

1 Article

2 The Young interferometer as optical system for 3 variable depolarizer characterization

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11 **Abstract:** In a depolarizing instrument, such as a broadband imaging spectrometer, the
12 depolarizers are placed on the system for stabilization the optical signal. They are also used to
13 reduce measurements offsets due to strong polarization dependence, which produce drastic
14 deterioration of the signal to noise ratio. Dynamic depolarizer with a controllable degree of
15 polarization is also required to study the effect of noise on quantum information. The article
16 described a new instrument for characterization the variable depolarizer with features which make
17 it different from a polarimetric system. The analysing system based on the simple structural design
18 and has good stability for real-time measurement. A practical application of the described
19 interferometer system for variable depolarizer characterization is also presented.

20 **Keywords:** Young interferometer; depolarization measurement; modulation of depolarization;
21 liquid crystal device
22

23 1. Introduction

24 Interference is a special example of the superposition principle. When two or more propagating
25 coherent waves are incidents on the same point, the resultant amplitude is equal to the vector sum of
26 the amplitudes of the propagating waves. The consequence of the superposition principle can be
27 observed as dark and bright stripes, and their distribution called as fringe pattern. In 1802 Thomas
28 Young performed the first experiment with interference between waves from two similar slits
29 illuminated by a single source of the light (double-slit Young's interferometer). Thenceforth
30 interferometers have found many technical applications. Regards they high accuracy and due to the
31 non-destructive property are often used for instance in medical diagnostics as optical coherence
32 topography instruments [1-2], blood flow [3], middle ear [4] or infectious diseases [5].

33 The interferometric measurement methods based on comparing images obtained from a
34 charge-coupled device (CCD camera) were proposed, also [6, 7]. They use a single CCD camera and
35 phase is calculated at every single pixel to give a phase map. From other side methods based on a
36 comparison of fringe pattern photos are limited. Complicated algorithms are supported to give a
37 value of the phase shift at each pixel, which is calculated with the help of neighbouring pixels. In
38 works [8-9], Mach-Zehnder interferometer configuration have been used with a single
39 photodetector. A quadrant photodetector and similar to the above technique was proposed to
40 measure the angular position of a parallel laser beam with an interferometric precision [10]. In
41 previously work, we proposed two-channel photodetector in Young interferometer using He-Ne
42 laser as a source of the light. The measurement itself is relative to the measurement using a CCD
43 camera, less time-consuming and does not require the use of complex algorithms. This is a
44 completely new tool for phase measurements adapted for liquid crystal (LC) materials [11].

45 Another interesting feature of a speckle is it polarization properties study. Polarization speckle
46 pattern consists of a constant polarization state in a reference beam and a random vector phasor sum

47 corresponding to the field scattered from an object in a second beam. Studying the polarization
48 changes of the light caused by a scattering media with a known initial state of the polarization of the
49 incident light is of great interest. The theoretical and experimental studies of polarization speckles
50 for different applications can be found in multiple papers [12-15]. All above applications use
51 polarized light with well-defined state of polarization (SOP) for their proper works according to
52 Fresnel -Arago conditions.

53 However many optical applications often require depolarized light. For instance in such
54 instrument as an optical spectrum analyzer, polarized incident light is strongly undesirable [16]. The
55 natural light is unpolarized light as well as light from thermal or gas sources. The unpolarized light
56 can be defined as light which vibrations of electric field take place randomly in directions
57 perpendicular to the direction of the wave propagation. According to this definition unpolarized
58 light is light for which the time averages of polarization component become equal to zero. Thus,
59 when the unpolarized light is transmitted through a polarizer, polarized light can be obtained with
60 constant efficiency. In contrast, depolarized light is obtained from polarized or partial polarized
61 light by special devices such as Lyott, Handle or Cornu depolarizer. It can be treated as the
62 composition of two component of equal intensity but contrary SOPs - two linear and perpendicular
63 SOPs, circular left and right SOPs or general two elliptical SOPs with perpendicular azimuths and
64 opposite circulation.

65 In this extended paper regarding the manuscript showed on I3S 2019: 7th International
66 Symposium on Sensor Science (I3S 2019) [17] we present an interferometric optical system for
67 variable depolarizer characterization, possesses the ability to study variable optical phenomena in
68 real time. We shall, therefore, be concerned with the SOP and the intensity of the light as it passes
69 through the variable depolarizer utilize a liquid crystal (LC) material.

70 2. Liquid crystal variable depolarizer

71 The polarization state of the light can be described by the Stokes parameters S_0 , S_1 , S_2 , S_3 . Then,
72 the degree of polarization (DOP) can be expressed as:

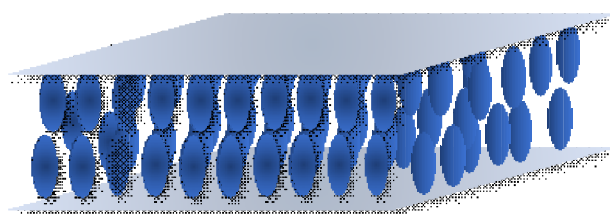
$$73 \quad DOP = \frac{\sqrt{S_1^2 + S_2^2 + S_3^2}}{S_0} \quad (1)$$

74 Depolarization effects can be related to spatially varying birefringent media, where DOP of a
75 partially coherent light decreases during propagation in the medium. Moreover, when a perfectly
76 polarized light beam passes through a depolarizing element, the light beam can be described as a
77 contiguous spatial distribution of a certain number of light beams, which are differently modulated
78 by the local birefringence.

79 The most known method of depolarizing light is the dispersion of light on porous structures
80 [18]. In these cases, we can observe optical losses inherently associated with light scattering. To
81 avoid losses, other methods of depolarization of light were investigated. Many works investigated
82 LC depolarizing properties [19-21], but there are still a lot of problems in this technology, as
83 instability of depolarizer with time or low depolarizing properties for sources with high coherence
84 length. In present work, we have proposed a depolarizing LC material with specific alignment
85 layers. The most detailed description of depolarizer is given by A. Shaham [22, 23]. All successful
86 designs have been based on his works, in which the depolarizer scheme is composed of a sequence
87 of birefringent crystals and wave plates. The wave plates were used instead of direct rotation of the
88 crystal to eliminate an unwanted angle dependent retardation. These methods suffer from bulkiness
89 and high cost.

90 LCs are functional materials possessing anisotropies originating from their inner molecular
91 alignment. At a nematic substrate interface as depicted in Figure 1, the tilt angle α is defined as the
92 angle between the easy axis of the nematic molecules and the normal to the surface. Depending on
93 the tilt angle, the alignment of the nematics can be categorized into two major groups: parallel
94 (planar) or perpendicular (homeotropic) alignment. In the first, the easy axis is parallel to the plane

95 of the surface (the tilt angle is $\alpha = 90^\circ$), whereas in second - the easy axis is vertical to the surface ($\alpha =$
96 0°). For optimum operation of variable depolarizer based on LC, a vertically aligned nematic (VAN)
97 LC with $\alpha = 0^\circ$ pretilts (Figure 1) was proposed. In the off state (voltage $V = 0$) is isotropic for light
98 impinging at normal incidence. However, the LC molecules orientation upon electric switching ($V \neq$
99 0) is undefined; therefore, the cell generates disordered birefringent medium related to undefined
100 switching direction of molecules which produce random polarization of the transmitted light.
101 Therefore depolarization effect is produced [24]. The symmetrical construction of the cell assures
102 that the performance will be the same for light coming from either side. The treatment of problems
103 involving depolarization of incident polarized light beam passing through a variable depolarizing
104 medium and general physical phenomena associated with it is the main element of our
105 investigation. A suitable tool for this treatment is previously reported Young's interferometer [25]
106 constructed with a new principle including the possibility to control the fringe pattern in real time
107 with the objective to study the dynamics of polarization fluctuation.



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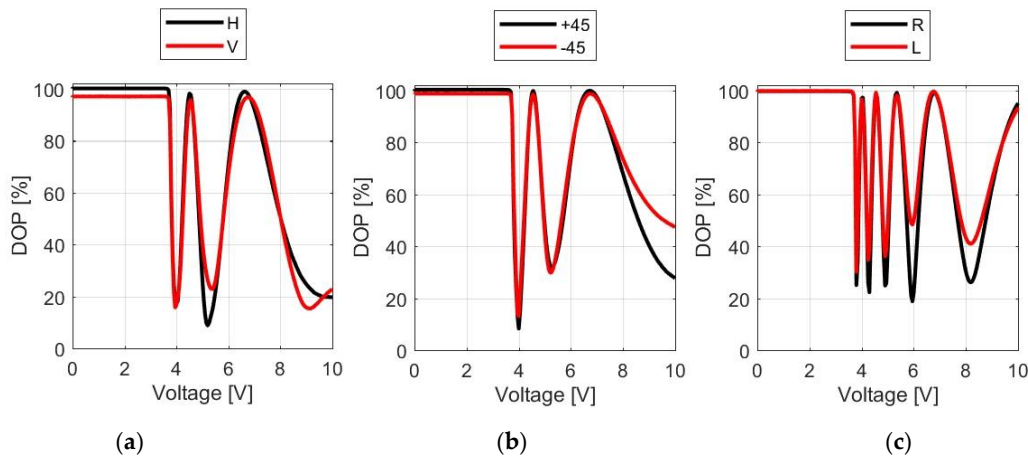
Figure 1. Homeotropic alignment in nematic LC cell.

110 3. The manufacturing process of the variable depolarizer

111 In our work, we have proposed a vertical aligned nematic liquid crystal cell as VAN depolarizer
112 (VAND) which uses 15 μm thickness cell filled with LCs having negative dielectric anisotropy.
113 Normally used conventional alignment layer induces a small pretilt in the vertical orientation angle.
114 Such VAN LC cell sandwiched between two crossed polarizers and orientated 45° concerning the
115 polarizer, is isotropic for light impinging at normal incidence when no voltage is applied to the cell.
116 After applying a voltage to the cell, preferred switching direction in VAN cell occurs, thus favoring a
117 specific switching plane. Therefore homogenous switching can be obtained. However, the organic
118 alignment layers like deoxyribonucleic derivatives crosslinked with surfactant complex such as
119 hexadecyltrimethylammonium chloride allow to obtain a vertical arrangement of LC molecules with
120 a non-pretilt ($\alpha = 0^\circ$). In this case, the LC orientation upon electric switching is undefined; therefore,
121 the cell generates chaotic structures. This produces the depolarization of the incident polarized light
122 because the switching direction of molecules is undefined and VAND is obtained.

123 To provide the polarization properties of the VAND, it is highly desirable known as the Stokes
124 vector of the transmitted light. Then the depolarization capability of the device for different SOPs of
125 the incident beam can be determined. To analyze the dependence of polarization properties of the
126 light passing through the VAND and to provide the full characterization of LC, the device should be
127 inserted into the special setup for polarization measurement. This setup must see unchanged light
128 intensity for any generated SOP. To maintain the intensity constant during the experiment, a
129 combination of a polarizer and a quarter-wave plate as a polarization state generator (PSG) has been
130 used [26]. As a detector, we implemented a polarimetric head to measure Stokes parameters, power
131 as well as DOP. During the measurements, VAND was inserted between PSG and polarimeter,
132 where the PSG enabled generation of the six input SOPs. For each of the six different SOPs, the
133 Stokes vector of the light transmitted by VAND is measured by the polarimeter. Therefore, the DOP
134 for VAND can be determined with high accuracy as is shown in Figure 2 for different input SOP [26].
135 These results show that with increasing voltage applied on structure, the DOP of transmitted light
136 decreasing because cell generates disordered birefringent medium related to undefined switching
137 direction of molecules. This phenomenon produces random polarization of the transmitted light.
138 The proposed VAND transmits the polarized component of incident light with a minimum DOP
139 equal about 0.08 for horizontal or ± 45 degree linear input SOP at 5.2 V or 4.0 V, respectively. In such

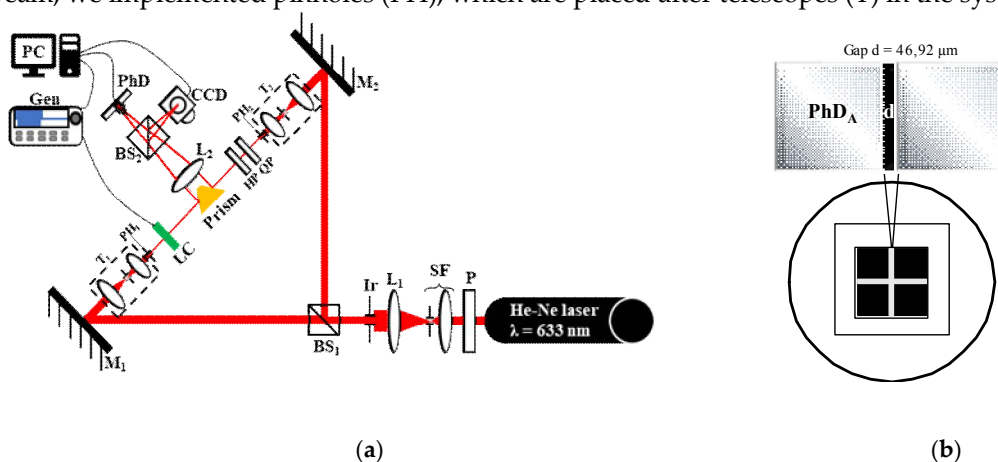
140 situation minimum intensity loss and scattering is observed. It is also worth to mention that the
 141 orientation of the depolarizer cell doesn't have an impact on obtained measurements.



142 **Figure 2.** Measurement results of the DOP for VAND as a function of applied voltage for different
 143 input SOP: (a) linear horizontal (H) and vertical (V), (b) linear with angle ± 45 deg. Respect to V, (c)
 144 circular right (R) and left (L).

145 3. Calibration and essential parameters of the applied interferometric measurement setup

146 We have investigated the intensity pattern of the light transmitted by VAND using mentioned
 147 above interferometer technique in experimental setup shown in Figure 3. The light from a He-Ne
 148 laser ($\lambda=633$ nm) passes through the polarizer (P) and is spatially filtered (SF) and collimated by a
 149 lens (L_1). Next, the light is splitting into two beams by the beam splitter (BS_1). The reference beam
 150 is reflected by a mirror (M_1), and a probe beam is reflected by a mirror (M_2). In both paths, telescopes
 151 consisting of two positive lenses were inserted to obtain a 400 μm diameter collimated beams. To
 152 adjust the equality of the diameter of the reference beam and the probe beam, two collimators with
 153 circular pinhole diameter were situated after telescopes. For depolarization properties
 154 characterization we have implemented a quarter-wave plate (QP) and a half-wave plate (HP) to
 155 generate six SOPs. Then, a right-angled gold coated prism bends the light coming from the
 156 collimators by 90° . Thus, the reflected beams become parallel to each other. To adjust the size of the
 157 beam, we implemented pinholes (PH), which are placed after telescopes (T) in the system.



158 **Figure 3.** The scheme of the interferometer setup: (a) general view, (b) the scheme of used PhD. Light
 159 source: He-Ne laser with $\lambda = 633$ nm; P - linear polarizer; SF - spatial filter; Ir - iris; BS - beam
 160 splitters; M - mirrors; T - telescopes, PH - pinholes; LC - liquid crystal cell; L_1 , L_2 - lenses; PhD -
 161 photodetector, Gen - generator, HP - half-wave plate, QP - quarter-wave plate.

162 The distance between two-point sources and the distance between two photodetectors
 163 significantly affects the performance of our setup. Due to the fact, that the distance between two

164 photodetectors is fixed, the calibration process requires the adjustment of the distance between two
 165 rays, which is affected by the position of the prism. If the position of the prism is changed, the
 166 intensities collected by photodetectors also change. Those intensities are collected in an acquisition
 167 card (DAC). LabVIEW software was prepared to record the data. Intensities from PhDA (I_A) and
 168 PhDB (I_B) are added or subtracted to each other:

$$169 \quad \text{Sum} = I_A + I_B, \quad \text{Diff} = I_A - I_B \quad (2, 3)$$

170 In reference [24], the detected signals are described as follows:

$$171 \quad S_R = a_1 + a_2 \cos \Delta\varphi - a_3 \sin \Delta\varphi \quad S_L = a_1 + a_2 \cos \Delta\varphi + a_3 \sin \Delta\varphi \quad (4, 5)$$

172 where S_L , S_R are the signals from the left and the right detectors, respectively and $\Delta\phi$ is a phase shift.
 173 Those signals depend on the combination of cosine and sine of the measured phase shift.
 174 Coefficients a_1 , a_2 , a_3 are constants depending on the wavelength, the distance between two beams d ,
 175 the focal length f of the Fourier lens and the size of the beam s and can be calculated from:

$$176 \quad a_1 = C \int_{d/2}^{\infty} \int_{-\infty}^{\infty} A^2(\rho) dy_f dx_f \quad (6)$$

$$177 \quad a_2 = C \int_{d/2}^{\infty} \int_{-\infty}^{\infty} A^2(\rho) \cos\left(\frac{4\pi dx_f}{\lambda f}\right) dy_f dx_f \quad (7)$$

$$178 \quad a_3 = C \int_{d/2}^{\infty} \int_{-\infty}^{\infty} A^2(\rho) \sin\left(\frac{4\pi dx_f}{\lambda f}\right) dy_f dx_f \quad (8)$$

179 where: $A^2(\rho)$ is the spatial distribution of amplitude in the Fourier plane, λ is the wavelength, d is the
 180 distance between two beams and f is a focal length of the Fourier lens and C is a constant value.
 181 Then, using the relationship describing the signals from the left and right side, the sum $\text{Sum} = (S_R +$
 182 $S_L)$ and the difference $\text{Diff} = (S_R - S_L)$ can be expressed as:

$$183 \quad \text{Sum}(\Delta\varphi) = 2a_1 + 2a_2 \cos \Delta\varphi \quad \text{Diff}(\Delta\varphi) = 2a_3 \sin \Delta\varphi \quad (9, 10)$$

184 According to equations (9), (10) a_1 is the amplitude of the sum function, a_2 is the average value
 185 of the sum function, and a_3 is the average value of the difference function. To determine the phase
 186 difference between the two beams we need to know the sum and the difference of the signal values
 187 of coefficients a_1 , a_2 , and a_3 :

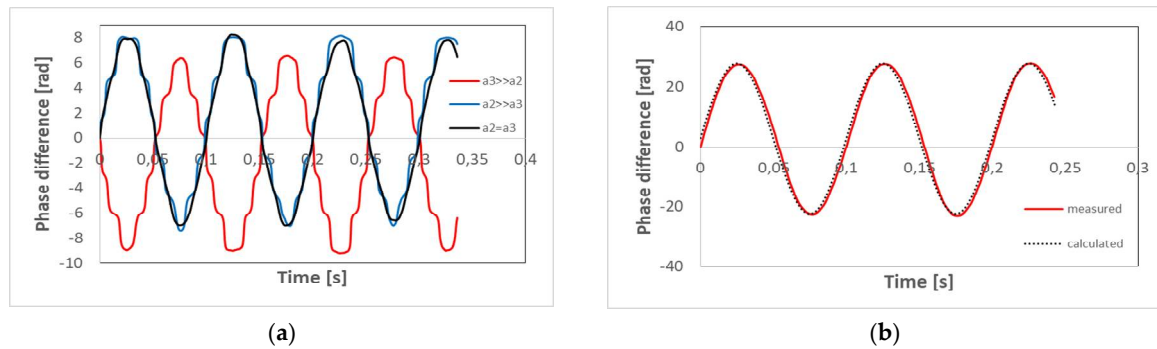
$$188 \quad \text{Sum}(\Delta\varphi) = 2a_1 + 2a_2 \cos \Delta\varphi \quad \text{Diff}(\Delta\varphi) = 2a_3 \sin \Delta\varphi \quad (11, 12)$$

189 The information about an error of the phase difference, induced by this system was analysed
 190 and described in reference and had the following expression [25]:

$$191 \quad \varepsilon = \frac{\rho - 1}{2} \sin(2\Delta\varphi) \quad (13)$$

192 where: $\rho = a_3/a_2$. According to equation (13), in the case of $\rho=1$ the error is equal to zero. Those results
 193 indicate that, when $a_3 = a_2$, the error is not dependent on the phase difference value.

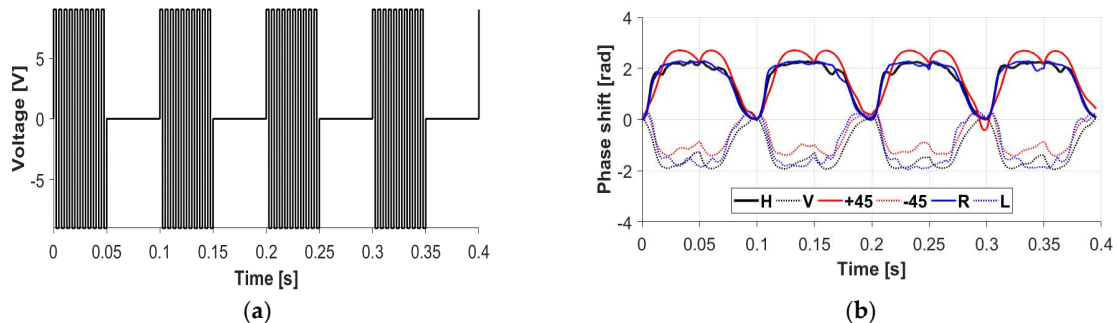
194 Calibration of the setup was performed using a piezoelectric mirror to induce a phase
 195 demodulation only in one arm of the interferometer. Results of phase demodulation as a function of
 196 time for three different positions of the prism is presented in Figure 4. The variation of the distance
 197 between two beams has a significant impact on coefficients a_1 , a_2 and a_3 , as well as on the quality of
 198 the performance of our device [Figure 4(a)]. At the same time in the case where: $a_2 = a_3$ experimental
 199 results are in good agreement with the theoretical model [Figure 4(b)].



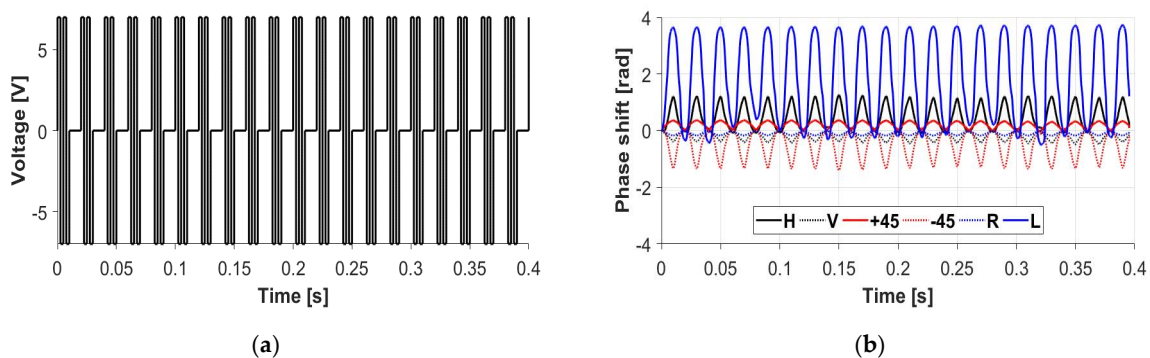
200 **Figure 4.** System adjustment: (a) Dynamic phase shift measurements at three different values of the
 201 distance between two beams d , (b) Comparison of the theoretical model (dotted line) and measured
 202 phase shift when coefficients a_2 and a_3 are equal.

203 4. Dynamic behavior of depolarizer VAND

204 The optical system, calibrated according to the procedure described above, performs an
 205 interferometric analysis for the spatial distribution of varying polarization in cross section of the
 206 depolarized beam transmitted by VAND. A more desirable depolarizer would operate with varying
 207 applied voltage. In the case of VAND, the applied waveform is sketched in Figures 5(a) and 6(a). The
 208 voltage pattern applied to VAND was 1 kHz AC voltage modulated by 10 Hz envelope with
 209 amplitude of 9 V [Figure 5(a)] and 50 Hz envelope with an amplitude of 7 V [Figure 6(a)]. We have
 210 measured with the investigation of an impact of the SOP of the reference beam on the depolarization
 211 capability of VAND. The beams in both arms are adjusted in such a way that their intensities are
 212 equal on recombination. In Figure 5(b) we have compared obtained response of VAND for the
 213 waveform shown in Figure 5(a).



214 **Figure 5.** The results of VAND investigation: (a) The voltage pattern applied to LC device (1 kHz AC
 215 voltage modulated by 10 Hz envelope with 9 V amplitude), (b) phase demodulation caused by
 216 VAND is driven by a signal (a) obtained for six SOPs measured for this waveform.



217 **Figure 6.** The results of VAND investigation: (a) the voltage pattern applied to LC device (1 kHz AC
 218 voltage modulated by 50 Hz envelope with 7 V amplitude), (b) phase demodulation caused by
 219 VAND is driven by a signal (a) obtained for six SOPs measured for this waveform.

220 For linear polarization, it can be noticed that the modulation depth is comparable for opposite
221 SOPs, i.e., horizontal and vertical or $+45^\circ$ and -45° of the reference beam. However, the sign of the
222 phase shift is different. This result reflects the correlation between orthogonal equal-intensity electric
223 field components at a single space-time point. This effect is manifested in Figure 5(b). In this case, the
224 DOP can be considered as the degree of correlation between the orthogonal components which is a
225 fundamental definition of unpolarized light. Increasing the modulation frequency of the applied
226 waveform [Figure 6(a)], the performance of the depolarizer has been changed. In this case for
227 circular polarization of the reference beam, we have obtained high demodulation for the circular left;
228 however, for the circular right, there is almost no modulation. Demodulation depth results
229 presented in Figure 6(b) give us information about the contribution of each polarization state caused
230 by the depolarizing device for a certain situation. In our case, the light after passing through VAND
231 device is depolarized maintaining right circular polarization the most dominant in the cross-section
232 of the beam.

233 This method implemented to investigate the polarization properties can give us new
234 information about tested depolarizer, which cannot be observed by standard methods. From the
235 analysis of the results of Figure 5(b) we conclude that the light transmitted by the investigated
236 VAND is totally depolarized, whereas in the case of Figure 6(b) is partially depolarized. This result
237 establishes a new, interferometric interpretation for the DOP of the unpolarized beam.

238 5. Conclusions

239 We have proposed a new approach of interpretation of the DOP directly from interference
240 obtained by Young interferometer setup in the time domain. The presented dynamic shift of the
241 interference pattern relates to the phase modulation controlled by VAND shows an ability of VAND
242 to generate polarization modulation when it is driven by modulated signal waveform. The proposed
243 technique can find future application in sensing devices as well as biomedical studies of
244 depolarization caused by different types of media.

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