1H9

\* Correspondence: kyle@ultracoustics.ca, rdecorby@ualberta.ca

**Abstract:** We used an ultrasensitive, broadband optomechanical ultrasound sensor to study the acoustic signals produced by pressurized nitrogen escaping from a variety of small syringes. Harmonically related jet tones extending into the MHz region were observed for a certain range of flow (i.e., Reynolds number), in qualitative agreement with historical studies on gas jets emitted from pipes/orifices of much larger dimensions. For higher turbulent flow rates, we observed broadband ultrasonic emission in the ~ 0 – 5 MHz range, likely limited on the upper end by attenuation in air. These observations are made possible by the broadband, ultrasensitive response (for air-coupled ultrasound) of our optomechanical devices. Aside from their theoretical interest, our results could have practical implications for the non-contact monitoring and detection of early-stage leaks in pressured fluid systems.

**Keywords:** jet tone; leak detection; air-coupled ultrasound; optical ultrasound detection; optomechanics; buckled dome microcavity

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## 1. Introduction

Sounds produced by flowing liquids and gases [1] play a central role in a myriad of commonplace phenomena, including human speech [2], whistles produced by animals and engineered objects [3], and of course the rich sounds produced by many musical instruments (e.g., wind instruments and pipe organs [4,5]). In spite of their 'everyday' nature, the physics of flow-induced acoustics is quite complex [6] (and 'fundamentally nonlinear' [1]), such that exact theoretical treatments (even for relatively simple geometries) are not routinely possible.

Nevertheless, the general features of flow-derived sound are well understood. Typically, acoustic signals arise due to turbulent conditions which correlate with vibrations (i.e., pressure waves) of the flow medium itself [3]. If appropriate feedback is present, periodically spaced vortexes can form in the turbulent flow and give rise to stable oscillations at resonant frequencies – corresponding to generation of 'flow tones', or in more common terms, 'whistling'. For a given geometry, periodic vortex shedding and associated discrete tones typically arise for certain ranges of flow velocity [1]. A practical application of this phenomenon is the so-called vortex flow meter [7], in which the vortex shedding is induced by an engineered obstruction (i.e., a 'bluff body' [1]) placed in the flow path, and flow rates are extracted from measurement of the vortex shedding frequencies.

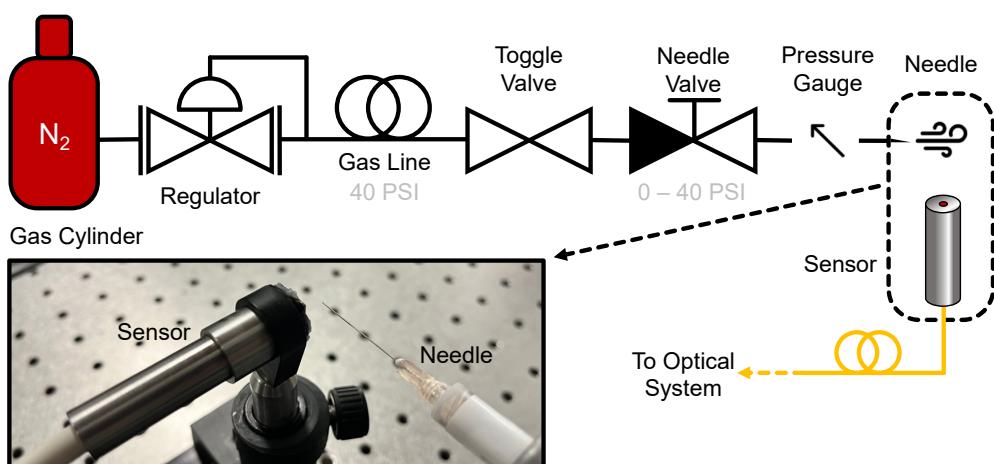
In the present work, we describe a detailed experimental study of ultrasound produced by nitrogen gas jets emitting from a variety of syringes. We furthermore show that our observations are consistent with historical studies on gas jets emitting from much larger 'pipes' [8–15] but scaled to significantly higher frequencies in the present case. The results illustrate some unique capabilities of our recently reported [16] optomechanical ultrasound sensors, in particular their ultrasensitive and omnidirectional response for air-coupled ultrasound extending over a bandwidth of several MHz. Implications for practical applications such as leak detection and metering of small-scale, high-pressure flows are discussed.

## 2. Materials and Methods

The sensor presented herein is based on a buckled dome microcavity, where two Bragg mirrors, one planar and one concave, are separated by a partially evacuated and sealed cavity. Our previous work details the buckled microcavity fabrication process in detail [16,17]. Nevertheless, we also provide an overview here. Briefly, a 3.5 period Si/SiO<sub>2</sub> Bragg stack centered at 1600 nm and terminated with Si was deposited on a quartz substrate via plasma-enhanced chemical vapor deposition (PECVD). Photolithography was performed with AZ1512 resist to pattern circular anti-features with a diameter of 100  $\mu$ m. A  $\sim$  15 nm fluorocarbon layer was then deposited, and lift-off was performed leaving behind circular fluorocarbon pads that ultimately determined the dimensions of the devices. A second, identical Bragg mirror was deposited directly on top of the fluorocarbon layer and exposed bottom mirror. The substrate was then heated on a hotplate to induce bucking at the fluorocarbon sites, resulting in the formation of half-symmetric Fabry-Perot microcavities.

Our previous work utilized a bulky optical table setup to conduct optical and ultrasonic measurements with our devices. This is not ideal for a field unit since rigid assembly is required to maintain optical alignment in extreme environmental conditions. To address these shortcomings, we designed and assembled a standalone probe unit using off-the-shelf optical components from Oz Optics and Thorlabs. A microchip containing our fabricated devices was affixed to threaded spacer, which was then attached to a pigtail style fiber focuser (Oz Optics). The fiber focuser was then connected to an optical circulator for interrogation and readout. A full description of the optical properties of our buckled dome microcavity devices is provided in previous work [16] along with a detailed description of the optical side of the experimental setup. For the set of measurements presented herein, we used  $\sim$  1 mW of optical power at  $\sim$  1505 nm to couple to the dome mode and read out to the photodetector. The photodetector was set to an 80 MHz sampling frequency with 300  $\times$  averaging.

The gas system consisted of a nominally 2500 PSI N<sub>2</sub> tank (Linde) initially regulated to 40 PSI. The regulator was connected to a toggle valve that was normally open during experiments and then to a needle valve (Swagelok) and pressure gauge (Baker Instruments), providing a pressure resolution of 0.1 PSI over the range of interest. The output of the pressure gauge was connected to the needle assembly under test. Needles of various gauges (Becton Dickenson PrecisionGlide, dimensions shown in Table 1) were attached to syringes, which were then attached directly to a section of gas line tubing. A fitting was attached to the other end of the tubing allowing each needle assembly to be easily attached and detached from the rest of the system. All measurements were performed in ambient laboratory conditions without any specialized acoustic treatment. Figure 1 shows a schematic representation of the gas handling system along with a photograph of the probe/needle measurement configuration used throughout this manuscript. A photograph showing the needle assemblies is available in the supplementary information.



**Figure 1.** Experimental schematic showing the gas handling setup. The setup served to both generate jet tones characteristic to the needle as well as to simulate a controlled gas leak at an arbitrary pressure in the range 0 ~ 40 PSI. The photograph shows the measurement configuration used throughout the manuscript, unless otherwise specified.

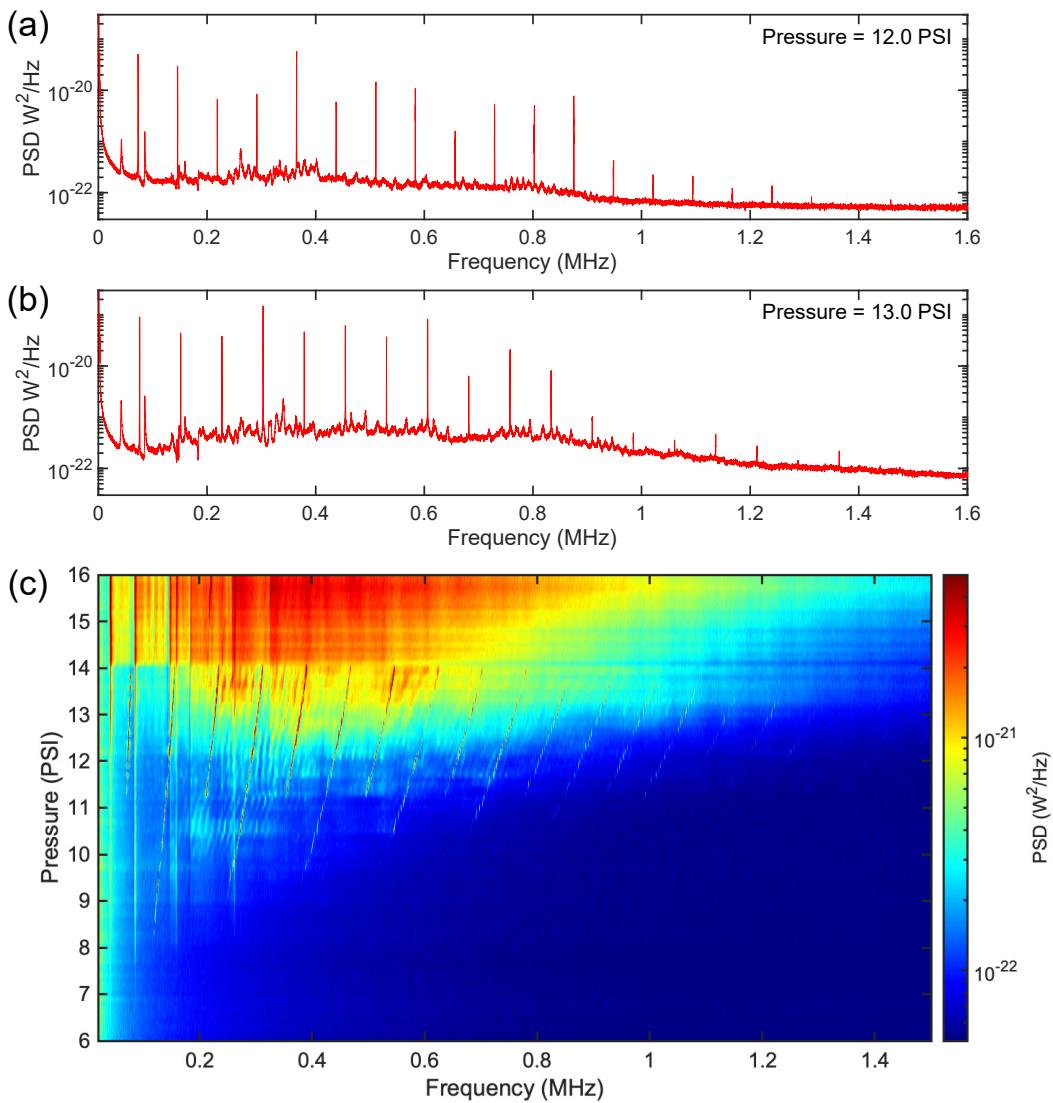
**Table 1.** Nominal dimensions of the needles used in this work.

Gauge	Inner Diameter (mm)	Outer Diameter (mm)	Length (mm)
22	0.413	0.7176	38
26	0.260	0.4636	13
30	0.159	0.3112	25

### 3. Results

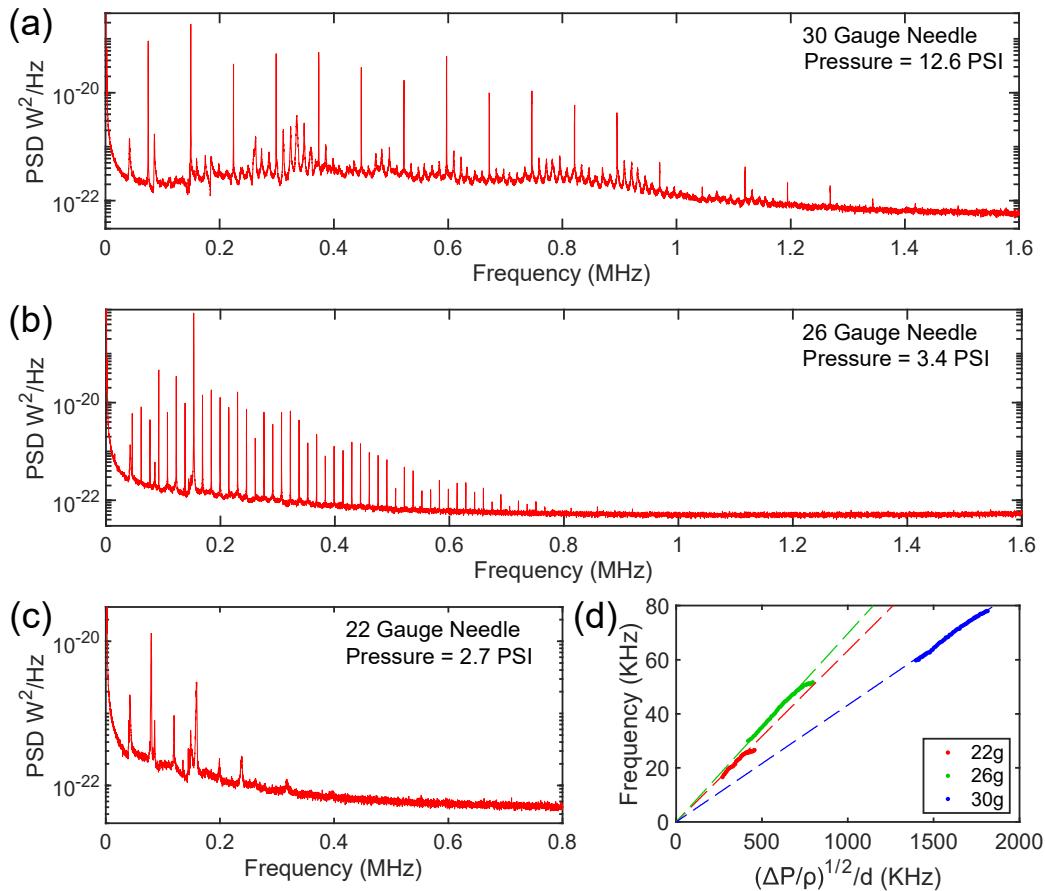
#### 3.1. Observation of jet tones in the MHz frequency range

Controllable pressures were achieved by first opening the toggle valve to allow the system to pressurize up to the supply side of the needle valve. The needle valve was subsequently adjusted while monitoring the pressure gauge, resulting in a stable leak through the needle orifice. Individual power spectral density (PSD) plots for the 30-gauge needle at different pressures are shown in Figure 2 along with a colormap that characterizes the PSD as a function of pressure. At low pressures, only low amplitude features that were invariant with pressure and characteristic to the gas handling system were observed. These features were also observed for the other needle gauges as well as without a needle assembly present, as shown in the supplementary information. At ~ 8 PSI, jet tones that were evenly spaced in frequency began to emerge. Consistent with observations from Anderson [11], the spacing of these features is not representative of the fundamental tone initially, as the fundamental is often neither the highest amplitude nor first-appearing resonance. The true fundamental frequency spacing begins to appear near 11 PSI and is on the order of 60 KHz for the 30-gauge needle. These jet tones are positively correlated to pressure and continue to increase with pressure until eventually combining with the noise floor around 14 PSI where the spectrum is dominated by white noise that extends into the MHz range. This rising noise floor can also be observed through comparing the individual PSD plots shown in Figure 2(a-b).



**Figure 2.** Generation of MHz frequency jet tones with a 30-gauge needle at various pressures. The sensor was placed 1 cm from the needle at a  $90^\circ$  angle as shown in Figure 1. (a) A power spectral density plot at 12.0 PSI. (b) A power spectral density plot at 13.0 PSI. (c) A colormap characterizing the jet tones as a function of pressure. The jet tones are present in the region  $8 \sim 14$  PSI, while other static features inherent to the gas handling system are present throughout a broader pressure range.

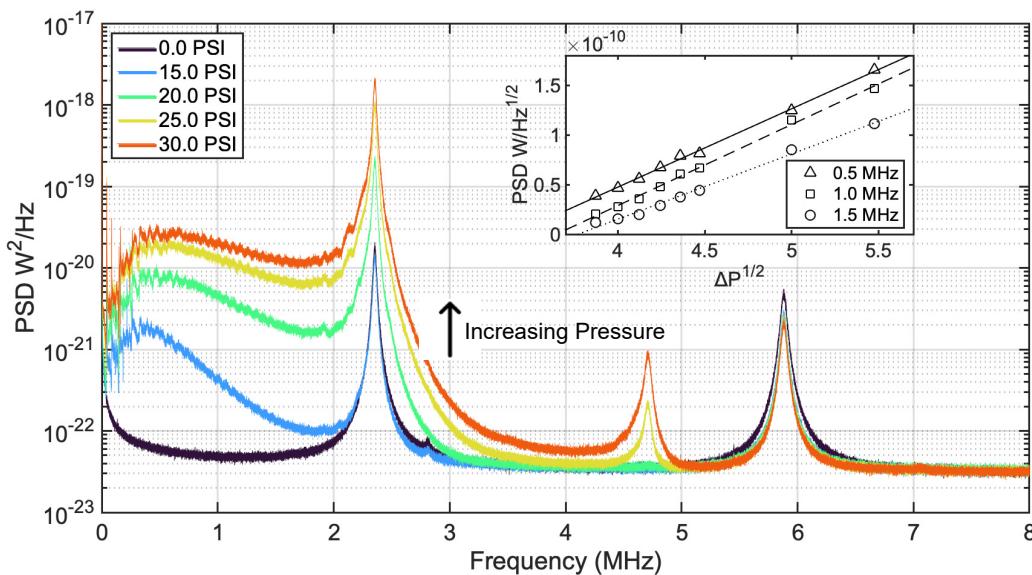
In addition to the 30-gauge needle, we performed similar experiments using both 22- and 26-gauge needles. Representative plots for each needle are shown in Figure 3, demonstrating frequency spacing that is a function of both the pressure and the dimensions of the needle. In general, the smaller the orifice diameter (i.e., higher needle gauge), the greater the spacing between jet tone harmonics and the higher they persist in frequency. As detailed in Section 4, our datasets are entirely consistent with historical observations [10,14] of acoustic signals emitted by gas jets emanating from pipe-like orifices.



**Figure 3.** Generation of jet tones with a variety of needles showing a clear dependence on the dimensions of each needle. The sensor was placed 1 cm from the needle at a  $90^\circ$  angle as shown in Figure 1. (a) A power spectral density plot for the 30-gauge needle at 12.6 PSI. (b) A power spectral density plot for the 26-gauge needle at 3.4 PSI. (c) A power spectral density plot for the 22-gauge needle at 2.7 PSI. (d) A comparison of the fundamental jet tone frequency for all needle gauges as a function of pressure differential and orifice diameter.

### 3.2. Broadband leak detection

We now turn our attention to the characterization of high pressure-differential signals where jet tones were not typically observed. Figure 4 shows the acoustic content of the 30-gauge needle in the pressure range of 15.0 – 30.0 PSI. We observed a white noise contribution at high pressures where the amplitude across the range 0 ~ 5 MHz was positively correlated with pressure. While the spectral content could be viewed as white noise in a flow rate sensing context, we note that the PSD is not entirely featureless, and could represent many densely spaced resonances. Regardless, the presence of spectral content in the MHz region, orders of magnitude above the noise floor, clearly demonstrates the potential of our sensor for industrial applications, particularly in noisy settings where analysis in lower frequencies might not be possible.



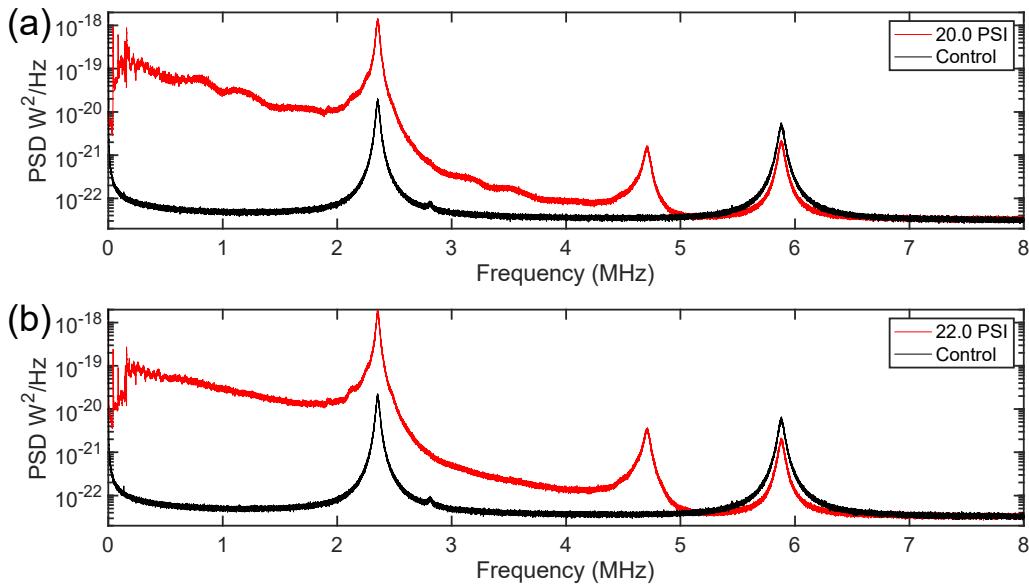
**Figure 4.** Sensing the broadband frequency content of high-pressure nitrogen jets. Each trace shows the measured PSD as the pressure of the gas line is varied. The sensor was placed 1 cm from the needle at a 90° angle as shown in Figure 1. The plot illustrates that high pressure gas jets through small orifices possess spectral content well into the MHz frequency range, and that our sensor can detect such signals.

We found that while PSD generally increased across the frequency range 0 ~ 5 MHz, higher frequencies seemed to be particularly sensitive to pressure. The inset of Figure 4 shows how the PSD evolves with pressure at three discrete frequencies (0.5 MHz, 1.0 MHz, and 1.5 MHz). The power measured at a constant location is proportional to the acoustic power emitted by the source (i.e., the gas jet) [18]. It is also the case that the power emitted by the source is proportional to the mass flow rate of the gas, which scales with the square root of pressure. These quantities can be related to the sound pressure level (*SPL*) using the expression:

$$SPL \propto 10\log(W/10^{-12}) \propto \log(\dot{m}RT/M). \quad (1)$$

Here,  $W$  is the sound power level at the source,  $\dot{m}$  is the mass flow rate of the jet,  $R$  is the gas constant,  $T$  is the temperature,  $M$  and is the molecular weight [18,19]. We plotted the measured power at three distinct frequencies against the square root of the pressure differential applied to the needle. A linear fit was applied for each frequency, revealing excellent agreement ( $R^2 > 0.99$ ), though there was increasing deviation at higher frequencies. We speculate that this could be explained by a combination of attenuation in air and the possibility that higher pressures possess higher frequency content. We also recognize that understanding jet noise associated with highly turbulent flow is complicated in its own right, and that numerous theories have been proposed [20–24].

We also observed additional non-linear contributions from our sensor at sufficiently high pressures in the form of a ghost resonance feature near 4.8 MHz in some cases. This feature was present regardless of the needle used, as shown in Figure 5. We attribute this to incoming pressure wave causing deflections that are a significant fraction of the linewidth of the optical resonance. In such cases, the relationship between pressure and optical power becomes nonlinear and harmonics of the natural vibrational modes of the dome appear in the noise spectrum (e.g., the feature at 4.8 MHz is a second-order harmonic of the dome fundamental vibrational resonance at 2.4 MHz). Figure 5 also illustrates that the broadband frequency content associated with higher pressures is not specific to the 30-gauge needle primarily studied in this work, but rather is present regardless of the orifice size used. Additionally, the dynamic range between 0 ~ 20 PSI spans several orders of magnitude in all cases.

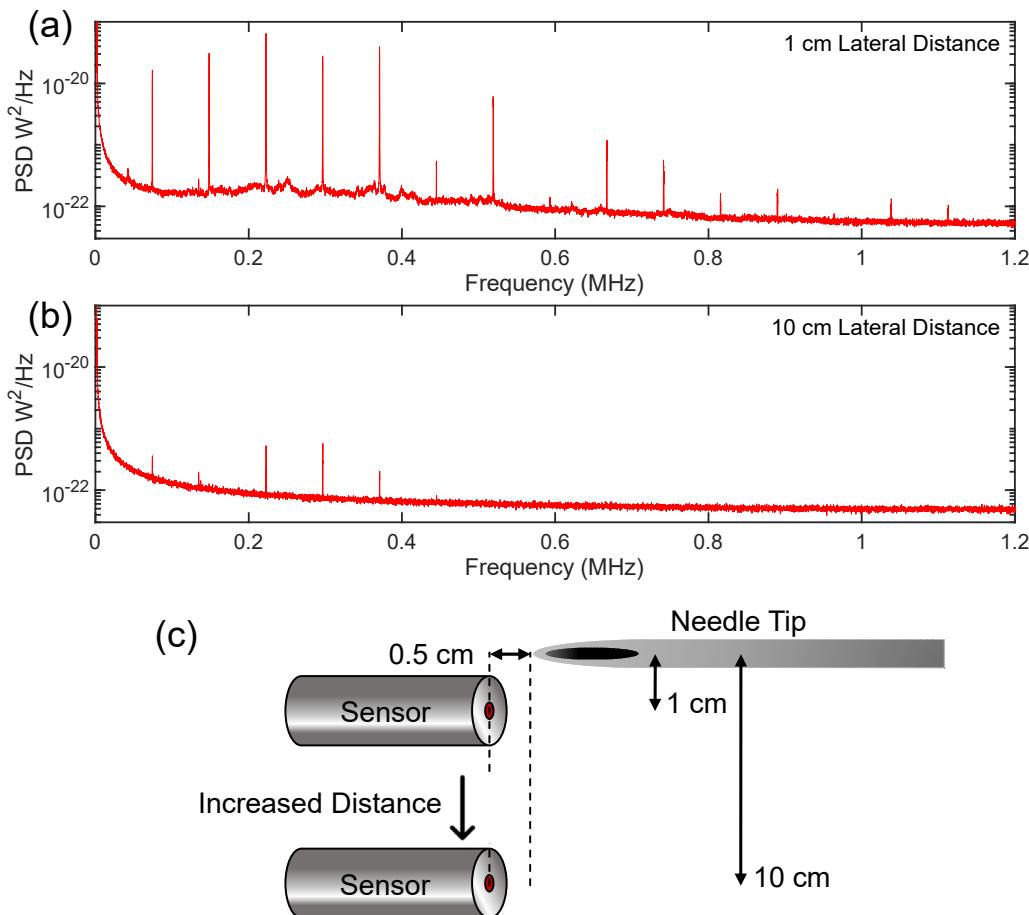


**Figure 5.** Broadband frequency content for additional needle gauges. Each was measured using the  $90^\circ$  needle-sensor configuration shown in Figure 1. A control measurement with the gas handling system depressurized is also presented for each case. (a) PSD plot for the 22-gauge needle at 20.0 PSI. (b) PSD plot for the 26-gauge needle at 22.0 PSI.

### 3.2. Omnidirectional detection

The comparatively small active area of our sensors ( $\sim 100 \mu\text{m}$ ) combined with the nature of the buckled microcavity structure provides inherent omnidirectionality [16]. To demonstrate this, we varied the lateral distance between the needle and sensor, while keeping the angle between them fixed at  $0^\circ$  as shown in Figure 6(c), as opposed to the  $90^\circ$  configuration used in previous measurements (Figure 1). The PSD plots in Figure 6(a-b) show results for two different lateral distances with the 30-gauge needle. We found even in this extreme configuration that spectral content was still visible in the  $< 500 \text{ MHz}$  region, above which air attenuation is suspected to be the limiting factor.

We also note that this distance is not representative of the ultimate device performance we project is possible. The primary performance-limiting factor for our probe was the coupling between the interrogation laser and device, and better performance is anticipated with future iterations.



**Figure 6.** Omnidirectionality demonstration using the 30-gauge needle. PSD plots are recorded as the sensor is moved laterally with respect to the needle tip. The gas system was held at a constant pressure of 12.3 PSI. (a) PSD plot at a lateral distance of 1 cm. (b) PSD plot at a lateral distance of 10 cm. (c) Schematic showing the configuration for each measurement.

#### 4. Discussion

As mentioned, our observations are consistent with the theoretical framework developed for gas jets emitting from pipe-like orifices. Here, the syringe needle itself plays the role of the pipe and a gas flow through this needle is driven by a pressure differential between the internal body of the syringe and the external lab environment. Regimes of behavior can be understood using the well-known (and dimensionless) Reynolds ( $Re$ ) and Strouhal ( $St$ ) numbers. Here,  $Re = \rho v d / \mu$  and  $St = f d / v$ , where  $\rho$  and  $\mu$  are the density and dynamic viscosity of the gas,  $v$  is flow velocity,  $d$  is a characteristic dimension (approximated by the inner diameter of the needle here), and  $f$  is the 'vortex shedding' frequency. In many flow problems,  $St$  is approximately constant over a wide range of  $Re$ , implying that the observed vortex shedding frequencies (and associated acoustic emissions) will scale as  $f \sim v/d$ . Thus, for very small values of  $d$  as studied here, one expects the acoustic noise and jet tones to extend to much higher frequencies than could be detected by conventional microphones in earlier studies [8–14], but which are well within the capabilities of our broadband ultrasound sensors.

For the pressurized syringe, high-level details of the flow properties and acoustic signals emitted can be understood as follows [9,10,12,15]:

- i. Pressurized gas flows into the needle through an orifice termed the 'vena contracta' [12], which is an effective aperture of diameter  $\delta$ , slightly smaller than the inner diameter of the needle (e.g.,  $\delta \sim 0.63d$ ). This orifice represents the primary obstruction in the flow path, and is thus the appropriate characteristic dimension to use in calculation of  $Re$  and  $St$ .
- ii. For low  $Re$ , flow in the syringe needle is laminar and negligible acoustic emissions are observed. Above some critical value of  $Re$ , however, eddies are expected to form near the

needle entrance, resulting in a vortex trail forming along the inside walls of the 'pipe' and flowing in the downstream direction [10]. Within a certain range of  $Re$ , this vortex trail is approximately periodic, resulting in the emission of harmonically related jet tones at the exit aperture of the needle. Notably, both harmonics and sub-harmonics of the vortex shedding frequency can be observed in the acoustic spectrum within this 'jet tone' regime, as observed and explained by Anderson [9].

- iii. For sufficiently high  $Re$ , the vortex formation becomes increasingly chaotic, and the flow becomes increasingly turbulent. In this regime, jet tones are subsumed into a broad background of 'white' noise, and the power spectral density of this 'turbulent noise' continues to increase as the flow (i.e.,  $Re$ ) is increased.

The results reported in Section 3 (and the SI file) are in line with these expectations. Using the relationship  $v = (2\Delta P/\rho)^{1/2}$  [5], where  $\Delta P$  is the pressure differential across the syringe 'pipe', the curves plotted in Figure 3(d) verify the expected scaling  $f \sim v/d$  discussed above. It should be noted that it is the fundamental jet tone frequency that is plotted. Since the tones observed at lower pressures spacing do not necessarily exhibit the full spectrum of harmonics [11], full colormaps for each needle were collected (and are available in the supplementary information), making it easier to identify the harmonic eigenfrequencies. However, it was somewhat difficult to extract the fundamental frequency for the 22-gauge needle due to the narrow pressure range where jet tones were observed as well as their comparatively low amplitude. We fit the data from each needle to a linear equation and found the slope to be  $\sim 0.063$  KHz/KHz,  $\sim 0.070$  KHz/KHz, and  $\sim 0.043$  KHz/KHz for the 22-gauge, 26-gauge, and 30-gauge needles, respectively ( $R^2 > 0.99$  in all cases). It is interesting, though perhaps expected, that all three needles seem to exhibit similar slopes when the dependence on pressure and orifice diameter were taken into account. We suggest that the variation in slope we observed might result from the fact that each gauge of needle has a different length, and that the characteristic dimension has some dependence on both  $d$  and  $L$  [9,11]. Moreover, the manufacturer does not specify a tolerance on any needle dimension, and we have not accounted for the needle bevel. Our data seems to suggest the absence of a jet tone in the case of a pressure differential below some threshold or for infinitely large orifice diameter (in the form of an origin crossing), which is again consistent with Anderson's observations [9]. Anderson performed a similar experiment with orifice plates affixed to a tube of length  $L$  (where  $L$  was the characteristic dimension of the system) and noted near identical slopes. Another curiosity is that the slope for each needle deviated near the upper pressure range where jet tones were observed, at least in the case of the 22- and 26-gauge needles. We attribute this to changes in the nature of vortex formation at high  $Re$  values [12].

The ability to measure fluid leaks has wide appeal within the oil and gas industry, and significant effort has been placed in developing early detection systems based on ultrasonic technology [25–29]. However, many of these systems are limited, at least in part, by their bandwidth and sensitivity. We believe that the ability to measure leaks from sub-millimeter holes at low pressures far into the MHz-frequency-range will be of particular interest for hazardous or explosive gases where electronic components cannot be placed in close proximity. In future work, we hope to target the direct measurement of gas leaks in an industrial setting.

One additional intriguing possibility suggested by our results is that a small needle emitting a controlled gas jet could represent one way of generating a tunable acoustic frequency comb especially since the pressures used here should be accessible to any space that already utilizes floating optical tables. This could represent a partial setup for photo-acoustic comb spectroscopy without requiring expensive acousto- or electro-optic modulators [30,31].

## 5. Conclusions

In summary, we have made three distinct contributions. First, a compact probe for all-optical detection of MHz-frequency-range, air-coupled ultrasound was constructed. Second, we generated MHz-range jet tones by passing pressurized nitrogen gas through a collection of small syringes and showed that previously established theory can be extended to this range. Finally, we showed that high-pressure gas leaks contain frequency content that extends far into the MHz range, lying orders

of magnitude above the noise floor of our devices. Additionally, gas leaks can be sensed both off-axis and off-position. Our buckled microcavity-based devices function as uniquely enabling leak sensors due to their sensitivity, bandwidth, and omnidirectionality.

**Supplementary Materials:** The following supporting information can be downloaded at the website of this paper posted on Preprints.org.

**Author Contributions:** Conceptualization, K.G.S. and R.G.D.; methodology, R.G.D.; validation, K.G.S. and R.G.D.; formal analysis, K.G.S. and R.G.D.; investigation, K.G.S.; resources, R.G.D.; data curation, K.G.S.; writing—original draft preparation, K.G.S. and R.G.D.; writing—review and editing, K.G.S. and R.G.D.; visualization, K.G.S.; supervision, R.G.D.; project administration, R.G.D.; funding acquisition, R.G.D. and K.G.S. All authors have read and agreed to the published version of the manuscript.

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**Conflicts of Interest:** Ultracoustics Technologies Ltd. (I,P) KGS, North Road Photonics Corp. (I,P) RGD.

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