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Application of 3D scanning as an indirect method to analyze and eliminate errors on the manufactured yoke-type forgings forged in SMED device on modernized crank press

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Abstract: The article proposes an indirect measurement method based on a dimensional and shape analysis of forgings for the evaluation of the manufacture and the proper operation of the key elements of the crank press, in which after modernization, a quick tool assembly based on SMED (Single Minute Exchange of Die) was implemented. As a result of the introduced changes aiming at improving the forging aggregate and increasing the production efficiency, errors were observed on the manufactured products-forgings in the form of twists and joggles. The preliminary analysis showed that they can be clearances and dynamic deformation in the kinematic chain, the occurrence of side forces during automatic forging of the forging in a two-component system (a long, thin element), as well as the design and construction errors in the joining of the SMED instrument with the table tops of the press. In order to solve the presented problem, in the first place, a separate dimensional and shape analysis was made of selected elements of the press and the instrumentation with the use of the 3D scanning method with the purpose to analyze the construction tolerances of the key elements of the press geometry. Next, an evaluation of the effect of clearances and dynamic deformations of the press as well as the force distribution during the forging process was made through numerical modelling. Despite all of the above, such an approach did not make it possible to solve the problem. A proprietary method with the use of 3d reverse scanning was proposed, which allowed to solve the problem of forgings errors. Based on the measurement results and analyses for a few variants of production cycles the necessary changes were obtained, making it possible to minimize the errors and obtain proper products in respect of geometry and quality.

Keywords: crank press; die forgings; joggles and shape errors; 3D scanning

1. Introduction

Die forging processes for large series of products used e.g. in the automotive industry are usually realized on mechanical or hydraulic presses [1]. As opposed to open-die and semi-free die forging, which makes it possible to punch large size ingots and produce "large forgings" in small series [2], e.g. for the aircraft industry, which are produced on aggregates with high pressures and energies [3, 4], such as steam-air hammers, wedge presses, etc [5,6,7]. For that reason, die forgings obtained on presses characterize in a much bigger dimensional and shape precision as well as quality compared to forgings obtained on hammers [8,9,9,11]. In the case of die forging on mechanical presses, crank presses are those usually used, mostly owing to their high efficiency with a relatively high precision of the obtained forged products [12]. However, the quality and precision of the forgings is a resultant of many factors, both technological and technical, e.g. the state and quality of the key elements of the

press, such as: the slide guides, crankshafts, bearings, base holders, strands, etc. as well as the instrumentation itself [13,14]. As a result of long-term operation and wear as well as deformation of the particular components of the forging aggregate, we can observe clearances, and also macro- and microshifts of the elements cooperating in the whole system, which can result in the occurrence of errors and defects of the forgings [15,16]. A similar situation can occur also during the scheduled modernizations or other improvements of the forging machines, as well as during new start-ups e.g. as a result of insufficiently well-developed technology or improperly designed forging instrumentation [17,18]. Moreover, in order to increase the efficiency in the production process quite often used approach is based on the ideology of SMED (Single Minute Exchange of Dies). SMED is one of the many lean production methods for reducing waste in a manufacturing process. Successful implementation of SMED requires full understanding and analysis of the retooling process as well as knowledge of the details of each operation and configuration [19,20]. According to the initiators of this issues, Shingo Japanese engineer [21]. set-up operations are divided into two types: internal operations performed while the machine is stationary, and external operations performed during the machine is running. Wherein, in the die forging processes, the term SMED very often comes down not to the ideology but to the nomenclature of a special system / device for quick forging tools replacement [22,23]. The implementation of such a technological solution, despite a significant acceleration of the replacement of dies, requires its adaptation to the forging unit, which in the early stage may contribute to production problems and errors of forged products [24]. In effect, this leads to obtaining less precise forgings and, in extreme cases, the occurrence of defects, such as underfills, laps, as well as twists and joggles, which partially or totally disqualify such products [25,26,27]. That is why each forging aggregate should periodically undergo a general overhaul including regeneration or replacement of the frictional elements of the lead, beside the typical current repairs. [28,29,30]. After each of such major repairs or modernization procedures of the aggregate, it is necessary to conduct a commissioning [31]. It should be added that, at present, there are no clear guidelines related to how such a commissioning should be performed. It is recommended to use the norm [32,33], which refers only to presses with low pressure forces up to 1000 tons, whereas in the case of presses with higher pressures, the acceptance conditions are different, provided by the producer of a given press, which are close to the norm: EN ISO 16092-1:2018 [34]. The whole process of the currently conducted acceptance procedures is mostly based on various measurements of the working surfaces of the table and the slide as well as errors related to the shift of those elements in respect of each other. These measurements are usually realized under static conditions, which include, beside measuring the dimensions and verifying their agreement with the figures, calibration of the control and measurement systems as well as verification of the key elements. So far, the acceptance examinations and tests have been conducted sporadically, and they have come down to measurements of the precision and quality of manufacture as well as the parallelism of the replaced elements through their measurement and calibration of the integrated measurement systems [GPS, inne]. During the commissioning procedure, no tests related to determining the quality of the forgings produced by the aggregate are usually performed, which is mainly caused by the usually practiced variants of cold commissioning (realized at the plant of the manufacturer on a machine which does not permanently adjoin the floor, making it impossible to apply high force). Unfortunately, such standard activities do not consider the dynamic phenomena, that is an analysis determining whether the whole aggregate operates properly during forging, where the deformation lasts only 0.2s, and high inertial forces as well as rotational masses operate, etc [35]. This creates a situation when the aggregate works properly under static conditions, but under dynamic ones, that is during its typical operation (periodical high pressures and temperature gradients on particular elements), it can already exhibit significant deviations from the norm.

At present, owing to the progress in measurement techniques as well as other (visual) systems, it is possible to apply a whole spectrum of methods for the analysis and verification of both the particular elements of the forging aggregate and the apparatus as a whole [37]. For the measurement of the selected geometrical features crucial for the components of a forging machine, the CMM techniques are applied, owing to their high precision, although they are more and more often used because of the mobility as well as increasing time precision offered by the presently produced 3D

scanners mounted e.g. on mobile measurement arms [38]. Of course, for calibration of the aggregate's measuring elements, classical measurement methods are applied (rectilinearity and perpendicularity masters, gauge blocks, time sensors), as well as much more advanced systems allowing a non-contact dynamic analysis with the use of an image and structured light analysis (e.g. Aramis and others). At the stage of design, a whole range of modern methods supporting the design and analysis is applied, that is CAD/CAM/MES programs, which also enable an analysis of deformations and dynamic accelerations during the forging process [39,40,41,42,43]. However, often, despite the use of many modern measurement methods and advanced CMM systems, both in new installations and those after reparation, modernization or improvement, we can encounter problems resulting in geometrically and qualitatively inappropriate products of the forging process, i.e. forgings [44], whose elimination is difficult in a real process [45,46,47]. Such problems are, unfortunately, very costly for the forge, as they are connected with additional shut-downs, as well as reduced production efficiency and expensive scrapping of the forgings which do not meet the quality control requirements [48]. That is why it is becoming necessary to search for new non-conventional methods, which, so far, have not been applied in solving problems of this kind [49,50, 51]. One of them may be the approach proposed by the authors, which consists in the use of the indirect measurement method based on measurements of selected geometrical features of the product – a yoke-type die forging, assigned for steering columns, for the evaluation of the manufacture correctness of the key press elements (Base holders, slide and guides) as well as the forging instrumentation mounted based on SMED.

2. Test subject, scientific problem and research methodology

The subject of investigations is a mechanical crank press Massey with the load of 13MN, which underwent modernization in order to perform a quick replacement of instrumentation as well as robotization of the work center (Fig. 1), used to manufacture a yoke-type forging, in a two-component system (Fig. 2a).

Forgings of this type, due to their geometry and the two-component system, can cause difficulties in obtaining a proper product, that is one being within the dimensional and shape tolerance, which, for the analyzed product, equals 0.2mm. During the start-up and testing of the modernized press, it turned out that the obtained products (forgings) exhibited defects in the form of joggles and twists, that is a shift and rotation of the upper part of the forging in respect of the lower one in the parting plane (Fig.2b).

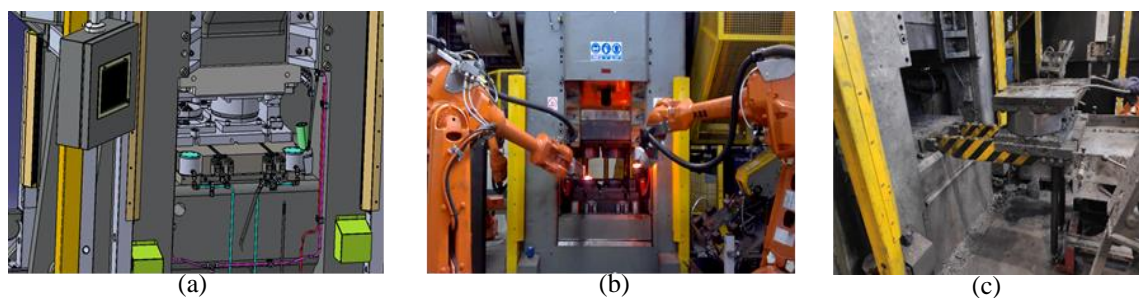


Figure 1. Photographs of: (a) the CAD model of the modernized press, (b) the main working part of the modernized press during forging, (c) the assembly of the SMED instrumentation in the working area of the crank press.

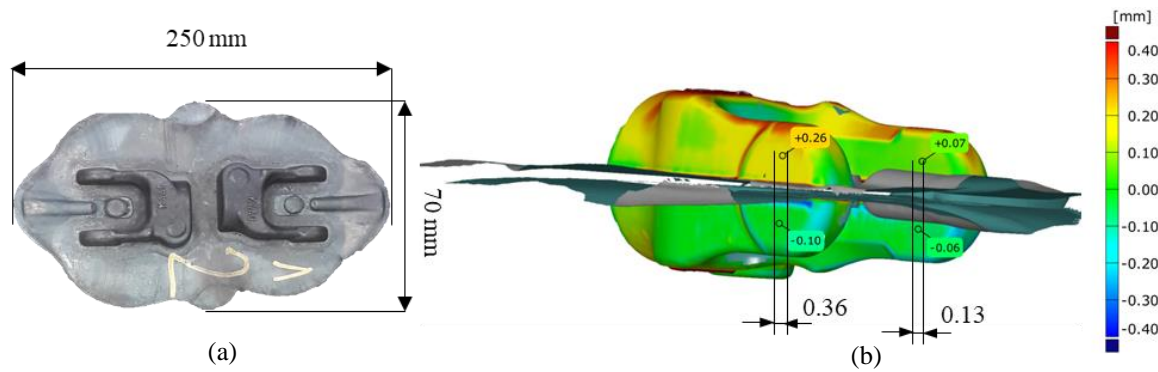


Figure 2. Photographs of: (a) a forging with the flash made on the analyzed press, (b) the results of scanning an exemplary defective forging with visible joggles – differences between the upper and lower part of the forging.

The presented results of joggles based on scanning (Fig. 2b) should make it possible to interpret the effect of the errors of the whole forging bay system (made of a press frame, a SMED system and the built-in tools) and the complex kinematic chain. An in-depth dimensional and shape analysis of the key elements in this chain should make it possible to determine the values of corrections whose introduction into the geometry of the forging bay would correct the geometry of the produced forgings and eliminate their defects.

2.1. Determination of the scientific problem

Fig. 3b shows an SMED system with the mounted tools assigned for forging in three operations. This instrument is built-in inside the work centre in such a way that the upper board is permanently connected to the slide by means of a stake keying (Fig. 3a), which is responsible for their positioning in respect of each other. The upper case is mounted to the upper board through a keyways/cleft joints and screws, connected to the upper tools. In turn, the lower board of the case, to which the lower tools are fixed, is mounted to the lower board also by means of a cleft joint: after the case has been driven into the key seats on feed rolls and reached the end stops, where it is blocked by the side wedges. The lower board is connected to the press table in a similar way to the upper one. In order to increase the precision of movement, the upper and lower board of the SMED system itself are joined by means of two massive poles visible in Fig.3a.

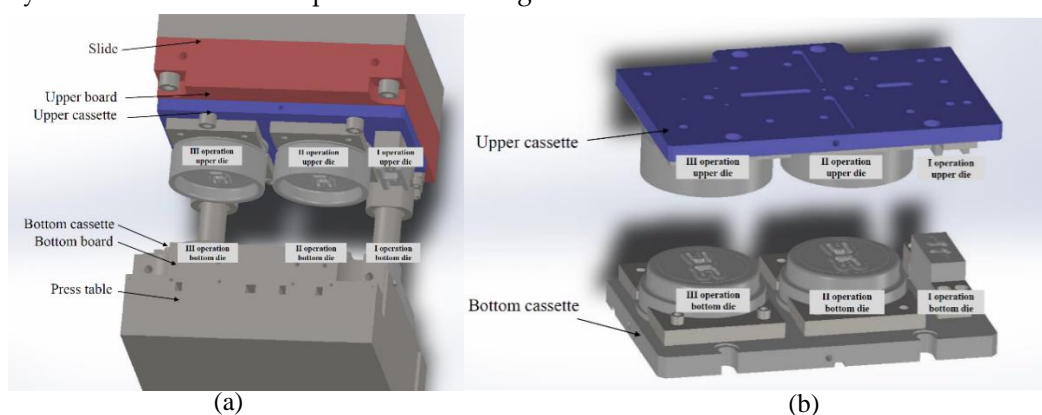


Figure 3. View of: (a) the CAD model of SMED system installed in main boards, (b) View of the CAD model of SMED system with the mounted tools assigned for forging in three operations.

For a press constructed this way, together with the SMED system and the described joints in the whole kinematic chain, errors occurred on the forgings in the form of joggles or joggles with twists (Fig. 2b). Unfortunately, defects of this type are very difficult to eliminate and they are formed as a

result of a combination of various factors and errors resulting from the manufacture tolerance of the component elements of the modernized press. The first error component is related with the press itself. The geometry of the slides in the press undergoes wear during the operation of the given tool. The occurring clearances are cancelled through regulation of the wear limit (by means of patterns, e.g. feeler gauges, gauge blocks). After the guides have crossed the minimal dimension of thickness or flatness, they undergo a general overhaul. However, this prevents the slide shifting along the guides from moving with an ideal rectilinear trajectory. The press, after each repair, is commissioned according to the norms, which pay a special attention to the measurement of the geometrical dimension components that describe the movement errors of the slide in respect of the press table, which enables an objective commissioning of the press. The second error component in the analyzed solution refers to the connection with the replaceable SMED system with the permanently mounted boards: the slide and the press table. By assumption, the geometry of both of these boards, as well as the SMED tool itself, are made according to the technical documentation, which assumes adequate manufacture tolerances for individual elements and dimensional chains. The individual errors of the controlled geometrical features of the elements are within the assumed tolerances. The third error component results from the precision of the forging instrumentation manufacture. An additional factor affecting the formation of the joggle error is the fact that the forging process is a dynamic phenomenon. The occurring forces cause elastic deformations of the particular elements being part of the instrumentation, whose presence is difficult to determine and consider at the stage of design, or during static measurements. Also, the occurrence of high side (horizontal) forces during the making of a forging in a two component system should be taken into consideration, due to the fact that the forging is a long and thin element (Fig. 2.a).

2.2. Scientific assumptions and methods

The determination of the causes of error resulting in the production of defective forgings was conducted in several stages. At the first stage, a standard (norm-based) measurement of the key elements of the press was made, including the slide, the table and the guides, with the use of classic measurement methods, as well as the component elements of SMED and the whole system in an open and close position, after the assembly on the press by means of 3D scanning. The following stage involved an analysis supported by numerical modeling of the process, as well as with the use of a fast system of measuring the dynamic deformations. The last key stage was, however, the application of the indirect method proposed by the authors, consisting in a measurement of the forging defects – joggles of the forgings made on the press, which provided a possibility to propose a solution of eliminating the geometrical errors of the products.

What is more, the possibility of occurring joggles of the slide and table axis as a result of elastic deformations in the mechanisms of the press was excluded due to the frame characterizing in high rigidity – it was assumed that, in the case of insufficient rigidity of the frame, a problem with the obtained precision would have been encountered already before the modernization of the station.

For the measurements of the forgings collected from the forging process and the component elements of the forging aggregate, a measuring arm ROMER Absolute ARM 7520si with an integrated RS3 scanner as well as the Polyworks software enabling 3D scanning were selected. The device makes it possible to perform contact measurements with the use of a contact measuring probe as well as non-contact measurements by means of a linear laser scanner RS3 integrated with the arm, which provides the possibility to collect up to 460 000 points/s for 4600 points on the line with the linear

frequency of 100 Hz and with the declared measurement accuracy of the scanning system being in agreement with the norm B89.4.22, equaling 0.053 mm.

For the numerical modelling of the forging process, the computing package ForgeNxt3.0 was used. To compare and for some of modelling was used Qform VX 9.0.10.1 with conditions similar to Forge NX software. The following boundary-initial conditions were assumed. A thermo-mechanical 3D model with rigid tools (die inserts – elements with a heat exchange) was developed. The geometry of the tools, the preform as well as the other technological parameters of the process were implemented into the program based on the original 3D models and operation sheets. For the discretization of all the tools, 488346 elements of the QUAD4 type were applied, whereas for the charge - 16532 elements, also of the QUAD4 type. For input material, automatic grid remeshing and rezone was applied. The shift velocity of the upper die inserts was assumed according to the kinematic parameters of the applied crank press Massey 2500T. The tribological conditions were assumed on the basis of the Tresca bilinear friction model with the factor of 0.3 for all the work surfaces of the tools, which was identical like in the industrial process, where a lubricant of a water with graphite solution was applied. The temperatures of the tools were assumed, measured by means of a thermovision camera Flir T440, equalled 250 °C, and of the charge material - 1150 °C. The times of the consecutive operations were determined by means of a camera with the option of recording 300 frames per second. The recorded average forging cycle of one forging (3 operations) at automatic work equalled 17 seconds. The heat transfer coefficients in the contact between the charge material and the tool material as well as with the environment were assumed as follows: 25 and 0.4 kW/m²K, respectively. The Forge software uses the Norton-Hoff law of plastic flow as a constitutive equation. The model of the material, steel C45, was collected from the Forge “FPD Base 1.3” database. Detailed information related to additional conditions can be found in [52].

For the precision analysis of the press movement together with the mounted forging instrumentation, the mobile system ARAMIS was used for non-contact three-dimensional dynamic measurements, in the variant equipped with video cameras with the resolution of 6 Mpx and a data acquisition module GOM Testing Controller, which makes it possible to take photographs with the maximum resolution of 335 Hz. In the applied configuration, the system provides the possibility to perform measurements in the measurement field of 1110 x 1110 x 1345 mm. The system makes it possible to perform dynamic measurements of objects with complex geometry and large sizes. Based on the photographs taken by means of digital cameras, the system recognizes the surface structure of the measured object or the special markers (relevant coordinates are assigned to each pixel in the photo). The system, after a sequence of movement, analyzes the recorded image and calculates the displacement and deformations on their basis [53].

3. Discussion of results

In the first place, the agreement of the manufacture of the particular component elements of the SMED device was analyzed separately, based on the technical documentation, as well as in the open and closed position on the press with the use of 3D scanning. Next an evaluation of the effect of clearances and dynamic deformations of the press as well as the force distribution, displacements, velocity of material flows during the forging process was made through FE modelling. Finally, due to the lack of satisfactory results, the proprietary method of indirect measurement with the use of 3D reverse scanning was proposed, which allowed to solve the problem of errors of forgings and, on this basis, to introduce improvements and design changes.

3.1. Results of analyses for particular CMED system components

In order to verify the press according to the norm ISO 6899:1984, examinations of the perpendicularity of the upper board in respect of the lower one were performed through a measurement by means of classical metrological tools. A time sensor was permanently fixed to the upper surface in the central point of the press, and an angular gauge was placed on the lower one. Through the movement of the slide, the deviations on the sensor were verified in the whole stroke range of the device. The measured perpendicularity deviations on the length of 254mm did not exceed the value of 0,03mm, either in the right-sided or left-sided measurement. Additionally, with the use of the 3D scanning method, a dimensional control of the key elements being part of the SME system was performed. Fig. 4 shows exemplary deviation maps (SMED system components-) of the case and the upper board presented in reference to the nominal CAD model.

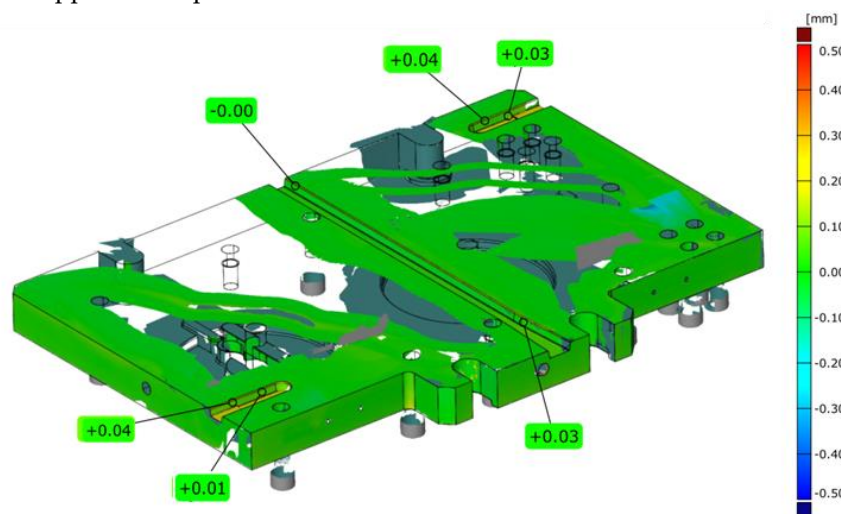


Figure 4. An example of measurements with view of colour deviation map of 3D scans of lower cassette.

The analyses of the performed measurements made it possible to clearly confirm that these elements had been manufactured according to the technological documentation. The selected key geometrical features were within the assumed fields of dimensional and shape tolerances. For example, the most important width of the key groove measured by way of scanning equalled: 0.05 mm, respectively, in reference to the figure tolerances equalling: 0.08 mm. The deviations from the nominal CAD model visible in the figures in the form of the blue and red colour prove the presence of acceptable deviations on the surfaces (non-cooperating), for which only roughing was to be applied. However, it should be noted that such a geometrical analysis of the particular components, even deepened by an analysis of the dimensional chains, does not make it possible to obtain a clear answer to whether the horizontal side forces as well as the inertial forces occurring during the forging process can negatively affect the obtained geometry of the product. It should also be emphasized that the quick exchange system SMED was designed as a prototype and this can also provide results which are difficult to analyze. That is why the next stage of research was performing 3D scanning of the SMED device mounted on the press.

3.2. Analysis results for particular SMED system components in the press, in the upper and lower slide position

The following step in the measurements of the analyzed forging bay was an analysis of the position change of the SMED system components on the press in the simulated forging process,

considering the fact that the guides in the press have the biggest clearance in its upper part and this value decreases with the slide's movement downwards, towards the contact with the tools. The differences after the slide comes back to the top upper position can result from a different position which it assumes then, where the initial movement has no significant effect on the process. It is, however, crucial that the system move repeatably in the lower extreme position of the slide. To that end, the 3D scanning method was applied to analyze the position in the lower extreme. In this case, there is no possibility to perform such a measurement in the real forging process. In order to simulate the forging process, a decision was made to cancel the clearances on a special element shown in Fig. 5a, placed in the area where the finishing tools should be located. A series of measurements was made for the same load to determine the repeatability. The performed measurements made it possible to obtain a colour map of deviations (Fig. 5b).

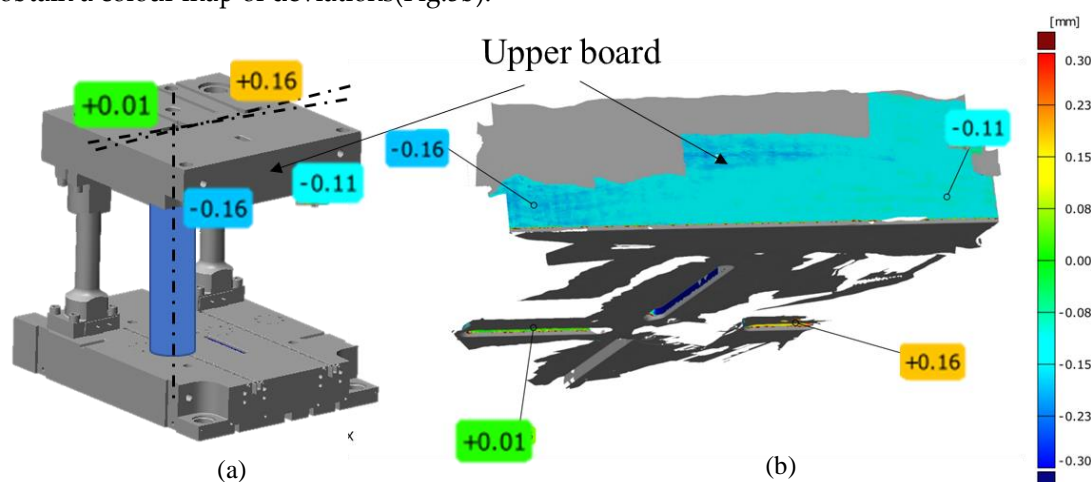


Figure 5. Results of the analysis of the change in the position of the SMED system components on the press in the simulated forging process: (a) diagram, (b) color map of deviations with 3D scanning results.

On the basis of the shown representative results, we can notice that, after the housing of the SMED device has been closed (without the tool cases), a shift from the value of 0.11 mm to 0.16 mm takes place to the right, causing a twist by a small angle value visible on the front of the board. However, while analyzing the position of one of the side walls of the cotter beds on the upper SMED board (view from the bottom), we can notice a shift from the nominal CAD values to the values from +0.06 mm to 0.16 mm, which makes it possible to mark the potential position of the axis of the board's twist. The performed analysis for a series of measurements confirms that the slide together with the SMED upper board moves repeatably in the forging process.

3.3. Results of dynamic displacements

Independently of the obtained 3D scanning results, an attempt was made to analyze the displacement of the so-called "marker – reflective - points" – placed on different elements of the press in order to examine the latter's rigidity as well as the distribution of forces during the forging process. Fig. 6 shows the measurement station used to examine the movement dynamics of the robotized press during forging as well as a diagram of the cases with tools with superimposed reference points. The environment in which the measurements are performed is burdened with a large amount of vibrations, which causes movement of the base in respect of the sensor of the Aramis measurement system. In order to eliminate them, measurements were carried out with the use of an algorithm of

movement correction of the rigid body incorporated into the measuring device on the basis of the measurement of the reference points connected with the base.

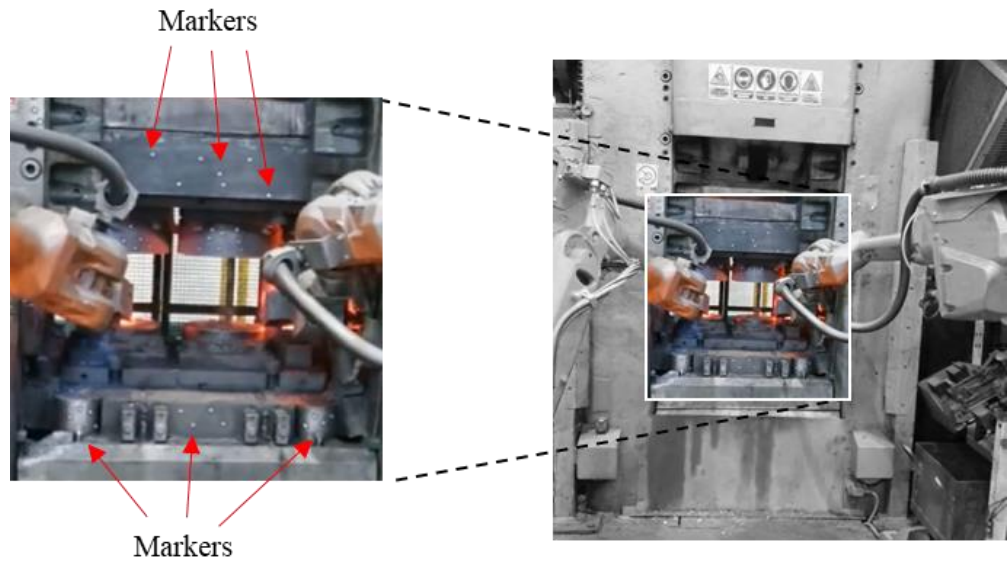


Figure 6.View of the press frame with visible markers.

In order to perform an analysis during the forging process, a measurement of four forging cycles was made, visible in the form of sinusoidal changes in the values of component position x of the selected reference points connected with the upper section (Fig.7b).

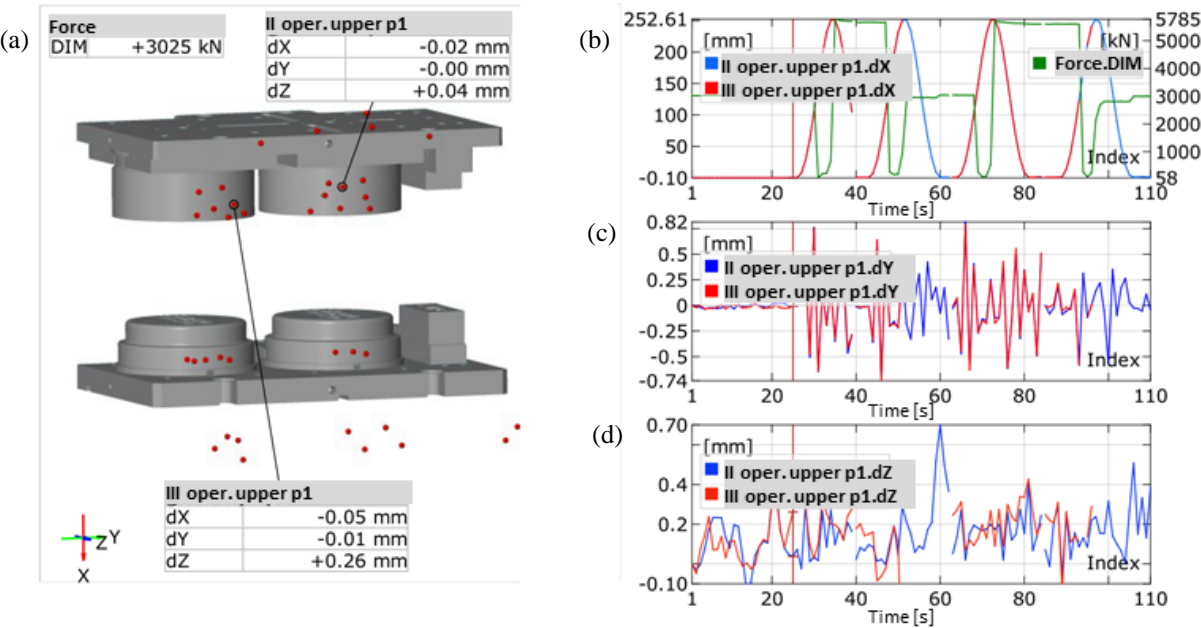


Figure 7. Example of the use of dynamic systems for the measurements of the forces and displacements in a forging operation: (a) measurement result for an open press, (b) change in the position value in axis x of selected reference points c) change in the position value in axis y of selected reference points, (d) change in the position value in axis z of selected reference points.

The performed measurements made it possible to record three components of displacement of the reference points connected with the tools mounted in the cases (Fig.7b to Fig.7c). The maximal force values were implemented through communication with the machine equipped with tensometric sensors and correlated with the analysis through the element connecting the systems,

which recalculates the crank angle into the movement of the slide. Figure 7 shows additionally the assembly of the upper and lower case, where we can see the shift component values at a given moment of the forging press slide movement. The press body was assumed as an immobile base and the shifts of the upper part were examined. The press stroke was assumed to be about 252 mm, which is in accordance with the machine specification, where the nominal value is 254mm, with an option of regulation +/- 6.5mm, depending on the height of the forging tools. The maximal deviations in direction Y, being transverse to the machine operator, oscillated within the scope of up to 0.8mm (Fig.7b). The result occurred in the area of free movement, where the guidance was exclusively the effect of the cooperation between the slide guides and the upper and lower board columns. At the moment of contact between the mountings guiding the tools, before the contact with the material, the clearance was minimized to 0.25mm, with the tendency for shifts towards the finishing impression at the final stage of forging. In the direction of axis Z (Fig.8d), being longitudinal in respect of the operator, the indications equaled 0.4mm in the direction of the operator in a dead motion and 0.1mm in contact as well as at the end of the process. The displacements after a few beats of the press, showing translation in the extreme open position gave the following results: 0.00 mm in Y and 0.04 mm in Z for the rouging insert as well as 0.01 mm in Y and 0.26 mm in Z for the finishing insert, in the case of a static measurement (Fig. 7c and Fig.7d). This confirms that the guides in the press have different clearances, depending on the height. The clearance is the smallest at the height of the slide's movement for the close press.

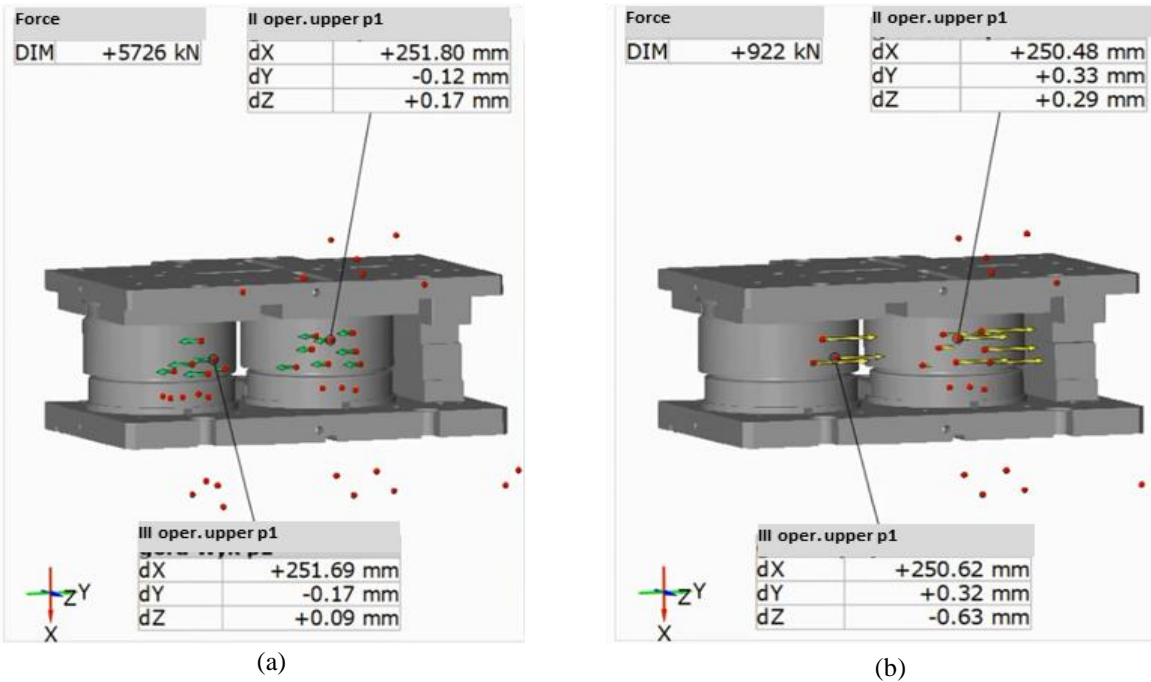


Figure 8. Vectors of upper insert displacements: (a) before reaching the lower stroke position (dx 251,69), (b) after reaching the lower stroke position (dx 250.62). The maximal deflection in 60 s of movement in the direction of Z probably resulted from the resonance caused by the machines at a small distance from the examined area. Additionally, we can notice that the recorded diagrams characterize in big randomness, which makes a thorough analysis significantly difficult. An analysis of the shift values at the moment of contact between the tools and the formed material as well as directly after its end was performed (Fig. 8). The measurement method

was based on dividing the examined points into the upper and lower ones, where the lower parts were assumed as an immobile base, and the upper parts - as free ones.

At the moment of reaching the extreme lower point of the press slide, the upper tools demonstrated deflections of 0.12 mm on the roughing tool and 0.17 mm on the finishing tool, in the direction of the left side of the press, as well as 0.17 mm and 0.09 mm in the direction of the operator (Fig.8). After the end of the cycle and beginning of the return movement, the values increased, with a change in the direction to 0.33 mm and 0.32 mm towards the right side of the press, and 0.29 mm towards the operator for the second operation, while 0.63 mm for the third one.

Much smaller deflections were demonstrated by the examination of the second part, where this same points on press body were assumed as the base, while the displacements of the lower section underwent verification (Fig.9). The values were verified at the moment of active forming on the roughing insert demonstrating the biggest deviations. The displacement towards the back of the press equaled 0.02 mm towards the left side of the device before forming (Fig.9a) and 0.16 towards the right side after forging during the return cycle (Fig. 9b). In the longitudinal directions, the values were: 0.06 towards the back of the press and 0.02 towards the operator. A comparison of both variants shows a much bigger rigidity of the lower tool packets as well as a tendency to maintain the base position. This is caused mainly by the static assembly of this part as opposed to the upper ones, where the dynamics cause bigger deviations from the base axis.

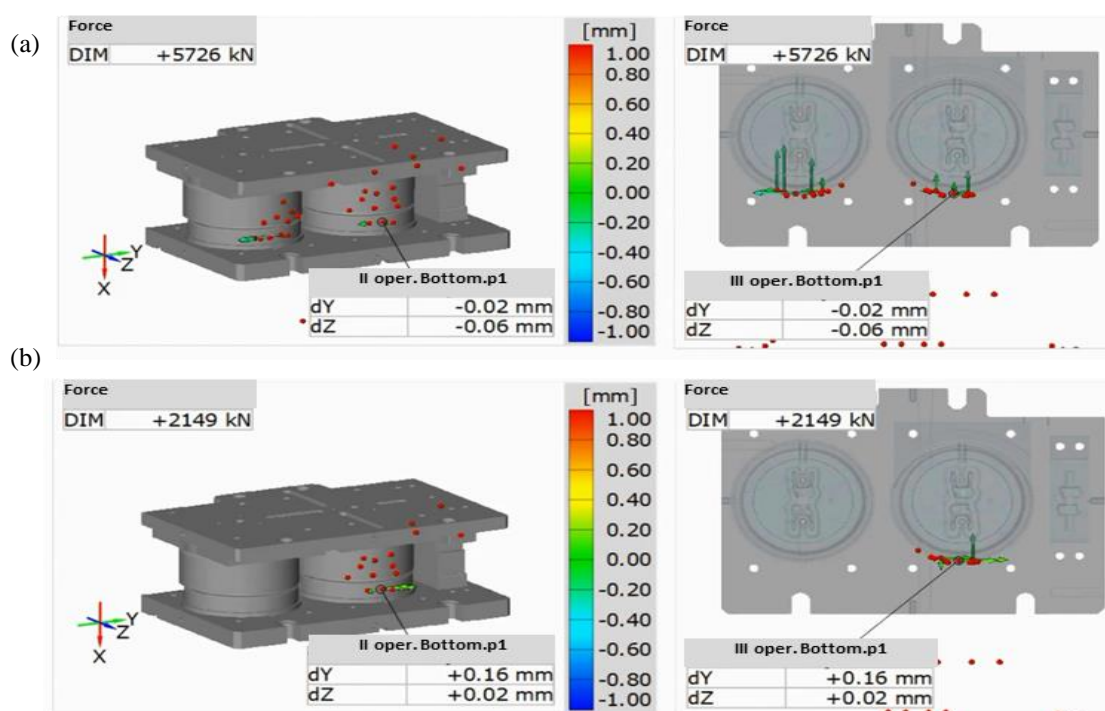


Figure 9. Vectors of lower insert displacements: (a) before reaching the lower stroke position, (b) after reaching the lower stroke position.

The examinations included an analysis of the vibrations of the base and the measurement results were corrected by means of an algorithm for the movement correction of the rigid body built into the measuring device (Fig.10). The obtained results point to a big measurement error in the process without a load, where the vibrating masses as well as the machines located in the environment (double-acting stamps and crank presses) introduced significant vibrations onto the floor on which the measurement was being made. In the extreme point of movement, the effect of

vibrations on the position of the scanner equaled up to 0.7mm in respect of the base position, from which the image calibration was performed.

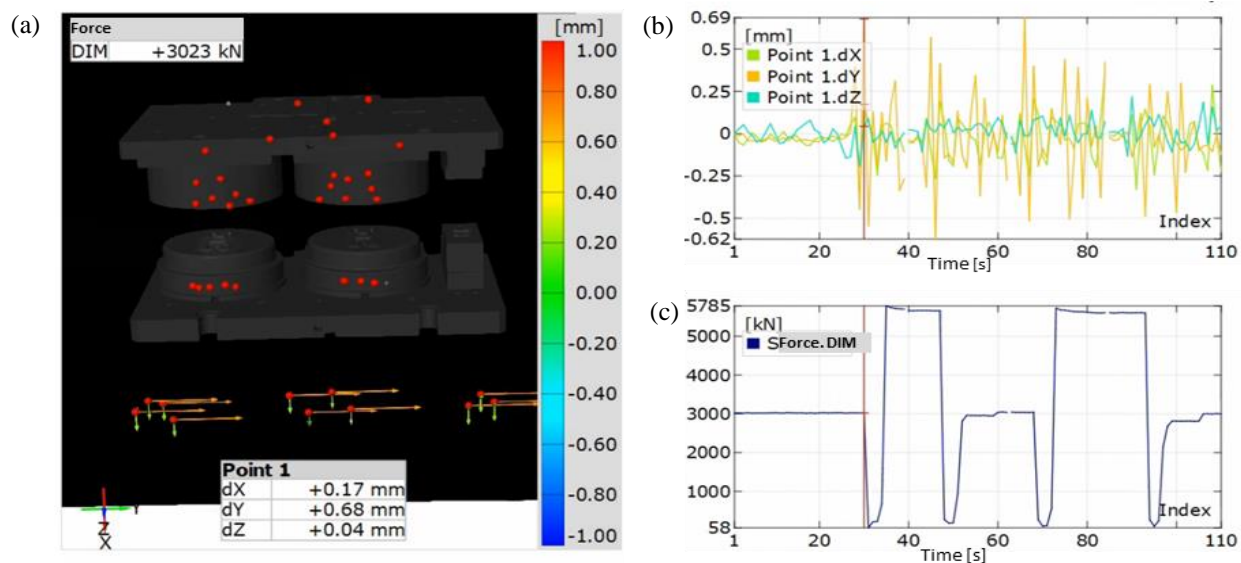


Figure 10. Analysis of vibrations of the measuring device without a load and during the operation.

In view of the measurement results correlated with the variables introduced through the floor's operation onto the measurement device, the implemented method should not be a basis for the determination of the displacements, as the obtained results can significantly deviate from reality, depending on the floor's vibration level at the moment of measurement. In turn, in the case of a prolonged examination, owing to which it is possible to obtain the exact course of vibrations, and assuming a harmonic and repeatable operation of the machines around the examined area, it is theoretically possible to perform an analysis by introducing a correction of movement based on the measured values. However, it is difficult to determine whether the introduced corrections enable a complete elimination of the floor vibrations and how much this affects the measurement results. In the examined case, due to the character of randomness, the reading error of indications was not eliminated.

3.4. Numerical modelling results

Numerical modelling of the forging process was also performed in order to determine the value of horizontal forces occurring during forging, especially during the roughing operation, where the highest vertical forces were recorded (along axis z), which equalled over 400tons (Fig. 11). Despite the fact that the side (horizontal) force values are not high in respect of the vertical forces, taking into account the dynamic character of the forging process (deformation time 0.2s), they can be of big importance, especially in the case of small clearances between the particular elements of the press itself, as well as the connection of the press with the SMED device.

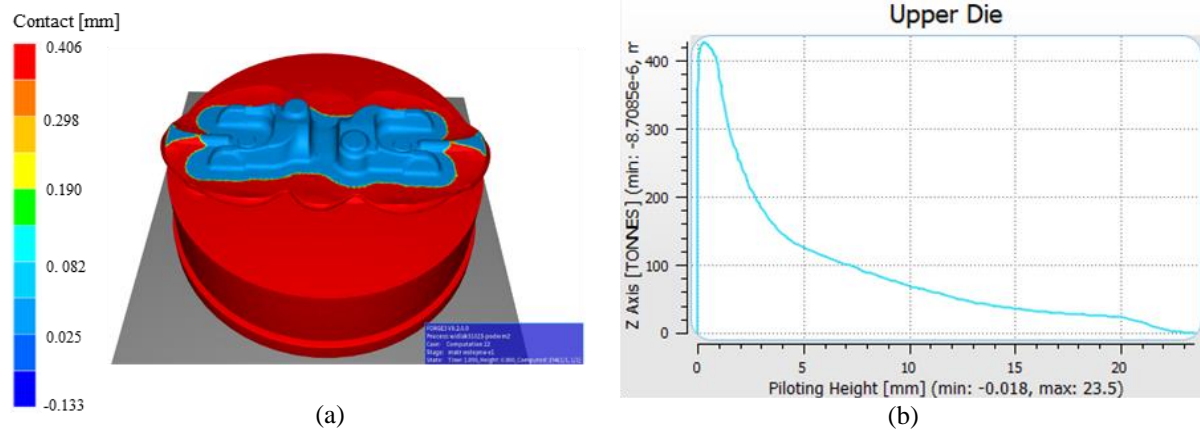


Figure 11. Results of analysis with the use of numerical modelling: (a) contact of the forging after the second forging operation, (b) course of forging forces in the function of displacement in the vertical direction.

In turn, the values of horizontal forces were much lower: 0.8ton (along axis x) and a little over 1 ton (along axis y), which has been shown in Fig. 12.

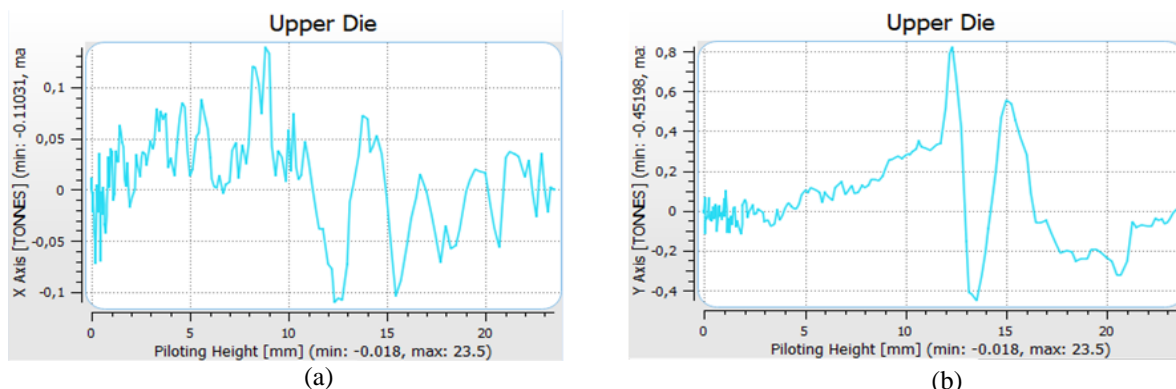


Figure 12. Results of analysis with the use of numerical modelling: (a) course of forging forces in the function of displacement in the horizontal direction in axis X, (b) in the horizontal direction in axis Y.

Also, the vectors of the material's displacement rates in the roughing operation, where the material's deformation is the biggest, were analyzed. The analysis showed a high coefficient oscillating around the values of about 500 mm/s in the vicinity of the forging's arms, with a tendency for clockwise twisting (Fig. 13a). After the analysis of the flow rate between the sides of the forging (Fig. 13a), we can observe a difference at the level of 50-80mm/s, which implies a tendency for unidirectional elastic rotation of the upper tools in respect of the lower ones in the production cycle. This is confirmed by the analysis of the rate distribution in direction Y (Fig. 13b), as, based on the results, we can notice that the highest rate values (with opposite signs) can be observed in the lower left and upper right part. The simulation shows higher values in the left lower part and in the right upper one. Also the high deformation rate in the roughing operation in some places equalling almost 200 s-1 points to high deformation rates, which, in combination with big masses and inertia, can be the cause of defects on the forgings.

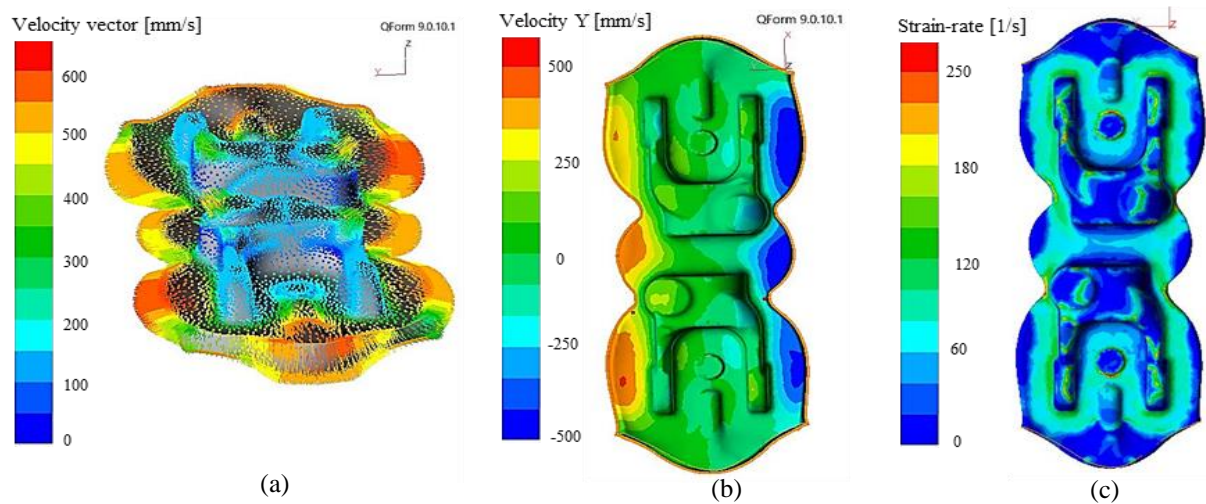


Figure 13. Results of numerical modelling: a) material flow rate during roughing, b) material flow rate in the transverse direction, c) deformation rate.

In order to confirm the results obtained on the forging model, a simulation was also performed on the tools by means of an analysis of deformations caused by the forging force (Fig. 14).

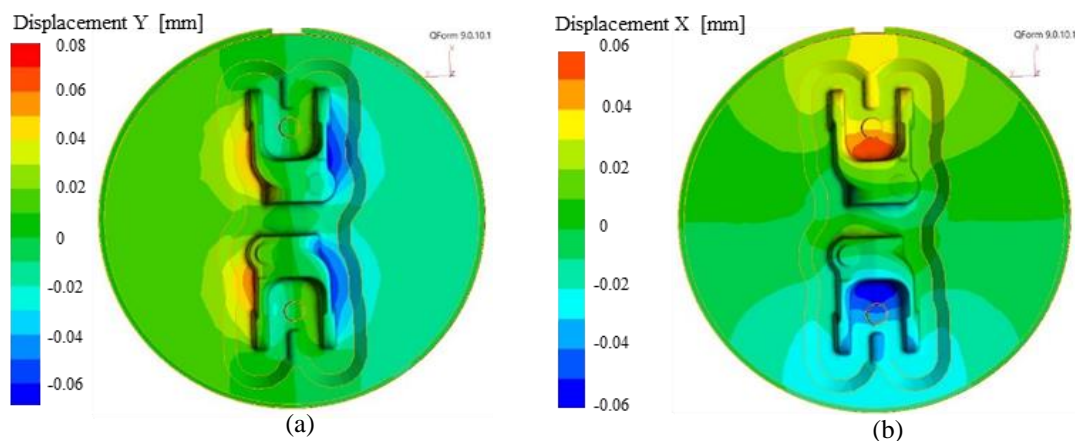


Figure 14. Results of modelling: a) transverse displacement of the tool, b) longitudinal displacement of the tool.

In the case of the transverse direction, the values were estimated at the level of 0.07mm in the direction which is in accordance with the rate results on the forging, and 0.04 in the opposite directions. And so, a bigger component of the force is applied one-sidedly, which causes lack of symmetry of the system and can result in a tendency for twisting in the dynamic movement. For the other examine direction, the displacement were maintained at the level of 0.05mm on both sides with a slight angular shift of the central point in the direction identical to the transverse shifts.

Based on the presented test and simulation results, it can be stated that the classic approach to solving such a complicated issue, due to very complex kinematic chains, is not sufficient. The performed measurements with the use of 3D scanning techniques of the particular key elements of the system which can possibly cause forging defects did not show any differences in respect of the technical documentation, and their values are within the assumed tolerance fields. It should be noted that the observed values of joggles and twists are relatively small (at the level of 0.2-0.3 mm) in respect of the sizes of the key elements of the press and instrumentations, where the manufacture tolerance for the smallest elements from the kinematic chain (base holders) is at a half of this level. In turn, in

the case of larger table tops, the manufacture tolerance is at the level of 0.05-0.2mm. Nevertheless, as it was demonstrated by examinations with the use of numerical modelling of the forging process, as well as a system for dynamic measurements of displacements, in the case of a long forging of this type, horizontal side forces occur, which, with high deformation rates (0.2s) and very high inertia of the whole system, can be of big importance.

That is why, in order to analyze the errors in the position of the boards facilitating the tool replacement (from the SMED system) in respect of each other, a decision was made to use the forgings. This method will make it possible to clearly determine the shift of the die set during the forging process, which causes (direct effect on the element quality) the specific errors in the form of joggles visible on the forgings. An advantage of the possibility to measure only the forgings is the fact that their dimensions are relatively small and they can be collected without difficulties from the forging process. These forgings describe the state of the forging aggregate in the extreme lower position of the slide under load. In order to eliminate random errors, an analysis will be performed on more series of periodically collected forgings and the measurement values will be averaged. Scanning the collected forgings will make it possible to determine the dimensions of the joggles, whose analysis will enable a correction of geometry, which, introduced into the forging bay, will, in turn, make it possible to obtain a forging being within the required dimensional tolerance scope

3.5. Application of the indirect method based on 3D scanning of a forging set

Fig. 15 shows photographs of two series of sets of cyclically collected pairs of consecutive forgings for the analysis of the joggle parameter with the use of 3D scanning. Both in the case of the first and the second series, every 100 items, two consecutive forgings were collected, in order to eliminate random errors (for example, the 100th and the 101st forging were collected), up to 500 items from the process, from instrumentation with geometrical joggle defects (dimensions before the correction – series I). The size of each series was assumed as 500 items, as, based on the analysis, after that period, intensive wear of the tools occurs, which could interfere with the analyses.

The second series (series II) of also two consecutive forgings (Fig. 15f to Fig 15j) was collected in a similar cyclic manner after introducing a correction of the instrumentation geometry in order to verify the properness of the introduced changes.

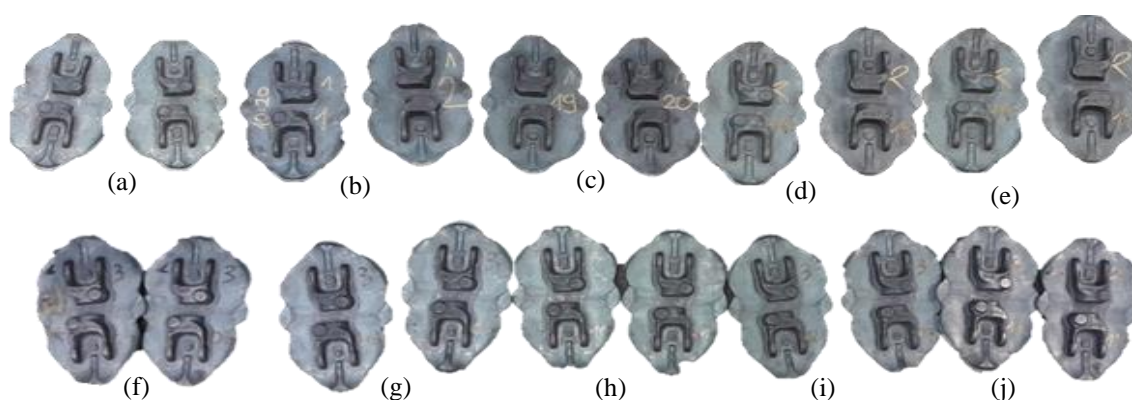


Figure 15. View of two consecutive forgings collected from the process: (a) the 100th and 101st item from series I, (b) the 200th and 201st item from series I, (c) the 300th and 301st item from series I, (d) the 400th and 401st item from series I, (e) the 500th and 501st item from series I, (f) the 100th and 101st item from series II, (g) the 200th and 201st item from series II, (h) the 300th and 301st item from series II, (i) the 400th and 401st item from series II, (j) the 500th and 501st item from series II.

Fig. 16a shows the assumed denotations for the joggle analysis and an exemplary compilation of results for the joggle defect for the whole forging consisting of two yokes forged in a two-component system. By means of the denotations assumed in Fig. 16b, exemplary results of the analysis of data obtained from 3D scanning for the joggle defect of a single forging from a two-component system were demonstrated (Fig.15).

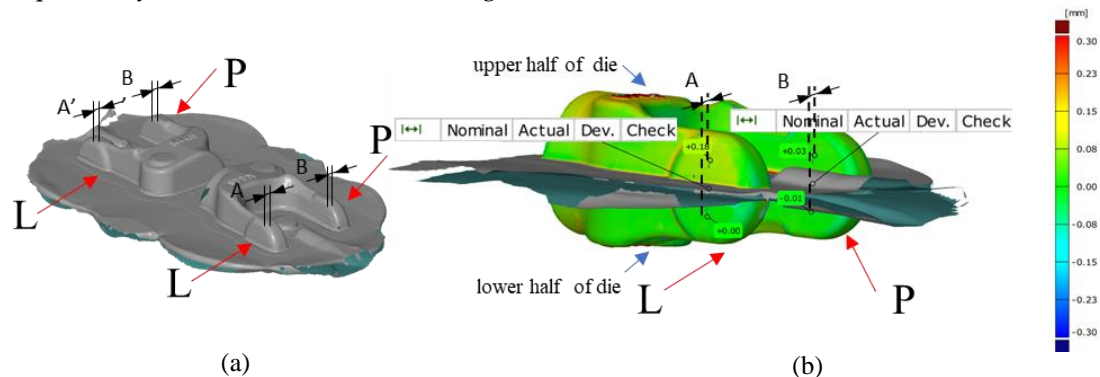


Figure 16. The View of: (a) Exemplary results of the joggle defect analysis: (a) the whole forging, (b) half of the forging, shown on a colour map of deviations.

Fig. 16b shows the two arms of the yoke – left (L) and right (R). For the analysis, 4 points were selected (Fig. 16b), two on each half (upper and lower) of the forging of the left (L) and right (R) arm, lying at a symmetric distance from the parting plane of the nominal forging. In the upper part of the left arm, we can notice a deviation at the level + 0.18 mm, whereas in the lower one – 0.00 mm, which globally causes the formation of the joggle defect (denoted as A) measured along the nominal axis X at the level of 0.18 mm. Analogically, on the right arm, at the top, we can see a deviation at the level of plus 0.03 mm, and at the bottom - minus -0.01 mm, which causes the formation of the joggle defect (denoted as B) measured along the nominal axis X at the level of 0.02 mm. The difference in the results for the left arm L and right arm R is caused by an asymmetric shift of the upper half and the lower die, which proves the existence of joggling and twisting.

In order to determine the resultant of the position deviation occurring at the moment when the slide is located in the extreme lower position consisting of a joggle component X and Y, it is necessary to determine the joggle value in the direction of axis Y analogically to the way it was carried out for the direction X (Fig. 17).

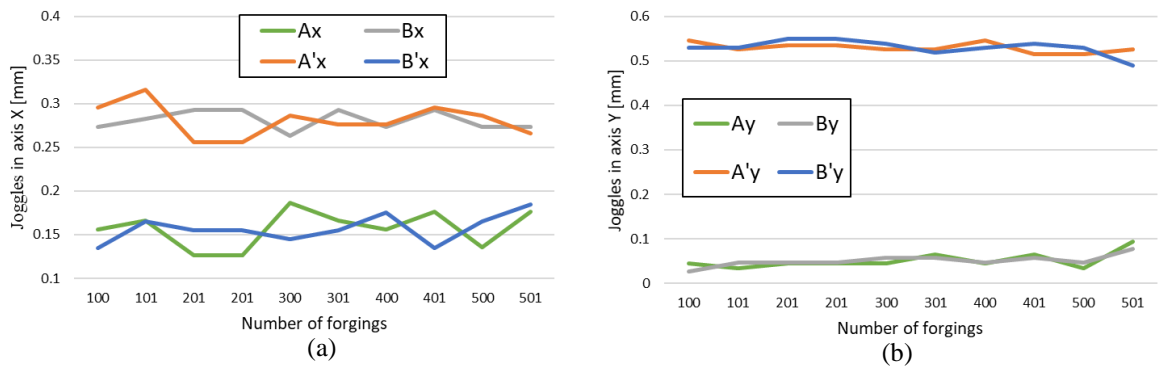


Figure 17. Diagram of the joggle values of two consecutive forgings cyclically collected every 100 items from the process, for the forging bay with geometrical defects: (a) components calculated in axis X, (b) components calculated in axis Y.

To that end, a 3D scanning measurement was performed for two consecutive forgings, which were cyclically collected every 100 items from the process, from the instrumentation (dimensions before correction) with geometrical defects in the form of joggle. Based on the analysis of the measurement data, diagrams were developed for forging series I (Fig.17) of the values describing the components X and Y of the joggle for four points A, B A' and B' of two consecutive forgings cyclically collected every 100 items from the process, from the instrumentation with geometrical defects.

For each of the four pairs of values calculated for two consecutive forgings (e.g. the 100th and 101st) cyclically collected every 100 items, we can notice that, for example, the shift of point B in both axes, X and Y, is bigger than the value of acceptable deviation for the forging (0.2 mm). What is more, based on other measurement points, we can see that their deviations in both directions are different, which suggests not only the presence of joggle but also of twisting of the upper part of the forging in respect of the lower one. Good news acquired from the performed analysis is that the particular values change, yet their scatter is not higher than 0.04 mm, which additionally proves the repeatability of the process. In order to increase the accuracy and eliminate the errors, a decision was made to average the values for each of the analyzed points separately and assume the average value of the joggle vectors for further analysis. This way, the joggle resultants were obtained for four selected points (blue vectors), shown in Fig. 18c, in respect of the nominal positions of the points of the lower half of the forging (die) (Fig.18b). The obtained results, after being connected with lines, make it possible to construct a characteristic geometry in the form of a rhombus ABA'B' (Fig.18d). Additionally, on the intersection of lines A'-D' and B'-C', point O' was marked for the upper half of the die and analogically for the nominal positions O of the lower half of the die. Also, it was noticed that, in order to correct the tool geometry, it is necessary to relocate the rhombus constructed based on the values described by the joggle parameter A₁B₁A'₁B'₁ (Fig.18c, upper half of the forging) to the position created based on the nominal values (Fig. 17b, lower half of the forging in the form of a rhombus ABA'B'). After the rhombi have been relocated, the center O will overlap with O', which will enable a rotation by the angle α marked in the figure (Fig. 18d). This made it possible to determine the two desired values of the joggle vector components $OO'_x = 0.219$ mm and $OO'_y = 0.290$ mm. Additionally, it was established that the twist axis crosses point O' by the angle $\alpha = 0.3145^\circ$. The analysis was performed with the use of CAD systems (solid_works). The determined values describe the shift together with the twist of the upper and lower half of the forging, which have been additionally shown in Fig.19a as well as the concept of introducing changes in geometry. To that end, a decision was made to perform a correction of the wedges and spline ways (Fig.19b) connecting the upper and lower SMED board causing a shift according to the values of the vector components $OO'_x = 0.219$ mm and $OO'_y = 0.290$ mm, as well as a rotation around the axis crossing the point of the angle $\alpha = 0.3145^\circ$ (Fig.18a).

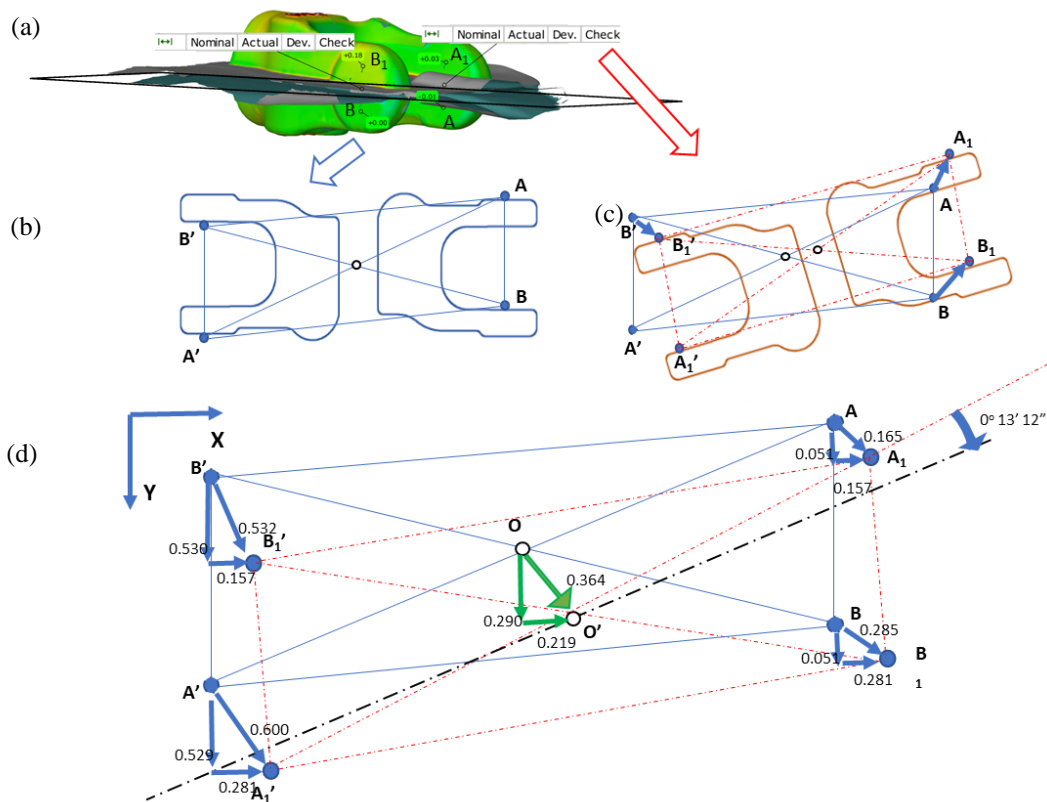


Figure 18. (a) An exemplary results of the analysis of the joggle defect for a single yoke, a diagram of a forging from a two-component system: (b) lower half of the die with the nominal position of the points, (c) lower half of the die with resultant joggle vectors, (d) Diagram of dimensional compensation with calculated values of mean joggle necessary to determine the corrections.

The changes consisted in widening the spline ways by as much as 3 mm per side as well as increasing their length (considering the new orientation) in order to increase the rigidity and stability of the connection between the cases and the boards. Introducing those changes makes it possible to correct the position and orientation of the upper and lower part of the tools in respect of each other (Fig 19).

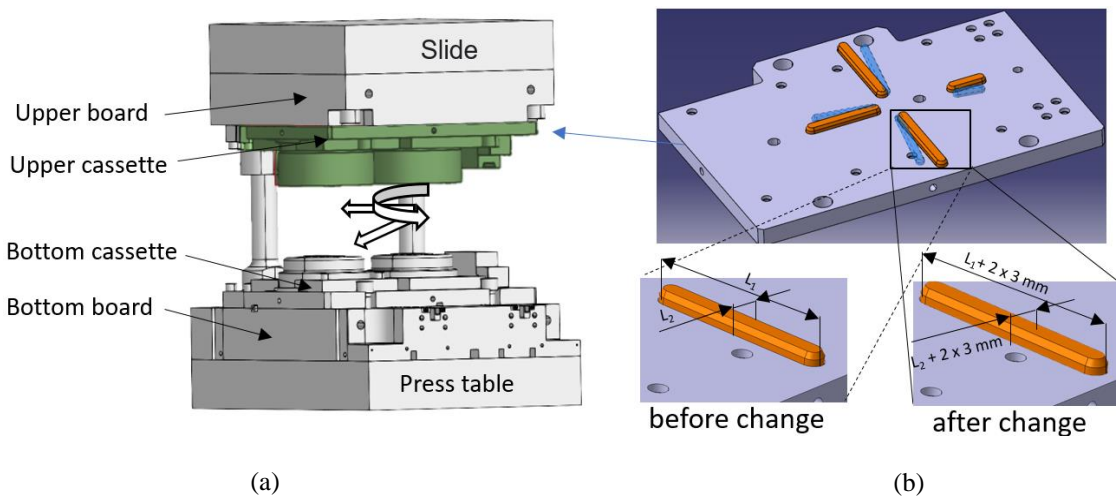


Figure 19. Concept of geometrical changes shown on a schematic diagram of the upper cassette SMED system: (a) the working space of the press, (b) introduced changes (the original arrangement/orientation of keyways are schematically marked in blue).

Such changes were introduced as the upper board and the slide were deemed as "large" and rigid elements of big masses, which causes their increased rigidity in respect of smaller boards of the SMED instrument. Additionally, the connection between the upper and lower board is beyond the guide posts, which increase the rigidity of the construction.

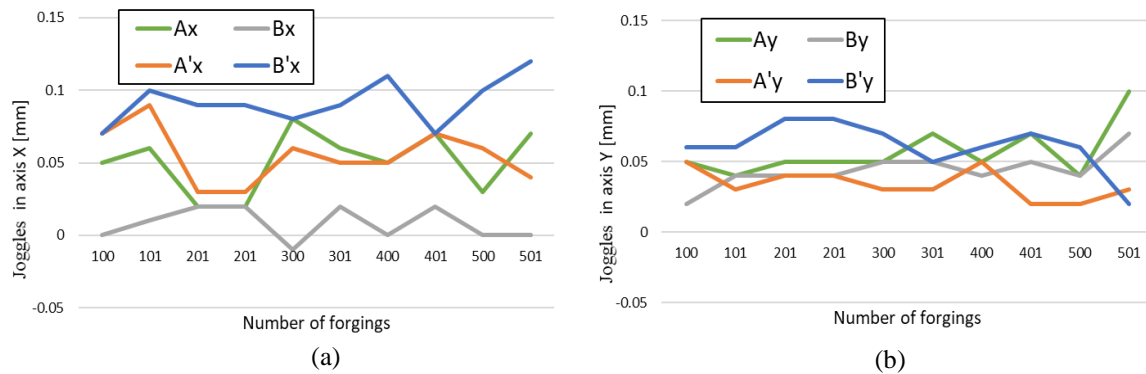


Figure 20. Diagram of the joggle values of two consecutive forgings cyclically collected every 100 items from the process, for a forging bay with corrected geometry: (a) components calculated in axis X, (b) components calculated in axis Y.

In order to verify the correctness of the introduced tool changes, another analysis of measurement data was performed for series II of forgings made by means of the tools with reduced geometry. The performed measurements with the use of the 3D scanning method made it possible to obtain results in the form of diagrams for the joggle value of two consecutive forgings cyclically collected every 100 items from the process, for the forging bay with a corrected geometry of the components X and Y (Fig.20). The obtained values confirm that the introduced changes make it possible to significantly reduce the errors by 65% in respect of the joggle values before their introduction. Fig. 21 shows exemplary results of a colour map of deviations with marked reduced joggle values determined from collected forgings in second series (Fig. 15f – 15j) .

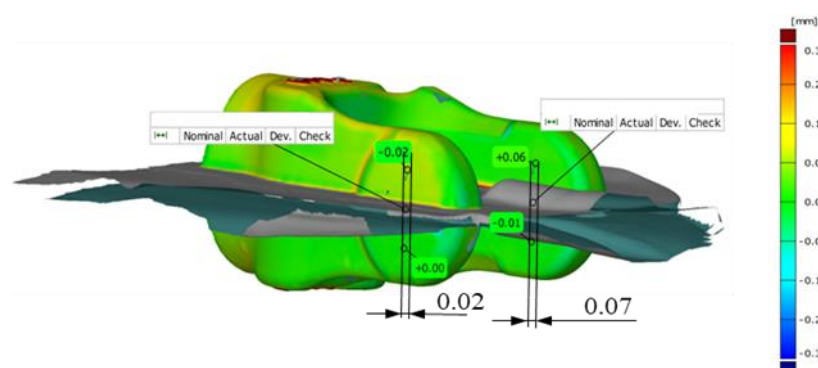


Figure 21. Exemplary results of a colour map of deviations with marked reduced joggle and twist values as a result of correctional changes in the kinematic chain.

The presented results confirm that introducing the proposed geometrical changes into the kinematic chain, determined based on the performed investigations by means of an indirect method consisting in measuring and analyzing the geometry of cyclically collected forgings, make it possible to eliminate the forging defects. It should be noted that changes in the connections were introduced only on the upper side of the kinematic chain, as, based on the obtained results (Fig. 20), this ensured

the forgings staying within the tolerance field equaling 0.2 mm with "large margins". It may be that introducing a similar solution into the lower part of the kinematic chain would cause even more advantageous changes, however, there was a concern of the side forces present during the forging process making the system over rigid as a result of long forging series and thus causing accelerated wear of the spline ways and wedges. This, however, is going to be the subject of further studies.

4. Conclusions:

The article proposes a proprietary indirect method consisting in determining difficult to eliminate forging defects in the form of joggles and twists of yoke-type forgings in a two-component system made in an automated way on a crank press. As it has been demonstrated, the results of the performed studies with the use of 3D scanning techniques of the particular key elements of the press, which may have caused forging defects, did not demonstrate any difference in respect of the technical documentation and were within the assumed tolerance fields. Nevertheless, both the investigations with the use of numerical modelling of the hot die forging process itself and those performed by means of a dynamic displacement measurement system showed that, in the case of this type of long yoked forgings, relatively small (in respect of the main direction) horizontal side forces occur, which, with very fast deformation (0.2 s) and high inertia of the whole system (many large rotating masses), can be of big importance. The results obtained from the system for a dynamic displacement analysis show that, at short time distances, as a result of the movement of the upper tools in respect of the lower ones, and with the assumption of the reference base both on the upper and lower tools, the top part of the press shifts much more than its bottom part. The highest shifts take place during the roughing operation (middle operation), which was also confirmed by the results of numerical modelling. The maximal displacement values of the tools reached even over 0.3 mm in the horizontal plane. What is interesting, higher displacement values were observed during the loading, that is right after deformation, which could have been caused by seizure of the forgings as a result of their complicated shape. Despite the numerous performed tests and their analyses based on the classic approach to the analysis of a complicated issue, due to a very complex kinematic chain, it was unfortunately impossible to perform a thorough diagnostic of the problem of forging defects occurring on the modernized forging bay. It should be noted that the analysis of the presented problem would be even more complicated if the forging process were realized manually by an operator, which would cause lack of repeatability in handling the forgings as well as introduction of additional changes resulting from the effect of the human factor.

That is why the authors have proposed a method of indirect measurements, consisting in a dimensional and shape analysis of the results of measurements obtained from 3D scanning for a few variants of production cycles, which make it possible to obtain the information necessary to correct the geometry of the kinematic chain. The performed analysis enabled the determination of the component values of the displacement vector of two halves of the die in respect of each other $OO'x = 0.219$ mm and $OO'y = 0.290$ mm as well as the torsional angle $\alpha = 0.3145^\circ$ (Fig.18). In order to perform a correction of the kinematic chain's geometry, a decision was made to introduce changes into the geometry of the wedges and splineways (Fig.19b) which connect the upper and lower board with the upper SMED board, causing the planned displacement of the die halves in respect of each other. The introduced changes consisted in widening the splineways by as much as 3 mm per side as well as increasing their length (considering the new orientation) in order to increase the rigidity and stability

of the connection between the cases and the boards. Introducing such changes makes it possible to correct the position and orientation of the upper and lower part of the tools in respect of each other. Additionally, the shapes of the wedges were changed from the conic ones to wider flatter ones (with a 30 degree phase on the height and next with a flat surface), which ideally/during the designing assumptions were to facilitate the assembly of the SMED tool in the upper board, but could also introduce additional yet small displacements and torsions of the forgings. The obtaining of geometrically and qualitatively correct products was verified by an analysis of another identical series of forgings.

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References:

1. D. Marini, J.R. Corney, Process selection methodology for near net shape manufacturing, *International Journal of Advanced Manufacturing Technology* 106 (2020) 1967-1987 .
2. M. Alves, A.F. Martins, Flexible forming tool concept for producing crankshafts, *Journal of Materials Processing Technology* 211 (2011) 467-474.
3. P. Hibbe, G. Hirt, Analysis of the bond strength of voids closed by open-die forging, *International Journal of Material Forming* 13 (2020) 117-126
4. J.F. Mull, C. Durand, C. Baudouin, A new tailored solution to predict blow efficiency and energy consumption of hammer-forging machines, *International Journal of Advanced Manufacturing Technology* 111 (2020) 1941-1954
5. B.A. Behrens, M. Stonis, N. Rasche, Influence of the forming angle in cross wedge rolling on the multi-directional forging of crankshafts, *Journal of Material Forming* 11 (2018) 31-41
6. I. Telegin, T. Shumilova, Comparing the efficiency of flowsheets for hot die forging on crank presses, *International Conference on Modern Trends in Manufacturing Technologies and Equipment*, Sevastopol Russia (2018)
7. M. Kapustova, B. Simekova, The Importance of Forging Line Modernization for Material Flow in Drop Forge Conference: 3rd Central European Conference on Logistics, Trnava Slovakia (2012)
8. X. Fang, J. Wu, X. Ou, Xue, Microstructural Characterization and Mechanical Properties of Ti-6Al-4V Alloy Subjected to Dynamic Plastic Deformation Achieved by Multipass Hammer Forging with Different Forging Temperatures ,*Advances In Materials Science and Engineering* 2019 (2019) no.6410238
9. P. Skubisz, A. Zak, M. Burdek, Design of controlled processing conditions for drop forgings made of microalloy steel grades for mining industry, *Archives of Metallurgy and materials* 60 (2014).
10. A. Gontarz, Thoretical and experimental research of hammer forging process of rim from az31 magnesium ally, *Metalurgija* 53 (2014) 645-648
11. A.M. Irisarri, A. Pelayo, Failure analysis of an open die forging drop hammer, *Engineering Failure Analysis* 16 (2009) 1727-1733
12. M. Cechura, M. Volejnick, Development and specifics of the construction of a lkmk 8000 large crank press, *MM Science Journal* 2019 (2019) 2804-2807

13. M. Hawryluk, Review of selected methods of increasing the life of forging tools in hot die forging processes, *Archives of Civil and Mechanical Engineering* 16 (2016) 845-866
14. Z. Enlai, J. Fang, Z. Sihong, Thermal modelling and characteristics analysis of high speed press system, *International Journal of Machine Tools and Manufacture* 85 (2014) 87-99
15. A. Taylan, N. Gracious, S. Gangshu, Cold and hot forging fundamentals and application. *ASM International Asm metals handbook* 14 (2005) 337-338.
16. K. Lange, L.Cser, M. Geiger, T.A.G. Kals, Tool life and tool quality in bulk metal forming, *Proceedings of the Institution of Mechanical Engineers Part B: Journal of Engineering Manufacture* November 207 (1993) 223-239.
17. H.S. Yan, W.R. Chen, A variable input speed approach for improving the output motion characteristics of Watt-type presses, *International Journal of Machine Tools & Manufacture*, 40 (2000) 675-690.
18. M. Hawryluk, M. Zwierzchowski, M. Rychlik, Analysis of the industrial process of a producing a lever-type forging used in motorcycles, *Archives of Metallurgy and Materials* 64 (2019) 1421-1432.
19. N.A. Raikar, Reduction in Setup Time by SMED Methodology: A Case Study. *International Journal of Latest Trends in Engineering and Technology* (2015) 56-60.
20. R.M. Sousa, R.M. Lima, J.D. Carvalho, A.C. Alves, An Industrial Application of Resource Constrained Scheduling for Quick Changeover, *IEEE International Conference on Industrial Engineering and Engineering Management* (2019) 189-193.
21. S. Shingo, *A Revolution in Manufacturing: The SMED System*. Cambridge, MA: Productivity Press (1985).
22. K. Namyong, O.I. Yeong, H.S. Wook, Advanced disk-forging process in producing heavy defect-free disk using counteracting dies, *International Journal of Material Forming*.
23. F. Meng, C. Labergere, P. Lafon, Methodology of the shape optimization of forging dies, *International Journal of Material Forming* 3 (2010) 927-930
24. R. Assaf, T. Haddad, An Application of Single Minute Exchange of Die Approach in an Aluminum Profiles Extrusion Production System: Case Study, *International Journal of Scientific Research and Innovative Technology* 4 (2017)
25. Z. Gronostajski, M. Hawryluk, M. Kaszuba, Measuring & control systems in industrial die forging processes, *Eksplotacja i Niezawodność – Maintenance and Reliability* 3 (2011) 62-69
26. D.C. Zhou, S.J. Yuan Z.R. Wang, Defects caused in forming process of rotary forged parts and their preventive methods, *Journal of Materials Processing Technology* 32 (1992) 471-479
27. G. Banaszek, S. Berski, H. Dyja, Theoretical Modelling of Metallurgical Defect Closing-Up Processes During Forming a Forging, *Journal of Iron and Steel Research International* 20 (2013) 111-115
28. V. Lazic, A. Sedmak, S. Aleksandrovic, Reparation of the damaged forging hammer mallet by hard facing and weld cladding, *Technicki Vjesnik-technical gazette* 16 (2009) 107-113
29. H. Dyja, G. Banaszek, S. Berski, Effect of symmetrical and asymmetrical forging processes on the quality of forged products, *Journal of Materials Processing Technology* 157 (2004) 496-501
30. L.A. Mortaio, L.A.M. Riascos, A low cost retrofitting technique for mechanical presses, *Conference: 24th IEEE International Symposium on Industrial Electronics, Rio de Janeiro, Brazil* (2015)
31. Y. Cen, Y. Sun, D. Yang, Investigations on the dynamic characteristics of a planar slider-crank mechanism for a high-speed press system that considers joint clearance, *Journal of Mechanical Science and Technology* 31 (2017) 75-85.
32. PN-M-55693:1970 - wersja polska Maszyny do obróbki plastycznej metali (Polish version Machines for metal forming), Prasy korbowe ramowe jednopunktowe ogólnego przeznaczenia (Crank, frame, single point and general purpose presses), Sprawdzanie dokładności (Checking accuracy)
33. ISO 6899:1984, Acceptance conditions of open front mechanical power presses — Testing of the accuracy .
34. Machine tools safety — Presses — Part 1: General safety requirements.
35. ISO GPS 10360-4:2000 Geometrical Product Specifications (GPS) – Acceptance and Reverification Tests for Coordinate Measuring Machines (CMM) – Part 4: CMMs used in Scanning Measuring Mode.
36. X. Wu, Y. Sun, Y. Wang, Dynamic analysis of the double crank mechanism with a 3D translational clearance joint employing a variable stiffness contact force model, *Nonlinear Dynamics* 99 (2020) 1937-1958 .
37. M. Zahalka, J. Stanek, Options of Advanced Simulations of Crank Presses Loading *Conference: 25th DAAAM International Symposium on Intelligent Manufacturing and Automation, Vienna, Austria* (2014).

38. Z. Gronostajski, M. Hawryluk, M. Kaszuba, Application of a measuring arm with an integrated laser scanner in the analysis of the shape changes of forming instrumentation during production, *Eksplotacja i Niezawodność Maintenance and Reliability* 18 (2016) 194-200
39. Z. Chval, M. Cechura, Monitoring Extremely Stressed Points on Stands of Forging Presses, 25th International Symposium on Intelligent Manufacturing and Automation 100 (2015) 841-846
40. W. Wang, F. Lin, L. Zhang, Experimental study and finite element analysis on the frame of multi-directional forging press, *Proceedings of the institutions of mechanical engineers part b, Journal of Engineering Manufacture* 231 (2017) 2112-2122
41. A.K. Tuleshov, A.A. Jomartov, M.J. Kuatova, Dynamic Analyses of a clutch of crank press, *News of the National Academy of Sciences of the Republic of Kazakhstan – Series of Geology and Technical Sciences* 5 (2019) 114-123
42. E. Zheng, R. Zhu, S. Zhu, A study on dynamics of flexible multi-link mechanism including joints with clearance and lubrication for ultra-precision presses, *Nonlinear Dynamics* 83 (2016) 137-159
43. A. Almandeel, A. Murray, P. Andrew, D.H. Myszka, A Function Generation Synthesis Methodology for All Defect-Free Slider-Crank Solutions for Four Precision Points, *Journal of Mechanisms and Robotics – Transactions of the ASME* 7 (2015) no.031020.
44. M. Hawryluk, J. Jakubik, Analysis of forging defects for selected industrial die forging processes, *Engineering Failure Analysis* 59 (2016) 396-409
45. H.G. Zhang, T.A. Dean, Computer modeling of tool loads and press tool deflections in multistage forging, *International Journal of Machine Tools & Manufacture* 35 (1995) 61-69
46. J. Hou, U. Stahlberg, H. Keife, A load model for closed-die forging of long components, *Scandinavian Journal of Metallurgy* 21 (1992) 159-164
47. R.F. Scrutton, A. Marasco, The dynamics of closed-die forging with mechanical presses, *Journal of Engineering for Industry – Transactions of the ASME* 117 (1995) 357-364
48. C. Labergere, S. Remy, P. Lafon, Benchmark of a forging process with a hammer: comparison between fem simulation results and real part shapes using 3D digitising scanner, *Mecanique & Industries* 21(5) 2011(12 222.
49. M. Hawryluk, J. Ziemba, Application of the 3D reverse scanning method in the analysis of tool wear and forging defects, *Measurement* 204-213)2018(128
50. M. Hawryluk, J. Ziemba, Ł. Dworzak, Wear analysis of forging tools used in the hot forging processes using 3D reverse scanning techniques and cooling-lubricating system, *International Journal of Advanced Manufacturing Technology* 97 (2018) 2009-2018
51. M. Hawryluk, J. Ziemba, Possibilities of application measurement techniques in hot die forging processes, *Measurement* 110 (2017) 284-295 .
52. M. Hawryluk, P. Kondracki, J. Krawczyk, M. Rychlik, J. Ziemba, Analysis of the impact of forging and trimming tools wear on the dimension-shape precision of forgings obtained in the process of manufacturing components for the automotive industry, *Eksplotacja i Niezawodność - Maintenance and Reliability* 21 (2019) 476-484.
53. M. Rychlik, M. Hawryluk, J. Ziemba, M. Kneć, The analysis of the movement dynamics for the robotized press Massey 2500T during forging by use dynamic system Aramis, Internal report SPR series no. 101/2020, Wrocław University of Science and Technology, Poland, Wrocław, 2020.