

Article

# Biomechanically Tunable Nano-Silica/P-HEMA Structural Hydrogels for Bone Scaffolding

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**Abstract:** Innovative tissue engineering biomimetic hydrogels based on hydrophilic polymers have been investigated for their physical and mechanical properties. 5% to 25% by volume loading PHEMA-nanosilica glassy hybrid samples were equilibrated at 37°C in aqueous physiological isotonic and hypotonic saline solutions (0.15 and 0.05 M NaCl) simulating two limiting possible compositions of physiological extracellular fluids. The glassy and hydrated hybrid materials were characterized both for dynamo-mechanical properties and equilibrium absorptions in the two physiological-like aqueous solutions. Mechanical and the morphological modifications occurring in the samples have been described. The 5% volume nanosilica loading hybrid nanocomposite composition showed mechanical characteristics in the dry and hydrated states that were comparable to those of cortical bone and articular cartilage, respectively, and then chosen for further sorption kinetics characterization. Sorption and swelling kinetics were monitored up to equilibrium. Changes in water activities and osmotic pressures in the water-hybrid systems equilibrated at the two limiting solute molarities of the physiological solutions have been related to the observed anomalous sorption modes using the Flory-Huggins interaction parameter approach. The bulk modulus of the dry and glassy PHEMA-5% nanosilica hybrid at 37°C has been observed to be comparable with the values of the osmotic pressures generated from the sorption of isotonic and hypotonic solutions. The anomalous sorption modes and swelling rates are coherent with the difference between osmotic swelling pressures and hybrid glassy nano-composite bulk modulus: the lower the differences the higher the swelling rate and equilibrium solution uptakes. Bone tissue engineering benefits of use of tuneable biomimetic scaffold biomaterials that can be “designed” to act as biocompatible and biomechanically active hybrid interfaces are discussed.

**Keywords:** Biomimetic hydrogels; hybrid nanocomposites; anomalous sorption; Tissue engineering

## 1. Introduction

The Authors developed novel hybrid structural materials presenting anomalous sorption behaviours characterized by a transition from hard glassy to rubber state in presence of aqueous environments that could be potentially used as bone scaffolding materials. Namely, hybrid nanocomposites based on fumed amorphous silica nanoparticles embedded in a hydrophilic poly-(hydroxyl-ethyl-methacrylate) (pHEMA) were deeply investigated [1-5]

The addition of amorphous silica improved the self-organization of the hydrophilic polymeric network promoting hydrogen bonding of the polymeric chains with the hydrophilic nanoparticles. The resulting initially glassy nanocomposites undergo significant hydration and swelling when exposed to aqueous environment resulting in more rigid and transparent hydrogel with surprisingly improved mechanical strength [5] that overcome one of the major disadvantages of the use of hydrogels in applications where structural mechanical properties are needed. Such more resilient

hybrid hydrogels have been shown to possess biomimetic and osteoconductive properties that are mandatory in the design of mechanically bioactive bone scaffolds [4,5].

Bone remodelling processes repair the damage removing and replacing the damaged tissues with new bone, this healing process can be strongly favoured by using biocompatible and biomechanically active hydrogels that can be “designed” to reproduce bone compatible and biomimetic structural properties.

In healthy conditions, bone growth and remodelling cooperate to define the more efficient functional structure. Natural biomechanics and bone growth dynamic equilibrium is completely altered when a stiffer than bone material is implanted (such is the case of metal implants) [6].

Loads on bones cause bone strains that generate signals that some OB cells can detect and respond to. Threshold ranges of such signals are involved in the control of modelling and remodelling [7-9].

Remodelling processes repair the injury by removing and replacing the damaged tissues with new bone. Moreover, overloading (or under-loading) alters such phenomenon [9]. Early studies by Wolff (1892) stated that mechanics could determine changes in the architecture of bones [10]. Frost mathematically expressed these reactions of the bone tissue to given stimuli to quantitatively assess bone deformations postulated by Wolff [11]. Remodelling processes repair the damage removing and replacing the damaged tissues with new bone. Different studies proved that the micro-damage threshold is about 3000 micro epsilon strains [6,8,11].

The structural hydrogels have been proposed as mechanically bioactive interfaces for implants early osteointegration. However, the correct utilization of any synthetic or natural hydrogel to be used in biomedical applications should require complete investigation and characterization of mechanical and physiological fluids equilibrium sorption characteristics.

The hydrogel interactions with aqueous environments can affect structural as well chemo-physical materials properties. Due to the different origin, function and clinical pathologies, in fact, physiological water may present different composition and properties that need to be investigated in order to understand any possible hydrogel material properties modification.

Generally, diffusion of small molecules in polymers above their glass transition temperature or in glassy polymers with a low chemical affinity with the diffusing species could be described by ordinary Fick's law. This first limiting transport process, which can be mathematically described for a planar geometry by an initially linear relationship between the weight gain and the square root of time (linearity is maintained up to a 50% of the equilibrium maximum uptake) and by a smooth and continuous concentration profile through the sheet thickness [12].

Conversely, more complex anomalous transport behaviours can be observed when physical phenomena due to the strong interactions between molecules and hosting polymer interactions provides the rate determining transport modes. These complex sorptions behaviours include time-dependent boundaries conditions, penetrant molecules concentration dependent diffusion coefficients, osmotic stresses generation in the penetrated polymer and solvent induced polymer physical relaxation [13-17].

In such cases, swelling and significant changes in the transport mechanism could be observed as a consequence of the depression of the glass transition of the increasingly plasticized absorbing polymer below the test temperature. Namely, a second limiting transport process (named Case II, since other than that exclusively driven by diffusion) is described to occur during the sorption of the high affinity molecules in glassy polymers [15, 18].

In Case II transport mode, the weight gain of a planar sample immersed in a liquid or vapor is linear in time until equilibrium is reached [18]. Moreover, a discrete discontinuity between the almost uniform penetrant concentration in the outer swollen layers and the unpenetrated central glassy core. However, thicker materials, as those utilized in bone scaffolding, may show a more complex behaviour driven by the different contributions to the absorbing process, polymer relaxation and diffusive phenomena [14,16].

The initially dry and glassy hydrophilic PHEMA-nanosilica hybrid composites developed by our group have been described to show similar complex swelling response in presence of the physiological fluids when used in *in vivo* animal testing [19,20]. Adaptive properties of bone can

benefit of use of scaffold biomimetic materials that adequately respond to the physiological fluids properties changes [19,22]. The basic phenomena describing the biomechanically active hybrid response to physiological chemical modification are discussed in the present paper.

## 2. Materials and Methods

### Materials

A commercial 2-hydroxyethyl methacrylate (HEMA), obtained from Sigma-Aldrich Chemicals Co., (St. Louis, MO, USA) has been used as hydrophilic matrix. Fumed silicon dioxide (Aerosil 300 Degussa, Germany) with a mean diameter of 7 nm and specific surface area of 300 m<sup>2</sup>·g<sup>-1</sup> was utilized as bioactive filler. The  $\alpha$ - $\alpha'$  azo-iso-butyric-nitrile (AIBN), obtained from Fluka (Milan, Italy) has been utilized as initiator of the radical polymerization reaction. HEMA monomers were mixed with the fumed silica in the ratio of 5%, 10%, 15%, 20% and 25% by volume. The resin was degassed and transferred in 2.5 mm thick planar molds and then polymerized in temperature-controlled oven set at 60°C for 24 h and then post-cured for 1 h at 90°C.

### Mechanical characterization

The elastic shear tests, measured on a dry and hydrate states at different concentrations of NaCl solutions of the PHEMA-nanosilica hybrids, were performed using dynamic mechanical shear analyzer (DMA - Mettler-Toledo, Zurich, Switzerland). The complex shear moduli were measured at a constant frequency of 10Hz and in isothermal conditions of 37°C. The as prepared glassy samples with different nanosilica loadings were further desiccated under vacuum at a temperature of 60°C for 24 hours prior to mechanical testing. In shear test mode, 10 mm diameter discs and two samples cut from the polymer 2.5 mm thickness plate were placed between three steel discs forming a symmetrical sandwich geometry working under controlled oscillatory displacements. Isothermal scans for glassy samples were performed in a dry nitrogen atmosphere. The deformation control was set at 10  $\mu$ m with a force limit of 0.9 N was applied an oscillating frequency of 10 Hz.

The same testing procedure was applied to the swollen wet polymer samples (without desiccation step) at 0.09N force limitation; Hypotonic and isotonic equilibrated P-HEMA-nanosilica hydrogels with 5 to 25 % by volume filler contents were isothermally tested at 37°C in a 100% relative humidity nitrogen atmosphere at the frequency of 10 Hz.

### Sorption and swelling tests

25 dry specimens of 5% loading nano-filled PHEMA of 2.5 mm thickness and 20 x 20 mm side length, prepared according to the conditions described in the previous section, were equilibrated in aqueous physiological isotonic and hypotonic saline solutions (0.15 and 0.05 M of NaCl). These two solutions were chosen to simulate two possible different conditions of physiological extracellular fluids and their influences on hydrogels sorption behaviours. [23,24].

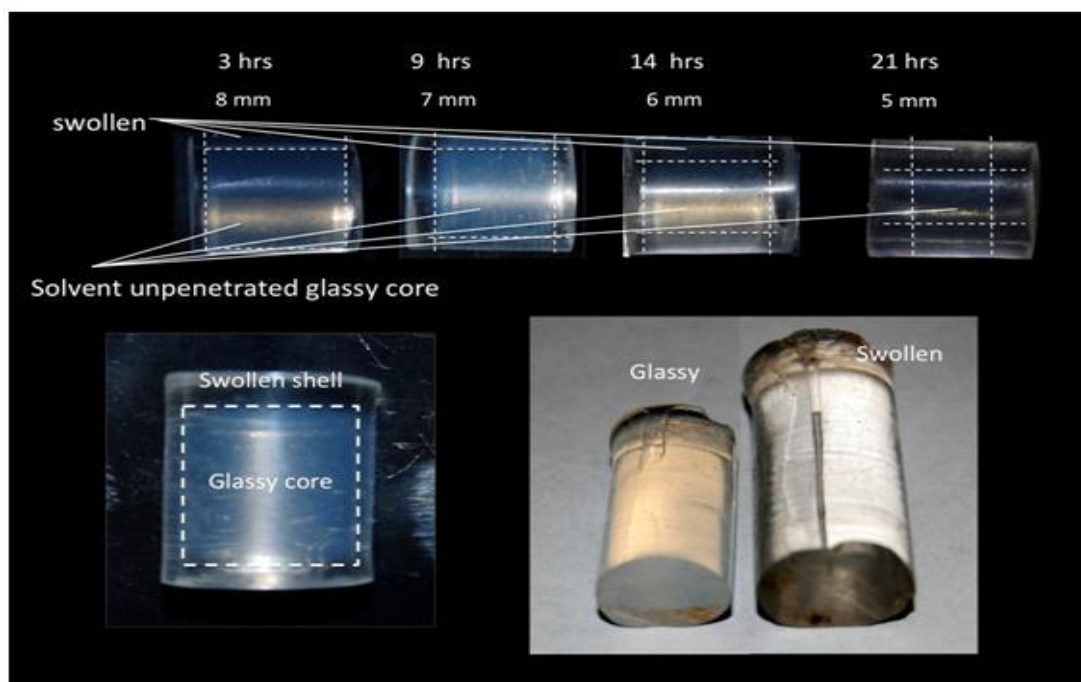
The plates, after immersion in the physiological solutions simulating the extracellular fluids, were monitored for sorption (by weight measurements) and swelling (by optical microscope measurements) kinetics. Equilibrium uptakes values in isotonic and hypotonic solution were statistically evaluated at equilibrium for all nanocomposite compositions.

Namely, samples weight gains due to the solution sorption in the initially dry samples were determined up to equilibrium by gravimetric measurements using a 0.1 mg resolution Mettler Toledo balance (Milan, Italy) and evaluated as percent increase of the initial dry sample weight.

The advancing swelling fronts associated to the anomalous sorption modes [13-18] and dimensional samples changes of the plate sample (thickness and side length increases along the Z-axis and the two orthogonal axes X and Y) were monitored as a function of the immersion time using an optical Leitz stereo-scan microscope. The sorption and swelling experiments were performed at 37°C (thermostatic water bath) until constant weight equilibrium up-takes and dimensional changes were monitored (*i.e.* 50 hrs). Three samples were extracted from the equilibrating solution for each measurement at different times, rapidly weighed and measured and then returned to the conditioning solutions.

## 3. Results

In a previous work [5] we reported that glassy hydrophilic PHEMA-nanosilica hybrid composites undergo a complex sorption process when immersed in water, see figure 1.



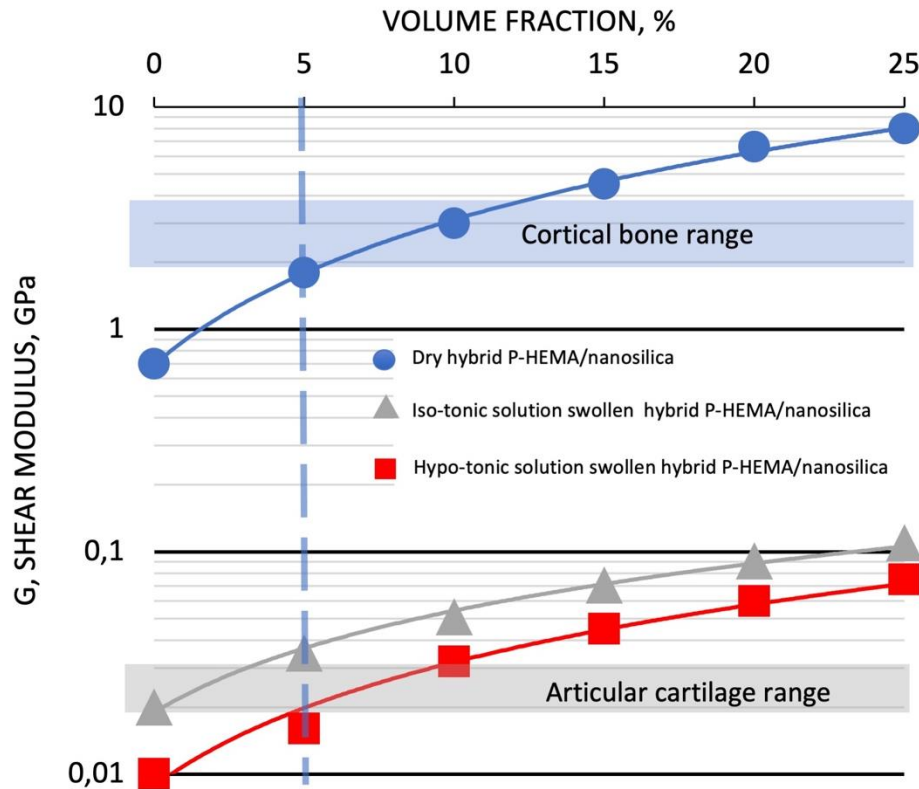
**Figure 1.** Swelling behavior of a hybrid hydrophilic nanocomposite in water [5]: Volumetric swelling from glassy to rubber states (Lower right), clear front between the internal unpenetrated glassy core and the water swollen outer shell (Lower left), the front progressively advance at increasing reducing the glassy core thickness (Upper part of the figure)

Diffusion of small penetrant molecules having a high chemical affinity with host glassy polymer, in fact, is characterized by an anomalous sorption behavior [15]. The highly hydrophilic glassy PHEMA-nanosilica hybrids used in our study are, in fact, been described to strongly swell when immersed in physiologic simulating aqueous media [4,5].

The physical phenomena occurring in the initially glassy P-HEMA polymer once exposed to the aqueous medium have been described in ref [5] and described in figure 1: the initially glassy hydrophilic sample is progressively externally swollen by the water sorption finally reaching an equilibrium fully swollen state (see right lower part of figure 1). Initially, (see lower left part of figure 1) a clear front separating an unpenetrated glassy core and a swollen outer shell is observed to progressively penetrating in sample glassy core.

The swelling process is accompanied by a significant increase of the sample water content leading towards final rubber hydrogels which mechanical characteristics can be differently influenced by the composition of the equilibrating aqueous medium and by the presence of fillers in the hydrophilic matrix. A mechanical characterization on our hybrid nanocomposites at different nanofiller loading in their dry and hydrogel forms after equilibration in Isotonic and Hypotonic physiological solutions has been then carried out in order to understand the level and intensities of the solvent-induced physical changes.

The complex shear moduli measured in Dynamic Mechanical Analysis (DMA) tests run at 37°C and 10 Hz on the glassy and hydrogels samples as a function of their nanosilica loadings are reported in the semi-logarithmic diagram of figure 2.



**Figure 2.** DMA Complex Shear Moduli of Dry (Blue circle), Hypotonic equilibrated hydrogels (Grey triangles) and Isotonic equilibrated hydrogels (Red squares) of P-HEMA-Nanosilica hybrid nanocomposites at increasing nanosilica loadings. Cortical bone and articular cartilage ranges of variation of shear modulus are also reported on the figure

The measured values of the shear moduli range from  $0.75 \pm 0.02$  to  $8.1 \pm 0.3$  GPa for the dry glassy hybrid nanocomposites, and from  $1.9 \pm 0.3$  to  $10.1 \pm 0.5$  MPa and from  $0.9 \pm 0.2$  to  $7.6 \pm 0.3$  MPa for the hybrid hydrogels equilibrated in Iso-tonic and Hypo-tonic physiological solutions, respectively.

As indicated in previous publications [5, 22], a not usual for particle reinforced composite linear increase of complex shear modulus of dry P-HEMA-nanosilica composites at increasing silica contents is observed. The shear modulus of the nanocomposite with 25% volume of nano-silica loading reaches a value (9.0 GPa) that is 10 times higher than the value of the dry unfilled P-HEMA (0.9 GPa). These significant increases of the shear moduli compared to the values expected applying the ordinary Halpin-Tsai equations approach [25] have been attributed to the hybrid nature of the resulting nanocomposites that is stiffened at segmental level by the entangled polymer structure interpenetrating the nano-silica inorganic network [26].

Characteristic ranges of variation of the shear moduli of for cortical bone ( $2.5 \pm 0.8$  GPa) [27] and for articular cartilages ( $2.4 \pm 0.3$  MPa) [28,29] have been also reported on figure 2 for comparison with the mechanical behavior of our materials.

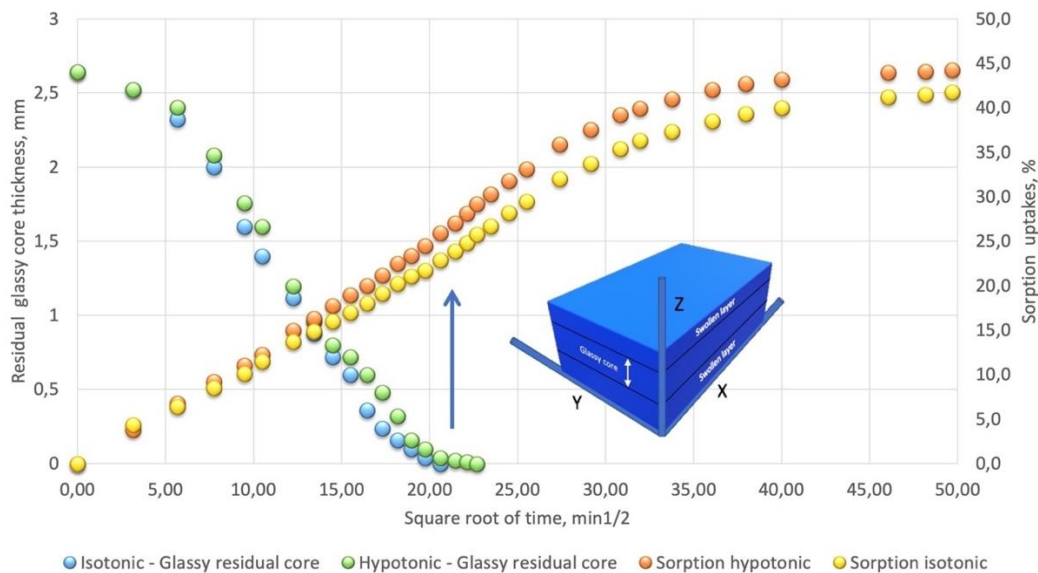
It can be inferred that for a content of about 5% by volume of nanosilica, the hybrid nanocomposites in their glassy and hydrogel states show elastic properties comparable with those of cortical bone and articular cartilage, respectively. This composition has been chosen as optimal hybrid formulation for bone tissue engineering and used in the prosecution of the research described in this paper.

Bone tissue engineering can positively benefit of use of tuneable biomimetic scaffolding biomaterials that can be “designed” to act as biocompatible and biomechanically active hybrid interfaces [19,20]. The proposed biomechanical design approach to evaluate the most opportune material composition, however, should be integrated with an appropriate study on its response to

physiological liquid variations. From figure 2, in fact, can be also inferred that these structural hydrogel systems are very sensitive to the composition of the physiological solutions. The shear moduli are, in fact, significantly influenced by these variations.

Further investigations on the kinetics and equilibria of the physical phenomena occurring to the hybrid nanocomposite have been performed on the chosen optimal composition of 5% by volume nanosilica loaded P-HEMA.

The kinetic raw data for physiologic fluids simulating NaCl aqueous solution measured as sorption uptakes and residual unswollen glassy core for are reported in figure 3 as a function of square root of time.



**Figure 3.** Swelling kinetics measured (left axis) as residual glassy core thickness and anomalous sorption behavior (right axis) in initially glassy 5% by volume nanosilica loaded PHEMA nanocomposite equilibrated in hypotonic and isotonic physiological solutions.

The sorption kinetics in the glassy samples from both equilibrating Hypo- and Iso-tonic solutions show a complex behavior characterized by a discontinuity at about 500 minutes (21 in the  $t^{1/2}$  axis of figure 3).

The samples during the equilibration in the physiological solutions showed the formation of a clear swelling front separating the unaffected glassy core and an outer swollen layer (see schematization in figure 3). By a parallel investigation carried out by measuring the kinetic of advancement of the swelling front considering the thickness of the residual core during the equilibration test (reported on the left axis in the same figure 3), it is evident that the discontinuity occurs when the residual glassy core disappears. In presence of the glassy rigid core, in fact, free swelling is principally occurring along the z axis (see sample schematization in figure 3). Once the constrain of the rigid glassy core in the X and Y directions disappears, the solvent penetrated layers can relax and expand in those directions leading to additional sorption.

It is, therefore, evident that several physical phenomena are simultaneously occurring during the test. Namely, penetrant molecules diffusion, polymer swelling, time-dependent boundary conditions, and an abrupt change in the transport mechanism due to the polymer relaxation at the glassy core interface should be considered [12-18]. A brief description of the possible limiting transport processes is given in order to better understand the observed complex sorption behaviors.

Generally, penetrant diffusion in polymers above their glass transition temperature or in glassy polymers with a low chemical affinity with the diffusing species could be described by ordinary Fick's law [12]. This first limiting transport process is characterized by a linear relationship between

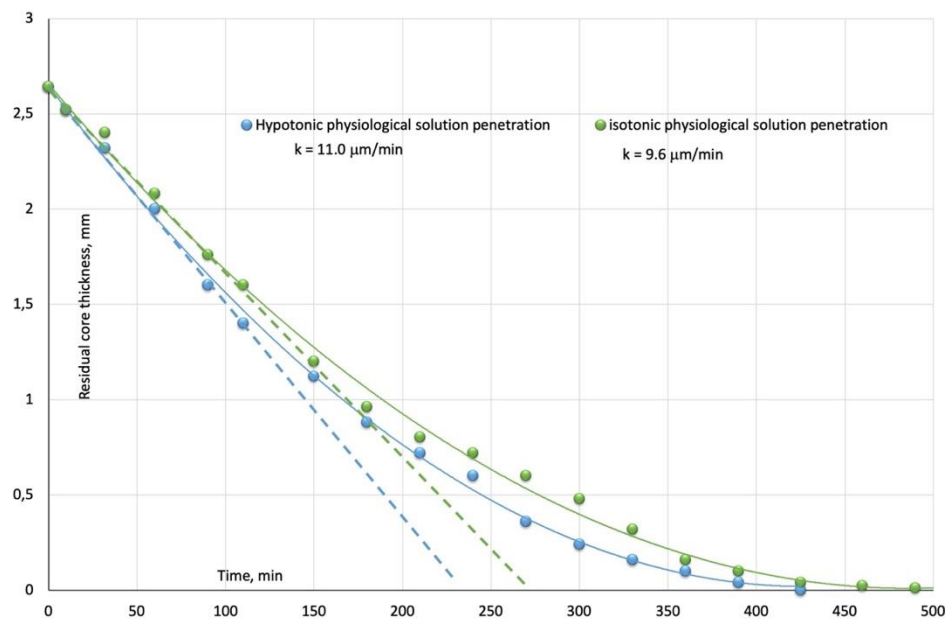
the initial weight gain and the square root of time, and it is characterized by a smooth and continuous concentration profile through the sheet thickness.

Conversely, a second limiting transport process, named Case II [16], occurring in thin glassy polymers films in contact with high chemical affinity diffusing molecules, is characterized by a step discontinuity of the penetrant concentration profile, that, other than be exclusively associated to Fickian diffusion, is principally driven by polymer relaxation. For this limiting Case II transport process, the weight gain is linear in time until equilibrium is reached. A discrete discontinuity, which separates the uniform penetrant concentration outer swollen shell and the glassy central core [-], is observed and moves through the samples at a constant rate.

In very general terms it can be stated that the initial sorption uptakes can be expressed as functions of time elevated to the exponent  $n$  ( $t^n$ ) with  $n=0.5$  (square root of time) for Fickian diffusion and  $n=1$  (linear in time) for Case II limiting sorption mode.

However, the penetrant molecules diffusive resistance generated in the outer swollen shell [24] can reduce the swelling front advancement rate [24,30-32]. Thicker samples, as those used in our experiments, in fact, can show a still more complex sorption behavior since the diffusive resistance in the outer swollen shell reduces the concentration of solvent at the glassy core interface lowering the sorption process. In fact, the diffusive resistance generates a smooth penetrant concentration profile in the swollen outer shell with its minimum at the swollen-glassy interface producing a lower plasticization of the polymer and, consequently, a slower penetration rate [27].

The water sorption expressed as initial dry weight percent increase as function of square root of time in figure 2, clearly shows an anomalous behavior where it is difficult to recognize between the two previously described limiting sorption modes (Fickian and Case II). For this reason, swelling advancing fronts have been plotted as a function of the time in figure 4.

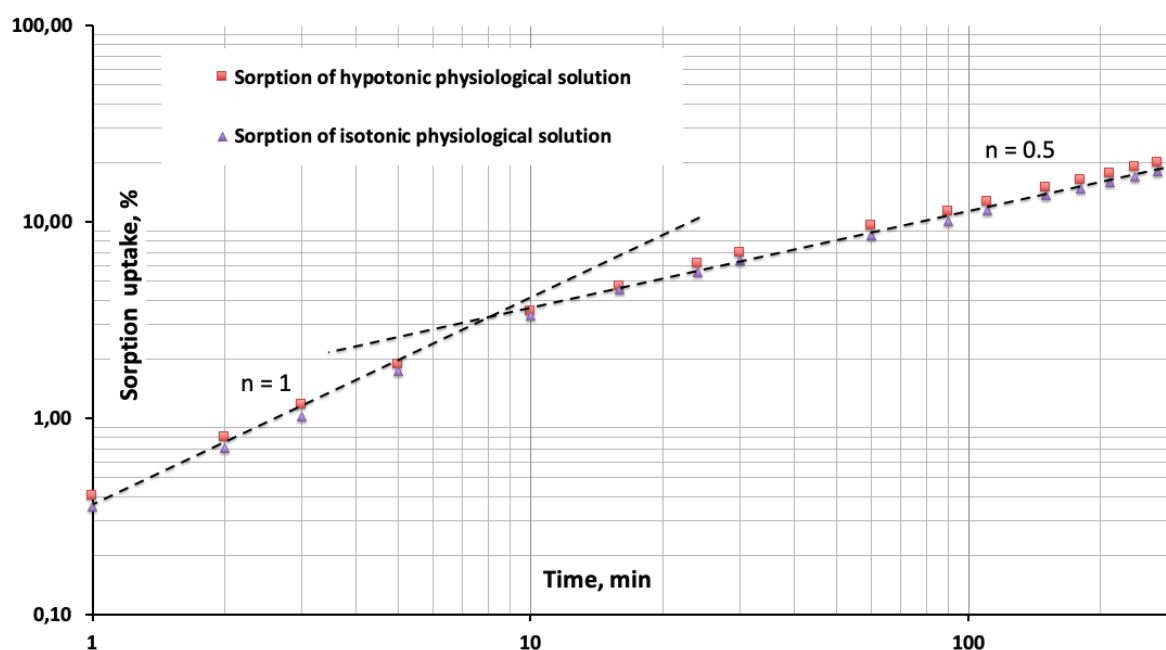


**Figure 4.** Swelling kinetics measured as residual glassy core thickness at different immersion times for initially glassy 5% by volume nanosilica loaded PHEMA hybrid nanocomposite equilibrated in hypotonic (blue square) and isotonic (orange circles) physiological solutions. Dotted lines represent the initial penetration rates.

The initially swelling kinetics (dotted lines in figure 3) for isotonic and hypotonic aqueous solutions are, respectively,  $11.0 \mu\text{m}/\text{min}$  and  $9.6 \mu\text{m}/\text{min}$ . The penetration rates progressively slow down as the swelling front advances in the unpenetrated glassy core indicating that a diffusion

resistance is developing in the outer swollen thickness. It can be, then, inferred that limiting Case II sorption occurs only in the early first stages of the solutions equilibration process. If a water uptake vs time diagram using log-log scales is used, the slope of the curve is the exponent  $n$  of the previously cited function of time  $t^n$ . In figure 5, where the sorption uptakes have been plotted in a log-log diagram, two linear portions characterized by slopes  $n=1$  and  $n=0.5$  are present. The first portion of both curves with slope  $n=1$  represents the condition of constant rate swelling front advancement (limiting Case II sorption). In these condition of constant rate sorption it can be stated that the process is only governed by the osmotic pressures generated at the swelling front where the penetrant concentration is constantly at its equilibrium value[.]. After 8 to 10 minutes, corresponding to a penetrated thickness of the 0.09 to 0.10 mm, the swelling process starts to become diffusion controlled (slope  $n=0.5$ ). In physical terms this means that the penetrant molecules concentration at the swelling front is lowered by the diffusive resistance encountered by the penetrant molecules in the progressively thicker external swollen layer [30-32]. The lower concentration of the swelling medium reduces the corresponding osmotic pressures at the interface progressively reducing the rate of advancement of the swelling process until glassy core disappearance (after 500 minutes and indicated by an arrow in figure 3). At longer times up to final equilibrium (about 2500 minutes), the sorption uptakes observed in figure 3 are due to the residual diffusion in the not fully saturated but swollen polymer.

Measurements of the final equilibrium dimensional changes in both equilibrating media resulted in linear expansions along the X, Y and Z axes of the order of 15%, 15% and 17%, respectively.



**Figure 5.** Early stages of the swelling process plotted in a log-log scale diagram. The slope  $n=1$  represents the limiting Case II sorption mode while the slope  $n=0.5$  represents a diffusion-controlled process (swelling front advancement) occurring during the equilibration in physiological solutions of the 5% by volume nanosilica P-HEMA hybrid material.

#### 4. Discussion

The sorption modes and physical phenomena occurring during the equilibration in physiological solutions of the initially glassy nanocomposite hybrids are to be attributed to the high affinity between of the proposed biomaterials and the physiological liquid simulating solutions. Change of the polymer water penetrant molecules activities and osmotic pressures in water solution sorption tests at increasing solute molarity have been investigated using the Flory Huggins theory approach [31].



The Flory-Huggins interaction parameter  $\chi_1$  measures the interactions of the polymeric chain segments with the penetrant molecules as well as the polymer-polymer interaction [31]. The free energy of mixing of a polymer chains with penetrant molecules was described by Flory-Huggins/Rehner theories [33] considering the two contributions of the enthalpy of mixing,  $\Delta H_{\text{mix}}$ , and the entropy of mixing,  $\Delta S_{\text{mix}}$ . The Entropy of mixing is calculated by the volume fractions of solvent and polymer, while the enthalpy of mixing is determined by a dimensionless interaction parameter  $\chi_1$ . The presence of a second component in a polymer solid solution lowers the chemical potential of the host molecule from its value in the pure condition. The evaluation of the chemical potential changes in differently water moisture saturated polymers is needed to calculate the osmotic pressure rise due to the penetrant molecule sorption.

A theoretical expression for the reduction of the chemical potential of the penetrant molecules is derived from the free energy of mixing since the chemical potential of a penetrant molecule (solvent) in non-ideal solutions relative to that in its pure state relates to its activity through the free energy of mixing [17,18,33],

$$\mu_1 - \mu_1^0 = RT \ln a_1 = RT \left[ \ln(1 - j_2) + \left(1 - \frac{1}{x}\right) j_2 + \chi_1 j_2^2 \right] \quad (1)$$

where,

$\mu_1^0$  is the pure penetrant molecule chemical potential,  $\mu_1$  is penetrant molecule chemical potential in solid solution with polymer, R is the gas constant and T the absolute Temperature. Moreover,  $a_1$  is the activity of the dissolving molecules (which in our experiments was the water activity in the NaCl saline solutions),  $j_2$  is the volume fraction of the polymer in the polymer-water equilibrium solution at different penetrant water activities.

The interaction parameter  $\chi_1$  accounts for the enthalpy changes occurring when polymer-polymer and penetrant-penetrant interactions are replaced by polymer-penetrant interactions.

Finally,  $x$  is the average degree of polymerization,  $x = \bar{V}_2 / \bar{V}_1$  with  $\bar{V}_1$  and  $\bar{V}_2$  the molar volumes of penetrant and polymer, respectively. This term, which is very big for polymers/water systems since representing how many solvent molecules are needed to form the polymer macromolecule or crosslinked network, lets to negligible  $1/x$  values in eq. 1 that can be then written as:

$$\ln a_1 = \left[ \ln(1 - j_2) + j_2 + \chi_1 j_2^2 \right] \quad (2)$$

This equation correlates solution water activity in the sorption tests and the experimentally measured water uptakes.

Using the experimental equilibrium sorption uptakes, in fact, we may evaluate the interaction parameter, which should theoretically depend on the penetrant molecule concentration, at different water uptakes in the amorphous PHEMA/nano-Silica Hybrid material. The calculated interaction parameters  $\chi_1$  at two different equilibrium water uptakes at 37°C are reported in table 1.

By knowing the interaction parameters  $\chi_1$  we may evaluate the osmotic expansion stresses generated by the presence of the water molecules sorption at different equilibrium moisture contents using this derivation:

$$\sigma = \pi = - \frac{(\mu_1 - \mu_1^0)}{V_1^0} \quad (3)$$

where  $V_1^0$  is the water penetrant molecules molar volume (i.e. 18.07 ml mol<sup>-1</sup> \* MPa<sup>-1</sup>).

Referring to eq. 2 considering the water volume fraction, and assuming the contribution of the  $1/x$  (the ratio between the molar volumes of the hosting polymer and the water penetrant) negligible,

we will obtain from eq. 4 the osmotic swelling pressures for Hypo and Isotonic solutions reported in table 1.

$$\rho = - \frac{RT}{V_1^0} \left[ \ln(1 - j_1) + \left(1 - \frac{1}{x}\right) j_1 + C_1 j_1^2 \right] \quad (4)$$

**Table 1.** Osmotic pressures and sorption properties of Hybrid Hydrogels<sup>1</sup>.

Swelling NaCl saline solution	$j_1$ Equilibrium Volume fraction,	$\chi_1$ Flory-Huggins interaction parameter	$\pi$ , GPa Osmotic swelling pressure	$\Delta$ GPa, Bulk modulus - osmotic pressure	$k$ $\mu\text{m}/\text{min}$ Swelling rate (Case II mode)
<i>Hypotonic</i>	0,35	0,91	-3,6	$\Delta_{\text{Hypo}} = -1.7$	11.3
<i>Isotonic</i>	0,33	0,86	-2,4	$\Delta_{\text{Iso}} = -2.8$	9.8

<sup>1</sup>5% by volume P-HEMA-nanosilica hybrid hydrophilic nanocomposite

The calculated osmotic swelling pressures/stress range from -2.5 GPa at the lower equilibrium water contents (volume fraction 0,41 when saturated in iso-tonic NaCl water solution) to a maximum of -3.6 GPa at higher equilibrium water contents (final water uptake of 44.2 % corresponding to 0.35 volume fraction when saturated in hypo-tonic NaCl water solution).

In Flory's theory [33], the isotropic stress generated by the absorbed molecules equates the total osmotic pressure to reach a static equilibrium state in the polymer. Namely, the penetrant swelling stress ( $\sigma$ ) in the polymer exerts a compressive pressure ( $\pi$ ) on the penetrant molecules. "... A close analogy exists between swelling equilibrium and osmotic equilibrium. The elastic reaction of the network structure may be interpreted as a pressure acting on the solution, or swollen gel...." [33].

The experimental values of the shear modulus in our DMA characterizations at 5 % by volume PHEMA-nanosilica hybrids material (which is the composition used in our sorption-swelling tests) is 2.0 GPa (see Figure 2). However, in order to compare osmotic pressure generated by the sorbed molecules in the hosting polymeric system, the material characteristic bulk modulus (hydrostatic compression rigidity) should be calculated. The relationships between Elastic, Shear and Bulk moduli depends on the material Poisson's ratio [35,36]. For most engineering plastics the Poisson's ratio in the range  $0.35 < \nu < 0.45$  and then, for quasi-isotropic crosslinked polymers and other glassy isotropic polymers, the elastic modulus equals the bulk modulus  $E \approx B$  while the ratio between the bulk and shear moduli is  $E \approx B \approx 8/3 G$ .

In the case of our PHEMA-nanosilica hybrids, the calculated bulk modulus B (elastic behavior under hydrostatic pressure) is 5.3 GPa that is of the same magnitude of the values of the osmotic pressures calculated from the sorption data for isotonic (-2.4 GPa) and hypo-tonic (-3.6 GPa) solutions.

The difference  $\Delta$  between the equilibrium internal osmotic swelling pressures generated at equilibrium by the absorbing species (essentially water molecules) and the material characteristic bulk modulus (hydrostatic compression rigidity) is reported in the last column of table 1,  $\Delta_{\text{Hypo}} = -1.7$  and  $\Delta_{\text{Iso}} = -2.8$  for hypo-tonic and iso-tonic aqueous solutions, respectively.

It can be inferred from table 1 and sorption/swelling kinetics (evaluated as  $\mu\text{m}/\text{min}$  from figure 4) that the lower the difference  $\Delta = B - \pi$  between material bulk modulus and internal osmotic pressure induced by the absorbing species, the higher and faster are the sorption uptakes, water diffusivity and swelling rates.

## 5. Conclusions

Hybrid ceramo-polymeric nanocomposites based on Hydroxyl-Ethyl-Methacrylate polymer (P-HEMA) filled with 7-15 nm fumed nanosilica particles (5% by volume) is a good candidate for a biomimetic material in bone tissue engineering. This material in presence of simulating hypotonic

and isotonic physiological liquid environments turns from rigid glass to rubbery hydrogel swelling up to 50% of its initial volume (14% linearly) and absorbing up to 40-45% by weight (depending on the composition of the external physiological medium).

The dynamic mechanical analysis performed on the exsiccated and on physiological like liquid swollen samples has shown that the elastic behavior of this hybrid material in its dry glassy state at the chosen filler composition is comparable with that of bone while, when hydrated to its rubbery hydrogel state, it possesses elastic properties comparable to those the cartilage.

The use of mechanically tuned biomimetic hybrid hydrogels as scaffolding materials is expected to further improve prosthesis adaptation mechanisms since introducing active interfaces that adapt implant biomechanics since better reproducing cartilage and ligaments functions [6,7,19-22]. Adaptive properties of bone could benefit of use of biomimetic (biomechanically compatible and bioactive) scaffold biomaterials coupled with new designed prostheses.

A biomimetic/physiological approach can be then pursued in designing custom formulations of these new tunable ceramo-polymeric hybrid structural hydrogels that better adapt to the patient bone characteristics acting as bioactive and biomechanical stimulation and potential improved bone scaffold mineralization and ossification.

Sodium ions concentration changes can induce modification of the physical and mechanical properties of hydrogels used for structural or scaffolding systems.

Our hybrid structural hydrogels are designed to act as biocompatible and mechanically bioactive scaffolds for implant with the scope of favor adaptive directionally organized bone growth. In order to achieve this result, both a proper scaffolding biocompatible and biomechanically active material has to be designed.

The biomimetic characteristics of our hybrid initially glassy materials have been investigated both for mechanical and swelling properties in order to better understand all the physical and morphological modifications occurring when exposed to mutating physiological like conditions. In the case of use as scaffolding material for bone tissue engineering, physiological bone material behavior to be mimicked by the bioactive scaffolding material relates to the chemical as well mechanical aspects.

Mechanical properties in the dry and swollen states as a function of the changing physiological fluid water contents, as well as bioactivity and swelling behavior sensitivity to external physiological modifications could play a relevant role in designing smart and biomimetic hydrogels. Hybrid ceramo-polymeric insert swelling could be used to stabilize implants in the bone and to create a biomechanically active interface that favors bone growth.

Stresses on the bone can be modulated by proper choice of scaffold swelling thickness and structural properties for healthy bone growth. In vivo tests performed using these new modified oral implants confirmed the improved capability of such hybrid hydrogels in promoting early osseointegration [19,22,29].

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