

Article

Effect of Coil Configuration Design on Al Solidified Structure Refinement

Jing Zhao ^{1,*}, Ji-hao Yu ², Ke Han ³, Hong-gang Zhong ², Ren-xing Li ² and Qi-jie Zhai ^{2,*}

¹ Department of Mechanical and Electrical Engineering, Tangshan University; zhj7906@163.com

² Center of Advanced Solidification Technology, Shanghai University; qjzhai@shu.edu.cn

³ National High Magnetic Field Laboratory, Florida State University; hanke666666@hotmail.com

* Correspondence: zhj7906@163.com; qjzhai@shu.edu.cn

Abstract: This paper outlines our effort on optimizing Pulsed Magneto-Oscillation (PMO) design in order to improve the efficiency of ingot manufacturing under PMO. Our calculation and experiment provided optimized PMO coil design and special configuration. Our optimized PMO design offered us a device that enabled the operator to examine and operate the melt without losing the efficiency. In one of the designs, the equipment even refined the grain sizes. Our work also showed an optimized distance range between the coil and the melt surface that maximized the refinement effects.

Keywords: configuration design; PMO; calculation; solidified structure refinement

1. Introduction

The quality of any final metal product is largely dependent on the solidification structure that emerges during the initial casting [1-4]. A refined microstructure with reduced defects in as-cast billets yields improved properties in end products [5-6]. Researchers have used many methods to refine solidified microstructure [7-13]. One of these technologies, Pulsed Magneto-Oscillation (PMO), has been found to significantly refine solidification structure and reduce ingot segregation. The coil in PMO generates a controllable electromagnetic force in the surface region as solidification begins. This electromagnetic force generates forced convection, which in turn promotes the flow within the melt. Because the PMO coil has no direct contact with the melt, this technology avoids both contamination and spattering [14-15].

Researchers who applied PMO to pure Al during its nucleation stage and the first half of its growing stage have consistently observed structural refinement and equiaxed-zone enlargement in the resulting ingot, leading them to deduce that the PMO treatment makes nuclei more likely to drop out of the solidifying top surface of the melt or from the mold walls themselves into the deeper liquid part of the melt. This process, known as nucleus drifting, enhances structural refinement [16-18]. PMO promotes heterogeneous nucleation near the solid-liquid interface, and the resulting forced convection causes the partly solidified grains to move away from the solid-liquid interface and become randomly distributed throughout the melt [19]. The convection induced by PMO in Al also changes the temperature distribution, which encourages the survival and growth of nuclei [20]. The main parameters of PMO, including the peak current, the output power, and the configuration of the PMO coil, can all be easily adjusted and controlled [21-27]. PMO treatment shows great promise in the production of heavy steel ingots on an industrial scale [28].

We have previously studied the effect of PMO coil configuration on the distribution of electromagnetic field, flow field, and solidification structure [28]. In this study, we expanded our studies from three to five configurations. For certain selected configurations, we launched an in-depth study of how the solidification structure can be affected by changing the distance between the

coil and melt surface. The results provide feasible suggestion for the application of PMO on the production of ingots.

2. Research procedures

2.1. Strategy

In order to refine microstructure in pure Al by optimization of the process parameters of PMO, we did both numerical simulation and experimental work. One parameter was the coil configuration. We modified SPMO [28] by SPMO-H (the coil was put on the top) and CPMO [28] by CPMO-H (the coil was put on and around the hot-top) (Figure 1). We also changed the distance between the coil and melt surface.

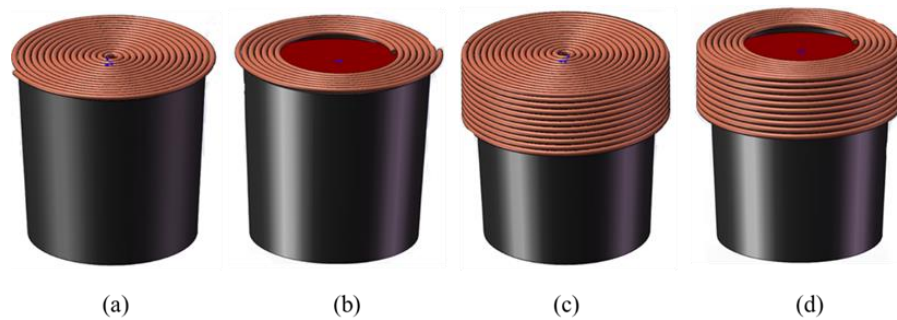


Figure 1. Coil configuration of PMO: (a) SPMO [28]; (b) SPMO-H; (c) CPMO [28]; (d) CPMO-H.

2.2 Numerical simulation

The induced magnetic field and electric current were calculated according to Maxwell's laws, which can be expressed as Equation (1):

$$\begin{cases} \nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t} \\ \nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} \\ \nabla \cdot \vec{B} = 0 \\ \nabla \cdot \vec{D} = \rho \end{cases} \quad (1)$$

where $\vec{H}$ is electric field intensity, $\vec{J}$ is total current density vector, $\vec{D}$ is electric flux density, t is time, $\vec{E}$ is magnetic flux density vector, $\vec{B}$ is magnetic flux density vector, ρ is electric charge density.

The casting setup consisted of a coil, air and the melt in the simulation. Two-D axisymmetric Finite Element Method (FEM) model was built on this setup by the ANSYS® software. PLANE13 was chosen for analyzing, which is a controlled combinatorically by the Maxwell equation, Lorentz's law and Joule's law. Different grid sizes were chosen for different portion of the model. The finest grid was used in melt and coil (Figure 2). This selection of the grid affected the automatically generated nodes in our simulation. We believe this difference has marginal impact on the simulated results.

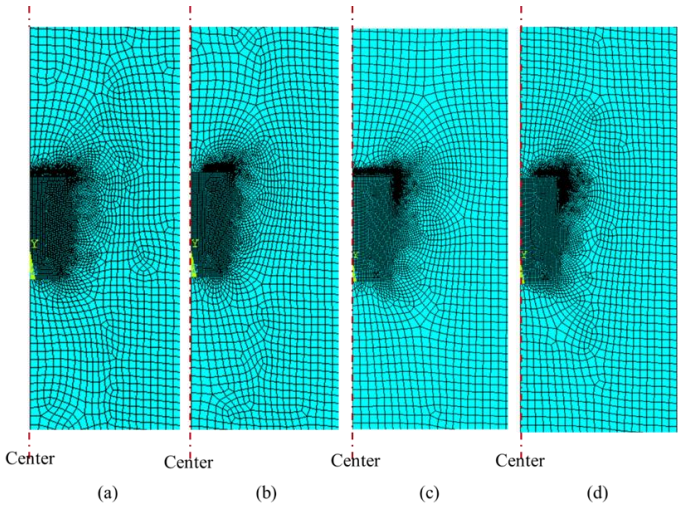


Figure 2. FEM models used in the simulation: (a) SPMO; (b) SPMO-H; (c) CPMO; (d) CPMO-H.

The current profile in the coil was similar to what we used before [28] (Figure A1 in Appendix). The relationship between the current and time was described as:

$$I(t) = I_0 \exp(-\zeta t) \sin(\omega t) \tag{2}$$

where I_0 is a peak value in current, and ζ and ω are constant for the circuit.

The main parameters of the pulse current used in the simulation include peak value and pulse width of electric pulse. The electrical resistivity was assumed to be 2.42×10^{-7} and $1.72 \times 10^{-8} \Omega \cdot m$ for the aluminum melt and the coil, respectively. The relative permeability was assumed to be 1 for the aluminum.

2.3 Experimental

The experimental setup is composed of a modulated PMO generator, water-cooled oscillation coils (Figure 1), and molds made of graphite. The cavity size of molds was designed as $\Phi 140$ mm $\times$ 200 mm, and the wall thickness of the mold is 10 mm. Prior to pouring, molds were preheated to 200 °C. About 7 kg commercial purity aluminum (Al: 99.7 wt.%, Fe: 0.2 wt.%, Si: 0.1 wt. %) with the liquidus temperature of 660 °C was melted in a resistance furnace and poured into molds at the pouring temperature of 750 ± 10 °C after being held for 30 min. The melts were treated immediately with PMO after pouring until the ingots solidified completely. The peak value and frequency of pulsed current were $450h_l$ A and $444k_t$ Hz, where h_l and k_t were the coefficients of the pulse generator and remained constant in the experiment. The solidified Al ingots were longitudinally sectioned along the center. The sections were etched in a mixture of 3 hydrochloric acid: 3 nitric acid: 5 water. Metallographic specimens were taken from these sections in the lower part of ingots (Figure 3). Specimens were mechanically polished by vibration polisher for 3 h and then electronically polished with a mixture of distilled water and fluorotic acid at 0.3–0.5 A/cm² for 20–40 s. The microstructure of etched samples was examined in a Zeiss optical microscope (Axio Imager A2m). The procedure for this experiment was the same as reported before [28].

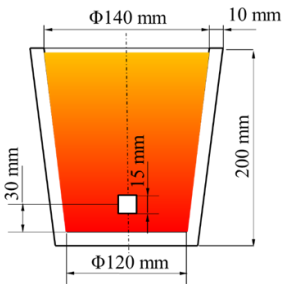


Figure 3. Geometry of the ingot and sampling location.

3. Results

3.1. Simplification of coil configuration to optimize PMO

In both small- and large-scale production of ingots, PMO coils have to be placed on top of the mold immediately after pouring. Consequently, slag control and surface examination are more difficult with PMO than without. Our Previous simulation results showed that magnetic field induced by SPMO tended to cluster near the melt surface and along the mold wall, not at the center of the melt [24,28]. We deduced that if the coil could be given the form of a ring rather than a disc, slag control and surface examination would be much easier. The coils can also be placed on top of the mold before pouring. In order to compare discs with rings, we performed simulations in this study on SPMO, CPMO, simplified SPMO-H and CPMO-H using both forms.

In SPMO configuration, we found that using ring (SPMO-H) rather than disc (SPMO) would slightly reduce the intensity of electromagnetic field. In CPMO configuration, using ring (CPMO-H) rather than disc (CPMO) would have little effect on the distribution of an electromagnetic field in CPMO (Figure 4).

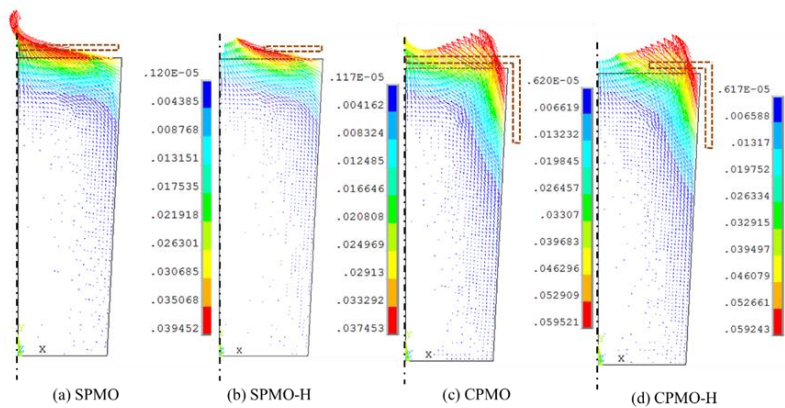


Figure 4. Distribution of magnetic flux intensity in melts at a quarter of one oscillation period of PMO (or T/4, see appendix. In our simulation, one oscillation period of PMO was divided into stages T/4, T/2, 3T/4 and 1T, where T is an oscillation period of PMO.).

The macrographs of SPMO, SPMO-H, CPMO and CPMO-H treated ingots under the same current parameters showed that refinement was achieved in both SPMO (see Figure 5(a) and Figure 5(e)) and SPMO-H treated ingots (see Figure 5(b) and Figure 5(f)) under the same current peak value and frequency. SPMO and SPMO-H increased the equiaxial zone from 2.5 vol% (untreated) [28] to 38.9% and 29.5%, respectively. The equiaxial grains were the coarsest in untreated ingot, whereas the average size grain size decreased from 1063 μm [28] to 409 μm and 435 μm for samples treated by SPMO and SPMO-H, respectively (Table1). The ratio of equiaxed zone and size of grains in the CPMO-H treated ingot (Figure 5(d), Figure 5(h)) were only marginally different from the CPMO treated ingot (Figure 5(c), Figure 5(g)). In other words, CPMO-H is almost as effective as CPMO.

The difference in coil configuration led to difference in inductance, which can be deduced by measurement of pulse width. We calculated the induction skin depth using the pulse width read from oscilloscope. Because the skin depth values for CPMO and CPMO-H were identical, CPMO and CPMO-H treated melts were almost the same. Because the skin depth values for CPMO and CPMO-H treated melts were about 16.7% greater than SPMO and the larger skin depth makes more nucleus fallen from the wall and increased the nucleation rate, CPMO and CPMO-H treated ingots were significantly better than samples treated by SPMO and SPMO-H. Modification of SPMO to SPMO-H decreased the skin depth by 8.3% and led to reduced equiaxed zone volume fraction. In

order to achieve the similar effect of SPMO by SPMO-H, more electrical current should be considered. The results showed that the coil could be modified for convenience in production.

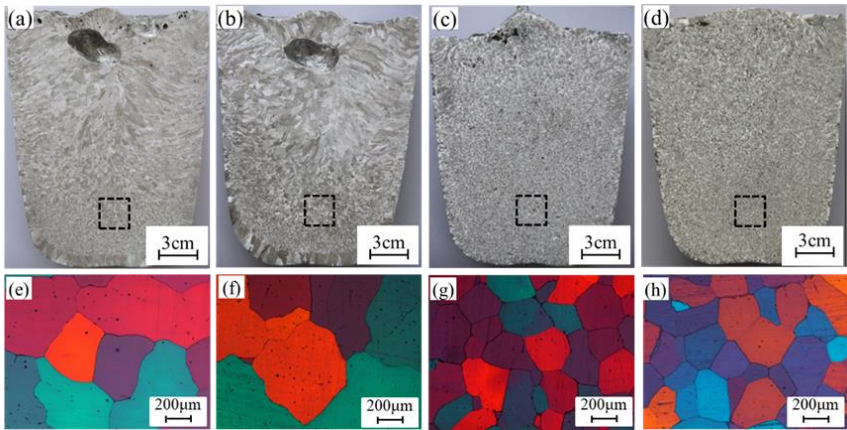


Figure 5. Effect of coil configuration on the solidified structure. (a), (e) with SPMO; (b) (f) with SPMO-H; (c), (g) with CPMO; (d), (h) with CPMO-H.

Table 1. Effect of coil configuration on PMO treatment

Coil configuration in PMO	SPMO	SPMO-H	CPMO	CPMO-H
Size of equiaxed grains (µm)	435	409	269	247
Ratio of equiaxed zone (%)	38.9	29.5	93.2	92
Calculated skin depth (cm)	1.2	1.1	1.4	1.4
Calculated power (K _p W)	789	605	1616	1610

3.2 Effect of liquid level on the refinement effect of Al ingot with CPMO treated

Because melt surface level is dropping during solidification and the induced electromagnetic distribute mainly near the coil, it is important to understand if the dropping of surface reduce the refinement effect. We conducted an experiment using CPMO-H coil to study the effect of the distance between the coil and the melt surface on refinement under PMO using the same peak current and frequency (450*h*_i A and 444*k*_i Hz) as above. To compare the situation with distance between the coil and melt surface of 1 cm (Figure 4(d)), we studied the casting using distance of 3 cm (Figure 6(a)) and 6 cm (Figure 6(b)). Our calculation results showed that the distance had little influence on the distribution of magnetic flux intensity in melt (Figure 7). Our experimental results showed that an increase in the distance resulted in decrease of the ratio of equiaxed zone from 83% (1 cm in Figure 5(d)), to 81% (3 cm in Figure 8(a)) and to 74% (6 cm in Figure 8(b)). There is no obvious difference in average grain size within equiaxed zone for three cases (Figure 9). In other words, if only ingot within equiaxed zone is used, the distance between the coil and melt level has nearly no effect on refinement by CPMO-H. In production, this is equivalent to section the top of ingots, which usually have shrinkage cavity on the top.

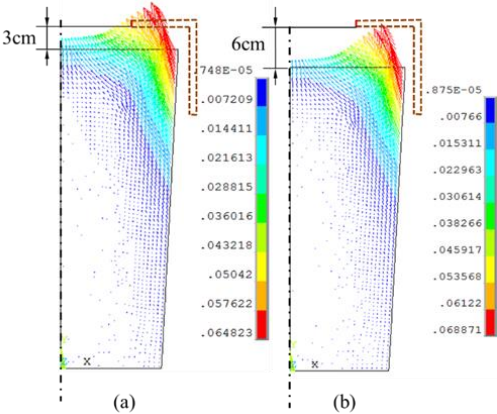


Figure 6. Distribution of magnetic flux intensity with different liquid level at T/4. (a) 3 cm to the coil; (b) 6 cm to the coil.

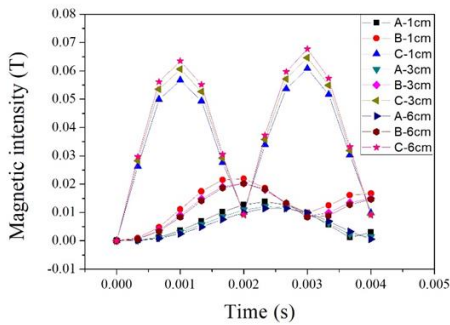


Figure 7. Comparison of magnetic intensity vs time at the same position in melt at identical locations: Position A is in the center; position B is at the half radius; position C is at the edge in melt. All are located about 10 cm to the surface. The grain sizes are 247 μm , 263 μm , 253 μm for samples treated with distance of 1, 3 and 6 cm, respectively.

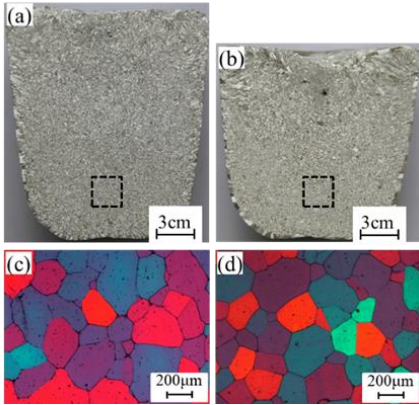


Figure 8. Effect of liquid level on the solidified structure of CPMO-H treated ingots: (a), (c), 3cm to the coil; (b), (d) 6cm to the coil.

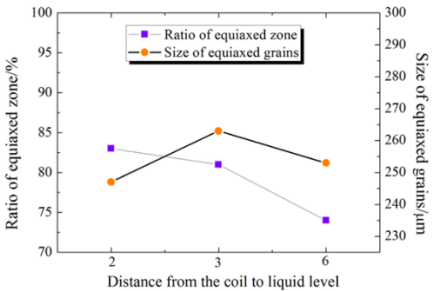


Figure 9. Comparison of ratio of equiaxed zone and size of equiaxed grains with different distance from the coil to liquid level in CPMO treated ingots.

4. Conclusions

- (1) Ring coils allow operator to examine the melt and undertake operation without interfering pouring.
- (2) Ring coil SPMO-H reduced the equiaxed grain size but decreased the ratio of equiaxed zone. Ring coil CPMO-H reduced the equiaxed grain size without significantly changing the ratio of equiaxed zone.
- (3) Within 1 cm and 6 cm, distance between the coil and melt has little effect on the grain sizes refined by CPMO-H.

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Jing and Yu Ji-hao; Methodology, Zhao Jing, Yu Ji-hao and Zhai Qi-jie; Project administration, Zhao Jing and Zhai Qi-jie; Resources, Li Ren-xing; Software, Zhao Jing and Yu Ji-hao; Supervision, Zhao Jing and Zhai Qi-jie; Validation, Zhao Jing, Han Ke and Zhong Hong-gang; Writing – original draft, Zhao Jing; Writing – review & editing, Han Ke.

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Conflicts of Interest: The authors declare no conflict of interest.

Appendix A

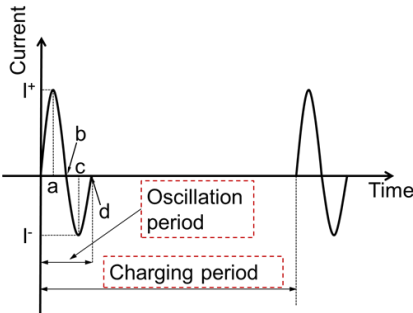


Figure A1. Variation of pulsed electricity in a coil

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