

Design of Spectral Filters Based on Mode Coupling of Optical Fibers

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Abstract

In this paper, design of optical spectral filters based on mode coupling of optical fibers is presented. The finite difference method is applied to find the dispersion characteristics of optical fiber coupler constructing from two fibers as a composite multi-dielectric waveguide with different cores but the same cladding. Also, the field distribution for both fibers as a separate and as a composite waveguide is investigated. The spectral characteristics of the filters are computed depending on the coupling of two linear polarized modes LP_{01} and LP_{11} . The dependence of the transmission coefficient on operating wavelengths is illustrated. Finally, the spectral bandwidth of filter as a function of the distance between the two cores is addressed.

1. Introduction

The rapidly increasing demand for optical signal processing and optical communication systems needs the development of the all optical fiber spectral filter characteristics which is one of the most important key passive components for optical communications and passive optical networks which mostly use wavelength division multiplexing and demultiplexing techniques. It has the advantage to integrate easily with the fiber optic networks. It also provides a low loss coupling due to its fabrication from optical fibers.

Many types of spectral filters are designed and analyzed such as: diffraction grating filters [1-3], Fabry-Perot filters [4-6], Mach-Zehnder

interferometer filters [7-9], all fiber filters [9-11] and others. Most of all fiber wavelength selective filters reports on the literature consists of two or three identical fibers or two dissimilar fibers with different refractive index shapes [12-21]. The two types of these filters depend on single mode fibers supporting LP_{01} in their coupling operation at range of interesting wavelengths.

In this paper, the finite difference method is used to find the optical properties of a directional coupler proposed by [22] is consisted of two dissimilar fibers, but only one fiber has single mode LP_{01} and the other has dual-mode capable of supporting two modes LP_{01} and LP_{11} . The Dispersion characteristics and field distribution of both separate fibers and as a composite waveguide are calculated by applying the finite difference method of Opti fiber software. Spectral characteristics of the coupler are investigated by using the coupled mode theory of parallel dielectric waveguides.

The paper is organized as follows.: section 2 deals with geometry and method of analysis. Discussion and numerical results are illustrated in section 3. Finally, conclusions of the work are drawn in section 4.

2. Geometry and Method of Analysis

The geometry of the coupler is shown in Fig.1. The geometry consists of two fibers one support single mode LP_{01} called fiber1 and the other support two modes LP_{01} and LP_{11} called fiber2 with cladding contains the two cores.

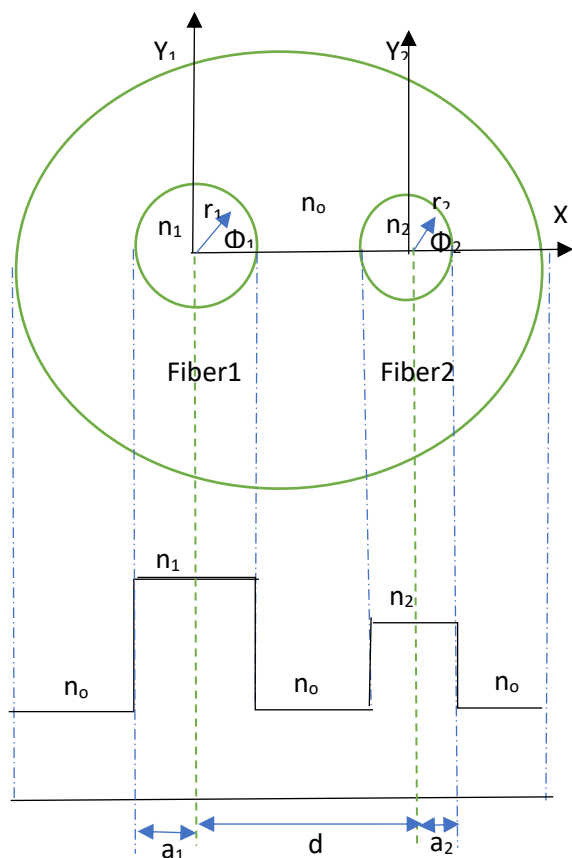


Figure 1: Geometry of the spectral filter.

Core radius of fiber1 is a_1 and for fiber2 is a_2 . The distance between the two centers of fibers is d . The refractive indices n_1 and n_2 represent cores index of fiber1 and fiber2, respectively. The refractive index of the cladding is represented by n_0 .

2.1 Dispersion Characteristics and Field Distributions

The weakly guiding approximation where the difference between refractive index of core and cladding of each fiber is very small. So, the scalar wave analysis can be applied. The solution of this equation using Finite Difference Method of optifiber software taking into consideration the boundary conditions of the fields between core and cladding gives the dispersion characteristics of modes LP_{01} and LP_{11} of fiber1 and LP_{01} for fiber2. The field and power distributions of each separate fiber modes LP_{11} for fiber1 and LP_{01} for fiber2 are calculated. Also, the field and power

distributions of composite mutidielectric waveguide are determined.

2.2 Spectral Characteristics of Optical Filter

The coupling mode equations of the parallel dielectric waveguides are applied to evaluate the coupling coefficients as:

$$k_{12} = \sqrt{\frac{2(n_2^2 - n_0^2)}{n_1 n_2}} \frac{K_1(w_1 d)}{K_1(W_2) \sqrt{K_0(W_1) K_2(W_1)}} \cdot \frac{u_1 u_2}{a_1 v_1} \frac{1}{U_2^2 + w_1^2 a_2^2} \{w_1 a_2 K_0(W_2) I_0(w_1 a_2) + W_2 K_1(W_2) I_0(w_1 a_2)\} \quad (1)$$

$$k_{21} = \sqrt{\frac{2(n_1^2 - n_0^2)}{n_1 n_2}} \frac{K_1(w_2 d)}{K_1(W_2) \sqrt{K_0(W_1) K_2(W_1)}} \cdot \frac{u_1 u_2}{a_2 v_2} \frac{1}{U_1^2 + w_2^2 a_1^2} \{W_1 K_0(W_1) I_1(w_2 a_1) + w_2 a_1 K_1(W_1) I_0(w_2 a_1)\} \quad (2)$$

where:

$$U_1 = u_1 a_1 = k_0 a_1 \sqrt{n_1^2 - \frac{\beta_{11}^2}{k_0^2}}$$

$$U_2 = u_2 a_2 = k_0 a_2 \sqrt{n_2^2 - \frac{\beta_{01}^2}{k_0^2}}$$

$$W_1 = w_1 a_1 = k_0 a_1 \sqrt{\frac{\beta_{11}^2}{k_0^2} - n_0^2}$$

$$W_2 = w_2 a_2 = k_0 a_2 \sqrt{\frac{\beta_{01}^2}{k_0^2} - n_0^2}$$

$$V_1^2 = U_1^2 + W_1^2 \text{ and } V_2^2 = U_2^2 + W_2^2$$

and $k_0 = 2\pi/\lambda$ is the free space wavenumber. It can be verified from Eqns.1 and 2 that the coupling coefficients k_{12} and k_{21} are equal when $n_1 = n_2$

and $a_1=a_2$. The transmission coefficient $T(\lambda)$ can be defined as ratio of power output from fiber1 and $z=L$ to the power input into fiber2 at $z=0$.

$$T(\lambda) = \frac{|k_{12}|^2}{|S|^2} \sin^2(SL) \quad (3)$$

where

$$S = \left[\left\{ \frac{\beta_{11} - \beta_{01}}{2} \right\}^2 + k_{12}k_{21} \right]^{\frac{1}{2}}$$

The transmission coefficient is a function of wavelength through S . So, the transmission coefficient can be obtained for a specific wavelength range and fiber parameters. Therefore, narrowband and broadband spectral filters can be designed by a suitable selection of these parameters. The coupling length L_c is defined as:

$$L_c = \frac{\pi}{2S} \Big|_{\beta_{11}=\beta_{01}} = \frac{\pi}{2\sqrt{k_{12}k_{21}}} \quad (4)$$

3. Numerical Results

To assess the performance of the proposed $LP_{01} - LP_{11}$ fiber coupler for applications in wavelength filtering, numerical results based on the above formulations are presented. To obtain the transmission characteristics, first dispersion characteristics for LP_{01} mode of fiber2 and LP_{11} mode of fiber1 are calculated using FDM of Optifiber software. The parameters and material compositions of fibers at $\lambda=1.33\mu\text{m}$ are summarized in Table 1. Fig.2 illustrates the dispersion characteristics for LP_{01} , LP_{11} for fiber1 and LP_{01} for fiber2.

Table.1 Fiber parameters and material compositions.

Fiber	Core radius (μm)	Δ at $\lambda=1.33\mu\text{m}$	Core material	Cladding material
1	3.4	0.8%	13.5m/o GeO2 86.5m/o SiO2	5.8 m/o GeO2 94.2 m/o SiO2
2	3.1	0.4%	9.1 m/o GeO2 90.9 m/o SiO2	

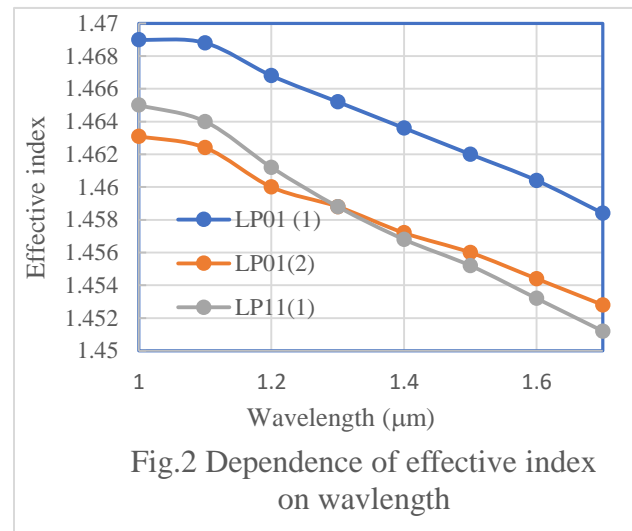


Fig.2 Dependence of effective index on wavelength

Fig.2 shows that, the effective index of LP_{01} mode for fiber2 equals the effective index of LP_{11} modes of fiber1 at $\lambda=1.33\mu\text{m}$. This means, these two modes have the same propagation constant and thus are phase matched at $\lambda=1.33\mu\text{m}$. It can be noted that, the dispersion characteristic for LP_{01} mode for fiber1 is not needed in the calculation of transmission coefficient, but is introduced to satisfy the fact that LP_{01} mode of the two fibers have different propagation constants and thus do not exchange power.

Distributions of power and field across the cross section of each fiber separately and across the cross section of the structure at $\lambda=1.33$ are calculated using FDM of Optifiber Software as in Figs.3, 4, 5, 6 and 7.

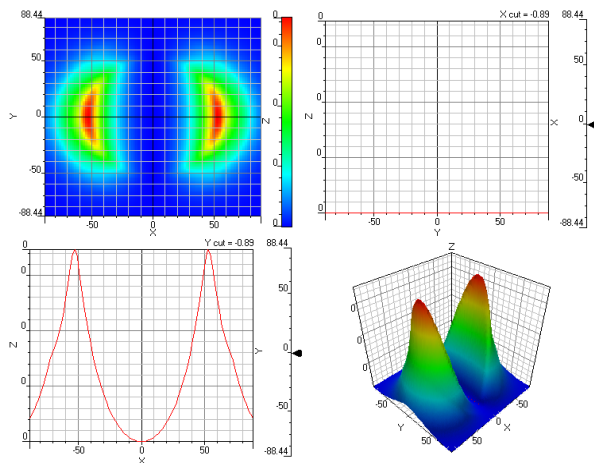


Fig.3 Power of LP₁₁ mode for fiber 1.

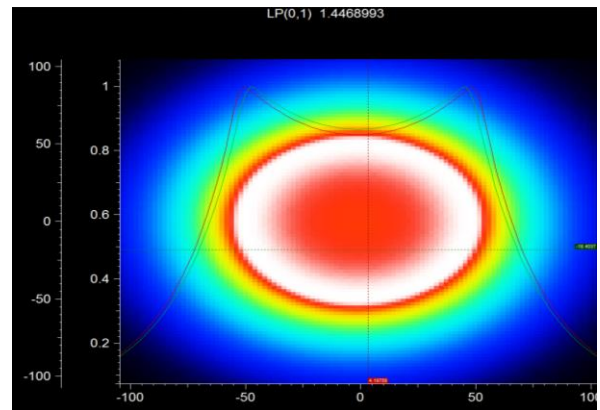


Fig. 6 Field distribution of LP₀₁ for fiber2.

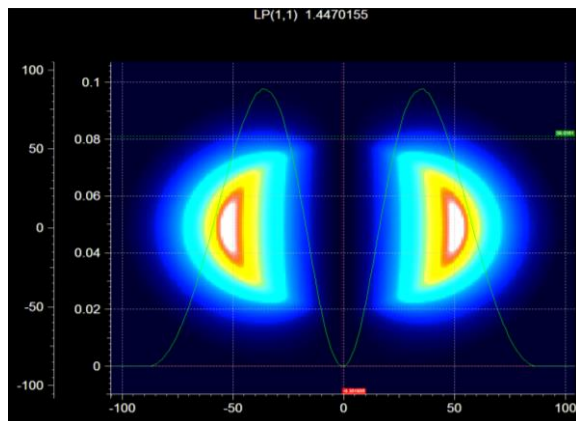


Fig. 4 Field distribution of LP₁₁ for fiber 1

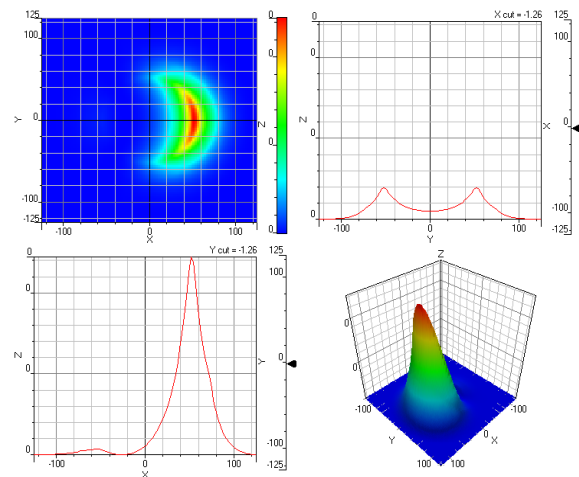


Fig.7 Power of the composite of LP₀₁-LP₁₁ across filter cross section

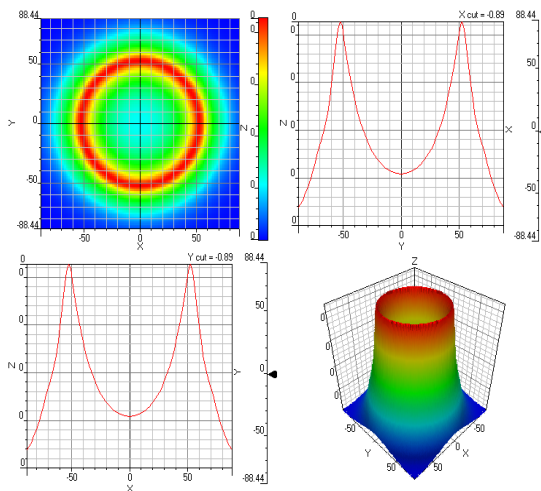


Fig.5 Power of LP₀₁ mode for fiber2.

Fig.8 illustrate the dependence of the spectral width of 1.33 μm spectral filter on the separation distance d between the centers of each core centers.

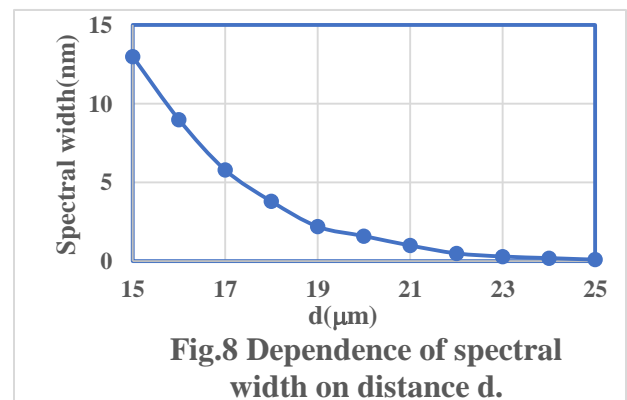
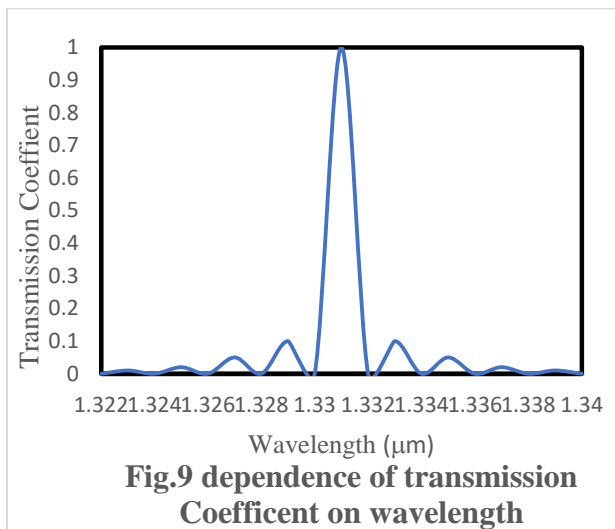


Fig.8 Dependence of spectral width on distance d .

The spectral width of the filter is governed by the slope difference between the dispersion characteristics of the interaction modes as well as the core separation d . The larger the slope difference the smaller the spectral width. Also, increasing the separation distance d , produces in a decrease in spectral width. Fig.9 shows the transmission characteristic of a $1.33 \mu\text{m}$ spectral filter with fiber parameters as given in Table.1.



The peak transmission occurs at $\lambda=1.33\mu\text{m}$ and the separation of the two cores is $d=20\mu\text{m}$. The half power spectral width for this value of d is $\Delta\lambda=1.5\text{nm}$ and the first side-lobe level is about 0.1. With these parameters, the coupler acts as a narrowband filter.

4. Conclusions

A two-fiber coupler based on LP₀₁-LP₁₁ mode coupling has been investigated using coupled mode theory. The coupler cross section is considered as a multielectric waveguides for evaluating the dispersion characteristics, power and field distributions. The finite difference method of Optifiber software is applied for solving the scalar wave equation. With a choice of appropriate parameters, the coupler can be designed to either narrowband or broadband spectral filter. Design information and transmission characteristics for couplers with maximum matching at $\lambda=1.33\mu\text{m}$ widely used

wavelength in fiber optic communications were calculated. This type of spectral filter has the advantage that it can be easily fabricated and the loss of connections is very small.

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