

1 A New Approach for Planning M.C.W.H. Systems with Annual 2 Rainfall-Runoff Data

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3 **Abstract:** In this study a new approach for planning Micro-Catchment Water Harvesting (M.C.W.H.) systems for irrigation in
4 semi-arid regions such as the Aegean islands, is presented. M.C.W.H. is a cheap solution for constructing irrigation
5 infrastructure with zero energy cost in regions where water is scarce. The proposed approach introduces simple linear
6 relationships for estimating the annual volume of water V_s collected mainly from the CA (Contributing Area), stored
7 in the root zone (Infiltration Basin, IB), according to the annual rainfall and runoff depths, after having determined
8 the ratio of areas of micro-catchment (MC) components i.e. $\lambda = A_{CA}/A_{IB}$ and its whole area A_{MC} . This procedure was
9 applied in Paros island of the Cyclades complex in the middle of the Aegean sea in east Mediterranean. Besides,
10 income-cost analysis was performed via NPV method for almond, peach and apricot trees. The new approach was
11 proved versatile and easy to use. Besides, the investment turned out to be advantageous two years after the MCs
12 construction.

13 **Key words:** M.C.W.H., semi-arid regions, rainfall, runoff, V_s , λ , A_{MC} .

14 1. INTRODUCTION

15 In many regions of southern Europe (e.g. in most east Mediterranean islands), water is not
16 enough for intensive irrigation development. In some other cases, due to various technical and
17 economic reasons, water cannot be transferred over long distances. As a result, large areas remain
18 without irrigation water and therefore, they are solely dependent on rainfall (Tsakiris 1991). In
19 order to increase the availability of water for crop production, several types of Rain Water
20 Harvesting techniques (RWH) are used. One of the most common is Micro-Catchment Water
21 Harvesting (M.C.W.H.), which is a method for inducing, collecting, storing and conserving local
22 surface runoff for agriculture in arid and semi-arid regions (Boers and Ben-Asher 1982,
23 Giakoumakis 2008). M.C.W.H. is a likely viable option to increase water productivity at the
24 production system level. M.C.W.H. and similar techniques have a significant potential for
25 improving and sustaining the rainfed agriculture in the region of application.

26 M.C.W.H. is not a recent discovery. Throughout history, archaeological evidence has revealed
27 M.C.W.H. sites that were implemented in arid environments (annual rainfall less than 200 mm)
28 such as Jordan, the Negev desert in Israel, Syria, Tunisia and Iraq. The earliest signs of M.C.W.H.
29 are believed to have been constructed over 9000 years ago in the Edom Mountains in southern
30 Jordan (Adham et.al. 2016).

31 Low rainfall, water scarcity and land degradation severely intimidate the production capacities of
32 the rangelands in the arid environments. Surface crusting by raindrops helps generating frequent
33 local runoff on degraded sloping land, but it is generally lost in transmission and seldom flows
34 down to streams. Micro-catchments can capture local runoff, reduce transmission losses and
35 concentrate it into the plant basins. Thus, an efficient water harvesting planning is necessary for
36 increasing the runoff production potential of micro-catchments and water storage capacity of the
37 soil in the plant basins (Ali et al. 2007, Ali et al. 2010).

38 The purpose of the present paper is to assess the effectiveness of M.C.W.H. technique in a semi-
39 arid environment using here a new approach for planning the system, based on annual rainfall and

40 runoff data. Paros island of Cyclades in the middle of the Aegean sea was selected as region of
41 application. The proposed approach can also be used without any changes, in arid environments.

42 2. METHODS

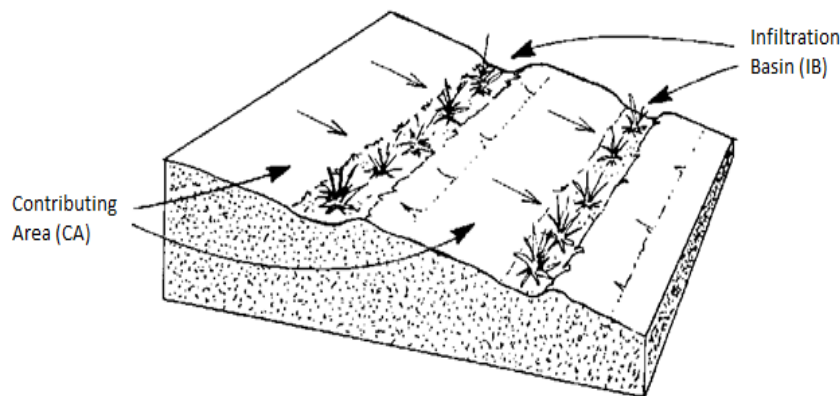
43 For determining design criteria in a M.C.W.H. system, the following was considered:

44 1. Based on measured annual rainfall data, design rainfall for a given return period (i.e. T=8
45 years, FAO 1991) is derived.

46 2. From the design rainfall, annual runoff is calculated via SCS-CN model (SCS 2004). The
47 latter has the advantage of incorporating rainfall losses as a function of CN number (Wanielista
48 1990) and it is preferable than other simplistic approaches (i.e. linear runoff model) in case of lack
49 of runoff data as in the present study. Other more complex rainfall-runoff models for designing
50 M.C.W.H. systems are used for single rainfall events such as the Kinematic Wave Equation and
51 experimental data are necessary for comparison purposes (Giakoumakis and Tsakiris 2001).

52 3. The annual water balance in the IB (Infiltration Basin) is a valid hypothesis, taking into
53 account that rainfall in semi-arid regions occurs mainly during the wet period of a hydrologic year
54 (from October to April) and almost not at all during the dry period.

55 A micro-catchment is composed from the Contributing Area (CA) where runoff occurs and the
56 Infiltration Basin (IB) where water is stored directly in the root zone for crop requirements (Fig. 1).



57

58 *Figure 1. Typical micro-catchment and its components (strip form IB), (FAO 1991).*

59 The annual runoff volume from CA to IB (m^3) is given by:

$$60 V_{CA} = 0.001 \cdot R \cdot A_{CA} \quad (1)$$

61 where:

62 R: runoff from CA (Contributing Area), (mm)

63 A_{CA} : area of CA (m^2)

64 The annual volume of water from rainfall P in the IB is:

$$65 V_{IB} = 0.001 \cdot P \cdot A_{IB} \quad (2)$$

66 where:

67 P: annual rainfall, (mm)

68 A_{IB} : area of IB (m^2)

69 If p is the percentage of volume of water infiltrating into IB and lost as deep percolation losses
70 or/and evaporation from soil surface, the water volume finally stored in the IB is:

$$71 V_s = (1-p) \cdot (V_{CA} + V_{IB}) \quad (3)$$

72 However, the annual volume necessary for crop water requirements in the IB is given by:

$$73 V_{RE} = 0.001 \cdot ET_c \cdot A_{IB} \quad (4)$$

74 where:

75 ET_c : potential evapotranspiration of the crop (mm).

76 Thus, for an effective planning it should be $V_s = V_{RE}$ Taking into account eqns 1, 2, 3 and 4, one
77 obtains:

$$78 A_{CA}/A_{IB} = [ET_c - P \cdot (1-p)] / [(1-p) \cdot R] \quad (5)$$

79 From eqn 5 the ratio $\lambda = A_{CA}/A_{IB}$ of areas of CA and IB can be calculated.

80 If A_{MC} is the total micro-catchment area in m^2 , then:

$$81 A_{MC} = A_{CA} + A_{IB} \quad (6)$$

82 Writing $\lambda = A_{CA}/A_{IB}$, from eqn 6, A_{CA} and A_{IB} can be expressed as follows:

$$83 A_{CA} = A_{MC} \cdot [\lambda / (1+\lambda)] \quad (7)$$

84 and

$$85 A_{IB} = A_{MC} \cdot [1 / (1+\lambda)] \quad (8)$$

86 Combining eqns 1, 2, 3, 7 and 8, yields:

$$87 V_s = 0.001 \cdot A_{MC} \cdot (P + R \cdot \lambda) \cdot [(1-p)/(1+\lambda)] \quad (9)$$

88 Eqn 9 can be viewed as a key-relationship, expressing the annual volume of water stored in the
89 IB (m^3) as a linear function of the total MC area, A_{MC} (m^2), with parameter λ being calculated from
90 eqn 5 for given annual rainfall and runoff depths, P and R (mm), respectively.

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97 3. STUDY AREA

98 The above was applied in Paros island in the middle of the Aegean sea (latitude 37° 5',
99 longitude 25° 14'), (Fig. 2). Although climatological conditions are appropriate for applying the
100 M.C.W.H. technique for irrigation, agricultural areas of the island are fed by drillings, leading to the
101 lowering of underground water level, increasing so the risk of salt water intrusion.

102



103

104 *Figure 2. Paros island and selected (dot) region's location for M.C.W.H application*

105 So, it was decided to select this island as a pilot region in order to prove that M.C.W.H.
106 technique may resolve with low cost the local irrigation problem and save so invaluable
107 underground water resources for other uses (i.e. drinking water after treatment). The region selected
108 has an area of 7 ha (200·350 m). Its position (in the north of the island, near Longovardas
109 monastery) is illustrated in Figure 2. It is ideal because all of the criteria for the installation of a
110 M.C.W.H. system are fulfilled (Rands 1980). Namely:

- 111 1. Soil slope between 2 and 8%
- 112 2. Medium soil texture
- 113 3. Soil depth greater than 1.5 m
- 114 4. Not cultivated land
- 115 5. Area of a few ha

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117 4. RESULTS AND DISCUSSION

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119 From the categories of M.C.W.H., the strip farming was selected because it is easily constructed
120 and well adapted in an inclined surface like the chosen one.

121 From the local station of National Meteorological Service having the same altitude as the mean
122 one of the selected area (i.e. 32 m a.s.l), a time series of annual rainfall date was used for the last 30
123 years. It was shown via χ^2 test that these data are well adapted to a normal distribution with mean
124 value $P_m=560.8$ mm and standard deviation $s=171.5$ mm. The well-known frequency factor
125 relationship was used for determining design rainfall depth, which, for a normal distribution is
126 written as:

127

$$128 P_T = P_m + s \cdot z \quad (10)$$

129 Where P_T is the design rainfall depth (mm) for a return period T and z is the variable of the unit
130 normal distribution:

$$131 \quad z = (P - P_m) / s \quad (11)$$

132 According to FAO (1991) a return period of 8 years was chosen. This corresponds to an
133 exceedance probability of 0,125 and thus $z = -1.15$. From eqn 10 one obtains $P_{T=8} = 363.5$ mm.

134 Using then SCS-CN model for initial losses 20% of the total with $CN=94$ (Wanielista 1990) for a
135 bare soil surface in the CA having previously been treated in order to minimize soil infiltrability
136 (category D), the corresponding total losses S were calculated as equal as 16.2 mm and annual
137 design runoff depth R was then derived as equal as 344.7 mm. The following relations have been
138 used:

$$139 \quad R = (P - 0.2 \cdot S)^2 / (P + 0.8 \cdot S) \text{ for } P > 0.2 \cdot S \quad (12)$$

$$140 \quad R = 0 \text{ for } P \leq 0.2 \cdot S$$

141 where:

142 P : rainfall depth (mm)

143 R : runoff depth (mm)

144 S : total losses (mm) given by (SI units): $S = (25.400 / CN) - 254$

145 Reference potential evapotranspiration was calculated via Thornthwaite formula because that
146 only mean monthly temperature and sunshine duration data were available from the nearby
147 meteorological station, that is the unique in the island. Monthly crop coefficients from April to
148 October for the arboricultures selected (i.e. almond, peach and apricot trees) were found in the
149 literature (Pontikis 1997). The annual values of crop evapotranspiration were as equal as $ET_c = 432.4$
150 mm for almond trees, whereas $ET_c = 603.7$ mm for peach and apricot trees.

151 Substituting the corresponding values of ET_c , P and R in eqn 5 with $p=0.3$, which sounds logical
152 for medium texture soils, the λ ratio for the MCs was calculated:

$$153 \quad \lambda = A_{CA} / A_{IB} = 0.7 \text{ for almond trees and } \lambda = A_{CA} / A_{IB} = 1.5 \text{ for peach and apricot trees.}$$

154 Thus, from eqn 9 one obtains:

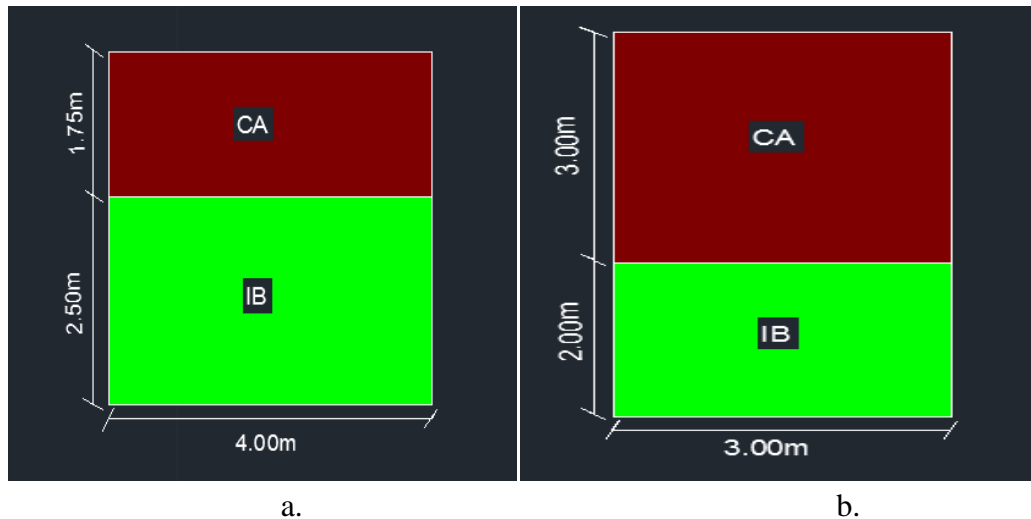
$$155 \quad V_s = 0.25 \cdot A_{MC} \quad (13)$$

156 for almond, peach and apricot trees. Thus, the annual volume of water V_s expected to be stored
157 in IB, equals for each kind of trees, the 25% of the total MC area.

158 Taking into account that for almond trees the root zone for each tree is of minimum diameter 2.3
159 m and that distance between trees should not be less than 4 m (Pontikis 1997), the proposed IB
160 dimensions for this arboriculture are: 2.5 m length and 4 m width, or $A_{IB} = 10 \text{ m}^2$. With computed
161 $\lambda = A_{CA} / A_{IB} = 0.7$, the area of the CA should be 7 m^2 with the same width as previously (i.e. 4×1.75
162 m). So, each MC in total will be 17 m^2 . According to eqn 13, the expected annual stored volume of
163 rainwater per IB for crop water requirements can reach 4.25 m^3 .

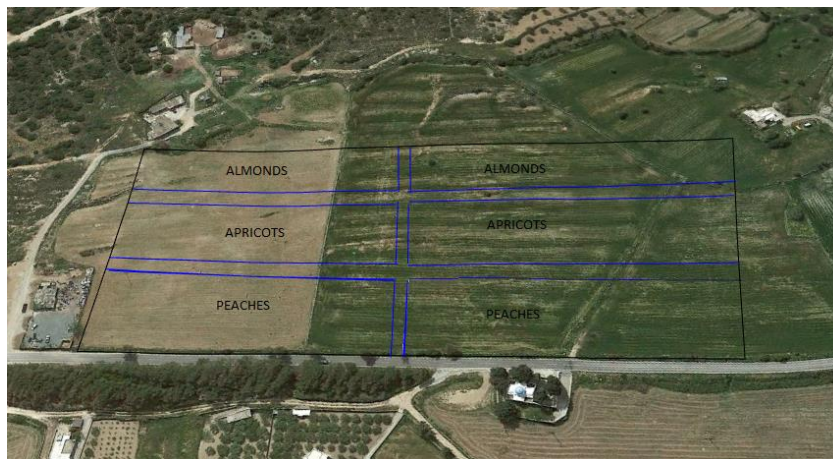
164 Besides, taking into account that for peach and apricot trees the root zone for each tree is of
 165 minimum diameter 1.8 m and that distance between trees should not be less than 3 m (Pontikis
 166 1997), the proposed IB dimensions for this arboriculture are: 2 m length and 3 m width, or $A_{IB}=6$
 167 m^2 . With computed $\lambda=A_{CA}/A_{IB}= 1.5$, the area of the CA should be $9 m^2$ with the same width as
 168 previously (i.e. 3x3 m). So, each MC in total will be $15 m^2$. According to eqn 13, the expected
 169 annual stored volume of rainwater per IB for crop water requirements can reach in this case $3.75 m^3$.
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171 MC's dimensions are illustrated in Figures 3a and 3b for almond and peach-apricot trees,
 172 respectively.



173
 174
 175 *Figure 3. MC's dimensions for: a). Almond trees b). Peach and apricot trees*

176 A rural road network will be constructed in the chosen area of 7 ha and so, the net irrigated will
 177 be of 6.6 ha or 2.2 ha per arboriculture. Thus, $22.000/17= 1.294$ almond trees will be planted, also
 178 $22.000/15=1.467$ peach trees and 1.467 apricot trees (Fig.4).



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 182
 183 *Figure 4. Region of application*

184 The cost of construction is summarized in the following Table:

185 *Table 1. Cost of construction (€)*

Category	
Earthworks + CAs surface treatment	21.000
Trees purchase and plantation (*)	85.000
SUM	106.000

186 (*) All kind of trees will be three year old for giving fruits immediately (Pontikis 1997).

187 The estimated total annual cost for fertilizers, pesticides and pruning for 4.228 trees is 10.000 €.

188 For almond trees the mean annual production is 10 kg/year/tree with selling price from the
189 producer 6 €/kg (Nanos 2018). For peach trees 40 kg/year/tree with 0.3 €/kg and for apricot trees 35
190 kg/year/tree with also 0.3 €/kg (Tavoularis 2012). Thus, the annual income for the producer is
191 expected to be (Table 2):

192 *Table 2. Annual income (€)*

Category	
Almond trees	$6.0 \cdot 10 \cdot 1.294 = 77.640$
Peach trees	$0.3 \cdot 40 \cdot 1.467 = 17.604$
Apricot trees	$0.3 \cdot 35 \cdot 1.467 = 15.404$
SUM	110.648

193 Economic evaluation of the application of the M.C.W.H. technique was performed by the well-
194 known NPV (Net Present Value) method (Tsakiris 2006):
195

$$196 \quad NPV(i, N) = \sum_{t=0}^N \frac{R_t}{(1+i)^t} \quad (14)$$

197 where:

198 t the time of the cash flow

199 i the discount rate

200 N the total number of periods

201 R_t the net cash flow (i.e. cash inflow – cash outflow), at time t .

202 $i=10\%$ (mean value for reclamation works in Greece).

203 Results from eqn (14) are presented in Table 3:

204

205 *Table 3. NPV (€)*

Year	Cash outflow	Cash inflow	R	NPV
0	106.000	0	-106.000	-106.000
1	10.000	110.648	100.648	91.498
2	10.000	110.648	100.648	83.180
SUM				68.678 > 0

206

207 From Table 3 one concludes that the investment is advantageous two years after the MCs
208 construction (i.e. $SUM > 0$).

209

210 5. CONCLUSIONS

211 In the present study a new approach for planning micro-catchments for the M.C.W.H. technique
212 is proposed. After having determined the ratio λ of the areas of the components of each micro-
213 catchment, the annual water volume expected to be stored in the root zone of each IB, can be
214 estimated. The relevant relationships derived in this work, are of linear form and easily applied,
215 provided that annual design rainfall and runoff depths are known. The new approach was applied in
216 a region of Paros island of the Aegean sea with semi-arid climatic conditions. It was proved via
217 NPV formula, that M.C.W.H. technique as irrigation method exploiting natural rainfall, is
218 advantageous for the region, two years after the MCs construction.

219

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