

1 Article

2 Updating the Role of Reduced Graphene Oxide Ink 3 on Field Emission Devices in Synergy with Charge 4 Transfer Materials

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20 **Abstract:** Hydroiodic acid (HI) treated - reduced graphene oxide (rGO) ink/conductive polymeric
21 composites are considered as promising cold cathodes in terms of high geometrical aspect ratio and
22 low field emission (FE) threshold devices. In this study, four simple, cost-effective, solution-
23 processed approaches for rGO-based field effect emitters were developed, optimized and
24 compared; rGO layers were coated on a) n⁺ doped Si substrate, b) n⁺-Si/P3HT:rGO, c) n⁺-
25 Si/PCDTBT:rGO and d) n⁺-Si/PCDTBT:PC₇₁BM:rGO composites, respectively. The fabricated
26 emitters were optimized by tailoring the concentration ratios of their preparation and field emission
27 characteristics. In a critical composite ratio, FE performance was remarkably improved compared
28 to the pristine Si, as well as n⁺-Si/rGO field emitter. In this context, the impact of various materials,
29 such as polymers, fullerene derivatives, as well as different solvents on rGO function reinforcement
30 and consequently on FE performance upon rGO-based composites preparation was investigated.
31 The field emitter consisted of n⁺-Si/PCDTBT:PC₇₁BM(80%):rGO(20%)/rGO displayed a field
32 enhancement factor of ~2850, with remarkable stability over 20h and low turn-on field in 0.6V/μm.
33 High-efficiency graphene-based FE devices realization paves the way towards low-cost, large-scale
34 electron sources development. Finally, the contribution of this hierarchical, composite film
35 morphology was evaluated and discussed.

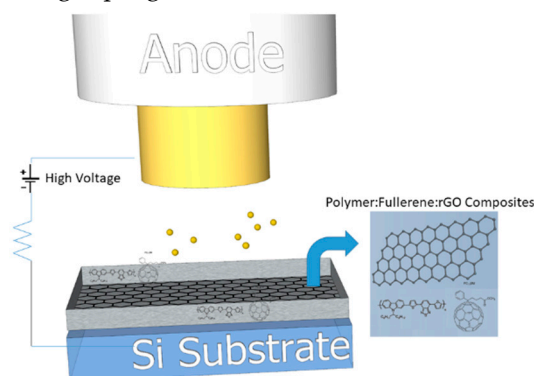
36 **Keywords:** Field emission; graphene; reduced graphene oxide; polymer composites; graphene ink;
37 cold cathode; Fowler-Nordheim

39 1. Introduction

40 Upon the existence of a strong electric field that passes through a barrier, high-density electrons
41 are emitted by a sharpened cathode tip. This quantum mechanical tunneling phenomenon is well
42 known as field emission (FE) or “cold cathode” emission. Since higher aspect ratios (height/tip radius)
43 are pursued for the generation of higher FE currents at lower applied electric fields, material
44 properties and cathode configuration are essential for FE characteristics [1]. The wide expansion of
45 FE in various applications including electron guns [2], microwave power amplifiers [3], X-ray tubes
46 [4], neutralizers used in space propulsion devices [5], electron beam lithography [6] and large area

47 field emission sources like flat panel field emission displays (FEDs) [7] stipulates intensive research
48 efforts towards the design and production of electron emitting cold cathodes with improved
49 performance (Figure 1). Aside from that, due to the high-performance requirements of FE materials
50 such as high FE current as well as electrical and mechanical durability in highly distorted geometries,
51 recent FE potential for the realization of integrated flexible devices still constitutes an additional
52 engineering and research challenge. The field enhancement factor β is considered as crucial
53 parameter for the performance of a FE cathode, which can be boosted by increasing the aspect ratio,
54 corresponding to the emitter height over its tip radius. In this context, nanotubes and nanosheets
55 have been considered as emerging materials for FE applications due to their unique 1D and 2D
56 nanostructured geometry, respectively [8-9]. Indeed, the fact that the aspect ratio becomes
57 increasingly high is attributed to their nanoscale tip curvatures and relatively long microscale
58 lengths. Therefore, such nanostructures promote the efficient electron emission at weak applied fields
59 through the generation of a large electric field enhancement.

60 Although various 1D nanostructures have been placed under the research scope, especially
61 carbon nanotubes (CNTs) have attracted industry's early interest as emerging FE [8-10] for CNT-
62 based FEDs commercialization [11] yet with questionable survival in market. One of the prime
63 concerns is the absence of long lasting FE stability [12] by virtue of the rapid degradation witnessed
64 in CNTs-based emitters, although their electron emission density is tremendous [13]. In addition, in
65 oxygen-rich conditions, CNTs display a perpetual decrease in the FE current density while on the
66 contrary, V_{th} increases [14]. Due to this fact a bottleneck occurs for CNT-based applications, especially
67 in FEDs, under low vacuum or gas purged conditions.



68

69 **Figure 1.** Schematic representation of a Field emitter cathode based on rGO-charge transfer materials
70 composites.

71 The research rush for graphene and 2D single layer semiconducting materials as inorganic
72 analogues of graphene that demonstrate exceptional physical, optical, and electrical properties has to
73 do mainly with its 2D atomic layer structure [15-16]. However, a low number of studies on the FE
74 properties from such materials, like MoS₂ sheets, have been undertaken [17]. Moreover, WS₂
75 nanotubes also exhibit good FE performance and stability comparable to carbon nanostructure-based
76 field emitters by virtue of their relatively small bandgap, limited number of dangling bonds,
77 mechanical stability and nontoxicity. Therefore, they pose a promise for a spectrum of technological
78 applications [18]. Yet, WS₂ nanotubes have to be complemented with semiconductive polymer,
79 mostly P3HT [19] in order to prevent aggregation of the NTs thus enhancing performance of cathodes
80 without polymer. What is more, a polymer matrix is often needed in order to observe protruding
81 nanotubes onto microstructured substrates. This may be ascribed to the low surface tension of
82 NTs/P3HT solution and the large substrate roughness [18]. Alternatively, since the conducting
83 polymer composite serves as an intermediate layer between the WS₂ nanotube or CNT emitters and
84 a conducting substrate, the electrical contact is improved through the reduction of contact resistance,
85 thereby enhancing overall FE performance [1]. Also, the low electron affinity, wide bandgap excellent
86 transport properties and flexibility of such polymer-based cathodes have rendered composites of
87 semiconductive polymers with 1D or 2D nanomaterials vital to final related FE optimization [21].

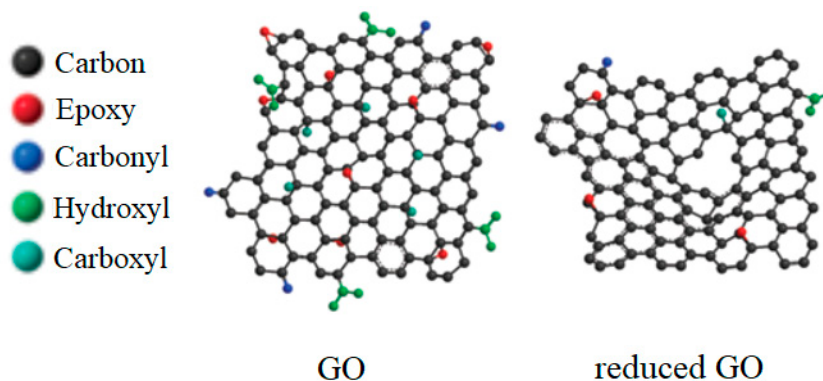
88 Furthermore, recently, the way to exploit transition metal dichalcogenide (TMD) in FE was cleared
89 with geometrically modulated, CVD-grown MoS₂ and MoSe₂ monolayer semiconductors that were
90 suspended with 1D nanoarrays of ZnO was demonstrated, thereby enabling the geometrical
91 modulation and tuning charge transfer [22].

92 An extended use of graphene nanosheets [15,23] for FE cathodes development is present, thank
93 to their extraordinary physical, mechanical and chemical properties [18-19,23]. Moreover, the planar
94 2D structure of graphene renders it to an ideal material for large-area FE devices realization. Since
95 graphene consists of flakes with high aspect ratio, as well as sub-nanometer edges, turning graphene
96 into a superior FE is easy, hence allowing the electrons' extraction at low threshold electric fields with
97 high geometric field enhancement. Although CVD is one of the most successful methods to produce
98 a graphene-based FE, since edge states dominantly contribute to emitting electrons, controlling the
99 orientation of edges perpendicular to substrates is indispensable. In the CVD case, the resulting
100 graphene must go through complex processes such as laser writing [1], plasma treatment [24] or
101 substrate modification [25] so as to create vertical edges, thereby engaging expensive fabrication
102 equipment and long-term procedures.

103 Other graphene-based FE cathode fabrication routes include liquid phase exfoliation from
104 graphite or exfoliation of graphene from a carbon cloth's fibers followed by coating graphene solution
105 on a conductive substrate (e.g. Cu) [26-27], electrophoretic deposition (EPD) [27-28], screen printing
106 accompanied with selective photoetching techniques [29], or even blade and ultrasonic spray coating
107 [30] to name just few of them.

108 Apart from the previous techniques, chemical oxidation of bulk graphite by Hummers is a strong
109 candidate for resulting to the high yield production of graphene oxide (GO). For instance, a low-cost
110 and successful chemical method to synthesize FE-applicable reduced GO, the Annual-Ring Graphene
111 (ARG) method [31], which demonstrates the advantage of facile synthesis, yields abundant vertical
112 edges on the cross-section of ARG, hence equaling or even surpassing FE performances of CNT [13],
113 cannon-structured graphene film [32] and rGO/MnO₂ composite [33], not to mention the ultralight
114 weight and flexible nature of the cathode. In general, albeit GO has a similar atomic single layer
115 structure to graphene, the existence of oxygen functional groups attached onto sp³ hybridized carbon
116 atoms impacts on its conductivity loss, mainly due to the presence of epoxy and hydroxide groups
117 on its basal plane [34], as illustrated in Figure 2. In order to come up against this side effect and to
118 partially recover the conductivity, various reduction methods have been developed to reduce GO
119 in the form of rGO towards the realization of efficient electronic functionalities.

120 Chemical reduction can in general be achieved in both liquid and gas phases [35]. Chemical
121 reducing methods include agents that range from hydrazine [36-39] and Hydrogen Iodide gas [40]
122 until even ascorbic acid [41], KOH or NaOH [42]. Aside from chemical, thermal reduction at high
123 temperature under inert atmosphere [34,43], and application of either electric [44] or electromagnetic
124 field [45] are also successful reduction routes.



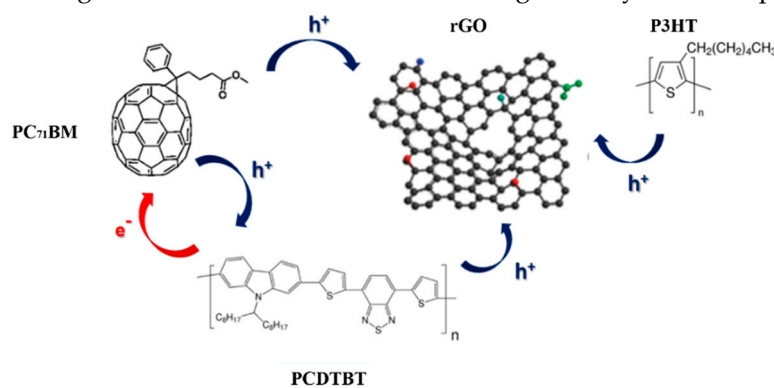
126 **Figure 2.** Depictions of GO and rGO structures. Reproduced with permission from P. K. Nayak,
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128 Before moving into plain comparison of FE parameters, considering the way of GO reduction is
 129 essential to deeper understanding the correlation between FE and GO, while taking into account only
 130 the geometric aspect ratio is insufficient on its own. Oxygen/Carbon atomic ratio of the rGO lattice
 131 determined by X-ray photoelectron spectroscopy (XPS) indicate that GO lattice parameters vary
 132 depending on the applied reduction technique. In the meanwhile, the Work Function (WF) among
 133 different rGO samples, validated by UPS measurements, gave similar trends and thus resulted in
 134 different FE characteristics. In general, lower content of oxygen-containing groups exhibits an
 135 enhanced FE performance mainly thanks to the WF increase [46]. Besides, the electron transfer at the
 136 interfaces between the substrate and the cathode material is expected to be highly promoted, since
 137 the states' density in the cases of oxygen elimination (e.g. HI-assisted rGOs) is also anticipated to be
 138 higher.

139 The role of GO concentration, namely flake density, impacts on the degree of reduction and
 140 morphology. Proper partial reduction leaves acidic groups on rGO surface and the polar nature of
 141 GO remains and accounts for stable, homogeneous dispersions in solvents, more notably in DMF and
 142 NMP [47]. In the case of low rGO-flake density films, the number of emitters is diminished, and the
 143 geometrical characteristics of the emitters are resultingly of minor importance are diminished, thus
 144 leading to a sharp decline in their performance as cold cathodes. On the one hand, the enhanced
 145 roughness at low rGO concentration suggests random sheets orientation onto the planar substrate,
 146 while on the other hand, screening effects are observed in the case of high density films [48-49]
 147 followed by an understated emission performance.

148 On the other hand, polymer concentration affects morphology in a significant manner, while a
 149 polymer:rGO concentration ratio exists for optimized FE performance. For high polymer contents
 150 fewer rGO sheets are exposed to vacuum, while thermal conductivity gets even 4 times higher than
 151 ambient air for the case of P3HT:rGO hence easing heat dissipation and achieving higher stability
 152 contrary to bare rGO. For low polymer content, rGO flakes become more preferentially oriented
 153 parallel to the substrate and fewer emitting edges are exposed to vacuum; as a result, the emission
 154 performance decreases again.

155 Edge density was also increased upon the deposition of an additional rGO layer onto the
 156 composite films, thanks to the smoother surface of the top rGO layer in the case of higher rGO
 157 content. In other cases, where the polymer concentration was higher, rGO arrays protruded from the
 158 polymer bulk, favoring the synergy of two conduction systems; conduction between rGO flakes of
 159 the same array, as well as between rGO flakes and the polymer [50]. The relevant charge transfer
 160 mechanisms are illustrated in Figure 3. Upon the additional rGO layer deposition onto the
 161 polymer:rGO composite layer, the DMF solvent of the rGO dispersion (or any other suitable solvent
 162 that might be applied) may dilute some polymer of the underlying layer, thereby a part of the rGO
 163 flakes and/or arrays penetrate the polymer. Therefore, since the polymer:rGO ratio increases together
 164 with the polymer content, rGO flake density into the polymeric scaffold gets consequently
 165 minimized, thus leading to a relevant deterioration in the edge density of rGO exposed to vacuum.



166

167 **Figure 3.** Comprehensive depiction of current conduction routes encountered in the studied
 168 composite cases.

169 Laser processing plays a crucial role in fabricating 2D-based field emitters. To begin with,
170 structuring Si substrate to create conical, well separated spikes that are perpendicular to substrate is
171 crucial to good GO deposition and edge protrusion. The micro-spike arrays are reportedly fabricated
172 by femtosecond (fs) laser texturing of n-type Si, usually followed by consequent removal of grown
173 oxides by HF on spikes' surface [36]. Secondly, Direct Laser Writing (DLW) is an additional promising
174 technique for the rapid and facile fabrication of graphene for various applications [1,51]. Proper laser
175 treatment gives rise to preferential protrusion of rGO sheets from the substrate and in series to FE
176 characteristics superior to those of pristine rGO. rGO bundles align themselves perpendicular to the
177 substrate, while at the same time sharp graphene edges are protruding out of the bundles. Epidermal
178 treatment of rGO prevents thermal damaging of substrate. As a side advantage, DLW retains the
179 performance of the developed flexible cathodes upon extensive bending conditions, thereby posing
180 good potential for graphene flexible FE cathodes. Finally, selective laser reduction of GO has received
181 attention due to its high potential [52-53] in a diversified field of applications, including FE among
182 them.

183 This study aims to offer a deeper insight on how three optimized FE enhancement routes
184 contribute to rGO-based FE enhancement. Section 2 discusses the realization of HI-assisted reduction
185 of GO and the subsequent rGO inks formation, as well as the optimization process of P3HT:rGO and
186 PCDTBT:rGO composites by diversifying polymer and rGO inks concentrations with a resulting
187 additional rGO ink dispersion coating on top of the composite, PCTDBT:PC₇₁BM blend in the place
188 of polymer in a similar manner. Results are presented in section 3, and compared between each other
189 in Section 4, while subjecting to discussion concerning FE enhancement in terms of morphology,
190 solvent, reduction agent or material type (plain rGO ink, polymer:rGO and polymer:fullerene
191 blend:rGO composite ink). Introducing a PCDTBT:PC₇₁BM blend to FE cathodes has to the best of
192 our knowledge never been suggested before. Furthermore, the different impacts of fullerene and
193 polymer constituents according to their relative concentrations, physical and chemical contribution
194 are interesting subjects for further investigation.

195 2. Materials and Methods

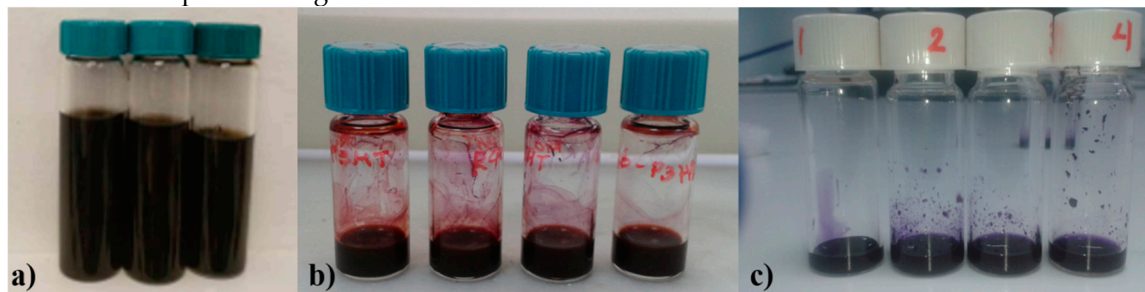
196 2.1. Preparation of starting GO powder

197 GO was prepared from purified natural graphite powder (Alfa Aesar, ~200 mesh) according to
198 Hummers' method [54][55]. H₂SO₄ (40 ml) was added to 500 mg graphite and stirred for several
199 minutes, followed by the addition of NaNO₃ (375 mg). Further stirring took place inside a cooled
200 beaker for 2 h, during which 3 g of KMnO₄ were added. Further stirring step lasted for other 4 h when
201 the reaction mixture was left to reach room temperature before being heated at 35 °C for 30 min. It
202 was then poured into a flask containing deionized water (50 mL) and the stirring temperature was
203 further raised to 70 °C for 15 min. The mixture was then decanted into 250 mL of deionized water;
204 the unreacted KMnO₄ was removed by subsequent addition of 3% H₂O₂ (2 ml). The obtained graphite
205 oxide was purified by repeated centrifugation, which initially yielded a sediment of acidic nature,
206 thus deionized water and HCl were added to capture sulfate ions so that sediment reaches pH 7.
207 Final product was oven-dried and sieved.

208 2.2. Production of rGO ink

209 A highly efficient HI/AcOH assisted reduction route was chosen to be implemented, as it is
210 described in our previous publication [56]. In a similar manner, our GO was reduced using a mixture
211 of hydriodic acid (HI, 55%)/acetic acid (AcOH). More specifically, the as-prepared GO powder (0.1
212 g) was sonicated in AcOH (37 mL) for 2 h. Then HI (2 mL) was added and the mixture was stirred at
213 40 °C for 40 h. Afterwards, the product was isolated by filtration and purified through a three-step
214 washing procedure: a) aqueous solution of saturated sodium bicarbonate (NaHCO₃, 3 x 2.5 mL), b)
215 DI water (3 x 2.5 mL) and c) acetone (2 x 2.5 mL). Finally, the resulting rGO was dried at 60 °C in a
216 vacuum oven overnight. In the aftermath, reduced GO powder underwent pulverization procedure
217 with mortar and pestle. Next, rGO powder (20 mg) was added in three vials containing THF (20 mL),

218 DCB (4 mL) and DCB:CB (3:1 v/v, 20 mL), respectively, in order to predetermine the initial
219 concentration to 1 mg/mL. Then, they were sonicated using an ultrasonic probe (Hielscher UP200Ht)
220 for 1 h and centrifuged at 4000 rpm for 45 min (Allegra X-22) to remove the large aggregates.
221 Afterwards, the supernatants were carefully collected with a pipette and surfactant-free viscous rGO
222 inks were formed (~0.5 mg/mL in THF, ~0.8 mg/mL in DCB and ~0.85 mg/mL in DCB:CB). Resulting
223 rGO inks are depicted in Figure 4a.



224

225 **Figure 4.** a) Unmixed rGO ink, b) P3HT:rGO and c) PCDTBT:rGO blends in controlled volume ratios.

226 2.3. Preparation of rGO-Polymers composite inks

227 P3HT (10 mg) and PCDTBT (4 mg) were dissolved in THF (1 mL) and DCB (1 mL), respectively.
228 Polymers:rGO composite inks were prepared by adding rGO ink to the P3HT and PCDTBT solutions,
229 respectively into different combinations of relative volume ratios (0%:100%, 20%:80%, 40%:60%,
230 60%:40% and 80%:20%). In order to prepare homogeneous polymers:rGO composite inks, the
231 mixtures were further sonicated in an ultrasonic bath (Elmasonic S30H) for another 1.5 h and finally
232 were left undisturbed for 15 min, in order to settle down any agglomerates. Polymers:rGO composite
233 inks are depicted in Figures 4b and 4c, respectively.

234 2.4. Preparation of rGO-PCDTBT:PC₇₁BM composite ink

235 PCDTBT:PC₇₁BM were dissolved in DCB:CB (3:1 v/v, 1mL) with 1:4 (4mg:16 mg) ratio and stirred
236 overnight at 70 °C. At next, PCDTBT:PC₇₁BM:rGO composites were realized by adding rGO ink,
237 prepared in DCB:CB, to the PCDTBT:PC₇₁BM blend in different combinations with relative volume
238 ratios (0%:100%, 20%-80%, 40%-60%, 60%-40% and 80%-20%). In order to prepare homogeneous
239 PCDTBT:PC₇₁BM:rGO composite inks, the above described procedure was also followed.

240 2.5. FE cathodes realization

241 Silicon wafers (n⁺ Si) were subsequently rinsed with acetone and isopropyl alcohol. Composite
242 inks were then realized and coated on top of substrate surface with the drop casting method.
243 Subsequent rGO layer was later on coated in the same manner. All films were placed in an oven for
244 an adequate time until the full removal of the solvents. Final FE cathode structure is illustrated in
245 Figure 1.

246 3. Results

247 3.1. Field emission measurements

248 FE measurements were executed under vacuum of less than 10⁻⁶ Torr. Samples were used as
249 cold cathodes in a short - circuit protected planar diode system, as depicted in Figure 1. More details
250 regarding the experimental FE setup can be found elsewhere [48]. Current Density–Voltage (*J*–*V*)
251 curves were obtained while the interelectrode distance, *d* = 200 μm in our case, was controlled by a
252 stepper motor. It is pointed out that FE characteristics remained unaffected by the anode location. In
253 order to confirm the stability of the devices, as well as *J*–*V* reproducibility, continuous emission cycles
254 were performed. A High Voltage (HV) source (PS350-SRS) supplied a voltage with variable sweep
255 step between electrodes. A digital pico-ammeter (Keithley 485) was used for the sake of measuring

256 FE current. The emission current stability versus time was investigated by monitoring the emitted
257 current density rate over a long time period of consecutive operation.

258 3.1.1. Fowler Nordheim theory

259 The FE properties of graphene can be determined by using Fowler Nordheim law [26]. In brief,
260 the relationship of FE current density (J) with the applied electric field E is demonstrated below as
261 equation (1):

$$J = \eta \alpha \frac{(\beta E)^2}{\varphi} e^{-b \frac{\varphi^{3/2}}{\beta E}} \quad (1)$$

262 where constants α and b correspond to $a = 1.54 \cdot 10^{-6} A eV V^{-2}$ and $b = 6.83 \cdot 10^3 eV^{-3/2} V^{-1}$,
263 φ represents the WF, g is related with the emitters' geometrical efficiency, β is the field enhancement
264 factor and E corresponds to the macroscopic electrical field in $V/\mu m$. E is calculated from $E = V/d$, in
265 which V respects to the applied potential and d the interelectrode distance. According to Fowler
266 Nordheim equation, the part of the $\ln(J/E^2) - (1/E)$ plot that is linear gives proof of electron movement
267 through the tunneling barrier of the emitter in the specific area.

268 The slope of the previous equation derives the field enhancement factor β according to the
269 following equation (2):

$$\beta = b \varphi^{3/2} / k_{FN} \quad (2)$$

270 Additional parameters for assessing FE quality include the E_{to} (turn-on field), E_{th} (threshold
271 field), the intensity of luminescence and the stability of emission. What is sought is minimum values
272 of E_{to} and E_{th} , maximum values of β and emission current density, as well as maximum stability so as
273 to yield an ideal field emitter.

274 3.1.2 First case: HI-reduced GO emitter

275 A set of FE cathodes with different rGO ink ratios was realized and subsequently characterized.
276 Figures 5a, 5b and 6 display FE response of the best FE cathodes per each rGO ink ratio. Indeed, β
277 factor exhibited a value of 660, while E_{th} value was $1.6 V/\mu m$. Numerical results are presented in Table
278 1.

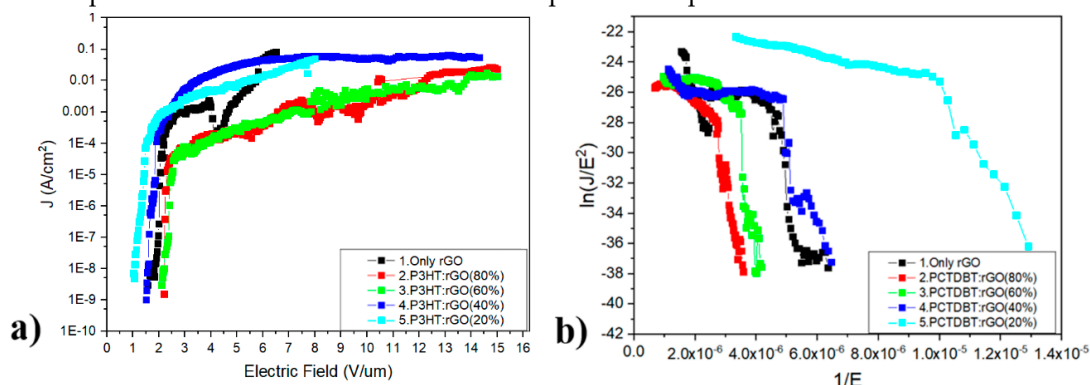
279 **Table 1.** Field enhancement factor and turn-on field figures classified per composite type (columns)
280 and for HI/AcOH- reduced rGO ink with diversified ratios.

rGO Ratio (%)	n ⁺ -Si/P3HT:rGO		n ⁺ -Si/PCDTBT:rGO		n ⁺ -Si/PCDTBT:PC ₇₁ BM:rGO	
	Field Enhancement β	Turn-on Field F_{to} ($V/\mu m$)	Field Enhancement β	Turn-on Field F_{to} ($V/\mu m$)	Field Enhancement β	Turn-on Field F_{to} ($V/\mu m$)
100%	660±10	1.60±0.1	660±10	1.60±0.1	660±10	1,60±0.1
80%	300±10	2.23±0.1	170±10	2.80±0.1	80±10	2.43±0.1
60%	420±10	2.05±0.1	625±10	2.40±0.1	360±10	2.16±0.1
40%	915±10	1.53±0.1	1090±10	1.58±0.1	950±10	1.53±0.1
20%	2500±10	1.03±0.1	2050±10	0.80±0.1	2850±10	0.60±0.1

281 3.1.3 Second case: Polymer:rGO composite emitter

282 Among all different volume ratio variants, that of 80% polymer (P3HT or PCDTBT) : 20% rGO
283 gave the best results. Here, a set of 5 different ratio batches have been fabricated and tested, while
284 each case includes 5 fabricated cathode samples. Accordingly, Figure 5a depicts a comparative chart
285 of the best samples per each one of all 5 ratios. Also, as demonstrated in Table 1, huge deviation in
286 FE values for certain concentration scenarios indicates inability in perfectly controlling process

287 parameters. Yet, bad results repeatability for these concentration ratios implies that only the
 288 optimized parameters of the ratio 80%:20% are of practical importance.



289

290

291 **Figure 5.** a) Logarithmic plot of the current density, measured as a function of the electric field E (J-

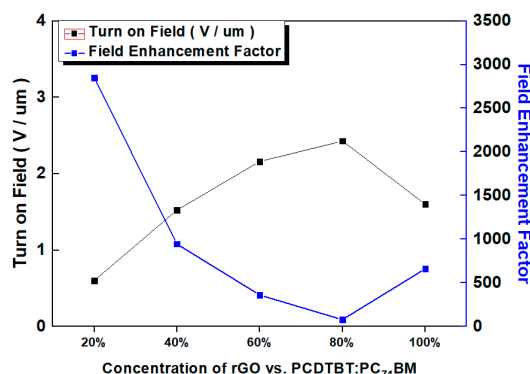
292 E), obtained by different concentration ratios of rGO ink in composite n⁺-Si/P3HT:rGO field emitters.

293 Lowest electrical field threshold appears for the P3HT:rGO(20%) case. b) Fowler-Nordheim curves of

the J-E plots of FE with different concentration ratios of rGO ink in composites n⁺-Si/PCDTBT:rGO.

294 3.1.4 Third case: PCDTBT:PC₇₁BM:rGO composite emitter

295 In a similar manner to polymer:rGO case, the batch with 80% blend : 20% rGO ink volume ratio
 296 gave the best results. Again, per each case, a set of 5 different ratio batches has been fabricated and
 297 tested, while each batch includes 5 fabricated cathode samples and all best cathode results per batch
 298 are presented in Figure 5b. Accordingly, Figure 6 and Figure 7 depict a comparative chart of the best
 299 batches per each ratio with respect to the Fowler-Nordheim characterization and the overall FE
 300 performance parameters respectively. All FE values per volume ratio set are included in Table 1.

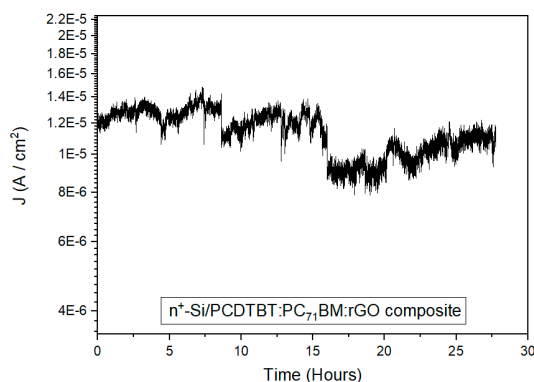


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302

303 **Figure 6.** Variation of the turn on field (black line) and the enhancement factor (blue line) in different

concentrations of PCDTBT:PC₇₁BM:rGO and P3HT:rGO composite inks.



304

305

306 **Figure 7.** The evolution of the emission current density at a constant bias voltage of 1500 Volts over a

long period of continuous operation for the best rGO cathodes measured.

307 3.1.5 Field Emitter stability

308 The evolution of the emission current density at a constant bias voltage of 1500 volts was tracked
309 over a long period of over 25 hours continuous operation for the best rGO-containing cathode that
310 had been chosen among all samples. Figure 7 demonstrates a respectable stability of the emitter's
311 current density over time that results in a final drop of approximately 16% with regard to the initial
312 current. These results explain why PCDTBT:PC₇BM:rGO composite emitter has a higher level of
313 long-term stability under the field emission experimental conditions related other emitters that have
314 been tested in the literature [34].

315 4. Discussion

316 In general, HI/AcOH is by far more efficient by other reducing agents like hydrazine; optimum
317 reduction dictates the compromise of yielding a partially reduced rGO. Although being of low
318 occurrence, acid groups are present on rGO surface and result to a remaining polar nature of rGO,
319 hence enabling rGO to form stable and homogeneous dispersions in THF [21].

320 On the other hand, the polymer-fullerene powder was unable to dissolve adequately 4mg/mL
321 PCDTBT:PC₇BM solution in THF, therefore a mixture of DCB:CB (3:1) was finally applied to dissolve
322 successfully the solid components with sufficient magnetic stirring. A possible explanation to this
323 fact is that blend residues which are insoluble may probably contain the highest molecular weight
324 fraction which could not be solubilized [57]. It can be said that high MW values adversely affect
325 polymer solubility. Low solubility of polymers may direct to a strong inter-chain bonding or even
326 chain aggregation. Seemingly, ortho-dichlorobenzene did not result to any further aggregation of
327 PCDTBT chain, while it could simultaneously decelerate drying of the wet film [58]. Furthermore,
328 the effect of THF additive in polymer and blend morphology mostly has to do with the solvent's
329 higher affinity for polymers than for PCBM. Diversifying the dipole moment by employing solvents
330 similar to THF may control this affinity. Moreover, it has to be mentioned that THF which has low
331 boiling point dissolves P3HT very easily, while such an easy dissolution for PCBM appears for the
332 higher boiling point o-DCB, let alone the good solubility of PCDTBT [59].

333 With respect to the case of P3HT:rGO composite-based FE cathodes, among all different
334 concentration variants, the volume ratio of 80% polymer : 20% rGO ink gave the best results. FE
335 trends are in accordance with relevant previous literature [21]. Indeed, component concentration
336 significantly affects composite morphology and the dependent FE performance; Lower rGO contents
337 favor the orientation of sheets at different angles with respect to the planar substrate, hence inducing
338 higher roughnesses. As the P3HT:rGO ratio decreases, i.e. the polymer content increases, the rGO
339 density into the polymer matrix decreases giving rise to a corresponding decrease in the density of
340 the rGO edges exposed to vacuum. On much higher rGO content, however, screening of coated
341 surface takes presumably place that deteriorates FE. Higher polymer content means fewer rGO sheets
342 that are exposed to vacuum, while it has been demonstrated that thermal conductivity favors heat
343 dissipation thus prolonging stability, in contrast with the case of bare rGO. On the other hand, lower
344 polymer content allows rGO sheets to orientate themselves parallel to the substrate, hence resulting
345 to less emitting edges and a decreased FE performance. In general, at higher rGO ink concentrations,
346 the base of the protruding bundles is a part of the rGO layer, whereas in the case of samples with
347 high polymer content, bundles are sticking out of a polymer bulk. This observation suggests that
348 there are two conduction processes present, conduction between rGO within flakes of a bundle and
349 between polymer and sheets [50]. A final remark is that lower emitter edge density has been observed
350 in high and low concentrations [21]. We conclude presuming that 80%:20% analogy of P3HT:rGO
351 better approaches the trade-off between screening and the density of protruding rGO edges.

352 The differences observed in field enhancement factor and in turn-on field between the composite
353 emitters with different polymers (P3HT and PCDTBT) are directly related to their morphology
354 instability and their different ionization state [60-61]. In this work, the highest field enhancement
355 factor observed on semicrystalline p-type polymer P3HT and the lowest electrical threshold for
356 amorphous p-type polymer of PCDTBT.

Besides, considering the third FE case of PCDTBT:PC₇₁BM blends complementing rGO, it is already known that for blend containing OSCs a low temperature annealing at approximately 70 °C suffices for optimizing PCE, thus also blend morphology and phase separation [62-63]. Same logic is valid in FE case as well, since charge carrier transfer is thereby optimized. It has been observed that the upper part of PCDTBT:PC₇₁BM films is relatively enriched in PC₇₁BM with negative gradient of fullerene concentration when examining deeper inside the annealed layer, yet in no case exceeds upper surface concentration of PC₇₁BM the one of PCDTBT. Of course, PC₇₁BM tends to reach the upper interface with air demonstrating a mild trend for phase separation, but PC₇₁BM accumulation on the upper surface does not at all increase roughness due to PC₇₁BM crystallites. Furthermore, a mild annealing at 70 °C neither impacts on PC₇₁BM distribution towards depth, nor does it significantly affect blend crystallization, but enables PCDTBT:PC₇₁BM blend to self-organize into an optimal morphology for charge generation and extraction and, most importantly, eases the removal of trapped blend solvent [64]. Similar to the previous case of HI-reduced GO, 20% rGO ink : 80% polymer-fullerene blend ratio appears to yield optimized FE characteristics. The fact that rGO contributes best with the same concentration as in polymer:rGO, may indicate a nonsignificant impact of fullerene on final FE contrary to rGO. Yet, in accordance with not directly FE-relevant studies that include PC₇₁BM [65] or PC₆₁BM [56], fullerene-rGO interaction is highlighted in terms of further improving charge transfer from the blend to emitting edges and a significant contact resistance reduction.

5. Conclusions

In this study, four rGO-based field effect emitters were developed, optimized and compared. rGO layers prepared by HI/AcOH reduction method and were coated on a) n⁺ doped Si substrate, b) n⁺-Si/P3HT:rGO, c) n⁺-Si/PCDTBT:rGO and d) n⁺-Si/PCDTBT:PC₇₁BM:rGO composites, respectively. We investigated the FE properties of different concentrations of polymer composite solutions to control the structural and electrical properties of the substrate. It is found that the cathodes based on PCDTBT:PC₇₁BM:rGO displayed a field enhancement factor of ~2850, with remarkable stability over 25 h and low turn-on field in 0.6V/μm

The threshold field, enhancement factor and the remarkable stability of FE current were remarkably improved compared to the pristine Si demonstrating that is a promising FE cathode with potential applications in vacuum microelectronics and FEDs.

Finally, taking into account the high potential of PCDTBT:PC₇₁BM as successful blend candidate in conventional OSC devices, its optimized coating on a TCO or TCO/HTL substrate, either rigid or flexible, might result in significant number of photogenerated electrons and a further decrease in contact resistance that might further boost FE figures of merit in future, therefore possibly promising a new alternative type of photodetectors.

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