

A duality principle and a concerning convex dual formulation suitable for non-convex variational optimization

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Abstract

This article develops a duality principle and a related convex dual formulation suitable for a large class of models in physics and engineering. The results are based on standard tools of functional analysis, calculus of variations and duality theory. In particular, we develop applications to a model in non-linear elasticity.

Key words: Convex dual variational formulation, duality principle for non-convex optimization, model in non-linear elasticity

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1 Introduction

In this article we establish a duality principle and a related convex dual formulation for a large class of models in non-convex optimization.

More specifically, the main duality principle is applied to a model in non-linear elasticity.

Such results are based on the works of J.J. Telega and W.R. Bielski [2, 3, 10, 11] and on a D.C. optimization approach developed in Toland [12].

About the other references, details on the Sobolev spaces involved are found in [1]. Related results on convex analysis and duality theory are addressed in [7, 4, 5, 6, 9]. Finally, the model in non-linear elasticity here presented may be found in [8].

Remark 1.1. *In this text we adopt the standard Einstein convention of summing up repeated indices unless otherwise indicated.*

At this point we start to describe the primal and dual variational formulations.

Let $\Omega \subset \mathbb{R}^3$ be an open, bounded, connected set with a regular (Lipschitzian) boundary denoted by $\partial\Omega$.

For the primal formulation, consider a functional $J : V \rightarrow \mathbb{R}$ where

$$J(u) = \frac{1}{2} \int_{\Omega} H_{ijkl} e_{ij}(u) e_{kl}(u) dx - \langle u_i, f_i \rangle_{L^2}. \quad (1)$$

Here $\{H_{ijkl}\}$ is a fourth order symmetric positive definite tensor and

$$\{e_{ij}(u)\} = \left\{ \frac{1}{2}(u_{i,j} + u_{j,i}) + \frac{1}{2}(u_{m,i}u_{m,j}) \right\},$$

where

$$u = (u_1, u_2, u_3) \in V = W_0^{1,4}(\Omega; \mathbb{R}^3)$$

denotes the field of displacements resulting from the action of the external forces $f = (f_1, f_2, f_3) \in L^2(\Omega; \mathbb{R}^3)$ on the elastic solid comprised by $\Omega \subset \mathbb{R}^3$.

Moreover, denoting $Y = Y^* = L^2(\Omega; \mathbb{R}^{3 \times 3})$, the stress tensor $\sigma \in Y^*$ is defined by

$$\{\sigma_{ij}(u)\} = \{H_{ijkl} e_{kl}(u)\}.$$

At this point we define the functionals $F_1 : V \times Y \rightarrow \mathbb{R}$, $F_2 : V \rightarrow \mathbb{R}$ and $G : V \rightarrow \mathbb{R}$ by

$$\begin{aligned} F_1(u, \sigma) = & - \sum_{i=1}^3 \frac{K}{2} \int_{\Omega} (u_{i,i})^2 dx \\ & + \sum_{i=1}^3 \frac{K_1}{2} \int_{\Omega} (\sigma_{ij,j} + (\sigma_{im}u_{m,j})_{,j} + f_i)^2 dx \\ & + \frac{K_2}{2} \int_{\Omega} u_{i,j}u_{i,j} dx - \langle u_i, f_i \rangle_{L^2}, \end{aligned} \quad (2)$$

for appropriate positive real constants, K, K_1, K_2 to be specified,

$$F_2(u) = \frac{K_2}{2} \int_{\Omega} u_{i,j}u_{i,j} dx,$$

and

$$G(u) = \frac{1}{2} \int_{\Omega} H_{ijkl} e_{ij}(u) e_{kl}(u) dx + \sum_{i=1}^3 \frac{K}{2} \int_{\Omega} (u_{i,i})^2 dx.$$

Here, it is worth highlighting that

$$F_1(u, \sigma) - F_2(u) + G(u) = J(u) + \sum_{i=1}^3 \frac{K_1}{2} \int_{\Omega} (\sigma_{ij,j} + (\sigma_{im}u_{m,j})_{,j} + f_i)^2 dx, \forall u \in V, \sigma \in Y^*.$$

Furthermore, we define the functionals $F_1^* : [Y^*]^3 \rightarrow \mathbb{R}$, $F_2^* : Y^* \rightarrow \mathbb{R}$ and $G^* : [Y^*]^2 \rightarrow \mathbb{R}$ by

$$F_1^*(\sigma, Q, \tilde{Q}) = \sup_{u \in V} \{-\langle u_{i,j}, \sigma_{ij} \rangle_{L^2} - \langle u_{i,j}, Q_{ij} \rangle_{L^2} + \langle u_{i,j}, \tilde{Q}_{ij} \rangle_{L^2} - F_1(u, \sigma)\},$$

$$\begin{aligned}
F_2^*(\tilde{Q}) &= \sup_{v_2 \in Y} \left\{ \langle (v_2)_{ij}, \tilde{Q}_{ij} \rangle_{L^2} - \frac{K_2}{2} \int_{\Omega} (v_2)_{ij} (v_2)_{ij} dx \right\} \\
&= \frac{1}{2K_2} \int_{\Omega} \tilde{Q}_{ij} \tilde{Q}_{ij} dx,
\end{aligned} \tag{3}$$

and

$$G^*(\sigma, Q) = \sup_{(v_1, v_2) \in Y \times Y} \{ \langle (v_1)_{ij}, \sigma_{ij} \rangle_{L^2} + \langle (v_2)_{ij}, Q_{ij} \rangle_{L^2} - \hat{G}(v_1, v_2) \},$$

where

$$\begin{aligned}
\hat{G}(v_1, v_2) &= \frac{1}{2} \int_{\Omega} H_{ijkl} \left((v_1)_{ij} + \frac{1}{2} (v_2)_{mi} (v_2)_{mj} \right) \left((v_1)_{kl} + \frac{1}{2} (v_2)_{mk} (v_2)_{ml} \right) dx \\
&\quad + \sum_{i=1}^3 \frac{K}{2} \int_{\Omega} ((v_2)_{ii})^2 dx,
\end{aligned} \tag{4}$$

so that

$$G^*(\sigma, Q) = \frac{1}{2} \int_{\Omega} (\overline{\sigma_{ij}^K}) Q_{mi} Q_{mj} dx + \frac{1}{2} \int_{\Omega} \overline{H}_{ijkl} \sigma_{ij} \sigma_{kl} dx,$$

if $\sigma \in B^*$ where

$$B^* = \{ \sigma \in Y^* : \|\sigma_{ij}\|_{\infty} \leq K/8, \forall i, j \in \{1, 2, 3\} \text{ and } \{\sigma_{ij}\} < -\varepsilon I_d \},$$

for some small parameter $\varepsilon > 0$ and where I_d denotes the 3×3 identity matrix. Observe that such a definition for B^* corresponds to the case of negative definite stress tensors, which refers to compression in a solid mechanics context.

Here

$$\begin{aligned}
\{\sigma_{ij}^K\} &= \begin{bmatrix} \sigma_{11} + K & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} + K & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} + K \end{bmatrix} \\
\overline{\sigma_{ij}^K} &= \{\sigma_{ij}^K\}^{-1},
\end{aligned} \tag{5}$$

and

$$\{\overline{H}_{ijkl}\} = \{H_{ijkl}\}^{-1}$$

in an appropriate tensor sense.

At this point we define

$$J^*(\sigma, Q, \tilde{Q}) = -F_1^*(\sigma, Q, \tilde{Q}) + F_2^*(\tilde{Q}) - G^*(\sigma, Q).$$

Specifically for

$$K_2 \gg K_1 \gg K \gg \max\{1/\varepsilon^2, 1, K_3, \|H_{ijkl}\|\},$$

we define

$$D^* = \{Q \in Y^* : \|Q_{ij}\|_{\infty} \leq K_3, \forall i, j \in \{1, 2, 3\}\}.$$

By direct computation, we may obtain

$$\left\{ \frac{\partial^2 J^*(\sigma, Q, \tilde{Q})}{\partial \sigma \partial Q} \right\} < \mathbf{0},$$

and

$$\left\{ \frac{\partial^2 J^*(\sigma, Q, \tilde{Q})}{\partial \tilde{Q}^2} \right\} > \mathbf{0},$$

on $B^* \times D^* \times Y^*$, so that J^* is concave in (σ, Q) and convex in $\tilde{Q}$ on $B^* \times D^* \times Y^*$.

2 The main duality principle and a related convex dual variational formulation

Our main duality principle is summarized by the following theorem.

Theorem 2.1. *Considering the statements and definitions of the previous section, suppose $(\hat{\sigma}, \hat{Q}, \hat{\tilde{Q}}) \in B^* \times D^* \times Y^*$ is such that*

$$\delta J^*(\hat{\sigma}, \hat{Q}, \hat{\tilde{Q}}) = \mathbf{0}.$$

Let $u_0 \in V$ be such that

$$(u_0)_{i,j} = \frac{\partial F_2^*(\tilde{Q})}{\partial \tilde{Q}_{ij}}.$$

Under such hypotheses, we have

$$\begin{aligned} J(u_0) &= \min_{u \in V} \left\{ J(u) + \sum_{i=1}^3 \frac{K_1}{2} \int_{\Omega} (\hat{\sigma}_{ij,j} + (\hat{\sigma}_{im} u_{m,j})_{,j} + f_i)^2 dx \right\} \\ &= \inf_{\tilde{Q} \in Y^*} \left\{ \sup_{(\sigma, Q) \in B^* \times D^*} J^*(\sigma, Q, \tilde{Q}) \right\} \\ &= J^*(\hat{\sigma}, \hat{Q}, \hat{\tilde{Q}}). \end{aligned} \tag{6}$$

Proof. Observe that there exists $\hat{u} \in V$ such that, defining

$$H(u, \sigma, Q, \tilde{Q}) = -\langle u_{i,j}, \sigma_{ij} \rangle_{L^2} - \langle u_{i,j}, Q_{ij} \rangle_{L^2} + \langle u_{i,j}, \tilde{Q}_{ij} \rangle_{L^2} - F_1(u, \sigma),$$

we have

$$\frac{\partial H(\hat{u}, \hat{\sigma}, \hat{Q}, \hat{\tilde{Q}})}{\partial u} = \mathbf{0}$$

and

$$F_1^*(\hat{\sigma}, \hat{Q}, \hat{\tilde{Q}}) = H(\hat{u}, \hat{\sigma}, \hat{Q}, \hat{\tilde{Q}}).$$

Moreover, from the variation in of J^* in $\tilde{Q}$, we obtain

$$-\frac{\partial F_1^*(\hat{\sigma}, \hat{Q}, \hat{\tilde{Q}})}{\partial \tilde{Q}_{ij}} + \frac{\partial F_2^*(\hat{\tilde{Q}})}{\partial \tilde{Q}_{ij}} = \mathbf{0},$$

where

$$\begin{aligned}
 & \frac{\partial F_1^*(\hat{\sigma}, \hat{Q}, \hat{\tilde{Q}})}{\partial \tilde{Q}_{ij}} \\
 &= \frac{\partial H(\hat{u}, \hat{\sigma}, \hat{Q}, \hat{\tilde{Q}})}{\partial \tilde{Q}_{ij}} \\
 & \quad + \frac{\partial H(\hat{u}, \hat{\sigma}, \hat{Q}, \hat{\tilde{Q}})}{\partial u} \frac{\partial \hat{u}}{\partial \tilde{Q}_{ij}} \\
 &= \hat{u}_{i,j}.
 \end{aligned} \tag{7}$$

From such last two equations we get

$$(u_0)_{i,j} = \frac{\partial F_2^*(\hat{\tilde{Q}})}{\partial \tilde{Q}_{ij}} = \frac{\partial F_1^*(\hat{\sigma}, \hat{Q}, \hat{\tilde{Q}})}{\partial \tilde{Q}_{ij}} = \hat{u}_{i,j},$$

so that from the concerning boundary conditions,

$$u_0 = \hat{u}.$$

On the other hand, from the variation of J^* in Q we have

$$-\frac{\partial F_1^*(\hat{\sigma}, \hat{Q}, \hat{\tilde{Q}})}{\partial Q_{ij}} - \frac{\partial G^*(\hat{\sigma}, \hat{Q})}{\partial Q_{ij}} = \mathbf{0},$$

so that

$$(u_0)_{i,j} - \overline{\hat{\sigma}_{im}^K} \hat{Q}_{mj} = 0,$$

and therefore

$$\hat{Q}_{ij} = \hat{\sigma}_{im}(u_0)_{m,j} + K\delta_{ij}(u_0)_{i,j}.$$

Finally, from the variation of J^* in σ we obtain

$$-\frac{\partial F_1^*(\hat{\sigma}, \hat{Q}, \hat{\tilde{Q}})}{\partial \sigma_{ij}} - \frac{\partial G^*(\hat{\sigma}, \hat{Q})}{\partial \sigma_{ij}} = \mathbf{0},$$

so that

$$(u_0)_{i,j} + \frac{1}{2}(u_0)_{m,i}(u_0)_{m,j} - \overline{H}_{ijkl}\hat{\sigma}_{kl} = 0.$$

Thus, since $\{H_{ijkl}\}$ is symmetric, we get

$$\hat{\sigma}_{ij} = H_{ijkl}e_{kl}(u_0).$$

From these last results and from

$$\frac{\partial H(\hat{u}, \hat{\sigma}, \hat{Q}, \hat{\tilde{Q}})}{\partial u} = \mathbf{0}$$

we obtain

$$\hat{\sigma}_{ij,j} + (\hat{\sigma}_{im}(u_0)_{m,j})_{,j} + f_i = 0, \quad \forall i \in \{1, 2, 3\},$$

so that

$$\delta J(u_0) = \mathbf{0}.$$

Finally, from such last results and the Legendre transform properties, we have

$$\begin{aligned} F_1^*(\hat{\sigma}, \hat{Q}, \hat{\tilde{Q}}) \\ = -\langle (u_0)_{i,j}, \hat{\sigma}_{ij} \rangle_{L^2} - \langle (u_0)_{i,j}, \hat{Q}_{ij} \rangle_{L^2} + \langle (u_0)_{i,j}, \hat{\tilde{Q}}_{ij} \rangle_{L^2} - F_1(u_0, \hat{\sigma}), \\ F_2^*(\hat{\tilde{Q}}) = \langle (u_0)_{i,j}, \hat{\tilde{Q}}_{ij} \rangle_{L^2} - F_2(u_0), \end{aligned} \quad (8)$$

and

$$G^*(\hat{\sigma}, \hat{Q}) = \langle (u_0)_{i,j}, \hat{\sigma}_{ij} \rangle_{L^2} + \langle (u_0)_{i,j}, \hat{Q}_{ij} \rangle_{L^2} - G(u_0).$$

From these results, we obtain

$$\begin{aligned} J^*(\hat{\sigma}, \hat{Q}, \hat{\tilde{Q}}) &= -F_1^*(\hat{\sigma}, \hat{Q}, \hat{\tilde{Q}}) + F_2^*(\hat{\tilde{Q}}) - G^*(\hat{\sigma}, \hat{Q}) \\ &= F_1(u_0, \hat{\sigma}) - F_2(u_0) + G(u_0) \\ &= J(u_0). \end{aligned} \quad (9)$$

Joining the pieces, we have got

$$\begin{aligned} J(u_0) &= \min_{u \in V} \left\{ J(u) + \sum_{i=1}^3 \frac{K_1}{2} \int_{\Omega} (\hat{\sigma}_{ij,j} + (\hat{\sigma}_{im} u_{m,j})_{,j} + f_i)^2 dx \right\} \\ &= \inf_{\tilde{Q} \in Y^*} \left\{ \sup_{(\sigma, Q) \in B^* \times D^*} J^*(\sigma, Q, \tilde{Q}) \right\} \\ &= J^*(\hat{\sigma}, \hat{Q}, \hat{\tilde{Q}}). \end{aligned} \quad (10)$$

The proof is complete. □

Remark 2.2. A similar result is valid if we would define

$$B^* = \{\sigma \in Y^* : \|\sigma_{ij}\|_{\infty} \leq K/8, \forall i, j \in \{1, 2, 3\} \text{ and } \{\sigma_{ij}\} > \varepsilon I_d\}.$$

This case refers to a positive definite tensor $\{\sigma_{ij}\}$ and the previous case to a negative definite one.

3 A closely related primal-dual variational formulation for a similar model

In this section we present a new primal-dual variational formulation for a closely related model of plates.

At this point we start to describe the primal formulation.

Let $\Omega \subset \mathbb{R}^2$ be an open, bounded, connected set which represents the middle surface of a plate of thickness h . The boundary of Ω , which is assumed to be regular (Lipschitzian), is

denoted by $\partial\Omega$. The vectorial basis related to the cartesian system $\{x_1, x_2, x_3\}$ is denoted by $(\mathbf{a}_\alpha, \mathbf{a}_3)$, where $\alpha = 1, 2$ (in general Greek indices stand for 1 or 2), and where $\mathbf{a}_3$ is the vector normal to Ω , whereas $\mathbf{a}_1$ and $\mathbf{a}_2$ are orthogonal vectors parallel to Ω . Also, $\mathbf{n}$ is the outward normal to the plate surface.

The displacements will be denoted by

$$\hat{\mathbf{u}} = \{\hat{u}_\alpha, \hat{u}_3\} = \hat{u}_\alpha \mathbf{a}_\alpha + \hat{u}_3 \mathbf{a}_3.$$

The Kirchhoff-Love relations are

$$\begin{aligned} \hat{u}_\alpha(x_1, x_2, x_3) &= u_\alpha(x_1, x_2) - x_3 w(x_1, x_2)_{,\alpha} \\ \text{and } \hat{u}_3(x_1, x_2, x_3) &= w(x_1, x_2). \end{aligned} \quad (11)$$

Here $-h/2 \leq x_3 \leq h/2$ so that we have $u = (u_\alpha, w) \in U$ where

$$\begin{aligned} U &= \{(u_\alpha, w) \in W^{1,2}(\Omega; \mathbb{R}^2) \times W^{2,2}(\Omega), \\ &\quad u_\alpha = w = \frac{\partial w}{\partial \mathbf{n}} = 0 \text{ on } \partial\Omega\} \\ &= W_0^{1,2}(\Omega; \mathbb{R}^2) \times W_0^{2,2}(\Omega). \end{aligned}$$

It is worth emphasizing that the boundary conditions here specified refer to a clamped plate.

We define the operator $\Lambda : U \rightarrow Y \times Y$, where $Y = Y^* = L^2(\Omega; \mathbb{R}^{2 \times 2})$, by

$$\begin{aligned} \Lambda(u) &= \{\gamma(u), \kappa(u)\}, \\ \gamma_{\alpha\beta}(u) &= \frac{u_{\alpha,\beta} + u_{\beta,\alpha}}{2} + \frac{w_{,\alpha} w_{,\beta}}{2}, \\ \kappa_{\alpha\beta}(u) &= -w_{,\alpha\beta}. \end{aligned}$$

The constitutive relations are given by

$$N_{\alpha\beta}(u) = H_{\alpha\beta\lambda\mu} \gamma_{\lambda\mu}(u), \quad (12)$$

$$M_{\alpha\beta}(u) = h_{\alpha\beta\lambda\mu} \kappa_{\lambda\mu}(u), \quad (13)$$

where: $\{H_{\alpha\beta\lambda\mu}\}$ and $\{h_{\alpha\beta\lambda\mu} = \frac{h^2}{12} H_{\alpha\beta\lambda\mu}\}$, are symmetric positive definite fourth order tensors. From now on, we denote $\{\bar{H}_{\alpha\beta\lambda\mu}\} = \{H_{\alpha\beta\lambda\mu}\}^{-1}$ and $\{\bar{h}_{\alpha\beta\lambda\mu}\} = \{h_{\alpha\beta\lambda\mu}\}^{-1}$.

Furthermore $\{N_{\alpha\beta}\}$ denote the membrane force tensor and $\{M_{\alpha\beta}\}$ the moment one. The plate stored energy, represented by $(G \circ \Lambda) : U \rightarrow \mathbb{R}$ is expressed by

$$(G \circ \Lambda)(u) = \frac{1}{2} \int_{\Omega} N_{\alpha\beta}(u) \gamma_{\alpha\beta}(u) \, dx + \frac{1}{2} \int_{\Omega} M_{\alpha\beta}(u) \kappa_{\alpha\beta}(u) \, dx \quad (14)$$

and the external work, represented by $F : U \rightarrow \mathbb{R}$, is given by

$$F(u) = \langle w, P \rangle_{L^2} + \langle u_\alpha, P_\alpha \rangle_{L^2}, \quad (15)$$

where $P, P_1, P_2 \in L^2(\Omega)$ are external loads in the directions $\mathbf{a}_3, \mathbf{a}_1$ and $\mathbf{a}_2$ respectively. The potential energy, denoted by $J : U \rightarrow \mathbb{R}$ is expressed by:

$$J(u) = (G \circ \Lambda)(u) - F(u)$$

More explicitly, recalling that

$$\gamma_{\alpha\beta}(u) = \frac{u_{\alpha,\beta} + u_{\beta,\alpha}}{2} + \frac{1}{2}w_{,\alpha}w_{,\beta},$$

we have

$$\begin{aligned} & J(u) \\ &= \frac{1}{2} \int_{\Omega} H_{\alpha\beta\lambda\mu} \left(\frac{u_{\alpha,\beta} + u_{\beta,\alpha}}{2} + \frac{1}{2}w_{,\alpha}w_{,\beta} \right) \left(\frac{u_{\lambda,\mu} + u_{\mu,\lambda}}{2} + \frac{1}{2}w_{,\lambda}w_{,\mu} \right) dx \\ & \quad + \frac{1}{2} \int_{\Omega} h_{\alpha\beta\lambda\mu} w_{,\alpha\beta} w_{,\lambda\mu} dx - \langle u_{\alpha}, P_{\alpha} \rangle_{L^2} - \langle w, P \rangle_{L^2} \\ &= -\langle \gamma_{\alpha\beta}(u), N_{\alpha\beta} \rangle_{L^2} + \frac{1}{2} \int_{\Omega} H_{\alpha\beta\lambda\mu} \gamma_{\alpha\beta}(u) \gamma_{\lambda\mu}(u) dx \\ & \quad + \frac{1}{2} \int_{\Omega} h_{\alpha,\beta,\lambda,\mu} w_{,\alpha\beta} w_{,\lambda\mu} dx + \left\langle \frac{u_{\alpha,\beta} + u_{\beta,\alpha}}{2} + \frac{1}{2}w_{,\alpha}w_{,\beta}, N_{\alpha\beta} \right\rangle_{L^2} \\ & \quad - \langle u_{\alpha}, P_{\alpha} \rangle_{L^2} - \langle w, P \rangle_{L^2} \\ &\geq \inf_{v \in Y} \left\{ \langle v_{\alpha\beta}, N_{\alpha\beta} \rangle_{L^2} + \frac{1}{2} \int_{\Omega} H_{\alpha\beta\lambda\mu} v_{\alpha\beta} v_{\lambda\mu} dx \right\} \\ & \quad + \inf_{\{u_{\alpha}\} \in [W_0^{1,2}(\Omega)]^2} \left\{ \frac{1}{2} \int_{\Omega} h_{\alpha\beta\lambda\mu} w_{,\alpha\beta} w_{,\lambda\mu} dx \right. \\ & \quad \left. + \left\langle \frac{u_{\alpha,\beta} + u_{\beta,\alpha}}{2} + \frac{1}{2}w_{,\alpha}w_{,\beta}, N_{\alpha\beta} \right\rangle_{L^2} - \langle u_{\alpha} P_{\alpha} \rangle_{L^2} - \langle w, P \rangle_{L^2} \right\} \\ &\geq -\frac{1}{2} \int_{\Omega} \bar{H}_{\alpha\beta\lambda\mu} N_{\alpha\beta} N_{\lambda\mu} dx \\ & \quad + \frac{1}{2} \int_{\Omega} h_{\alpha,\beta,\lambda,\mu} w_{,\alpha\beta} w_{,\lambda\mu} dx + \left\langle \frac{1}{2}w_{,\alpha}w_{,\beta}, N_{\alpha\beta} \right\rangle_{L^2} - \langle w, P \rangle_{L^2} \\ &= J_1^*(u, N), \end{aligned} \tag{16}$$

$\forall u \in U, N \in B^*$, where $B^* = B_1^* \cap B_2^*$,

$$B_1^* = \{N \in Y^* : N_{\alpha\beta,\beta} + P_{\alpha} = 0, \text{ in } \Omega\},$$

$$B_2^* = \{N \in Y^* : \|N\|_{\infty} \leq K\},$$

for an appropriate constant $K > 0$

At this point, we also define

$$V_1 = \{u \in U : \|w_{,\alpha\beta}\|_{\infty} \leq K_3, \forall \alpha, \beta \in \{1, 2\}\},$$

for an appropriate constant $K_3 > 0$

We highlight the constants $K_3 > 0$ and $K > 0$ must be such that the restrictions which define B_2^* and V_1 are not active at a concerning critical point.

Here we present the following primal-dual formulation suitable for an optimization of the original primal variational formulation

$$J_2^*(u, N) = J_1^*(u, N) + \frac{K_1}{2} \int_{\Omega} \left((h_{\alpha\beta\lambda\mu} w_{,\lambda\mu})_{,\alpha\beta} - (N_{\alpha\beta} w_{,\beta})_{,\alpha} - P \right)^2 dx.$$

More specifically,

$$\begin{aligned}
J_2^*(u, N) = & -\frac{1}{2} \int_{\Omega} \overline{H}_{\alpha\beta\lambda\mu} N_{\alpha\beta} N_{\lambda\mu} dx \\
& + \frac{1}{2} \int_{\Omega} h_{\alpha,\beta,\lambda,\mu} w_{,\alpha\beta} w_{,\lambda\mu} dx + \left\langle \frac{1}{2} w_{,\alpha} w_{,\beta}, N_{\alpha\beta} \right\rangle_{L^2} \\
& - \langle w, P \rangle_{L^2} \\
& + \frac{K_1}{2} \int_{\Omega} \left((h_{\alpha\beta\lambda\mu} w_{,\lambda\mu})_{,\alpha\beta} - (N_{\alpha\beta} w_{,\beta})_{,\alpha} - P \right)^2 dx.
\end{aligned} \tag{17}$$

We may observe that for

$$K_1 \approx \mathcal{O} \left(\frac{1}{4 \|H\| K_3^2} \right)$$

and $K_3 > 0$ sufficiently small, J_2^* is convex in u and concave in N and on $V_1 \times B^*$.

Finally, we may also define J_3 by

$$J_3(u) = \sup_{N \in B^*} J_2^*(u, N).$$

We observe that J_3 has a large region of convexity around any critical point.

4 Conclusion

In this article we have developed a convex dual variational formulation suitable for non-convex variational primal formulations.

It is worth highlighting, the results may be applied to a large class of models in physics and engineering.

We also emphasize the duality principle here presented is applied to a model in non-linear elasticity. In a future research, we intend to extend such results for other related models of plates and shells.

References

- [1] R.A. Adams and J.F. Fournier, Sobolev Spaces, 2nd edn. (Elsevier, New York, 2003).
- [2] W.R. Bielski, A. Galka, J.J. Telega, The Complementary Energy Principle and Duality for Geometrically Nonlinear Elastic Shells. I. Simple case of moderate rotations around a tangent to the middle surface. Bulletin of the Polish Academy of Sciences, Technical Sciences, Vol. 38, No. 7-9, 1988.
- [3] W.R. Bielski and J.J. Telega, A Contribution to Contact Problems for a Class of Solids and Structures, Arch. Mech., 37, 4-5, pp. 303-320, Warszawa 1985.
- [4] F.S. Botelho, Functional Analysis, Calculus of Variations and Numerical Methods in Physics and Engineering, CRC Taylor and Francis, Florida, 2020.
- [5] F.S. Botelho, *Variational Convex Analysis*, Ph.D. thesis, Virginia Tech, Blacksburg, VA -USA, (2009).

- [6] F. Botelho, *Topics on Functional Analysis, Calculus of Variations and Duality*, Academic Publications, Sofia, (2011).
- [7] F. Botelho, *Functional Analysis and Applied Optimization in Banach Spaces*, Springer Switzerland, 2014.
- [8] P.Ciarlet, *Mathematical Elasticity*, Vol. I – Three Dimensional Elasticity, North Holland Elsevier (1988).
- [9] R.T. Rockafellar, *Convex Analysis*, Princeton Univ. Press, (1970).
- [10] J.J. Telega, *On the complementary energy principle in non-linear elasticity. Part I: Von Karman plates and three dimensional solids*, C.R. Acad. Sci. Paris, Serie II, 308, 1193-1198; Part II: Linear elastic solid and non-convex boundary condition. Minimax approach, *ibid*, pp. 1313-1317 (1989)
- [11] A.Galka and J.J.Telega *Duality and the complementary energy principle for a class of geometrically non-linear structures. Part I. Five parameter shell model; Part II. Anomalous dual variational principles for compressed elastic beams*, Arch. Mech. 47 (1995) 677-698, 699-724.
- [12] J.F. Toland, A duality principle for non-convex optimisation and the calculus of variations, Arch. Rat. Mech. Anal., **71**, No. 1 (1979), 41-61.