A Study on Circular Economy Material Using Fish Scales as Natural Flame Retardant and the Properties of Its Composite Materials

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Abstract: In this study, a composite flame retardant was created by combining fish scale (FS), fishery waste, and ammonium polyphosphate (APP), a commercially available flame retardant. The composite flame retardant was added to epoxy resin (EP) to form an EP/APP/FS composite that prevents burns and is environmentally friendly. The use of FS conforms to the concept of circular economy and lowers costs by reducing the consumption of APP. Thermogravimetric analysis (TGA), integral procedural decomposition temperature (IPDT), pyrolysis kinetics, limiting oxygen index (LOI), the Underwriters Laboratories 94 (UL94) flammability test, scanning electron microscopy, Raman spectroscopy, and energy-dispersive X-ray spectroscopy were used to determine the thermal properties, flame retardant properties, flame retardant mechanism, char morphology, and composition of the composites. The TGA results indicated that the addition of 40% flame retardant raised the char residue from 16.45 wt% (pure EP) to 36.07 wt%, IPDT from 685.6 °C (pure EP) to 1143.1 °C, LOI from 21% (pure EP) to 30%, and UL94 classification from fail (pure EP) to V-0. These results suggest an increase in char residue, which indicates better protection of the polymer matrix material. The improvements in IPDT, LOI, and UL94 classification, which indicate greater thermal stability, lower flammability (from flammable to fireproof), and higher flammability rating (from fail to V-0), respectively, suggest that the composite material has favorable thermal properties and is less inflammable.

Keywords: fishery waste, epoxy, fish scale, ammonium polyphosphate, flame retardant

1. Introduction

Epoxy resin (EP) has been used in various fields, such as aeronautics, chemistry, civil engineering, automobiles, recreation, electronics, and shipbuilding. It is used as a material for circuit boards, movable parts, coatings, and numerous other applications because of its excellent insulating and chemical-resistant properties as well as its minimal cure shrinkage. However, EP has problems such as high flammability, low impact resistance, and poor weather resistance, which prevent it from having a wider range of applications [1–4].

EP is highly flammable, and when it burns, it releases a large amount of smoke and volatile gases. Thus, the presence of EP in a fire can make egress difficult and lead to serious casualties. For this reason, this study proposed introducing a composite fish scale (FS)–phosphorus flame retardant to make EP less flammable.
FS was chosen as an additive because Taiwan is an island surrounded by sea with a prosperous fishing industry but has little use for FS. Most of the FSs removed from fish are discarded, and only a small portion are used for compost, collagen extraction, and corneal cell culture. FS consists of collagen and hydroxyapatite (Ca₅(PO₄)₃). Hydroxyapatite contains phosphorus and calcium elements, which accelerate the formation of a char layer and increase char yield (CY). Collagen contains nitrogen, which releases a large amount of nonflammable gas when burnt that lowers the concentration of oxygen in the air. These properties allow FS to effectively reduce the inflammability of a material, so it is one kind of natural flame retardant [5–8].

This study developed a composite material that combines EP with a flame retardant to reduce the inflammability of EP. The flame retardant consists of a flame retardant agent, ammonium polyphosphate (APP), which contains highly incombustible phosphorus and nitrogen, and FS. The composite material was tested using thermogravimetric analysis (TGA), limiting oxygen index (LOI), the Underwriters Laboratories 94 (UL94) flammability test, scanning election microscopy (SEM), and Raman spectroscopy to determine its thermal properties, flame retardant properties, flame retardant mechanism, and morphology.

2. Experimental

2.1 Materials

DGEBA-type epoxy was kindly supplied by Nan-Ya Plastics Corporation, Taipei City, Taiwan. 4, 4’-Diaminodiphenylmethane (DDM) as a curing agent for epoxy and ammonium polyphosphate (APP) was purchased from San-Jin Chemicals Co. Kaohsiung, Taiwan. Fish scales (FS) were obtained from the local market. Anhydrous stabilized tetrahydrofuran (THF) was obtained from Lancaster Co., Morecambe, Lancashire, UK.

2.2 Preparation of Epoxy/APP/FS composites

The FSs were sieved, cleansed with fresh water, and ultrasonicated to remove foreign matter. Subsequently, they were baked at 105 °C for 4 h and shredded into powder. After the FS powder was prepared, 2.83 g of APP and 5.67 g of FS at a weight ratio of 1:2 were added to 60 mL of tetrahydrofuran and evenly mixed at 60 °C for 2.5 h. Then, 10 g of EP was evenly mixed into the APP/FS composite flame retardant, and 2.75 g of diaminodiphenylmethane (curing agent) was stirred into the mixture until it thickened, at which point the mixture was poured into a mold and left to set overnight. The next day, it was baked at 60 to 160 °C at increasing intervals of 20 °C every 2 h to complete the preparation of the EP/APP/FS composites.

2.3 Measurements

The samples were treated at 180 °C for 2 h and then ground into a fine powder. The thermal degradation of the composite was examined using a thermogravimetric analyzer (TGA) (Perkin Elmer TGA 7) from room temperature to 800 °C at a rate of 10 °C min⁻¹ under an atmosphere of nitrogen. The measurements were made on 6–10 mg samples. Mass-loss/temperature curves were plotted. The LOI is defined as the minimum fraction of O₂ in a mixture of O₂ and N₂ that will just support flaming combustion. The LOI test was performed according to the testing procedure of the ASTM D 2836 Oxygen Index Method, with a test specimen bar 7–15 cm long, 6.5±0.5 mm wide, and 3.0±0.5 mm thick. The sample bars were suspended vertically and ignited by a Bunsen burner. The flame was removed and the timer was started. The concentration of oxygen was increased if the flame on the specimen was extinguished before burning for 3 min or burning away 5 cm of the bar. The oxygen content was adjusted until the limiting concentration was determined. The vertical burning test was done inside a fume hood. Samples were held ver-
tically with tongs at one end and burned from the free end. Samples were exposed to an ignition source for 10 s then they were allowed to burn above cotton wool until both sample and cotton wool extinguished. Observable parameters were recorded to assess fire retardancy. The UL 94 test classifies the materials as V-0, V-1, and V-2 according to the time period needed before self-extinction and the occurrence of flaming dripping after removing the ignition source. V-0 is the most ambitious and desired classification. The morphology of the fractured surface of the composites was studied under a scanning electron microscope (SEM) (JEOL JSM 840A, Japan). The distributions of Si atoms in the char were obtained from SEM EDX mapping (JEOL JSM 840A, Japan). Raman spectra were recorded using a Lab Ram I confocal Raman spectrometer (Dilor, France). An He-Ne laser with a laser power of about 15 mW at the sample surface was utilized to provide an excitation wavelength of 632.8 nm. A holographic notch filter reflected the exciting line into an Olympus BX40 microscope, Tokyo, Japan.

3. Results and discussion

3.1 Thermal properties

3.1.1 TGA

TGA involves the use of a microbalancer to record a specimen's mass loss with temperature and determine the material's thermal stability. In TGA, different amounts of the APP/FS flame retardant are introduced to EP under a nitrogen environment at a heating rate of 20 °C/min to observe the mass loss of the mixture with temperature. Figure 1, Figure 2, and Table 1 present the results.

As shown in Figure 1, the temperature at 5% mass loss (T_d5) decreased considerably, from 397.1 °C (pristine EP) to 238.5 °C (EP/FS/APP 40%). Likewise, char yield rose from 16.45 wt. % (pure EP) to 36.07 wt. % (EP/FS/APP 40%). This result can be explained by the presence of phosphorus in the flame retardant, which caused the material to break down at a lower temperature. This process contributed to the formation of a char layer that insulated the inner part of the specimen from heat, thus protecting the EP and increasing the overall thermal stability of the material [9–10].

Figure 2 presents the derivative thermogravimetric (DTG) curves, which demonstrate the trends of the materials reaching their maximum thermal degradation temperatures with time and temperature. According to Figure 2, the maximum thermal degradation temperature decreased from 432.7 °C (pure EP) to 376.9 °C (EP/FS/APP 40%). This result can be explained by the presence of phosphorus in the flame retardant, which caused the material to break down at a lower temperature, contributing to the formation of a protective char layer. The maximum thermal degradation rate decreased considerably, from −24.5 wt.%/min (pristine EP) to −13.9 wt.%/min (EP/FS/APP 40%), indicating a substantial improvement in EP's thermal stability after the addition of the composite flame retardant.

Table 1 indicates that T_d5 shifted leftward, the thermal degradation rate decreased, and CY increased substantially with the increase in flame retardant. This result can be attributed to the presence of phosphorus, which induced the formation of phosphorus-containing char at a lower temperature, thereby protecting the matrix material. Hence, the composite flame retardant can effectively improve the thermal stability of polymeric composite materials.
**Figure 1** TGA curves of Epoxy and Epoxy/APP/FS composites in N₂.

**Figure 2** Derivative curves of pure Epoxy and Epoxy/APP/FS composites in N₂.
<table>
<thead>
<tr>
<th>Sample NO.</th>
<th>( ^aT_{d5}(^\circ C) )</th>
<th>( ^bT_{\text{max}}(^\circ C) )</th>
<th>( ^cR_{\text{max}}(\text{wt}%/\text{min}) )</th>
<th>IPDT((^\circ C))</th>
<th>CY(\text{wt}%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>pure epoxy</td>
<td>397.1</td>
<td>432.7</td>
<td>-24.5</td>
<td>685.6</td>
<td>16.45</td>
</tr>
<tr>
<td>EP/APP/FS 10%</td>
<td>288.7</td>
<td>392.4</td>
<td>-19.6</td>
<td>802.7</td>
<td>23.56</td>
</tr>
<tr>
<td>EP/APP/FS 20%</td>
<td>260.4</td>
<td>384.9</td>
<td>-19.3</td>
<td>866.1</td>
<td>26.44</td>
</tr>
<tr>
<td>EP/APP/FS 30%</td>
<td>258</td>
<td>378.7</td>
<td>-17.2</td>
<td>980.4</td>
<td>30.80</td>
</tr>
<tr>
<td>EP/APP/FS 40%</td>
<td>238.5</td>
<td>376.9</td>
<td>-13.9</td>
<td>1143.1</td>
<td>36.07</td>
</tr>
</tbody>
</table>

\( ^aT_{d5} \) is the temperature when the weight loss of sample reaches its 5%.

\( ^bT_{\text{max}} \) corresponds to the temperature of the maximum degradation rate.

\( ^cR_{\text{max}} \) corresponds to the maximum thermal degradation rate.

3.1. Subsection
3.1.1 IPDT [11-12]

Integral procedural decomposition temperature (IPDT) is mainly used as an indicator of the thermal stability of polymeric materials. IPDT can be obtained by integrating the area under the thermal decomposition curve and substituting it into an integration equation. A high IPDT indicates favorable thermal stability. IPDT can be affected by initial thermal decomposition temperature and CY, which are also used as indicators of thermal stability. High initial thermal decomposition temperature and CY indicate high thermal stability and heat resistance and therefore high IPDT. IPDT can be calculated by substituting \( T_i, T_f, S_1, S_2, \) and \( S_3 \) into the following equations:
Figure 3 The TGA curve of the sample

\[
\text{IPDT (°C)} = A^* \times K^* \times (T_f - T_i) + T_i
\]

\[
A^* = \frac{(S_1 + S_2)}{(S_1 + S_2 + S_3)}
\]

\[
K^* = \frac{(S_1 + S_2)}{S_1}
\]

\[
T_i = \text{the initial experimental temperature (30°C)}
\]

\[
T_f = \text{the final experimental temperature (800°C)}
\]

Table 1 presents the IPDTs of the EP/APP/FS composites. These IPDTs are 685.6 °C (pristine EP), 802.7 °C (EP/APP/FS 10%), 866.1 °C (EP/APP/FS 20%), 980.4 °C (EP/APP/FS 30%), and 1143.1 °C (EP/APP/FS 40%). The EP/APP/FS composites had IPDTs higher than that of pristine EP, confirming that the addition of the flame retardant improved the thermal stability of EP. The data in Table 1 and Figure 4 also support the TGA results.

Figure 4 The IPDT data of pure Epoxy and Epoxy /APP/FS composites.
3.1.2 Kinetics of thermal degradation using Ozawa’s method

The combustion of a polymeric material involves burning of the material with oxygen and the eventual formation of char residue and gas. However, before the polymeric material can begin to burn, an energy barrier must be overcome for the material to enter the thermal decomposition process. This energy barrier is the activation energy required for thermal decomposition. In this study, Ozawa’s method [13] was adopted to calculate the activation energy, the results of which are presented in Table 2. The R values of both pure EP and EP/APP/FS 40% exceeded 0.9, indicating excellent linearity. The activation energy of pure EP and EP/APP/FS 40% was 217 kJ/mole and 230 kJ/mole, respectively, suggesting that the addition of the flame retardant increased the activation energy required by the EP/APP/FS composites and improved their thermal stability. These results also support the TGA results.

<table>
<thead>
<tr>
<th>α</th>
<th>Epoxy (E(kJ/mole))</th>
<th>R Value</th>
<th>Epoxy/APP/FS 40% (E(kJ/mole))</th>
<th>R Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.1</td>
<td>241</td>
<td>0.935</td>
<td>93</td>
<td>0.901</td>
</tr>
<tr>
<td>0.2</td>
<td>230</td>
<td>0.966</td>
<td>202</td>
<td>0.938</td>
</tr>
<tr>
<td>0.3</td>
<td>216</td>
<td>0.984</td>
<td>242</td>
<td>0.920</td>
</tr>
<tr>
<td>0.4</td>
<td>195</td>
<td>0.992</td>
<td>228</td>
<td>0.951</td>
</tr>
<tr>
<td>0.5</td>
<td>183</td>
<td>0.998</td>
<td>202</td>
<td>0.974</td>
</tr>
<tr>
<td>0.6</td>
<td>184</td>
<td>0.999</td>
<td>186</td>
<td>0.985</td>
</tr>
<tr>
<td>0.7</td>
<td>188</td>
<td>0.999</td>
<td>200</td>
<td>0.996</td>
</tr>
<tr>
<td>0.8</td>
<td>218</td>
<td>0.999</td>
<td>419</td>
<td>0.993</td>
</tr>
<tr>
<td>0.9</td>
<td>299</td>
<td>0.990</td>
<td>304</td>
<td>0.989</td>
</tr>
</tbody>
</table>

| ΔE(av) | 217 | 230 |

3.2 Flame retardant property

3.2.2 UL-94

The UL94 flammability test involves the ignition of specimens of a specific size, whose burning durations are added to determine whether a material meets the UL94 standard and whether melt-dripping occurred (evidenced by a cotton layer beneath the specimen being ignited by drips of molten material). On the basis of the test results, the flammability is rated as V-0, V-1, V-2, or fail. [14-15]

A specimen is burnt for 10 sec, after which the heat source is removed. The time from the removal of the heat source until the burning stops is recorded (t1). Subsequently, the specimen is burnt again for 10 sec, and the time from the removal of the heat source until the burning stops is also recorded (t2).

- **V-0**: If \(t_1 + t_2 < 10\) sec and no melt-dripping occurred, it is classified as V-0 rating.
- **V-1**: If \(t_1 + t_2 < 30\) sec and no melt-dripping occurred, it is classified as V-1 rating.
V-2: If \( t_1 + t_2 < 30 \) sec and melt-dripping occurred, it is classified as V-2 rating.
Fail: If \( t_1 + t_2 > 30 \) sec, it is classified as fail rating.

As shown in Table 3, pristine EP was classified as fail, whereas the addition of the composite flame retardant resulted in EP/APP/FS 40% being classified as V-0 rating. This result indicates that adding the flame retardant can effectively make a matrix material more difficult to burn, causing by phosphorus-containing fish scales and APP promote the formation of char and prevent the polymer matrix further degrade.

### Table 3 The flame retardance of Epoxy/APP/FS composites by UL-94 and LOI values.

<table>
<thead>
<tr>
<th>Sample</th>
<th>UL-94</th>
<th>LOI</th>
<th>ΔLOI</th>
</tr>
</thead>
<tbody>
<tr>
<td>pure Epoxy</td>
<td>Fail</td>
<td>NO</td>
<td>21</td>
</tr>
<tr>
<td>EP/APP/FS 10%</td>
<td>Fail</td>
<td>NO</td>
<td>21</td>
</tr>
<tr>
<td>EP/APP/FS 20%</td>
<td>Fail</td>
<td>NO</td>
<td>23</td>
</tr>
<tr>
<td>EP/APP/FS 30%</td>
<td>V-0</td>
<td>NO</td>
<td>27</td>
</tr>
<tr>
<td>EP/APP/FS 40%</td>
<td>V-0</td>
<td>NO</td>
<td>36</td>
</tr>
</tbody>
</table>

### 3.2.2 LOI

LOI is widely used to test the flammability of the materials through various oxygen concentrations. LOI involves increasing or decreasing the oxygen content of a confined space to determine the flammability of a material. The concentration of oxygen in the atmosphere is approximately 21%. A material can be classified as flammable, self-extinguishing, or fireproof depending on the test standards. [16-17]

- Flammable: \( \text{LOI} < 21\% \)
- Self-extinguishing: \( 22\% < \text{LOI} < 25\% \)
- Fireproof: \( \text{LOI} > 26\% \)

LOI is calculated by using the following equation, where \( O_2 \) and \( N_2 \) represent the flow rates (mL/sec) of oxygen and nitrogen, respectively:

\[
\text{LOI} = \frac{O_2}{O_2 + N_2} \times 100 \%
\]

According to the results of the test, pristine EP had an LOI of 21%, marking it as a flammable polymer. After the addition of flame retardant, however, the LOI of the EP/APP/FS 40% composite reached 36%, a 15% increase, suggesting that the composite had become a fireproof material in Table 3. This result can be attributed to the presence of the phosphorus-based flame retardant, which quickly formed a char layer under high temperatures that protected the polymer matrix (EP) from further decomposition.

As shown in Table 4 and Figure 5, the amount of flame retardant was fixed at 40 wt%, and the proportions of FS and APP were changed to determine the synergy between the two components. When only one component was used in the flame retardant, the LOIs of the resultant composites were 46% (EP/APP) and 23% (EP/FS). When the ratio of FS:APP was 1:2 and 2:1, the LOIs were 47% and 36%, respectively. Figure 6 shows that when the FS:APP ratio was 1:2, the difference between the experimental and theoretical (calculated) LOI was 8.7, and when the FS:APP ratio was 2:1, the difference was 5.4. Thus, the experimental value was greater than the theoretical value in both cases, indicating that the commercial fire retardant and natural fire retardant synergize with each other. An FS:APP ratio of 2:1 was selected as the recommended ratio because of cost considerations in this study.
### Table 4 Comparison of calculated and experimental LOI data of the composites

<table>
<thead>
<tr>
<th>Sample No.</th>
<th>FS:APP</th>
<th>LOI</th>
</tr>
</thead>
<tbody>
<tr>
<td>EP/APP 40% (experimental)</td>
<td>0:3</td>
<td>46</td>
</tr>
<tr>
<td>EP/APP 40% (experimental)</td>
<td>1:2</td>
<td>47</td>
</tr>
<tr>
<td>EP/APP/FS 40% (experimental)</td>
<td>2:1</td>
<td>36</td>
</tr>
<tr>
<td>EP/FS 40% (experimental)</td>
<td>3:0</td>
<td>23</td>
</tr>
<tr>
<td>EP/APP/FS 40% (calculated)</td>
<td>1:2</td>
<td>38.3</td>
</tr>
<tr>
<td>EP/APP/FS 40% (calculated)</td>
<td>2:1</td>
<td>30.6</td>
</tr>
</tbody>
</table>

**Figure 5** Comparison of calculated and experimental LOI of the composites

3.3 Morphological properties

3.3.1 SEM

SEM involves using a beam of electrons to scan a specimen in a vacuum chamber, in which the specimen’s electrons are excited by the beam and detected by a scan coil, which generates signals that are converted into images and displayed on a screen. SEM enables the observation of a material’s morphological properties, including its surface...
structure, grain size, and other morphological phenomena that occur on the surface, such as surface nucleation. [18]

Figure 6(a) and (c) presents the surface of pure EP and EP/APP/FS 40% before burning. In Figure 6(a), the particles visible on the surface are grains of APP/FS that were added. In Figure 6(c), the presence of numerous particles and the irregular surface structure are the result of the addition of a large amount of flame retardant. Figure 6(b) presents EP/APP/FS 10% after burning. A light layer of char was observed, and the holes and pits were formed by the gas released by APP when burning. These holes and pits compromised the protection on the polymer matrix material because they allow flame to pass through and reach the base material. For this reason, the performance of this composite was deemed unsatisfactory. Figure 6(d) presents EP/APP/FS 40% after burning. A dense char layer on the surface barred the transmission of oxygen and heat, thereby raising the thermal stability of the composite.

![Figure 6 SEM micrographs of composites (a) Epoxy/APP/FS 10%(before burning)(×1K) (b) Epoxy/APP/FS 10%(after burning)(×1K) (c) Epoxy/APP/FS 40%(before burning)(×1K) (d) Epoxy/APP/FS 40%(after burning)(×1K).](image)

3.3.2 EDS

In energy-dispersive X-ray spectroscopy (EDS), an electron in an inner electron shell of an atom is excited by an external energy source (e.g., an electron beam) and leaves the atom. This causes an electron in an outer, high-energy shell to migrate to the vacancy left by the escaped electron, causing excessive energy to be released. The energy, which is the difference in energy levels between the two shells, is either released in the form of X-rays or excites another electron in an outer shell to leave the atom. Because each element has its distinct energy level, analyzing the X-rays released enables the elemental composition of a specimen to be identified, which in turn indicates the composition of the specimen’s surface material.
Figure 7 and Table 6 present the EDS results of the EP/APP/FS composites containing different proportions of the APP/FS flame retardant. Before being burned, EP/APP/FS 10% contained C, O, N, P, and Ca with weight percentages of 66.3 wt.%, 13.08 wt.%, 19.62 wt.%, 0.66 wt.%, and 0.35 wt.%, respectively. After raising the flame retardant to 40%, the contents of N, P, and Ca in EP/APP/FS 40% increased. This was caused by the addition of the flame retardant, which contained these elements. Specifically, P increased from 0.66 wt.% to 2.61 wt.%, and Ca rose from 0.35 wt.% to 1.45 wt.. When burned, the P in EP/APP/FS 40% dehydrated the material, forming a phosphate-based char layer that raised the weight percentage of P to 12.13 wt. % after the material was burned. This indicates that in the burning process, the presence of P increases CY, thereby facilitating the formation of a char layer that covers the surface of the matrix material and prevents it from being burned further.

![Figure 7 EDS of (a) Epoxy/APP/FS 10% (before burning) (b) Epoxy/APP/FS 10% (after burning) (c) Epoxy/APP/FS 40% (before burning) (d) Epoxy/APP/FS 40% (after burning).](image)

### Table 6 EDS for Epoxy/APP/FS composites.

<table>
<thead>
<tr>
<th>Sample No.</th>
<th>Elements</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>C(wt.%)</td>
</tr>
<tr>
<td>EP/APP/FS 10% (before burning)</td>
<td>66.3</td>
</tr>
<tr>
<td>EP/APP/FS 10% (after burning)</td>
<td>56.03</td>
</tr>
<tr>
<td>EP/APP/FS 40% (before burning)</td>
<td>63.19</td>
</tr>
<tr>
<td>EP/APP/FS 40% (after burning)</td>
<td>41.95</td>
</tr>
</tbody>
</table>

### 3.4 Char analysis

Raman spectroscopy is used to determine the vibrational and rotational modes of a crystal lattice or molecule. When light hits a molecule and interacts with the electronic
cloud and molecular bonds within the molecule, it causes a Raman effect, that is, when an excited molecule releases a photon, it returns to a vibrational or rotational mode that is different from the ground state. The energy difference between the ground state and the new state causes the frequency of the released photon to be different from the excitation wavelength of the light, which means its spectrum carries the characteristics of the material in frequency, intensity, and polarization. Therefore, Raman spectroscopy can be used to determine the compositions of a substance.

This study used Raman spectroscopy to analyze the char of the EP/APP/FS composites, which were left in a high-temperature environment (600 °C) for 1 and 5 min. The Raman spectrum was observed for changes in the disorder (D)-band and graphitic (G)-band [19-20]. The D-band, which is located at 1350 cm⁻¹, represents an irregular sp3 structure formed by linear carbon chains. After being burned, it becomes char, turning from the D-band into the G-band. The G-band is located at 1580 cm⁻¹ and represents an sp2 structure formed by hexagonal carbon rings, the structure of graphite. The presence of a larger number of G-bands indicates an abundance of char, that is, a favorable carbonized state (because char is mainly composed of hexagonal carbon rings). Dividing the area of D-band by that of the G-band produces a D:G ratio; smaller ratios indicate a larger abundance of graphite, which indicates that more char that is formed (Table 7).

Figure 8 and Figure 9 present the changes in the D-band and G-band of EP/APP/FS 10% and EP/APP/FS 40%. According to the analytic results presented in Table 7, both low and high concentrations increased the amount of char. This indicates that the addition of the composite flame retardant effectively increased the amount of char that was formed in the burning process, which made the material more difficult to burn, and that the flame retardant effect was greater at a higher concentration.

![Raman spectra](image)

**Figure 8** The Raman spectra of char products from Epoxy/APP/FS 10% at 800°C (a) 1min (b) 5min.

| Table 7 | The area ratio of Raman shift from the char of Epoxy/APP/FS composites |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | |
4. Conclusions

This study addressed the problems that EP that is highly flammable and that it does not self-extinguish once on fire. The solution proposed in this study was the introduction of a composite flame retardant comprising both APP and FS which was proven to lower the flammability of the polymeric base material and make it more difficult to burn. The inclusion of FS can lower the consumption of APP and is also a suitable use for a waste material. Therefore, it is a cost-efficient and environmentally friendly approach that can serve as an element in a circular economy. When the proportion of the APP/FS flame retardant in EP was raised to 40%, it effectively raised CY to 36.07 wt. %, IPDT to 1143.1 °C, UL94 classification to V-0, and LOI to 36%, thus turning EP from a flammable material into a fireproof material. These results indicate that adding the APP/FS flame retardant to EP to form an EP/APP/FS composite increases the thermal stability of the material and reduces its flammability considerably.

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References