

## Article

# Effect of precious metals on NO reduction by CO in oxidative conditions

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**Abstract:** Carbon dioxide has become a global challenge, where the emissions have become more than what could be handled. In this regard, conversion of CO<sub>2</sub> to value added chemicals and thus recycling CO<sub>2</sub> became a viable option. One of these options is the use of a process in strong development: oxycombustion. However, the gases resulting from this process contain some traces of impurities that can hinder the recovery of CO<sub>2</sub> such as NO and CO. This work has therefore focused on the study of the reaction of NO reduction by CO in an oxidizing medium, using catalytic materials based on various supported noble metals. These materials were extensively characterized by a variety of methods including BET surface area measurements, hydrogen chemisorption, Transmission Electron Microscopy (TEM) and H<sub>2</sub> temperature programmed reduction (H<sub>2</sub>-TPR). The obtained results show that the catalytic behaviour of M/Al<sub>2</sub>O<sub>3</sub> catalysts in CO oxidation and NO reduction with CO in oxidative conditions depends mainly on the nature of the metal. The best result for these both reactions is obtained with Pt/Al<sub>2</sub>O<sub>3</sub> catalyst. The Pt nanoparticles existing in the metallic form (Pt<sup>0</sup>) showed by TPR could explain the activity.

**Keywords:** Environmental chemistry; Oxyfuel Combustion; NO-CO reaction; Heterogeneous catalysis.

## 1. Introduction

Greenhouse gases (GHG) emissions generated by human activity led to an increase in the radiation which is trapped in the atmosphere and induced an increase in the greenhouse effect. This is mainly due to carbon dioxide (CO<sub>2</sub>), the main greenhouse gas with an impact of 79%. The CO<sub>2</sub> emitted from anthropic activities, is perceived as a constraint in industrial activity with taxes, stringent environmental regulations, impact on global warming... To limit these CO<sub>2</sub> emissions, it could be considered as a gas with industrial advantage and/or as a new source of carbon for the production of minerals or organic compounds with commercial interest. Reuse of CO<sub>2</sub> represents a promising alternative, with important applications in chemical industry and for power generation.

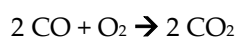
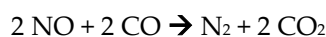
The processes for the valorization of CO<sub>2</sub> can be divided into three different categories:[1]

- Direct use without transformation: industrial use (water treatment, supercritical CO<sub>2</sub> ...).
- Chemical transformation: organic chemical synthesis, methanation, hydrogenation (methanol), reforming: dry (CO<sub>2</sub>), steam reforming (CO<sub>2</sub> + H<sub>2</sub>O)...
- Biological transformation: microalgae, biocatalysis.

However, CO<sub>2</sub> valorization process requires a gas as pure as possible [1].

Oxyfuel-combustion is therefore a promising method to get a nearly pure CO<sub>2</sub> that enables to obtain a CO<sub>2</sub> rich stream (80%) [2]. In the oxyfuel system, the combustion flow consists of O<sub>2</sub> separated from air. Therefore, the flue gas is dominated by CO<sub>2</sub>. The oxidation of N<sub>2</sub> for NO<sub>x</sub> emissions is limited which are considered as one of the main pollutants of the atmosphere, since they are responsible for a lot of environmental problems like photochemical smog, acid rain, ozone layer depletion [3]. This Process emits also water vapor, unburned components (in function of the waste burned) such as carbon monoxide (generated by incomplete combustion) and nitrogen monoxide [2]. CO is the cheapest and the most available from industrial sources and it could be used as a reductant of NO, but it is known to be one of the worst reductant. P. Malfoy classified, on noble metals, several reducers on the base of the NO half-conversion temperatures. The sequence obtained is as follows: H<sub>2</sub> > NH<sub>3</sub> > CO > C<sub>3</sub>H<sub>5</sub> [4]. So it seems possible to purify the CO<sub>2</sub> issued from oxyfuel-combustion by NO-CO reaction.

In oxyfuel combustion systems, NO, CO, O<sub>2</sub> are simultaneously present and the following reactions may occur [5]:



Therefore as oxygen is present in excess, it competes with NO for oxidizing the reducing agent (CO) [6]. Due to this effect, many authors studied the competitions between CO-NO and CO-O<sub>2</sub> reactions. Shelef et al. found that the second reaction is predominant over a number of transition metal oxides and supported Pt [7]. Other authors proved that the NO addition to CO+O<sub>2</sub> reduces drastically the rate of CO<sub>2</sub> formation on Rh catalyst [8] and Pt supported catalyst [9].

The NO-CO reaction has been widely applied and investigated over various catalysts. The reduction of NO by CO occurring over three-way catalysts (TWC), composed of noble metals (Rh, Pd and Pt), is very important because it converts CO, NO, and hydrocarbon simultaneously [10]. Rh is employed for NO removal because it combines a good activity and selectivity to form nitrogen [11]. On the other hand, Pt and Pd ensure the oxidation of CO and hydrocarbon [12]. Kobylinski and Taylor [15] studied NO reduction over supported Pt, Rh, Pd and Ru. They found that, when CO is used as reducing agent, the reaction over Ru catalyst is accelerated. The activity sequence of the catalysts was: Ru > Rh > Pt > Pd. It was also studied over this reaction in presence of O<sub>2</sub> [6,16]. It has demonstrated that Ir effectively promotes the NO-CO reaction in the presence of an excess of oxygen.

To summarize, the objective is to reduce NO by CO in an oxidizing environment with a CO<sub>2</sub> rich stream without any additives like SCR reaction. The important amount of CO<sub>2</sub> could be a problem for some basic materials that's why we chose alumina because of its strong Lewis acid center which ensures the stabilization of species in active state and disperses them adequately, as well as its intrinsic catalytic activity in various reactions [12,17]. This paper will present you this work with materials prepared with different precious metal (Pt, Pd, Rh, Ru and Ir) loadings supported on alumina.

## 1. Introduction

The introduction should briefly place the study in a broad context and highlight why it is important. It should define the purpose of the work and its significance. The current state of the research field should be reviewed carefully and key publications cited. Please highlight controversial and diverging hypotheses when necessary. Finally, briefly mention the main aim of the work and highlight the principal conclusions. As far as possible, please keep the introduction comprehensible to scientists outside your particular field of research. References should be

numbered in order of appearance and indicated by a numeral or numerals in square brackets, e.g., [1] or [2,3], or [4–6]. See the end of the document for further details on references.

2. Materials and Methods

1.1. Catalysts preparation

Alumina (Aluminum Oxide C from Degussa) with a specific surface area of 100 m<sup>2</sup>.g<sup>-1</sup> was used as support. After calcination of support for 4 h at 500 °C under air, the catalysts were prepared by wet impregnation of alumina with corresponding precursors in the following table (table1). For all catalysts, the nominal contents were of 1.0 wt%.

Table 1. Metal precursors

Metal	Iridium	Palladium	Platinum	Rhodium	Ruthenium
precursor used	Ir(acac) <sub>3</sub>	Pd(acac) <sub>2</sub>	Pt(NO <sub>2</sub> ) <sub>2</sub> (NO <sub>3</sub> ) <sub>2</sub>	Rh(NO <sub>3</sub> ) <sub>3</sub>	Ru(acac) <sub>3</sub>

The impregnated support was left overnight in an oven at 120 °C. It was then calcined in dry air at 500 °C for 4 h and reduced in H<sub>2</sub> flow for 4 h at 500 °C.

1.2. Characterization of the catalysts

Before any impregnation, the support used (Al<sub>2</sub>O<sub>3</sub>) was characterized by nitrogen physisorption (BET, BJH) H<sub>2</sub> chemisorption.

Specific surface areas of samples were measured by nitrogen adsorption and desorption at -196 °C with BET surface analyzer (Micromeritics Model TRISTAR 3000) using BET-BJH method. Before the analysis, the samples were outgassed at 250 °C under vacuum overnight.

The hydrogen chemisorption capacity was determined by a static volumetric vacuum technique at room temperature. Firstly, the catalyst was cleaned under ultra-high vacuum overnight to eliminate the adsorbed molecules. Then, the catalyst was reduced under 750 mbar of H<sub>2</sub> for 1 h at 300 °C, and purged under vacuum until reaching a low pressure (P < 10<sup>-5</sup>mbar). Two series of hydrogen adsorption isotherms were performed with an increasing hydrogen pressure, from 10 to 70 mbar with an augmentation of 10 mbar. Between the two series, the sample was submitted to ultrahigh vacuum in order to remove weakly bound hydrogen. The adsorbed hydrogen quantity was calculated by extrapolating the isotherm to P = 0. The first isotherm allows determining the total amount of adsorbed hydrogen and the second one the amount of physisorbed hydrogen. The chemisorbed hydrogen amount was calculated by difference between these two values. The metal particle size was calculated considering a stoichiometry of H/M = 1, and assuming that particles correspond to cubes deposited on the sup-port and exposing 5 faces [18], with an equal distribution between (1 1 1), (1 1 0) and (1 0 0) planes.

In order to provide a check of the results obtained with hydrogen chemisorption, transmission electron microscopy (TEM) analysis were performed with a JEOL 2100 electron microscope operating at 200 kV with a theoretical resolution of 0.19 nm. Catalysts were finely ground, dispersed in ethanol using an ultrasonic bath and finally deposited on the carbon film of a copper grid. The particle size distribution was estimated on the basis of several pictures. The average particle size was then calculated using the relation  $\sum n_i d_i^3 / \sum n_i d_i^2$  where  $n_i$  is the number of particles with size  $d_i$ . The correlation between the metallic accessibility determined by hydrogen adsorption and the average particle size from TEM was evaluated on the basis of a model of cubic particles lying on one face. The particle size distribution was obtained from TEM pictures calculating the average particle diameter from the measurement performed on at minimum 100 particles.

H<sub>2</sub> temperature programmed reductions (TPR) were performed on a Hiden Catlab equipped with QGA Hiden quadrupole mass spectrometer. The catalysts were first pretreated at 200°C for 1 hour under argon (20 mL/min Air Liquide 5.0). The sample was then cooled down to 80°C and exposed to a mixture of 0.25 % H<sub>2</sub> in inert atmosphere. The TPR was then carried out using a ramp of

10 °C.min<sup>-1</sup> up to 500 °C. Hydrogen Sensitivity factor was determined before the ramp for further quantification.

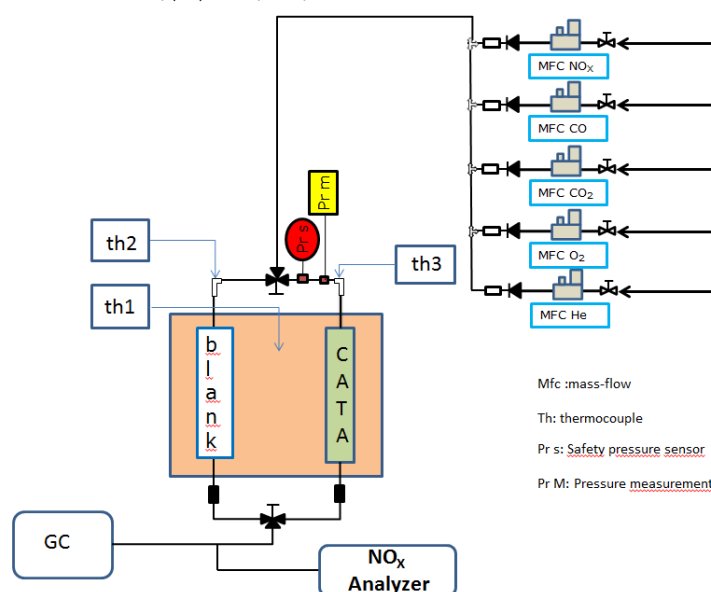
### 1.3. Catalytic tests

Before each test, the catalyst was treated in situ under He flow (40 mL.min<sup>-1</sup>) at 200 °C for 1.5 h. Then, CO<sub>2</sub> purification was carried out at atmospheric pressure in a fixed-bed flow reactor containing 150 mg of catalyst. The catalysts were sieved in order to retain grains with diameters between 0.315 and 0.500 mm and diluted to a constant volume by SiC (exhibited no activity in CO<sub>2</sub> purification from 50 to 500 °C) so that all the experiments were carried out under the same conditions (GHSV = 2.24 10<sup>4</sup> h<sup>-1</sup>).

The flow of the reactant gases is composed of: 20 % CO<sub>2</sub>, 10 % O<sub>2</sub>, 0.5 % CO and 0.02 % NO (He as eluent gas) with a total flow of 200 mL.min<sup>-1</sup>, in the temperature range 50–500 °C. The reaction products (CO<sub>2</sub> and N<sub>2</sub>) were analyzed on line by a gas chromatograph (GAS analyzer XXL1300), NO was analyzed with Xentra 4900C analyzer (Servomex). The measurement of NO<sub>2</sub> is done indirectly using a NO<sub>2</sub> to NO converter BÜNOx (Bühler Technologies) by comparison.

The conversion, selectivity and yields of the main products are defined in the following way:

- Conversion:  $X_i (\%) = \frac{n_i^{int} - n_i^{out}}{n_i^{int}} * 100$  where  $n_i^{int}$  and  $n_i^{out}$  are number of mole of the corresponding compounds "i" at the inlet and the outlet of the reactor.
- Selectivity:  $S_i (\%) = \frac{n_i}{\sum_i n_i} * 100$
- Yield:  $Y_i (\%) = X_i * S_i * 100$



**Figure 1:** Experimental setup for catalytic purification of CO<sub>2</sub> from oxyfuel combustion

In order to compare the different materials, T<sub>50</sub> and T<sub>90</sub> factors will be taken into account. These factors correspond respectively to the temperature at which 50% or 90% of carbon monoxide is converted. For NO reduction, the catalysts will be compared according to their maximum efficiency (yield) at total conversion of CO.

### 3. Results

The Alumina supported catalysts prepared by wet impregnation with precious metal were studied in the catalytic purification of CO<sub>2</sub>. In this study we bring out the effect of nature of metal in this reaction.

### 3.1. BET surface area

The specific surface area of the alumina and its pore volume were determined by adsorption of nitrogen. Table 2 summarizes the results obtained by the BET and BJH methods.

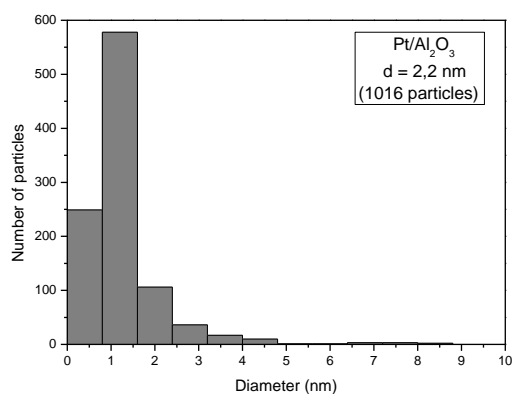
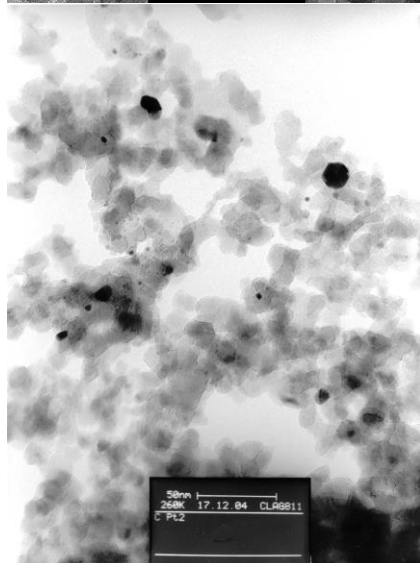
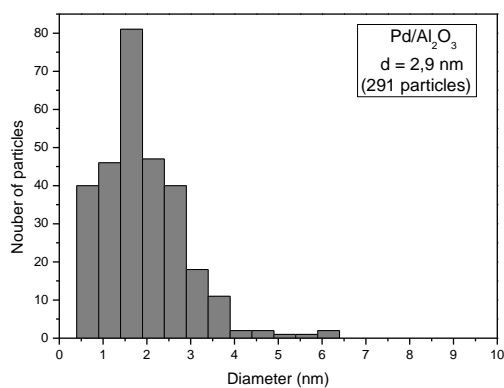
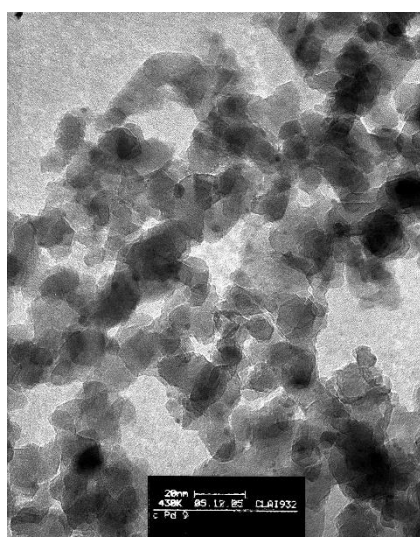
**Table 2.** Specific surface area and porous volume of alumina

Sample	$S_{\text{BET}}$ ( $\text{m}^2\cdot\text{g}^{-1}$ )	$V_{\text{porous}}$ ( $\text{cm}^3\cdot\text{g}^{-1}$ )	Average pore size (nm)
Alumina	100	0,74	31

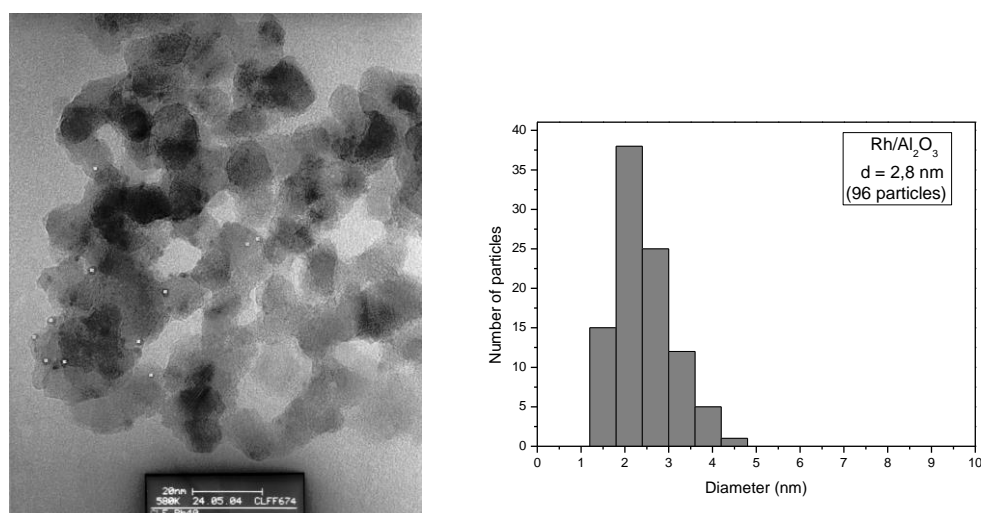
From these results, the alumina used as support for our catalysts is a mesoporous solid with a large specific surface area.

### 3.2. TEM and $\text{H}_2$ chemisorption

In order to compare the catalytic activity for our catalysts, we tried to synthesize size-controlled uniform material. We can see in Figure 2 that the synthesized catalytic materials have a homogeneous distribution of particle size.







**Figure 2.** TEM pictures and size distribution of the  $\text{Al}_2\text{O}_3$  supported noble metallic Pd, Pt and Rh.

**Table 3.** Properties of catalysts: particles size and metallic accessibility.

Catalysts	Reference	Metallic accessibility (%)	$\langle d \rangle^a$ (nm)	$\langle d \rangle^b$ (nm)
1% Ir/ $\text{Al}_2\text{O}_3$	Ir	42	2.2	---
1% Pd/ $\text{Al}_2\text{O}_3$	Pd	40	2.4	2.9
1% Pt/ $\text{Al}_2\text{O}_3$	Pt	40	2.3	2.2
1% Rh/ $\text{Al}_2\text{O}_3$	Rh	41	2.2	2.8
1% Ru/ $\text{Al}_2\text{O}_3$	Ru	28	3.8	3.8

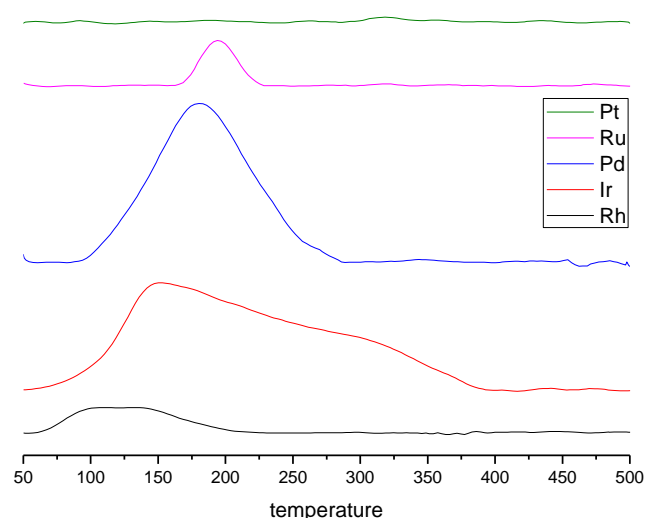
<sup>a</sup> Obtained by  $\text{H}_2$  chemisorption analysis. <sup>b</sup> Estimated by TEM pictures.

The results obtained by  $\text{H}_2$  chemisorption in the table 2 shown that, the Ir, Pd, Pt and Rh on  $\text{Al}_2\text{O}_3$  catalysts presents the similar particle size leading to  $d=2.2$  nm. In the case of Ru/ $\text{Al}_2\text{O}_3$ , the particles were larger than those on the other catalyst samples.

In order to have more specific information about the morphology and composition of the prepared samples, TEM measurements were performed. As shown in the table 2, for all of the catalysts, the particles size obtained by TEM was in accordance with the results obtained by  $\text{H}_2$  chemisorption.

### 3.3. Temperature programmed reduction by $\text{H}_2$

The  $\text{H}_2$ -TPR measurements were performed to determine the reduction behaviors and chemical compositions of various catalysts as depicted in Fig 3. Since the  $\text{Al}_2\text{O}_3$  support is irreducible from room temperature to  $500^\circ\text{C}$ , the peaks of reduction in this temperature range should correspond to the reduction of the different kinds of active phase species.



**Figure 3.** H<sub>2</sub>-TPR patterns of the different catalysts (°C)

The TPR profile of Pd supported is characterized by one broad pic centered at around 180°C. According to Ferrer and al. [19] this peak is attributed to the reduction of PdOx species that strongly interacts with the support. However, no negative peak was observed at 80°C corresponding to the desorption of hydrogen from PdHx which could be formed at low temperature [17,20].

No reduction peak was observed for Pt. Pt nanoparticles should mainly exist in the metallic form (Pt<sup>0</sup>) not accessible for further reduction. [21] But, generally a reduction peak is found by TPR. These Pt<sup>0</sup> nanoparticles should then be especially active for CO oxidation.

The profile of Ru shows a peak with a maximum at about 194°C, which is attributed to Ru oxide reduction already demonstrated by Koopman & al [22].

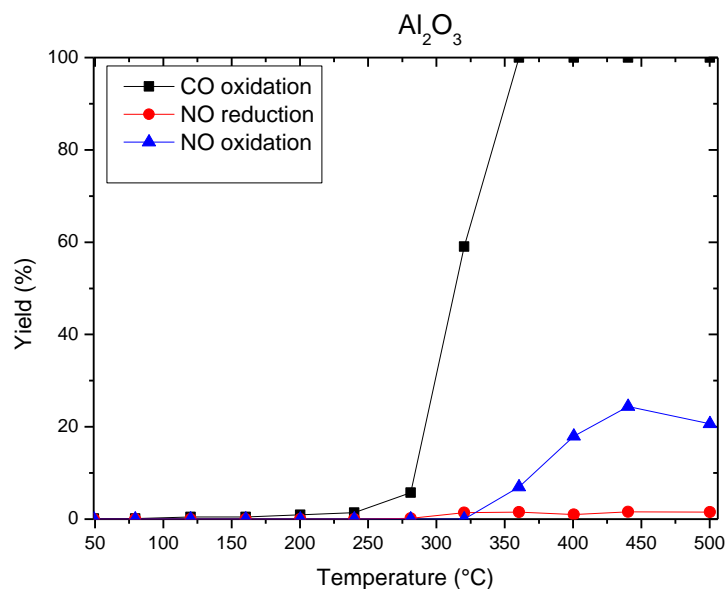
The Ir catalyst exhibits a broad reduction peak between 100-400°C, which can be attributed to the reduction of IrO<sub>2</sub> phase [21,23]. But, usually the reduction IrO<sub>2</sub> phase is found at higher temperature. This phase should then be more active for CO oxidation than expected.

The Rh profile is composed of a broad reduction peak from ambient to 250°C which is attributed to the reduction of surface RhOx species, according to the literature [24–25].

### 3.4. Catalytic reaction

The general catalytic performance of different materials have been studied and determined for the catalytic total CO oxidation and NO reduction with CO in oxidant atmosphere (10% O<sub>2</sub>) and CO<sub>2</sub> rich stream under identical conditions.

Light-off curve of support (Al<sub>2</sub>O<sub>3</sub>) have been determined and is reported in fig 4.

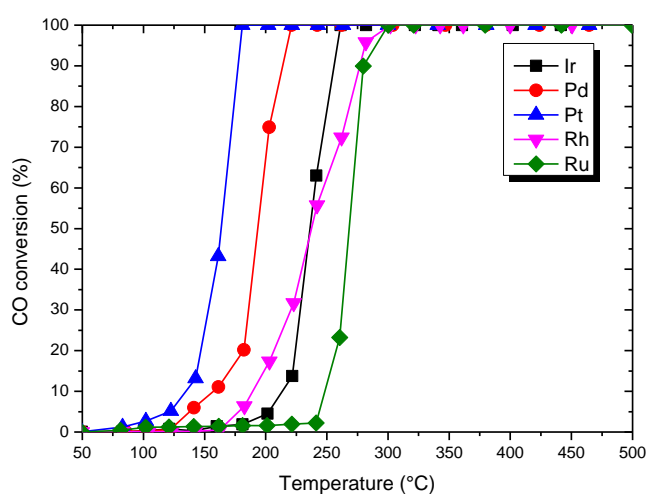


**Figure 4.** Light-off curves for  $\text{Al}_2\text{O}_3$  support

It can thus be seen in fig 4 that on the alumina, it is possible to have a complete oxidation of the CO. For the conversion of NO, there is a slight oxidation of NO at very high temperature but no reduction.

Fig 5 shows the activities of the catalysts for CO oxidation. They exhibit the activity for this reaction at the temperatures higher than 100°C and the conversion increases with the reaction temperature. For all tests, catalytic performances were compared by considering  $T_{50}$  and  $T_{90}$  for CO oxidation, which respectively correspond to the temperatures at which 50 and 90% of CO were converted. The obtained results are illustrated in fig 5. The conversion of CO to  $\text{CO}_2$  was 100% for all used catalysts. Ir and Rh have a similar activity values with  $T_{50}$  at 236 °C. The general order of catalytic activity, based on the temperature required for 50% conversion ( $T_{50}$ ) is the following:  $\text{Pt} > \text{Pd} > \text{Ir} \sim \text{Rh} > \text{Ru}$ .

Considering  $T_{90}$ , Pt shows the better performance (176°C), Rh and Ru present a similar activity values with 280°C. The ranking for catalysts does not much change to that at  $T_{50}$ :  $\text{Pt} > \text{Pd} > \text{Ir} > \text{Rh} \sim \text{Ru}$ .



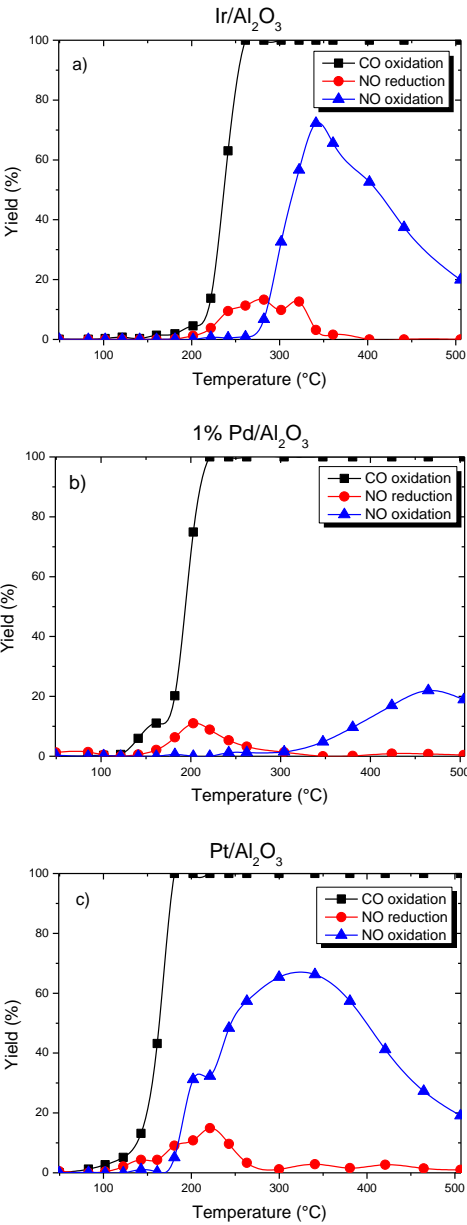
**Figure 5.** Light-off curves of CO conversion for the different materials. Feedstream composition: 0.02%NO, 0.5% CO, 10%  $\text{O}_2$  and 20%  $\text{CO}_2$ , and balance He. Space velocity:  $2.24 \cdot 10^4 \text{ h}^{-1}$

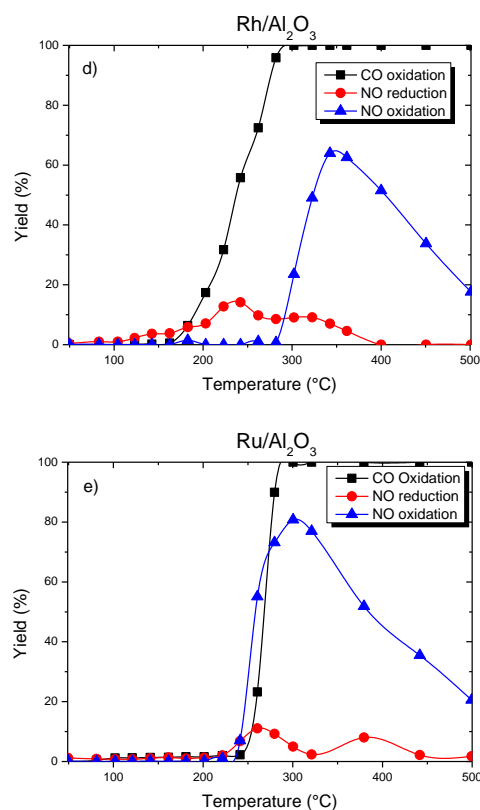


**Table 4.** T<sub>50</sub> and T<sub>90</sub> of catalysts catalytic CO oxidation

Catalysts	T <sub>50</sub> (°C)	T <sub>100</sub> (°C)
Ir	236	260
Pd	194	212
Pt	164	176
Rh	236	280
Ru	268	280

The oxidation of CO, reduction of NO and oxidation of NO over the impregnated Al<sub>2</sub>O<sub>3</sub> with Ir, Pd, Pt, Rh, Ru were evaluated, and the obtained results have been reported in Fig 6.





**Figure 6.** Catalytic activity for the impregnated alumina with Pt, Rh, Ru, Pd, Ir. Feedstream composition: 0.02% NO, 0.5% CO, 10% O<sub>2</sub> and 20% CO<sub>2</sub>, and balance He. Space velocity:  $2.24 \cdot 10^4 \text{ h}^{-1}$

Fig 6-a. represents the activity of Ir in these reactions. The CO is completely oxidized at 260°C with a 13% of NO reduction. The oxidation of NO reaches 72.3% at 340°C.

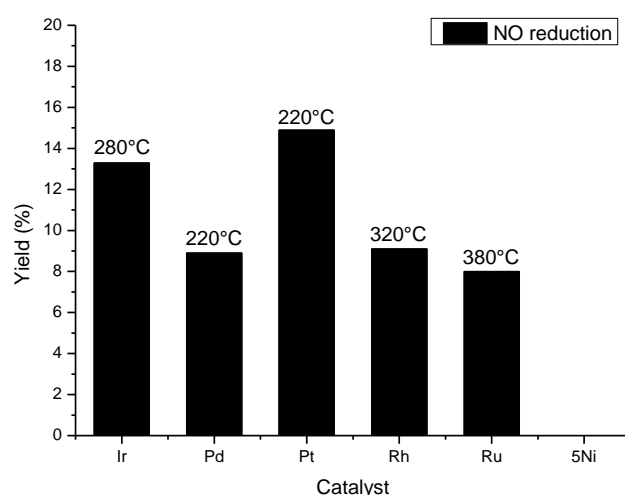
Fig 6-b. shows the activity of Pd in CO and NO reactions. The oxidation of CO is carried out at 220°C. NO reduction reaches a maximum with 11% at 200°C but the CO is not completely oxidized at 220°C, only 9% of NO is reduced.

Fig 6-c. shows the activity of Pt in NO-CO reaction. The CO is totally oxidized at 180°C. The NO reduction begins from the start of the CO oxidation. Pt/Al<sub>2</sub>O<sub>3</sub> reduces the NO from 140°C to 300°C with a maximum reduction (14.9%) at 220°C, the oxidation phase is also bell-shaped with an optimum (66.2%) at 340°C.

Fig 6-d. represents the activity of Rh in CO and NO reactions. The oxidation of CO with the supported Rh occurs later than with Pt or Pd, in fact the total conversion of CO is obtained at 300°C. This is in full agreement with the literature on three-way catalysts that use Rh to convert NO<sub>x</sub> [10]. With regard to the conversion of NO, the reduction of NO is 14.4% at 240°C. On the other hand, at higher temperatures, NO oxidizes 64.2% for alumina at 340°C.

Fig 6-e. represents the activity of Ru in oxidation of CO and reduction of NO. Like Rh the total conversion of CO is obtained at 300°C and the NO is converted at 85% but with 80% is oxidized and only 5% is reduced.

In order to compare and highlight the influence of nature of the metal on the NO reduction with CO in an oxidative conditions, we presents you, in fig 7 the maxima of NO reduction at total oxidation of CO over all catalysts. The Pt/Al<sub>2</sub>O<sub>3</sub> and Ir/Al<sub>2</sub>O<sub>3</sub> catalysts are the best ones of NO reduction by CO in presence of an excess of oxygen and a CO<sub>2</sub> rich stream. Pd, Rh and Ru show similar activity and yield but at different temperatures: 220°C for Pd, 320 °C for Rh and 380°C for Ru.



**Figure 7.** NO reduction at total oxidation of CO. Feedstream composition: 0.02%NO, 0.5% CO, 10% O<sub>2</sub> and 20% CO<sub>2</sub>, and balance He. Space velocity:  $2.24 \times 10^4 \text{ h}^{-1}$

In our results the low activity of the Pd compare to Ir catalyst could be explain by an oxygen poisoning of the Pd. Almusaiteer and Chuang [27] proved that the presence of O<sub>2</sub> in NO-CO reaction flows plays a role of poison on Pd/Al<sub>2</sub>O<sub>3</sub> catalyst. The adsorbed oxygen inhibits N-O dissociation thus causing an accumulation of Pd-N=O and diminution of conversion of NO. Ir, on the other hand, has a superior ability than other precious metal to convert NO under oxidizing environment due to its ability to adsorb NO dissociatively in the presence of an excess of O<sub>2</sub> [16]. Tauster and Murell [6] confirmed this result and they proved that Ir is the only catalyst favoring the NO-CO reaction over CO-O<sub>2</sub>.

#### 4. Conclusion

This work deals with the identification of the best metal catalysts for CO<sub>2</sub> purification in oxidative conditions. In this work, we focus on the NO reduction on alumina supported precious metal using carbon monoxide as reduction agent in oxidizing conditions. First of all, it is possible to achieve a reduction of the NO in an oxidizing medium using a catalytic material by using one of the worst reducer, often present in the industrial process outputs, thus not requiring to add one thus to add an injection system of a reducer such as ammonia.

**Author Contributions:** J.A. prepared the materials, conducted the experiments and wrote the first draft of the paper. C.P. and S.S. supervised the work. D.D. and F.D. realized the TPR measurements. All authors contributed to the data interpretation, the discussion and the revision of the paper.

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**Conflicts of Interest:** The authors declare no conflict of interest.

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