

An Efficient FPGA-based Frequency Shifter for LTE/LTE-A Systems

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The Physical Random Access Channel (PRACH) plays an important role in LTE and LTE-A systems. It is through the PRACH channel that the user equipment (UE), based on eNodeB's timing estimates, aligns its uplink transmissions to the eNodeB's uplink and gain access to the network. One of the initial operations executed by the PRACH receiver at eNodeB side is the translation of the PRACH signal back to base band, *i.e.*, center the PRACH signal around DC. This operation is a necessary step for preamble detection and can be carried out through a time-domain frequency shift operation. Therefore, in this paper we present the hardware architecture and implementation details of a configurable and optimized FPGA-based time-domain frequency shifter. It is a hardware-efficient and accurate architecture for converting the relevant received PRACH signal into base band before further signal processing. The architecture is mainly based on a customized Numerically Controlled Oscillator (NCO), which is used for generating complex exponentials employing only adders, a Look-Up Table (LUT) and plain logic resources. The main advantage of the proposed hardware architecture is that it completely eliminates the need for storing a large number of long complex exponential sequences by employing a single LUT and exploiting quarter wave symmetry of the basis waveform. Our simulation results show that the proposed customized NCO architecture provides high Spurious Free Dynamic Range (SFDR) signals using a minimal amount of FPGA resources. Moreover, the proposed architecture exhibits spur-suppression ranging from 62.13 to 153.58 dB without using Taylor Series correction.

Keywords: LTE, LTE-A, 4G, PRACH, NCO, time-domain frequency shift, FPGA

1. Introduction

Long Term Evolution (LTE) is the next step forward in cellular 3G services. LTE is a 3GPP standard that provides for an uplink speed of up to 50 megabits per second (Mbps) and a downlink speed of up to 100 Mbps. LTE brings many technical benefits to cellular networks. Bandwidth is scalable from 1.25 MHz to 20 MHz [1–4].

In order to make LTE a true 4th generation (4G) technology, it was enhanced to meet the IMT-Advanced requirements issued by the International Telecommunication Union (ITU). The necessary improvements are specified in 3GPP Release 10 and also known as LTE-Advanced (LTE-A). LTE-A further increases peak data rates towards 1 Gbit/s in the downlink and 500 Mbit/s in the uplink. The technology components of LTE-A are Carrier aggregation, MIMO extension (up to DL: 8x8; up to UL: 4x4), Uplink access enhancements (clustered SC-FDMA and simultaneous data and control information (PUSCH and PUCCH) transmission) and Improvement of cell edge performance by supporting

enhanced inter-cell interference coordination (eICIC) and Relay Nodes (RN) [3].

In LTE and LTE-A, uplink physical random access channel (PRACH) is used for initial access requests from the user equipment (UE) to the evolved base station (eNodeB) and to obtain time synchronization [3], [4]. In case of need to access the network, a UE requests access by transmitting a random access (RA) preamble through PRACH [5]. The RA preamble is then detected by the PRACH receiver at eNodeB side, which estimates both the ID of the transmitted preamble and the propagation delay between UE and eNodeB. Then, UE is time-synchronized according to a time alignment (TA) value (derived from the propagation delay estimate) transmitted from the eNodeB before the uplink transmission [6].

PRACH transmission opportunity is set by higher layers [7] and determines the frequency-domain location of the random access preamble within the physical resource blocks. In this way, at eNodeB side, a fundamental operation before any attempt to detect random access preambles takes place is the extraction of relevant preamble signals through a time-domain frequency shift operation. This operation translates the PRACH signal from the frequency-domain location set by higher layers back to base band so that preamble detection can be totally carried out in base band [4].

This paper is an extension of a previous conference paper [8]. Differently from [8], where we provided only some very superficial aspects of the proposed algorithm and architecture, the current paper presents a meticulous analysis on its design and implementation aspects. Therefore, the main contributions of the current paper are (i) the design of a low computational complexity time-domain frequency shifter algorithm and hardware architecture to be employed in the PRACH receiver at eNodeB side; (ii) a thorough analysis of design and implementation details; (iii) discussion of the computational complexity of the proposed architecture in terms of FPGA resource utilization and speed; and (iv) careful analysis of the implementation results considering spur-suppression, *i.e.*, SFDR, SNR, probabilities of correct and error detection and average error between time-domain frequency shift operations carried out by a floating-point model, referred here as Golden Model (GM), and by the fixed-point FPGA implementation of the proposed architecture.

This paper contributes with a method and architecture optimized and tested for reduced complexity on a Xilinx Virtex 6 LX240T FPGA device. Results show that the architecture presents spur-suppression better than 62 dB and when it is employed in the PRACH receiver the probability of correct detection achieved by the receiver is greater than 99% at a SNR of -21 dB.

The remainder of the paper is organized as follows. In section II we offer some background on the Physical Random Access Channel and its features. Section III presents an efficient algorithm for a time-domain frequency shifter. Section IV gives important practical considerations on the implementation of the proposed algorithm as well as detailed description of the units composing the main architecture. Test methodology, simulation and implementation results are then presented in Section

V. Finally, Section VI provides some concluding remarks.

2. Physical Random Access Channel

The PRACH is the physical channel that initiates communication with the eNodeB. It allows the eNodeB to calculate the time delay to the User Equipment (UE) and identify it prior to establishing a packet connection. To establish a connection with the eNodeB the UE initiates the random access procedure by sending a random access preamble using the PRACH. The physical layer random access preamble consists of a cyclic prefix and a sequence part as shown in [7] Table 5.7.1-1. This preamble is orthogonal to other uplink user data to allow the eNodeB do differentiate each UE. The subcarrier spacing for the PRACH is 1.25 KHz for formats 0 to 3, and 7.5 KHz for format 4. See example in Figure 1. Formats 0 to 3 are used for frame structure type 1, *i.e.*, Frequency Division Duplexing (FDD) and Format 4 is used for the frame structure type 2, *i.e.*, Time Division Duplexing (TDD) only [3]. As will be discussed later, the PRACH can be positioned at different frequency locations, *i.e.*, RBs, depending on a parameter configured by higher layers. Figure 1 shows an example of a possible PRACH's frequency-domain location.

Prime-length Zadoff-Chu (ZC) sequences are adopted as random access preambles in LTE and LTE-A systems due to its CAZAC properties, *i.e.*, all points of the sequence lie on the unit circle and its auto-correlation is zero for all time lags other than zero [10], [11]. These properties make ZC sequences very useful in channel estimation and time synchronization and also enable improved PRACH preamble detection performance [4]. The ZC sequences employed in the PRACH channel have form given by Equation 1 [7].

$$z_u(n) = \exp\left(\frac{-j\pi un(n+1)}{N_{ZC}}\right), \quad 0 \leq n \leq N_{ZC} - 1 \quad (1)$$

where u is a positive integer known as ZC sequence index, n is the time index and N_{ZC} is the length of the ZC sequence, which for FDD systems is equal to 839 [7]. Random access

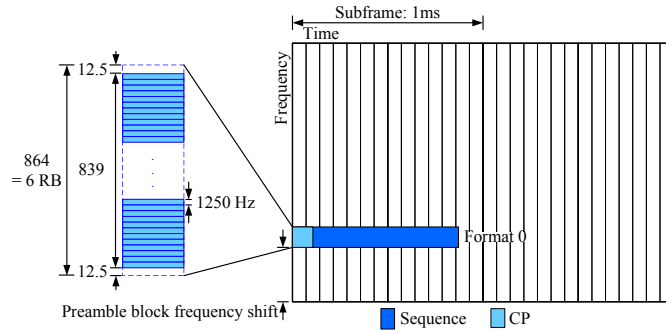


Figure 1. Example physical random access channel (PRACH), format 0.

preambles with zero correlation zones are defined from the u -th root ZC sequence.

This sequence length, N_{ZC} , corresponds to approximately 69.92 Physical Uplink Shared Channel (PUSCH) subcarriers in each SC-FDMA symbol, and offers a band protection of $72 - 69.92 = 2.08$ PUSCH subcarriers, which corresponds to approximately one PUSCH subcarrier protection on each side of the preamble [7]. PUSCH sub-carriers are spaced 15 KHz apart from each other.

The PRACH occupies a bandwidth of 1.08 MHz that is equivalent to 6 Resource Blocks (RB). Differently from other uplink channels, PRACH uses a subcarrier spacing of 1250 Hz for preamble formats 0 to 3 [7]. The ZC sequence is specifically positioned at the center of the 1.08 MHz bandwidth, *i.e.*, at the center of the block of 864 available PRACH subcarriers, so that there is a guard band of 15.625 KHz on each side of the preamble, which corresponds to 12.5 null PRACH subcarriers. These guard bands are added to PRACH preamble edges in order to minimize interference from PUSCH. Figure 1 depicts the PRACH preamble mapping according to what was just exposed.

The PRACH sequence, which for formats 0 and 1 is 800 us long, is created by cyclically-shifting a root ZC sequence of prime-length N_{ZC} , defined as in Equation 1. Random access preambles with zero correlation zones of length $N_{CS} - 1$ are generated by applying cyclic shifts to the u -th root ZC sequence, according to Equation 2.

$$x_{u,v}(n) = x_u((n + Cv) \bmod N_{ZC}) \quad (2)$$

where v is the sequence index and Cv is the cyclic shift applied to the root ZC sequence and calculated as $Cv = vN_{CS}$ for unrestricted sets [7]. Parameter N_{CS} gives the fixed length of the cyclic shift. All the possible values for these parameters are defined in [7].

2.1. PRACH Receiver

In the literature there are two approaches for PRACH receivers, the full frequency-domain one and the hybrid time/frequency domain one [4, 9]. Although the full frequency-domain approach provides the optimal detection performance, this approach uses considerably large size discrete Fourier transform (DFT), to be more precise a 24576-point DFT. On the other hand, the hybrid time/frequency domain approach uses FFT/IFFT blocks of the same size, *i.e.*, 2048-point FFT when the decimation factor adopted is 12. Thus, the hybrid time/frequency domain substantially reduces the complexity of the hardware implementation. Therefore, in order to reduce the implementation complexity of the PRACH receiver we adopt the hybrid time/frequency domain approach, which results in more practical implementations [4]. Figure 2 depicts the PRACH receiver architecture implemented and being used in our L1 solution.

The received signal, *i.e.*, possible random access preamble signal, is first pre-processed in time domain, then transformed into the frequency domain by a FFT

block, multiplied by a Fourier transformed root Zadoff-Chu (ZC) sequence and then the resulting sequence is searched for peaks above a predefined threshold which is calculated to produce a given probability of false alarm. Figure 2 depicts the main components of the PRACH receiver at eNodeB side, for further details refer to [12].

The first block in Figure 2 is the Cyclic Prefix remover, which discards all samples from the CP part of the preamble. Next, the PRACH pass-band signal is shifted to base-band by multiplying it with a complex exponential. In the sequence, the base-band signal is fed into a decimator block, which decimates the signal by a factor of 12, now instead of 24576 samples in the case of format-0 we have only 2048 samples. The FFT engine transforms the SC-FDMA symbols from time domain into frequency domain. The sub-carrier de-mapping block extracts the RACH preamble sequence from the correspondent FFT bins. The result of sub-carrier de-mapping is multiplied by the root ZC sequence and then fed into a zero-padding block. Finally, the IFFT engine is used to produce the cross-correlation between the root ZC sequence and the received preamble signal. All samples coming out of the IFFT block have their square modulus calculated producing what is known as Power Delay Profile (PDP) samples. Finally, the preamble detection block employs the PDP samples to estimate the noise power, set a detection threshold and then decides whether a preamble is present or not. As output of the detection process this block reports to the MAC layer all detected preambles and its respective Time Advance (TA) estimates. For further information on this receiver architecture and detection algorithm, refer to [4], [12].

2.2. Preamble Format

The PRACH preamble, illustrated in Figure 3, consists of three parts: a Cyclic Prefix (CP) with length T_{CP} , which is added to the preamble in order to effectively eliminate Inter Symbol Interference (ISI), a signature or sequence part of length T_{PRE} and of a guard period T_{GP} which is an unused portion of time

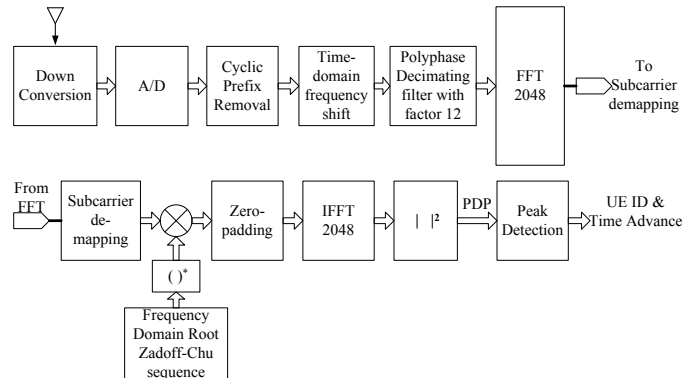


Figure 2. Architecture of a hybrid time-frequency domain PRACH receiver.

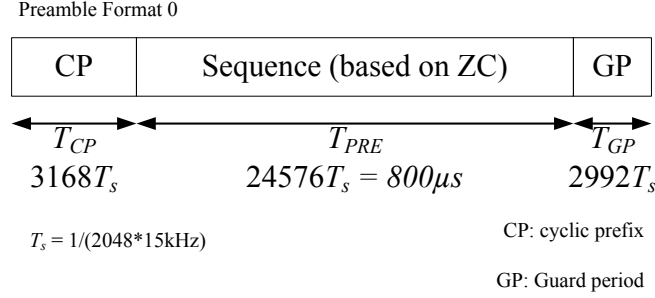


Figure 3. Random Access Preamble Format 0.

at the end of the preamble used for absorbing the propagation delay. The standard defines four different preamble formats for FDD operation [7]. Parameters T_{PRE} , T_{CP} and T_{GP} are set according to the chosen preamble format.

Figure 3 shows the parameter values for format-0 and the values for all formats are listed in Table 1 where T_s is known as the standard time unit which is used throughout the LTE specification documents. It is defined as $T_s = 1/(15000 \times 2048)$ seconds, which corresponds to a sampling rate of 30.72 MHz.

2.3. PRACH Preamble Signal

The PRACH preamble signal $s(t)$ can be defined as follows [7]:

$$s(t) = \beta_{PRACH} \sum_{k=0}^{N_{ZC}-1} \sum_{n=0}^{N_{ZC}-1} x_{u,v}(n) \cdot \exp \left[-\frac{j2\pi nk}{N_{ZC}} \right] \cdot \exp [j2\pi [k + \varphi + K(k_0 + 1/2)] \Delta f_{RA}(t - T_{CP})] \quad (3)$$

where $0 \leq t < T_{PRE} + T_{CP}$, β_{PRACH} is an amplitude scaling factor and $k_0 = n_{PRB}^{RA} N_{SC}^{RB} - N_{RB}^{UL} N_{SC}^{RB} / 2$. The location in the frequency domain is controlled by the parameter n_{PRB}^{RA} also known as $n_{PRB_{offset}}^{RA}$, (it is the input *frequency_offset_i* of the Time Domain Frequency Shifter module) expressed as a resource block number configure by higher layers and fulfilling $0 \leq n_{PRB}^{RA} \leq N_{RB}^{UL} - 6$, this inequality is only valid for formats 0, 1 2 and 3, *i.e.*, FDD. The factor $K = \Delta f / \Delta f_{RA}$ accounts for the ratio of subcarrier spacing between the PUSCH and PRACH and it is equal to 12 as $\Delta f = 15$ KHz and $\Delta f_{RA} = 1250$ Hz. The variable φ (equal to 7 for LTE FDD) defines a fixed offset determining the frequency-domain location

Table 1. Random Access Preamble Formats

Preamble format	T_{CP}	T_{PRE}	T_{GP}
0	$3168.T_s$	$24576.T_s$	2976
1	$21024.T_s$	$24576.T_s$	15840
2	$6240.T_s$	$2.24576.T_s$	6048
3	$21024.T_s$	$2.24576.T_s$	21984

of the random access preamble within the resource blocks. N_{RB}^{UL} is the uplink system bandwidth (in RBs) and N_{SC}^{RB} is the number of subcarriers per RB, i.e. 12.

By noticing that the inner summation is the DFT of $x_{u,v}(n)$ of length N_{ZC} we can rewrite equation 3 the following way:

$$s(t) = \beta_{PRACH} \sum_{k=0}^{N_{ZC}-1} X_{u,v}(k) \cdot \exp[j2\pi k \Delta f_{RA}(t - T_{CP})] \cdot \exp[j2\pi(\varphi + K(k_0 + 1/2)) \Delta f_{RA}(t - T_{CP})] \quad (4)$$

Again, by noticing that the first part of the summation in 4 is a time shift applied to the DFT of $x_{u,v}(n)$ we can rewrite that first part of the equation as follows by replacing t by Δt , which is referred in [7] as the standard time unit T_s , i.e., the sampling rate.

$$s(t) = \beta_{PRACH} \sum_{k=0}^{N_{ZC}-1} X_{u,v}(k) \cdot \exp[j2\pi k \Delta f_{RA} \Delta t (n - N_{CP})] \quad (5)$$

where N_{CP} is the number of samples corresponding to the CP interval as shown in Figure 3 and $\Delta f_{RA} \Delta t = 1/N_{PRE}$ (where for formats 0 and 1, $N_{PRE} = 24576$). Then rewriting equation 5 we have

$$s(t) = \beta_{PRACH} \sum_{k=0}^{N_{ZC}-1} X_{u,v}(k) \cdot \exp\left[\frac{j2\pi k(n - N_{CP})}{N_{PRE}}\right] = \beta_{PRACH} \cdot x'_{u,v}(n - N_{CP}) \quad (6)$$

Therefore as it can be easily seen the result of the above equation is nothing more than the application of the DFT's time-shift theorem. It is also easy to see that this equation is the IDFT of $X_{u,v}(k)$ with length N_{PRE} . With that in mind equation 4 can be rewritten as

$$s(t) = \beta_{PRACH} \cdot x'_{u,v}(n - N_{CP}) \cdot \exp\left[\frac{j2\pi(\varphi + K(k_0 + 1/2))(n - N_{CP})}{N_{PRE}}\right] \quad (7)$$

Equation 4 can be reorganized the following way

$$s(t) = \beta_{PRACH} \cdot \exp\left[\frac{-j2\pi N_{CP}(\varphi + K(k_0 + 1/2))}{N_{PRE}}\right] \cdot \left\{ x'_{u,v}(n - N_{CP}) \cdot \exp\left[\frac{j2\pi n(\varphi + K(k_0 + 1/2))}{N_{PRE}}\right] \right\} \quad (8)$$

The part of equation 8 between curly braces represents a circular frequency shift applied to $x'_{u,v}(n - N_{CP})$, i.e.,

$$x'_{u,v}(n - N_{CP}) \cdot \exp\left[\frac{j2\pi n m}{N_{PRE}}\right] \xrightarrow{DFT} X_{u,v}(K - m) \quad (9)$$

where m is the frequency shift applied to the PRACH signal before it is transmitted and it is given by the following equation

$$m = \varphi + K(k_0 + 1/2) \quad (10)$$

Once we are only dealing with FDD, equation 10 can be further simplified as

$$m = 13 + 144n_{PRB}^{RA} - 72N_{RB}^{UL} \quad (11)$$

Therefore, at the PRACH receiver side, after removing CP and GP the preamble is still shifted in frequency-domain by an offset factor given by m . For further processing, it is necessary to convert the shifted preamble into base-band. This conversion is performed by the Time-domain frequency shift module (see figure 2), which multiplies the received preamble by the conjugate of the complex exponential term given in equation 9.

3. Efficient Algorithm of a Time-Domain Frequency Shifter

In this section, we present an efficient algorithm used to apply frequency-domain shifts to random access preamble signals in time-domain (*i.e.*, without the need to convert them to the frequency-domain) through the use of a customized NCO and a complex multiplier. We also discuss the advantage presented by the proposed algorithm.

3.1. Numerically Controlled Oscillator

Numerically controlled oscillators (NCO), are important components in many digital communication systems. They are generally employed in quadrature synthesizers, which are used for constructing digital down and up converters, demodulators and here for time-domain frequency shifters. A common method for digitally generating complex or real valued sinusoids employs a look-up table (LUT) scheme [14]. The LUT stores samples of a sinusoid.

A digital integrator is used to generate a suitable phase argument that is mapped by the LUT to the desired output waveform. The integrator computes a phase slope that is mapped to a sinusoid (possibly complex) by the LUT. This value is presented to the address port of the LUT that performs the mapping from phase-space to time [15].

The LUT traditionally stores uniformly spaced samples of a cosine and a sine wave. These samples represent a single cycle of a length $N = 2^{B_{\Theta(n)}}$ prototype complex sinusoid and correspond to specific values of the sinusoid's argument $\Theta(n)$ as shown in Equation 12.

$$\Theta(n) = n \frac{2\pi}{N} \quad (12)$$

where n is the time series sample index and $B_{\Theta(n)}$ is the number of bits employed in the phase accumulator which is calculated as shown in Equation 13.

$$B_{\Theta(n)} = \log_2 \left\lceil \frac{f_{clk}}{\Delta f} \right\rceil \quad (13)$$

where $\lceil \cdot \rceil$ denotes the ceiling operator, f_{clk} is the system clock frequency and Δf is the frequency resolution of the NCO. The frequency resolution, Δf , of the NCO is a function of f_{clk} and $B_{\Theta(n)}$. Then Δf can be determined using the following equation

$$\Delta f = \frac{f_{clk}}{2^{B_{\Theta(n)}}} = \frac{f_{clk}}{N} \quad (14)$$

The output frequency, f_{out} , of the NCO waveform is a function of f_{clk} , $B_{\Theta(n)}$ and the phase increment value $\Delta\theta$. That is, $f_{out} = f(f_{clk}, B_{\Theta(n)}, \Delta\theta)$ which is given in Hertz and is defined in Equation 15. The phase increment, $\Delta\theta$ is an unsigned value which defines the NCO output frequency.

$$f_{out} = \frac{f_{clk}\Delta\theta}{2^{B_{\Theta(n)}}} = \frac{f_{clk}\Delta\theta}{N} \quad (15)$$

The fidelity of a signal formed by recalling samples of a sinusoid from a LUT is affected by both the phase and amplitude quantization of the process. The length and width of the LUT affect the signal's phase angle resolution and the signal's amplitude resolution respectively. These resolution limits are equivalent to time base jitter and to amplitude quantization of the signal, and add spectral modulation lines and a white broad-band noise floor to the signal's spectrum [16].

Quarter wave symmetry in the basis waveform can be exploited to construct a NCO that uses shortened tables. We will discuss this approach next.

3.2. Iterative Time-Domain Frequency Shift Algorithm

The optimized algorithm representing the Time Domain Frequency Shift operation is presented in Algorithm 1. It depicts the data processing executed by each one of the units in Figures 4.

At first, during eNodeB's initialization, the parameters *offset* and *bandwidth* (*bw*) are sent by higher layers to the PHY which in turn feeds them into the Time Domain Frequency Shifter module so that the Discrete Frequency Shift Calculator unit is able to calculate the actual frequency shift to be applied to the received PRACH signal. Whenever a subframe in which random access preamble transmissions are allowed happens (it is set according to Table 5.7.1-2 in [7]) and after CP is removed the Customized NCO unit generates a complex exponential signal with frequency set earlier by the Discrete Frequency Shift Calculator unit and multiplies it sample-by-sample with the incoming PRACH complex signal samples, note that it is a complex multiplication once both are complex signals.

The procedure inputs are *re_ad*, *im_ad*, *offset*, *bw* and *cos_table* where *re_ad* and *im_ad* are the already CP removed quadrature samples coming from the Analog to Digital Converter (ADC), *offset* and *bw* are the configuration parameters coming from higher layers and used to calculate the frequency shift necessary to translate the pass-band preamble signal back to base band and *cos_table* is the LUT containing the samples of a sinusoid used to generate the complex exponential signal. The Angle Mapper is the main part of the Customized NCO algorithm

shown in Algorithm 1 once it maps θ into a value of a 1/4-length cosine table.

In the light of what was presented in the previous section we now discuss the Algorithm 1. The first part of the algorithm is responsible for calculating the discrete frequency of the complex exponential signal that the NCO must generate in order to shift the received pass-band preamble signal to base-band. The discrete frequency shift, m , is calculated as shown in Equation 11. By remembering that $\Delta f_{RA}\Delta t = 1/N_{PRE}$ and then rewriting the exponential part of Equation 9 as

$$\exp[j2\pi(m\Delta f_{RA})t] \quad (16)$$

By analyzing the equation above it is noticeable that all frequency shifts are integer multiples of Δf_{RA} and this way we state that the output frequency of the NCO must be $f_{out} = m\Delta f_{RA}$. Before proceeding we must define the values for some parameters presented in the previous section. The frequency resolution $\Delta f = \Delta f_{RA} = 1250\text{Hz}$, the system clock frequency $f_{clk} = 1/T_s = 30.72\text{MHz}$, the length, $N = 2^{B_{\Theta(n)}}$ of the single cycle of the basis complex waveform is made equal to 24576 samples. The cycle length can be expressed as $N = f_{clk}/\Delta f_{RA}$. Then, using the aforementioned definitions and rewriting Equation 15 letting $\Delta\theta$ in evidence we have:

$$\Delta\theta = \frac{f_{out}N}{f_{clk}} = \frac{m\Delta f_{RA}N}{f_{clk}} = m \frac{\Delta f_{RA}}{f_{clk}} \frac{f_{clk}}{\Delta f_{RA}} = m \quad (17)$$

In case m is negative it is necessary to calculate its module in relation to N_{PRE} before feeding it into the customized NCO. Note in Algorithm 1 that the module operation is simply done by adding N_{PRE} to the negative value of m .

In a traditional NCO algorithm, *i.e.*, one that adopts full-period waveforms, there would be two main parts, namely, Phase Accumulator and LUT. In its simplest form, there would be 2 LUTs storing samples of a cosine and a sine wave. However, this approach generally results very large tables, which sometimes are impractical. Therefore, for a practical implementation with reduced tables, the proposed algorithm employs only one LUT exploiting quarter-wave symmetry in the basis waveform and the constant phase offset ($\pi/2$) between sine and cosine signals. In this approach we use one LUT with $N/4$ samples. However, when exploiting quarter-wave symmetry the mapping from phase-space to time is not direct as in the traditional NCO algorithm.

In order to exploit quarter-wave symmetry it is needed an algorithm to map the angle values (phase-space), θ , output by the phase accumulator into valid positions of a shortened LUT containing the samples of a cosine signal. This task is performed by the Angle Mapper part of Algorithm 1. The Angle Mapper maps angle values in the 2nd, 3rd and 4th quadrants into the 1st one and tracks the signals that must be applied to cosine and sine values. As can be seen in Algorithm 1 the indices for generating the cosine signal are calculated first and then a $N/4$ -phase offset, which is equivalent to a $\pi/2$ offset, is applied to it in order to generate the sine indexes.

In order to store values ranging from 1 to 0, *i.e.*, the 1st quadrant of a cosine signal, it would be necessary $(N/4) + 1$ samples where the last one is

Algorithm 1 Time Domain Frequency Shifter Algorithm

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1: procedure TDFREQSHIFTER(re_ad, im_ad, offset, bw, cos_table)
2:
3:   ▷ ***** Discrete Frequency Shift Calculator *****
4:    $m = 13 + 144 * offset - 72 * bw$ ;
5:   ▷ — Frequency Control Word (FCW) —
6:    $\Delta\theta = m$ ;
7:   if  $m < 0$  then
8:      $\Delta\theta = N + m$ ;
9:   end if
10:
11:   ▷ ***** Customized NCO Algorithm *****
12:    $\theta = 0$ ;
13:   for  $i \leftarrow 0$  to  $N - 1$  do
14:     ▷ — Angle Mapper —
15:      $\cos\_signal = 1$ ;
16:      $\sin\_signal = 1$ ;
17:     if  $\theta > 3 * N/4$  then
18:        $\cos\_idx = (N - \theta)$ ;
19:     else
20:       if  $\theta > N/2$  then
21:          $\cos\_idx = (\theta - (N/2))$ ;
22:          $\cos\_signal = -1$ ;
23:       else
24:         if  $\theta > N/4$  then
25:            $\cos\_idx = ((N/2) - \theta)$ ;
26:            $\cos\_signal = -1$ ;
27:            $\sin\_signal = -1$ ;
28:         else
29:            $\cos\_idx = \theta$ ;
30:            $\sin\_signal = -1$ ;
31:         end if
32:       end if
33:     end if
34:
35:      $\sin\_idx = (N/4) - \cos\_idx$ ;
36:
37:     if  $\cos\_idx == N/4$  then
38:        $\cos\_idx = ((N/4) - 1)$ ;
39:     end if
40:     if  $\sin\_idx == N/4$  then
41:        $\sin\_idx = ((N/4) - 1)$ ;
42:     end if
43:
44:     ▷ — Phase to Value Mapping (LUT) —
45:      $re\_nco(i) = \cos\_signal * \cos\_table(\cos\_idx)$ ;
46:      $im\_nco(i) = \sin\_signal * \cos\_table(\sin\_idx)$ ;
47:
48:     ▷ — Phase Increment (Phase Accumulator) —
49:      $\theta = (\theta + \Delta\theta)$ ;
50:     if  $\theta \geq N$  then
51:        $\theta = (\theta - N)$ ;
52:     end if
53:
54:     ▷ ***** Complex Multiplier *****
55:      $re\_bb(i) = re\_ad(i) * re\_nco(i) - im\_ad(i) * im\_nco(i)$ ;
56:      $im\_bb(i) = re\_ad(i) * im\_nco(i) + im\_ad(i) * re\_nco(i)$ ;
57:   end for
58:   return  $re\_bb$ ,  $im\_bb$ 
59: end procedure

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zero. The zero value can be mapped to the value stored at the $N/4$ -th position with minimal degradation on SFDR performance. Therefore, as can be seen in the algorithm, when either sine or cosine indexes are equal to $N/4$ their values are changed to $(N/4) - 1$, which is the closest value to zero.

As the LUT only stores samples from the 1st quadrant of a cosine signal, *i.e.*, only positive values, the Phase to Value Mapper part of the algorithm must apply the correct signals (provided by the Angle Mapper) to the LUT's output.

The Phase Increment (also referred as Phase Accumulator) part of the algorithm acts as an integrator. It calculates at each iteration of the algorithm a new phase value, θ , by using the phase increment $\Delta\theta$ value provided by the Discrete Frequency Shift Calculator part. Once the Angle Mapper algorithm can only map values ranging from 0 to $N - 1$ into the range 0 to $(N/4) - 1$ it is necessary to apply a module operation in case the resulting phase value is equal or greater than N . The module operation is easily performed by subtracting N from the phase value.

The last part of the algorithm multiplies sample-by-sample the generated complex exponential signal by the ADC signal. That complex multiplication operation then translates the pass-band PRACH signal into base-band.

3.3. Advantage of the Proposed Algorithm

The main advantage of the proposed algorithm is the memory savings attained by the use of a $1/4$ -length cosine table instead of storing in RAM each one of the $2N$ possible samples of a complex exponential signal. Table 2 shows the memory utilization for some data widths if we were to store all the $2N$ samples (sine and cosine waves) corresponding to one complete period of the basis complex exponential waveform necessary to translate the received PRACH signal into base band.

In Xilinx FPGAs, a Block RAM (BRAM) is a dedicated, *i.e.*, they cannot be used for anything but RAM, two-port memory containing several kilobits of RAM. A FPGA contains a limited number of these blocks. The configuration logic blocks (CLB) in most of Xilinx FPGA's contains a small RAM. They are called distributed (LUT) RAM because they are distributed throughout the FPGA once they are part of a CLB. This kind of RAM can normally store only a dozen bits.

A reasonable rule of thumb when designing with FPGAs is that if you need a lot of RAM, as is the case here, you should use BRAMs, otherwise the FPGA resources will be eaten up implementing the RAM in distributed RAM. It is im-

Table 2. Memory utilization when storing the full period of the complex exponential.

Data Width	Size in K-bits	# 36K BRAMs
8	384	11
12	576	16
16	768	22
24	1152	32

Table 3. Memory utilization when employing quarter-wave symmetry.

Data Width	Size in K-bits	# 36K BRAMs	Reduction in %
8	48	2	81.8
12	72	2	87.5
16	96	3	86.4
24	144	4	87.5

portant to say that a Virtex-6 FPGA device has only 416 36K-bits BRAMs which makes it a very precious resource when implementing a large project as a L1 PHY and in this way its usage must be taken into account during planning and development. One alternative to decrease the number of occupied BRAMs is the exploitation of quarter-wave symmetry in the basis waveform. This alternative results in a customized NCO that employs a shortened LUT. As can be seen in Table 3.

The fourth column in Table 3 shows the reduction of used BRAMs when exploiting quarter-wave symmetry. As can be noticed, this approach results in a more area efficient implementation because the memory requirements are minimized, *i.e.*, fewer FPGA BRAMs are required. Therefore this approach saves on valuable chip area and also reduces power consumption.

4. Implementation Details

This section presents some discussions on implementation details of the proposed architecture. It is suitable for implementation on devices that employ hardware description language (HDL) as part of its design process such as Field Programmable Gate Arrays (FPGA) and Application Specific Integrated Circuits (ASIC). Figure 4 shows the hardware architecture of the Time-domain Frequency Shifter module. The architecture employs only one LUT and exploits quarter wave symmetry for shortened tables.

The architecture works with two different system clocks, the first one of 30.72 MHz, is the clock used by the ADC unit and therefore dictates the rate the com-

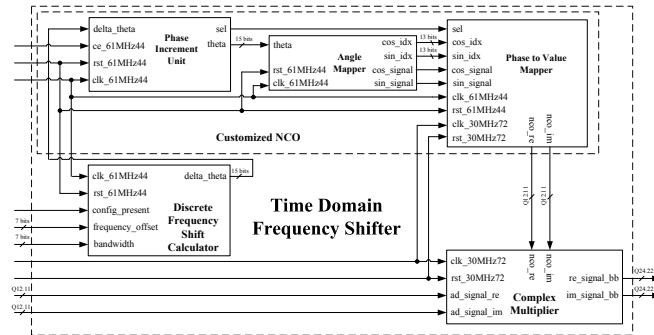


Figure 4. Blocks composing the Time-Domain Frequency Shifter module.

plex multiplication must be carried out. Only two units run at this rate, namely, Complex Multiplier and Phase to Value Mapper. The second system clock, 61.44 MHz, is employed so that 2 samples of the complex exponential can be retrieved from the same LUT within the period of one sample coming from the ADC. This double system clock mechanism further reduces the amount of RAM needed. All units run at this rate with only one exception, the Complex Multiplier unit.

The input parameters *frequency_offset* and *bandwidth* are fed into the module only when the eNobeB is being initialized. They can be considered static parameters of a eNodeB. The input signal *config_present* is asserted by higher layers during the initialization process to inform when the input parameter values are valid.

The Time-domain Frequency Shifter module needs to be informed by means of the *ce.61MHz44* signal when the sequence part of the preamble starts so that it can be multiplied by the complex exponential the Customized NCO unit generates. Signal *ce.61MHz44* is asserted by the PRACH receiver module after it discards the CP part of the preamble and must stay high for the whole duration of the sequence part, for example, for format-0 it must stay high for 24576 30.72 MHz-clock cycles, *i.e.*, 2×24576 when the 61.44 MHz system clock is considered. Once all units have registered outputs some latency is expected and then must be accounted for by the PRACH receiver when asserting the chip enable signal.

Other characteristic of the architecture is that it uses a total of 4 multipliers which are employed in the Complex Multiplier unit. Besides that, the architecture only employs bit-shift and add operations to evaluate trigonometric functions, *i.e.*, complex exponentials, turning it into a very efficient hardware architecture in terms of logic resource usage.

The proposed architecture can have its outputs and inputs totally configured, *i.e.*, input and output widths can be configured for one the following options: 8, 12, 16 and 24 bits. In our case we are using an ADC which outputs 12 bits for each one of the quadrature components I and Q and has fixed-point representation (Q Format) Q12.11, *i.e.*, 1 integer bit and 11 fractional bits. The quadrature components of the complex exponential generated by the Customized NCO have the same fixed-point representation of the input. In this regard, after the complex multiplication between ADC and NCO quadrature samples which involves multiplication and subsequent addition, the fixed-point representation of the output is Q25.22. As the maximum possible value produced by the complex multiplication operation is 2 the integer part only needs 2 bits instead of 3. In this way, depending on the configuration the fixed-point representation of the output complex signal can be set to Q8.6, Q12.10, Q16.14 and Q24.22.

4.1. Discrete Frequency Shift Calculator Unit

Figure 5 shows the architecture of the Discrete Frequency Shift Calculator unit. This unit is used to calculate the frequency shift, m , that must be applied to the received PRACH signal in order to bring it to base-band. Therefore, the unit implements

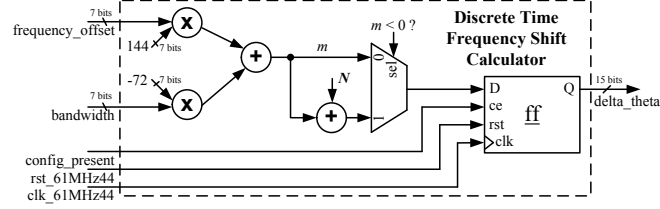


Figure 5. Architecture of the Discrete Frequency Shift Calculator unit.

Equation 11. All multiplications are performed through bit-shifting the input values n_{PRB}^{RA} and N_{RB}^{UL} by the constant values 144 and -72 respectively and then adding the result to the constant 13. Before feeding m into the Customized NCO unit it is necessary to check if the resulting value is negative, if so, the constant value N is summed to the resulting value then turning m into a positive value. It is done because the Phase Increment Unit composing the Customized NCO expects only positive values. As shown in Equation 17 the discrete frequency shift, m is equal to $\Delta\theta$ that is the input value necessary for the Customized NCO to operate.

4.2. Customized Numerically Controlled Oscillator

As can be seen in Figure 4 the Customized Numerically Controlled unit is made up of three blocks, namely, Phase Increment, Angle Mapper and Phase to Value Mapper. The first two units operate at 61.44 MHz and the last one operates at 30.72 and 61.44 MHz as it is the unit responsible for retrieving both quadrature values I and Q from the LUT within one period of the 30.72 MHz system clock.

Figure 6 shows the architecture of the Phase Increment unit. This unit implements a digital integrator which generates the phase argument, θ , fed into the Angle Mapper unit. At each iteration $\Delta\theta$ is added to θ which starts with 0. If the resulting θ value is greater than $N + 1$ the constant value $-N$ is added to it so that it stays less than N and thus can be correctly mapped into a valid value. This procedure is the direct implementation of a module operation, $\text{mod}(\theta, N)$. The unit only outputs a valid θ value when the selection, sel , signal is asserted. The sel signal is generated by a clock divisor which divides the 61.44 MHz clock by 2, i.e., the unit outputs a valid value at a rate of 30.72 MHz. The selection signal is also output by the unit in order to feed the Phase To Value Mapper unit. As Equation 13 is equal to N and it is not a power of 2, the data width of the Phase Increment unit, $B_{\Theta(n)}$, should be ceiled, resulting in 15 bits.

Figure 7 depicts the architecture of the Angle Mapper unit. This unit is responsible for translating the phase argument, θ , which can vary between 0 and $2 * \pi$ (0 to N) into a phase value within the first quadrant, i.e., a value between 0 and $\pi/2$ (0 and $N/4$). The resulting value gives the cosine index which is used as address to access one of the $N/4$ values stored in the LUT. In order to get the sine index a constant phase offset of $\pi/2$ i.e., $N/4$, is applied to the cosine index. As the value corresponding to $\cos(\pi/2)$, i.e., 0, is

not stored in the LUT whenever either cosine or sine indexes are equal to $N/4$ their values are changed to $(N/4) - 1$, which is the closest value to zero.

The unit is also in charge of tracking the signals that must be applied to the quadrature values I and Q at the output of the Phase to Value Mapper unit. These signals translate the phase argument, represented by the cosine and sine indexes, back to its original quadrant. At the input of this unit the phase argument, θ , has a data width of 15 bits so that it could access N samples, *i.e.*, all the four quadrants, however, as the Angle Mapper unit translates θ to the first quadrant the data width can be reduced to 13 bits that is the number of bits necessary to access the $N/4$ samples of the 1st quadrant (quarter wave symmetry) and which are stored in the LUT. It runs at 61.44 MHz and generates two new indexes, cosine and sine, at a 30.72 MHz rate once the phase argument θ is fed into the unit at that rate.

Figure 8 shows the architecture of the Phase to Value Mapper unit which is responsible for the mapping from phase-space to time. The cosine and sine indexes are used as addresses to access positions of the LUT. It is the LUT that performs the translation from phase-space to time. The LUT stores only $1/4$, *i.e.*, $N/4$, of the cosine signal used as basis waveform. The selection, *sel*, signal chooses whether cosine or sine index is used to read the LUT. As can be seen in Figure 8 the cosine index is used as address when *sel* is low and the sine index when it is high.

Both cosine and sine indexes stay constant for a 30.72 MHz clock cycle. As the LUT operates at a rate of 61.44 MHz and both indexes are simultaneously present at its input it is possible to retrieve 2 samples within one period of the 30.72 MHz clock. By creating a delayed data path (with the use of a register) at the output of the LUT it is possible to divert the in-phase (I) and quadrature (Q) samples to two different data paths and thus generating the complex exponential necessary to shift the received PRACH preamble to base band. At this point, the generated quadrature signal is synchronized to the 61.44 MHz system clock, however, each quadrature pair lasts for one period of the 30.72 MHz

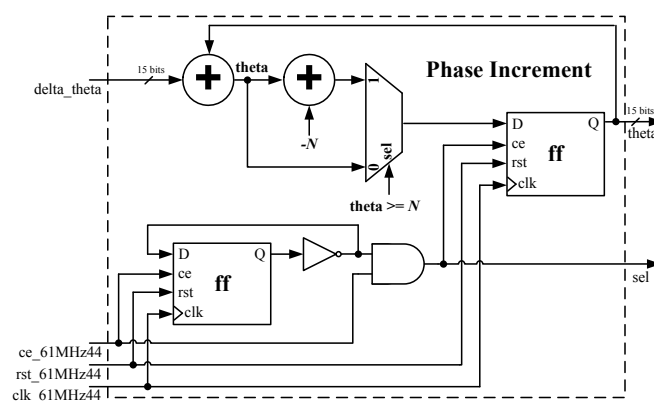
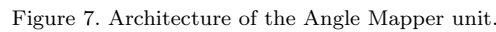


Figure 6. Architecture of the Phase Increment unit.



In order to translate the quadrature samples to their original quadrants the cosine and sine signals generated by the Angle Mapper unit are applied to their respective data paths. The signal change when due is easily performed by applying the two's complement to the sample value.

The diagram illustrates the Phase to Value Mapper architecture. It consists of four main stages, each containing a 2-to-1 multiplexer, a Look-Up Table (LUT), a D flip-flop, and a comparator. The first stage uses 'sel' and 'cos_idx[1:0]' to select between two inputs for the LUT. The LUT outputs are connected to the D flip-flop and the comparator. The comparator's output is connected to the D flip-flop and the next stage's multiplexer. The second stage uses 'sin_idx[1:0]' and 'clk_61MHz/40' as inputs. The third stage uses 'sin_signal' and 'cos_signal' as inputs. The fourth stage uses 'rst_30MHz/2' and 'clk_30MHz/2' as inputs. The final output is 'out[1:0]' labeled 'nco_0'.

Figure 8. Architecture of the Phase to Value Mapper unit.

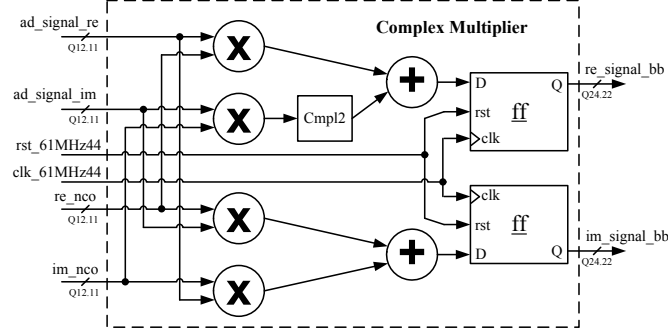


Figure 9. Architecture of the Complex Multiplier unit.

exponential signal is ready to be multiplied by the incoming PRACH preamble.

4.3. Complex Multiplier Unit

Figure 9 depicts the architecture devised for the Complex Multiplier unit. Once samples coming from both NCO and ADC are complex, it is necessary a complex multiplier to multiply then and perform the necessary frequency shift in time domain. The complex multiplier or also known as mixer multiplies the ADC samples, *i.e.*, the PRACH signal, by the complex exponential samples generated by the Customized NCO unit. The multiplication of two complex numbers, $a + jb$ and $c + jd$, results in the complex product given by Equation 18.

$$\begin{aligned} real + j * imag &= (a + j * b) * (c + j * d) \\ &= (ac - bd) + j * (ad + bc) \end{aligned} \quad (18)$$

As can be realized, the complex multiplication requires 4 multiplications and 2 additions once we consider a subtraction as being an addition in 2's complement. The Complex Multiplier unit operates at the system clock of 30.72 MHz once we must always respect the data rate dictated by the ADC.

5. Simulation and Implementation Results

In order to assess the efficiency of the Customized NCO and Time Domain Frequency Shifter units proposed in this paper some simulations were carried out. The proposed Time Domain Frequency Shifter architecture was developed in VH-SIC Hardware Description Language (VHDL) and a corresponding bit-accurate Matlab model, referred here as Golden Model (GM), was developed for verification. The full design was targeted to a Xilinx Virtex 6 xc6vlx240t FPGA.

The results presented next are split into parts, the first one provides simulation results for the Customized NCO architecture implementation and the second part presents results regarding the implementation of the Time Domain Frequency Shifter architecture.

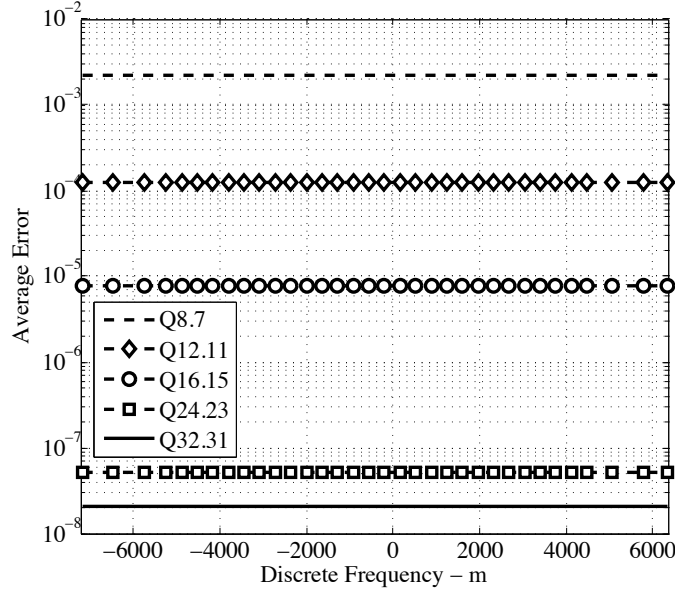


Figure 10. Average error between GM and DUT implementations of the Customized NCO.

5.1. Customized Numerically Controlled Oscillator

This section presents results regarding the Customized NCO implementation. The first simulation result, showed in Figure 10, compares floating-point precision Matlab generated complex exponential sequences with fixed-point precision sequences generated by the device under test (DUT) along all possible discrete frequency shifts, m , and for some Q-formats. PRACH format-0 preambles were considered for this and all other simulation results.

Figure 11 presents the SFDR variation of the implemented NCO unit, *i.e.*, the DUT, along all possible discrete frequency shifts, m and for some Q-formats. SFDR is the power ratio between the fundamental signal and the strongest spurious signal, *i.e.*, the most prominent harmonic, present at the output of the Customized NCO. By analyzing this result it is noticeable that the SFDR attained by the DUT is almost the same for formats Q24.23 and Q32.31. The SFDR values achieved by the DUT for formats Q24.23 and Q32.31 are 153.58 and 154.2 dB respectively. These high SFDR values are due to the fact that the phase increment bits are not truncated and all output frequencies, f_{out} , are integer multiples of the system clock frequency, f_{clk} , which is the frequency used to sample the basis waveform, and therefore, eliminating the spectral artifacts resultant from phase jitter [16].

As an illustrative example of the performance presented by the Customized NCO, figure 12 shows its Power Spectrum for some fixed-point formats with SFDR indication for frequency shift, m , equal to 7187, *i.e.*, 8983750 Hz. These results clearly show the cleanness achieved by the proposed Customized NCO even for

format Q8.7. The noise floor for format Q24.23 is so small that it is imperceptible.

Figure 13 depicts the SNR variation of the Customized NCO along all possible discrete frequency shifts, m and for some Q-formats. The SNR results are obtained by the ratio between the signal average power and the noise average power.

5.2. Time Domain Frequency Shifter

This section presents results regarding the implementation of the Time Domain Frequency Shifter architecture. From this point on we refer to the architecture implementation as the DUT. This time a Matlab floating-point model (GM) of the whole Time Domain Frequency Shifter architecture is used to assess the performance of the circuit.

Table 4 presents information on the resource utilization of the proposed time domain frequency shifter. It summarizes the main results obtained from the implementation of the proposed architecture on a FPGA device. The number of registers, occupied slices, LUTs, memory resources and Digital Signal Processor (DSP) resource blocks are presented. The maximum operation frequency reached by the module is 239.981 MHz.

From the results of Table 4, it can be noticed that 3 Block RAM (BRAM) memories are used instead of the 2 mentioned earlier. The synthesis tool maps the content of the LUT to 3 BRAMs because the number of bits used to address the LUT is 13, therefore, $\text{ceil}((2^{13} * 12)/36K) = 3$ instead of 2. Note that each position of the BRAM stores a 12-bit value sampled from the basis waveform. The 4 instantiated xilinx's DSP48 resources are employed by the Com-

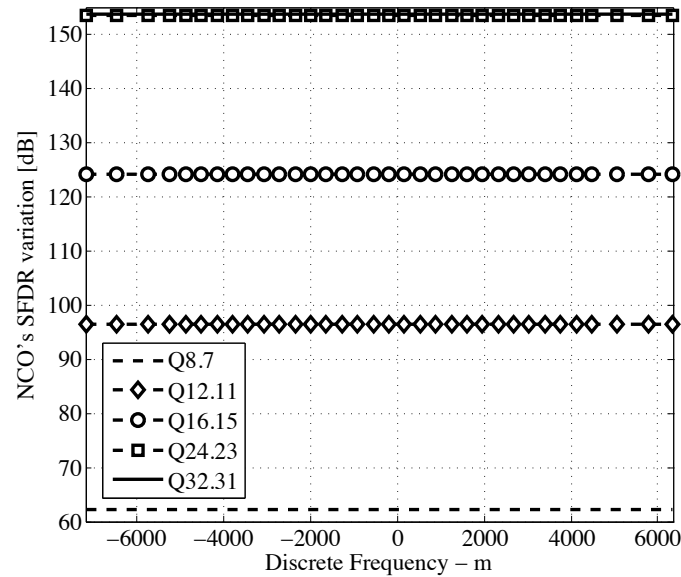


Figure 11. SFDR variation of the Customized NCO.

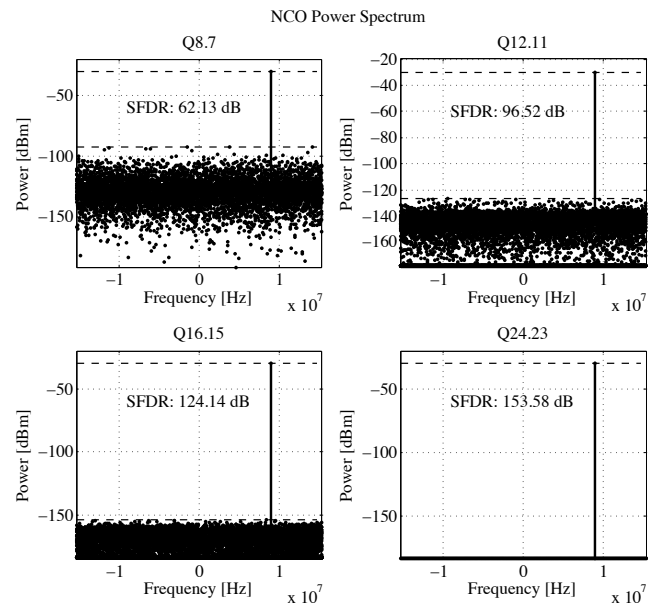


Figure 12. Customized NCO Power Spectrum.

plex Multiplier unit to implement the multiplication shown in equation (18).
In Virtex 6 family, 1 slice corresponds to 4 LUTs and 8 flip-flops. Block RAM/FIFOs are embedded resources of 36-bit memory. DSP48 is an embedded processing resource

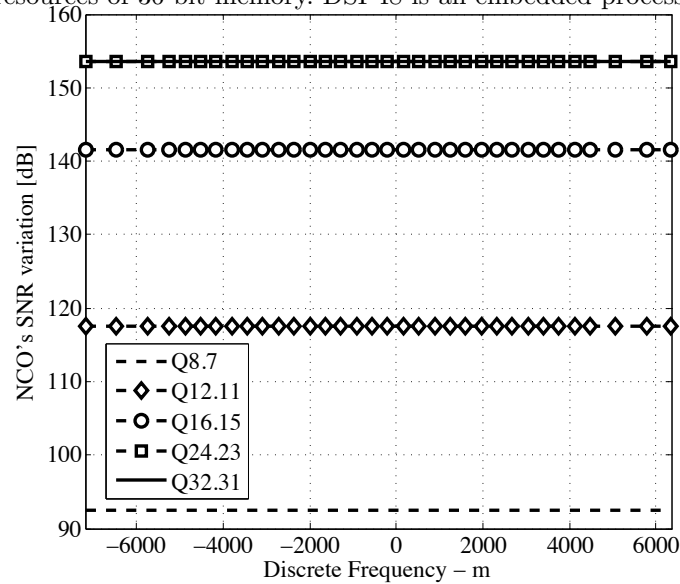


Figure 13. SNR variation of the Customized NCO.

equivalent to 1 multiplier with two 18-bit inputs and one accumulator of 48 bits.

The reuse of DSP48 resources is a feasible strategy that can further optimize FPGA area at the expense of an increased clock operation and additional control logic. For example, the four full-parallel multiplications present in the Complex Multiplier unit can be serialized saving 3 out of the 4 DSP48 already in use.

As can be noticed by analyzing Table 4, the proposed architecture occupies less than 1% of all Virtex 6 logic resources. The use of low cost FPGAs is allowed once the implementation of the proposed architecture on FPGA presents a very low occupancy rate. There are two points to take into account when choosing a low-cost FPGA: 1) the maximum achievable frequency, since low-cost FPGAs tend to have worse timing characteristics and 2) slice count could increase for technologies below Virtex-6, once other families may use 4-bit LUT instead of the 6-bit LUT per slice.

Figure 14 shows the average error between frequency shifted preambles produced by the GM and DUT. In order to get a concise plot the average error for a given preamble is averaged over all possible offsets applied to that preamble, *i.e.*, the figure presents the average of the average error over all possible offsets applied to a given preamble. The figure shows the average error for some Q-formats when the bandwidth parameter, N_{RB}^{UL} , is set to 25 and 50 RBs, *i.e.*, bandwidths of 5 and 10 MHz respectively, and the offset parameter, n_{PRB}^A , is varied along all possible values.

Figure 15 shows an exploded view of the results presented in Figure 14. Each subplot, representing the error for a specific Q-format, depicts the average of the average error over all possible offsets applied to a given preamble for 25 and 50 RB bandwidths. It is clearly seen that the error has a very small variation, almost constant, along the preambles.

Next we present results regarding the use of the Time Domain Frequency Shifter architecture proposed in this work in the context of the PRACH receiver at eNodeB PHY side. The PRACH receiver architecture adopted in this work is shown in Figure 2 and a bit-accurate Matlab model was developed for its verification.

At the receiver side, the eNodeB attempts to detect a transmitted preamble by first extracting the PRACH signal from a received OFDM signal. The extraction involves applying down conversion, analog to digital conversion, CP removal, frequency shift, demapping and decimation to the received PRACH signal. Next the receiver performs a matched filtering across the pool of preambles allocated to the eN-

Table 4. Resource Utilization

Part number	XC6VLX240T-1ff1156 (Virtex 6)
Number of Slice Registers	170 out of 301440 0%
Number of Slice LUTs	215 out of 150720 0%
Number of Occupied Slices	84 out of 37,680 0%
Number of RAMB36E1/FIFO36E1s	3 out of 416 0%
Number of DSP48E1s	4 out of 768 0%
Maximum Frequency	239.981 MHz

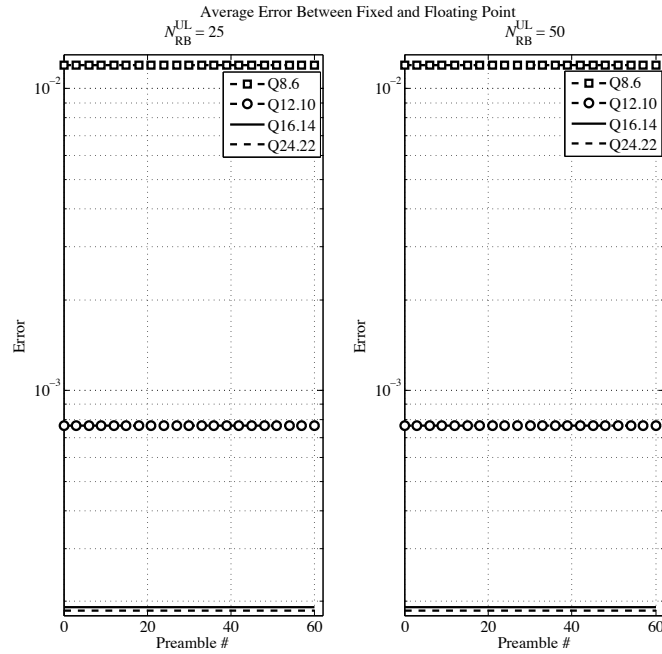


Figure 14. Average error between GM and DUT.

odeB. Matched filtering is performed as a circular cross-correlation between the extracted PRACH signal and each of the known preambles dedicated to the eNodeB.

The last block in the processing flow shown in Figure 2 is the preamble detec-

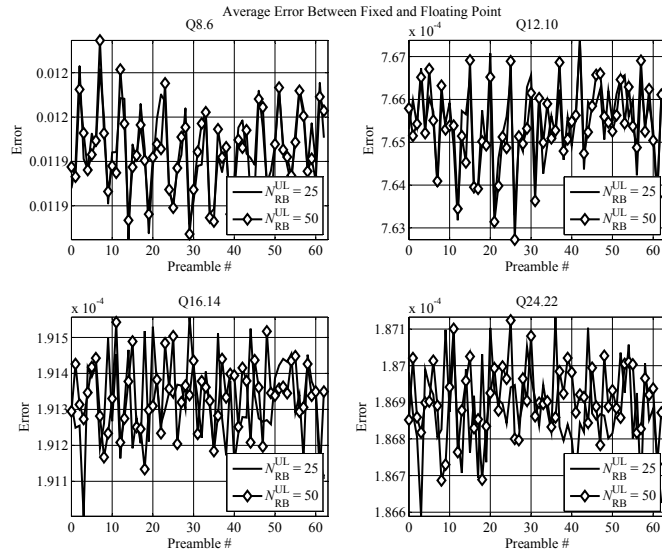


Figure 15. Exploded view of the average error between GM and DUT.

tion block which is used for detecting the transmission of random access preambles in the LTE PHY layer. This block implements the detection algorithm proposed in a previous work from the authors [12]. All samples coming out of the IFFT block have their squared modulus calculated producing the Power Delay Profile (PDP) samples. The block employs the PDP samples to estimate the noise power (it is done by identifying samples that can be considered as containing only the presence of noise) and set a detection threshold, based on that noise power estimate that minimizes the probability of false alarm rate. Based on that threshold the PRACH receiver can decide whether a preamble is present or not. As output, the detection block reports to the MAC layer the IDs and timing offset estimates of all detected preambles. The interested reader is referred to [4], [13] for a more detailed explanation on the proposed architecture and algorithm.

The bit-accurate PRACH receiver model incorporates the proposed algorithm for time domain frequency shifting. Format 0 preambles with $N_{CS} = 13$ and corrupted with Additive White Gaussian Noise (AWGN) were fed into the receiver model. With $N_{CS} = 13$ all the 64 preambles allocated to a specific cell can be generated from a single root ZC sequence.

By performing only one circular cross-correlation in the frequency domain between the noisy preambles and the corresponding root ZC sequence it is possible to detect random accesses attempts by UEs. The detection process follows the al-

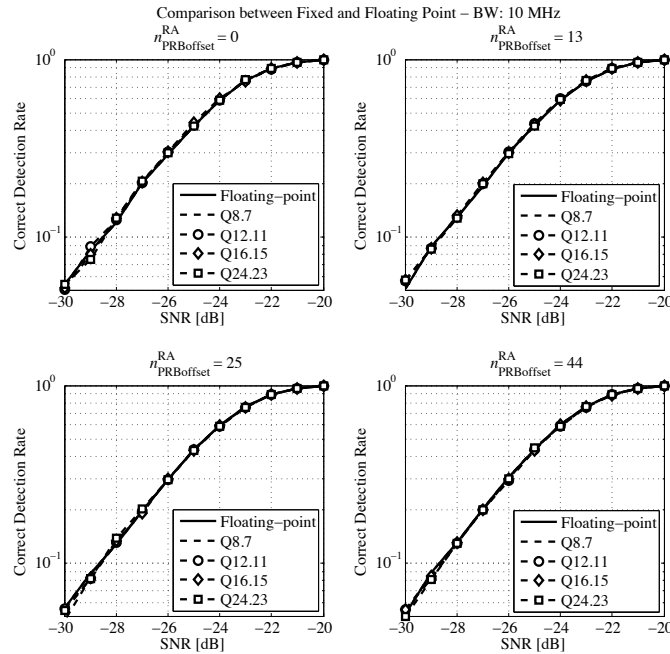


Figure 16. Comparison of the correct detection rate between the bit-accurate and the floating-point model.

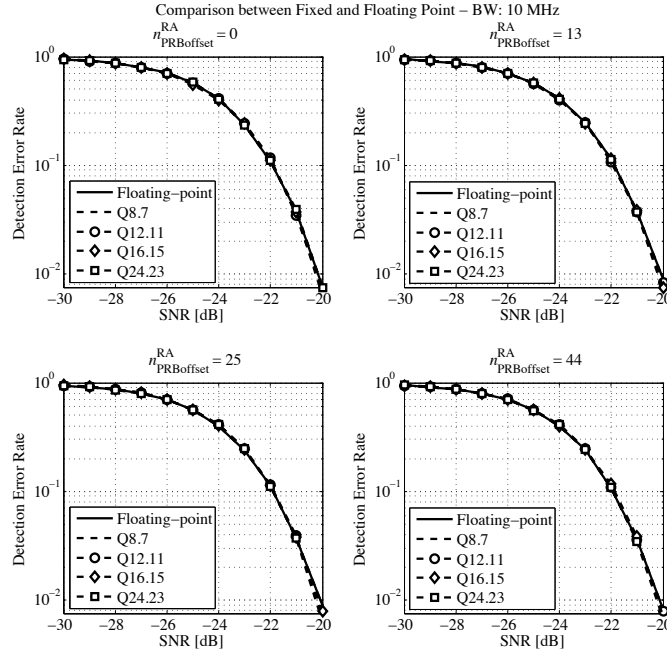


Figure 17. Comparison of the detection error rate between the bit-accurate and the floating-point model.

gorithm described in [12]. For the following results the bit-width of the output data-path of the proposed architecture was set to 8, 12, 16 and 24 bits, resulting in the fixed-point representations Q8.6, Q12.10, Q16.14 and Q24.22 respectively.

Figures 16 and 17 present the complementary results of preamble detection when the time domain frequency shifter is employed along with the preamble detection algorithm proposed in [12]. They depict comparisons between floating-point and some fixed-point

detection results when bandwidth parameter, N_{RB}^{UL} , is set to 50 RBs (10 MHz).

Each subplot in Figure 16 presents the comparison of the achieved correct detection rates versus signal-to-noise ratio (SNR) in dB for a given offset, n_{PRB}^{RA} . Figure 17 presents the comparison of the achieved detection error rates versus SNR for a given offset. For both plots the probability of false alarm (P_{fa}) is made equal to 0.1%. The plots demonstrate the high accuracy of the proposed algorithm and corresponding architecture in translating the received PRACH preambles to base band.

An important requirement for the PRACH receiver is that it must be capable of supporting a large number of users per cell with quasi-instantaneous access to the radio resources, and sustain a good detection probability, while maintaining a low false alarm rate. The probability of correct detection of random access preambles at PRACH receiver must be greater than or equal to 99% at an SNR of -8.0 dB, as defined [17], section 8.3.4.1.

By analyzing Figure 16 it is possible to see that the proposed algorithm achieves a probability of correct detection greater than 99% at a SNR of -21 dB, clearly outperforming [17] in 13 dB.

6. Conclusions

A hardware-efficient algorithm and architecture for translating PRACH preambles into base band featuring high-accuracy and low complexity characteristics has been presented. This paper is an extension of a previous work where we only introduced some superficial aspects of the proposed hardware architecture. In this paper we present theoretical derivations showing how to arrive at the equations used to design and implement the proposed architecture. We provide the pseudo-code for the proposed algorithm and discuss the advantage of the proposed architecture in terms of memory utilization when comparing our proposed solution with an approach where the full period of the complex exponential is stored in FPGA memory. The proposed architecture is optimized to shrink the use of BRAMs, multipliers and logic resources. The low resource utilization exhibited by the proposed architecture demonstrates its feasibility to be employed as part of large physical layer designs or to be used in FPGAs with small amount of logic elements.

Corresponding hardware architecture has been developed and employed in the PRACH receiver. Implementation and simulation results have demonstrated the efficiency, accuracy and low complexity of the proposed algorithm and architecture. Finally, this paper provides detailed information on the architectural design that was tested on a FPGA device for real time LTE applications.

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