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Article

Confined Polymers as Self-Avoiding Random Walks on Restricted Lattices

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Abstract: Polymers in highly confined geometries can display complex morphologies including ordered phases. A basic component of a theoretical analysis of their phase behavior in confined geometries is the knowledge of the number of possible single-chain conformations compatible with the geometrical restrictions and the established crystalline morphology. While the statistical properties of unrestricted self-avoiding random walks (SAWs) both on and off-lattice are very well known, the same is not true for SAWs in confined geometries. The purpose of this contribution is a) to enumerate the number of SAWs on the simple cubic (SC) and face-centered cubic (FCC) lattices under confinement for moderate SAW lengths, and b) to obtain an approximate expression for their behavior as a function of chain length, type of lattice, and degree of confinement. This information is an essential requirement for the understanding and prediction of entropy-driven phase transitions of model polymer chains under confinement. In addition, a simple geometric argument is presented that explains, to first order, the dependence of the number of restricted SAWs on the type of SAW origin.

Keywords: freely jointed chain; confinement; enumeration; conformational entropy; phase transition; self-avoiding random walk; face-centered cubic; simple cubic; lattice model

1. Introduction

Self-avoiding random walks (SAWs) have long been used in polymer science as one of the simplest and most useful descriptions of polymeric chains. The relative simplicity of SAWs has made them an ideal tool to investigate static and dynamic properties of polymers both analytically and computationally [1–7] . They have proved particularly useful in the determination of universal behavior and scaling laws for polymer systems ranging from individual chains to melts. The critical behavior of SAWs is also closely related to that of the Ising model and to percolation [8–18].

Besides their extensive application in polymer science, SAWs have been a subject of mathematical interest in their own right [19], [20], mainly because of their close relationship to Brownian motion and stochastic processes in general soft matter physics [21–23]. In spite of the very simple idea underlying SAWs, comparatively few results have been rigorously solved in a mathematical sense [19]. As a consequence, a great deal of computational work has been carried out to complement analytical approaches. From the numerical point of view, a currently active research area is the efficient computation of the number of distinct conformations for a SAW of a given length on a lattice, which is very closely related to the single-chain classical partition function [24]. Over the last years increasingly sophisticated enumeration algorithms [25–27] have been continually pushing the upper SAW length limit for which numerical results on enumeration can be obtained within reasonable computational time.

Detailed knowledge of SAW properties in restricted geometries is an essential ingredient in the study of confined polymeric systems, which can range from single macromolecules to highly entangled melts in pores, slits, narrow gaps and nanocavities. Such properties include the number of distinct SAWs for a given length, mean squared end-to-end vector, distribution of size etc. Although SAWs in such restricted geometries have also been studied [11,12,28–32], they have received far less attention than unrestricted SAWs, one of the reasons being the apparent lack of applications in polymer science. The relatively recent [33–45] increased interest in confined polymeric systems, accompanied by significant advances in molecular simulations and the availability of

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experimental techniques able to probe the behavior of individual macromolecules in channels, slits, etc [46–50] is a strong motivation for the investigation of SAWs in such confined geometries. Recent Monte Carlo (MC) simulations [51] of highly confined, dense assemblies of linear, freely jointed chains of strictly tangent hard spheres of uniform size shows that such athermal polymer systems display an unexpectedly broad range of morphologies, presumably connected by phase transitions.

In the following, "polymer" will refer to a linear chain of strictly tangent hard spheres, unless explicitly stated otherwise. "Monomer" will refer to each of the hard spheres that make up a chain, and "site" will refer to each of the points of a lattice. We will also refer interchangeably to the cubic P and F lattices and the corresponding simple cubic (SC) and face centered cubic (FCC) crystals obtained by placing a spherical base motif on all lattice points.

As stated earlier the present work is motivated by the simulation results of Ref. [51] where linear, freely-jointed chains of tangent hard spheres of uniform size are generated and successively equilibrated under various conditions of confinement. The latter is realized through the presence of flat, impenetrable parallel walls in one or more dimensions. Extreme confinement corresponds to the state where inter-wall distance approaches monomer diameter leading eventually to the formation of quasi 1-D (tube-like) and 2-D (plate-like) polymer templates. Typical computer-generated polymer configurations can be seen in Figs. 1 and 2 in lateral and cross-sectional views, respectively. They correspond to systems containing a total of 720 monomers and average number of bonds per chain $N = 7$, 17 and 35 at a packing density $\varphi = 0.50$. In all cases chains are packed in an approximately 3.11×3.11 square tube of dimensions 77.8. All lengths are reported in units of monomer diameter (equal to the SAW step length). Periodic boundary conditions are applied on the long dimension, hard walls exist in the short ones. More details on the simulation algorithm, the systems studied and the corresponding model parameters can be found in [51].

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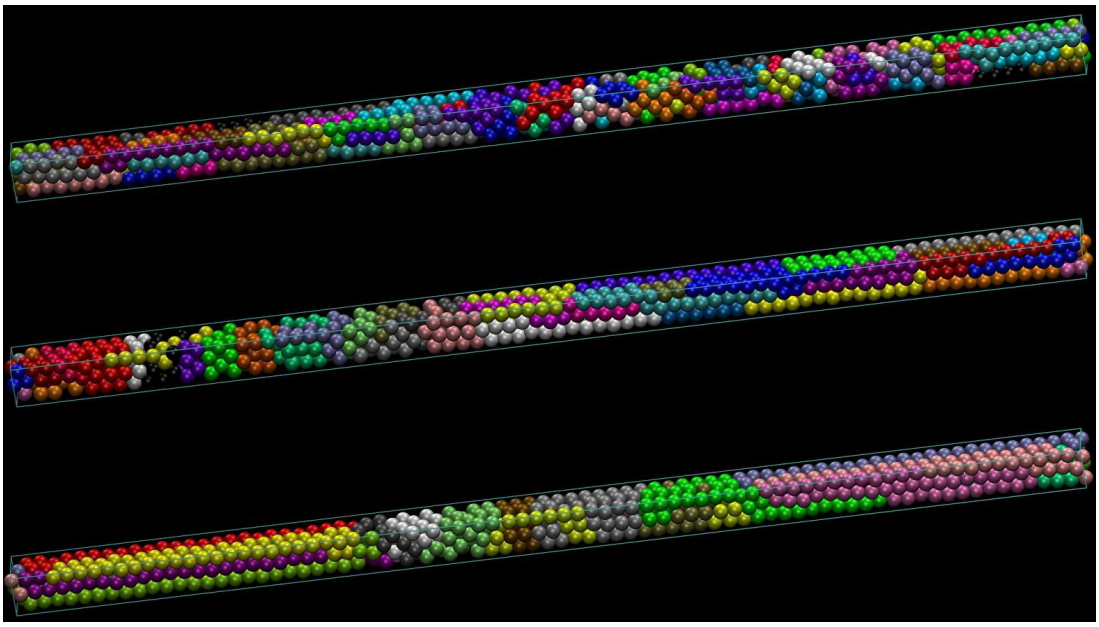

Figure 1. Lateral views of computer-generated, linear freely jointed chains of tangent hard spheres of uniform size confined in tubes of square cross section at $\varphi = 0.50$. All systems contain a total of 720 monomers. From top to bottom: chains consist, on average, of $N =$, 7, 17 and 35 bonds. In all cases chains are packed in an approximately 3.11×3.11 square tube of length 77.8. Periodic boundary conditions are applied on the long dimension and impenetrable flat walls in the short ones. Ordered regions with crystalline defects can easily be recognized by visual inspection. A precise analysis shows them to be slightly defective, coexisting FCC crystals of different orientations. Monomers have been colored according to the chain they belong to. The tube axis direction in both panels is along a direction of the crystallographic type $\langle 100 \rangle$. Image created with the VMD software [52].

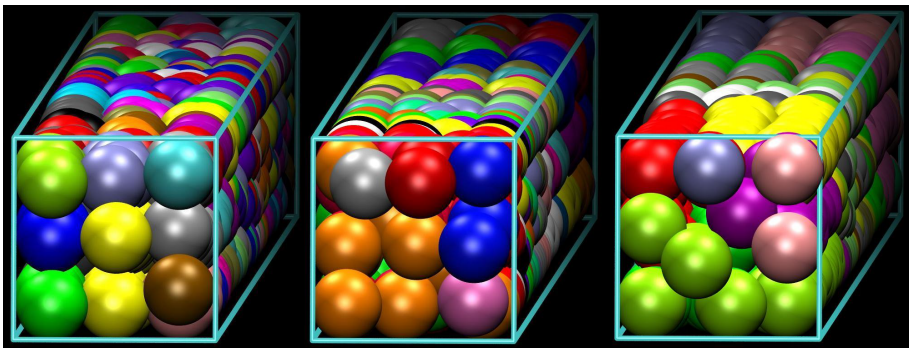

Figure 2. Same as in Fig.1 but for cross-sectional views. From left to right: chains consist, on average, of $N =$, 7, 17 and 35 bonds.

An analysis, based on the Characteristic Crystallographic Element (CCE) norm [53–55], of the geometrical environment around the spherical monomers shows the ordered regions in such highly-confined polymer structures to very closely correspond to an FCC crystal. One remarkable aspect of such dense polymer systems in the bulk (i.e. without spatial confinement) is the existence of highly ordered, crystalline phases [56]. In previous MC work [55–62] it was shown that the apparent loss of entropy, caused by the regular organization of monomers in the sites of a crystal lattice, is more than compensated for by the increase of available volume for monomers, and

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hence translational entropy, as evidenced by sharp decreases in asphericity and acilindricity of the Voronoi cells associated with each monomeric site. The resulting crystalline structures strongly resemble those appearing in Molecular Dynamics (MD) and MC simulations of *single* (monomeric) spheres, well known since the pioneering work of Alder and Wainwright [63–65]. These crystalline *polymer* structures can be simplistically viewed as built from crystals of single hard spheres and overlaying on them all possible linear paths of a given length that connect tangent spheres. Viceversa, configurations of single hard spheres can be obtained trivially from available configurations of polymers by deleting all bonds in chains.

As a matter of fact, if chain connectivity is ignored and the monomers are considered as individual spheres, the resulting orderd structures are virtually undistinguishable, except for one main feature, from those appearing in single hard sphere systems [66–68]. The distinguishing feature is the absence of twinned structures in polymer systems [69]. In computer simulations, packings of single hard spheres often form quite perfect tetrahedral clusters which tend to aggregate in pentatwins [70]. The entropic conformational entropy loss associated with twinning in polymeric systems rises the entropic barrier to the extent that individual crystals with single or multiple stacking directions and abundant defects are observed predominantly in simulations.

Since difference in entropy is the only hindering or driving force for phase transitions in athermal polymeric systems [6,71–73], the entropy calculation in confined geometries is an essential requirement in understanding and predicting their phase behavior. Although all previously described characteristics have been obtained from off-lattice simulations, the appearance of highly ordered crystalline phases in 1-D (tube-like) confined polymer systems, as the ones shown in Figs. 1 and 2, motivates the calculation of their entropy on crystal lattices under equivalent spatial restrictions.

Fig.3 is a simplified, generic, two-dimensional representation of the ordered structures observed in MC simulations of highly confined polymeric systems [51]. The left panel represents a typical system configuration (MC-snapshot) confined between parallel walls. The centers of the spherical monomers (circles in solid line) are, on average, close to the sites of the perfect crystal (circles in dashed line). Configuration space is sampled through changes in the positions of the monomers as the MC progresses (such changes being compatible with chain connectivity, packing density, confinement and crystalline morphology; see for example the corresponding MC algorithms in [51,74]), much as monomer vibrations about the equilibrium position sample configurations in MD simulations. At high densities, monomers remain close to the sites of the crystal lattice (shown in the right panel), so that on-lattice polymer chains, built by joining the corresponding sites of the perfect crystal, closely approximate the original off-lattice system from the conformational point of view. Each of these chains is thus effectively a restricted SAW on the crystal lattice.

In typical classical MC simulations [75–79], configurations for off-lattice polymer systems are generated with a probability proportional to their statistical (Boltzmann) weight and correspond to individual points in a configuration space spanned by continuously varying degrees of freedom, e.g. Cartesian coordinates of monomer centers in an MD formulation based on Newton's equations of motion, or Euler, torsion and bond angles in a Lagrangian formulation, etc. Entropy or free energy calculations require then the evaluation of a high-dimensional integral in configuration space [75].

On the other hand, configuration space for lattice SAWs (Fig.3, right panel) is discrete and entropy is evaluated as a sum of Boltzmann probabilities or weights. Since all feasible configurations are equally probable in athermal systems, entropy is proportional to the logarithm of the number of different SAWs. While extensive work on the exact enumeration of SAWs on unrestricted lattices in several dimensions (typically the d-dimensional hypercubic lattice $\mathbb{Z}^d$) has been carried out, enumeration of SAWs on restricted cubic P and F lattices has not been reported to date. In this contribution we evaluate, by direct enumeration, the number of SAWs on the cubic P and F lattices subject to geometrical restriction and calculate the SAW size as a function of lattice type, number of bonds and level of confinement.

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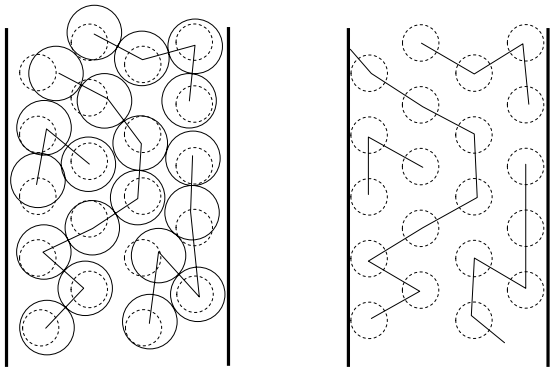

Figure 3. Schematic representation of ordered polymer structures in a confined geometry. Circles in solid line represent spherical monomers, polygonal lines represent polymer backbones. Monomers along a chain are strictly tangent (circles in solid line on left panel), monomers belonging to different chains need not, but can also be tangent. On both panels, circles in dashed line represent sites of the perfect crystal. On average, polymer backbones can be considered SAWs on the sites of the perfect crystal (right panel).

2. Methods

In the following, an N-step three dimensional SAW ω^N on a lattice is defined as the ordered sequence of sites $\underline{\omega}^N(0), \underline{\omega}^N(1), \ldots, \underline{\omega}^N(N)$, where $\underline{\omega}^N(0)$ is the position vector of the SAW origin, satisfying the condition $\underline{\omega}^N(i) \neq \underline{\omega}^N(j)$ for $i \neq j$, and such that $|\underline{\omega}^N(i+1) - \underline{\omega}^N(i)| = 1,\ i \in \{0, 1, \ldots, N-1\}$, where it is assumed that the step length of the SAW is taken as the unit of length, and $|\underline{x}| = \sqrt{\underline{x} \cdot \underline{x}}$ denotes the usual Euclidean norm.

According to the previous definition of step length two neighboring sites are 1 length unit apart on both the cubic P and the F lattices. For the cubic P lattice, the edge length of the conventional cell is therefore also unit, whereas in the cubic F lattice the edge length of the conventional cell is $\sqrt{2}$.

The individual components of the position vector of the i-th site of an N-step SAW are denoted by $\omega_j^N(i)$ with $j = 1, 2, 3$. The squared end-to-end distance of the SAW $\left|\omega^N\right|^2$ is given by $\left|\omega^N\right|^2 = (\underline{\omega}^N(N) - \underline{\omega}^N(0)) \cdot (\underline{\omega}^N(N) - \underline{\omega}^N(0))$. With the previous definitions of unit length, $|\omega^N|^2 = N^2$ for a fully extended SAW, whereas the minimum SAW length is $\min(|\omega^N|^2) = 1$. These two values bracket the range over which the distribution of $(\omega^N)^2$ is defined. If we denote by c_N the number of distinct N-step SAWs, the average squared end-to-end distance is given by:

$$\left\langle \left|\omega^N\right|^2 \right\rangle = \frac{1}{c_N} \sum_{\omega^N} \left|\omega^N\right|^2$$

where the sum is over the c_N SAWs starting at a given lattice point $\underline{\omega}^N(0)$. For unrestricted SAWs, $\underline{\omega}^N(0)$ can be any one of the countable infinity of lattice points, since the set $\{\omega^N\}$ of all SAWs starting at all points of a given lattice has the same space group symmetry as the lattice itself. Let us define the following equivalence relation on the set $\{\omega^N\}$ of all three-dimensional SAWs of a given length N starting at all points of a given lattice: two SAWs $\omega^N, \omega'^N \in \{\omega^N\}$ are equivalent, and we write $\omega^N \approx \omega'^N$, if there exists a geometrical transformation T (group element) in the space group $Ia\bar{3}d$ such that $T(\underline{\omega}^N(i)) \approx \underline{\omega}'(i)^N \quad i \in \{0, 1, \ldots, N-1\}$. The set of all distinct c_N SAWs is then the set of all equivalent classes $\{\omega^N\}/c_N$. For confined SAWs the introduction of geometric restrictions will reduce this trivial multiplicity (which is due to the maximal symmetry of the unconfined lattice).

For unrestricted lattices the number c_N and thus the computational effort for the exact enumeration problem for SAWs are believed to grow exponentially with power law corrections as N increases, instead of the purely

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exponential growth for simple non-SAWs. More specifically, it is conjectured, and there is strong numerical and nonrigorous evidence, that c_N and $\left\langle \left|\omega^N\right|^2 \right\rangle$ depend on N as:

$$c_N \backsim A\mu^N N^{\gamma-1} \tag{1}$$

$$\left\langle \left|\omega^N\right|^2 \right\rangle \backsim DN^{2\nu} \tag{2}$$

where A, D, μ, γ and ν are (dimension dependent) positive constants.The constant A is known as the amplitude, μ as the connective constant, while γ (the entropic exponent) and ν are critical exponents. For simple non-SAWs $\gamma = 1$ and $\nu = \frac{1}{2}$. Estimates and bounds for μ, ν and γ for SAWs are available [25,80–86]. Approximate values in three dimensions are $\mu \approx 4.684$, $\gamma \approx 1.157$ and $\nu = 0.588$.

The value of c_N has been the object of increasingly refined and extensive calculations. Milestone calculations for the 3-D cubic P lattice are: Orr's $N \leq 6$ [24], Fisher and Sykes $N \leq 9$ [17,87,88], Guttmann $N \leq 21$ [80,85,88–91], MacDonald et al. $N \leq 26$ [81,85], Clisby et al. $N \leq 30$ [84], Schram et al $N \leq 36$ [25–27], this latter value being the current record, obtained by the length doubling method. The later group has also determined the current highest values of c_N on the BCC (body-centered cubic) ($N = 28$) and FCC ($N = 24$) unrestricted lattices. The continual growth of the range of known values of c_N has made it possible to obtain more accurate numerical estimates of the various parameters appearing in Eqs.1 and 2. Extrapolation by means of differential approximants and direct fitting to asymptotic expansions yields values for γ and ν in good agreement with those obtained by MC renormalization group, conformal bootstrap and field theory.

In this contribution we present results for the cubic P (SC) and cubic F (FCC) lattices restricted to a pore or "tube" of square cross section. While the complete set $\{\omega\}$ of SAWs on the unrestricted lattice possesses the maximal crystallographic symmetry of space group $Ia\bar{3}d$, the introduction of geometrical restrictions reduces the symmetry on the one hand and, on the other, introduces additional freedom in the definition of the problem. For polymers confined in a pore or tube, the natural correspondence would be to a SAW whose growth is limited in the plane transversal to the tube direction. The new degrees of freedom, which are not meaningful for unrestricted SAWs, are the orientation of the tube axis, the size of its cross-section and the origin of the SAW: the orientation of the tube axis will be defined by direction indices according to crystallographic practice: $[ijk]$. The cross section will be assumed to be a square of side L, measured in units of SAW step length. Finally, c_N will be calculated for each distinct origins located on the tube cross section at $x = 0$.

The value of c_N will of course depend on the choice of the origin and on the double countable infinity of degrees of freedom: direction $[ijk]$ and tube cross section L. In the MC simulations of confined polymers that motivate this work, hard-sphere chains confined to tubes of square cross-section are observed to preferentially form quite perfect FCC crystalline domains with their $[100]$ aligned along the tube axis. For both the SC and FCC lattices we will thus consider the geometrically restricted lattice $\mathbb{RL}(L)$ to consist of all the lattice points of coordinates $\underline{x}$ contained in the square-section "tube" defined by:

$$\mathbb{RL}(L) = \{\underline{x} \,|\, x_1 \in \mathbb{Z}\,, |x_2|, |x_3| < L\} \tag{3}$$

where the unit of length is the SAW step length. In Eq. 3 the tube has been assumed to be oriented parallel to one of the three standard cubic crystallographic axes, or, equivalently, to belong to the direction type $\langle 100 \rangle$. The x_1 (or x) axis [92] has been chosen without loss of generality due to the equivalence of all three axes in the cubic system. The sides of the tube are contained in planes of the crystallographic form $\{100\}$.

Unlike in the references cited above, and again motivated by the MC simulations of hard-sphere model polymers confined to tubes, the range of SAW lengths investigated in this work has been kept modest. The reason is double: the rich morphological behavior of confined polymers is already clearly observable in MC simulations of comparatively short chains ($N \approx 5 - 15$). This can be understood by observing the structural similarity of the ordered chain morphologies presented in the panels of Figs.1 and 2 and which correspond to systems characterized by different chain lengths (from $N = 7$ to 35). Furthermore, once c_N in this range is known, it can be used as the basis of reliable approximations for the prediction of entropy-driven phase transitions

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for much longer chains as well. For these two reasons, we have employed the direct enumeration procedure to determine c_N.

The introduction of the tube restriction reduces the symmetry of the full cubic lattice to that of tetragonal space group $I4_1/acd$. As a consequence, lattice sites in the tube cross section are not all identical any more, but split into subsets of SAW origins O_i, all sites in a subset being crystallographically equivalent. We will refer to the cardinality $|O_i|$ of these subsets as their *multiplicity* and will label each of the distinct origins by a *type* which effectively corresponds to the number subindex, i, of each subset. For example, there are three possible origins for SAWs on an SC lattice restricted by a tube of size 3×3, with multiplicities (*type* 1) $|O_1|=4$, (*type* 2) $|O_2|=8$, (*type* 3) $|O_3|=4$ (Fig.4), and six possible origins for SAWs on an FCC lattice restricted by a tube of size $3\sqrt{2}\times3\sqrt{2}$, with multiplicities $|O_1|=4$, $|O_2|=8$, $|O_3|=4$, $|O_4|=4$, $|O_5|=4$ and $|O_6|=1$ (Fig.5).

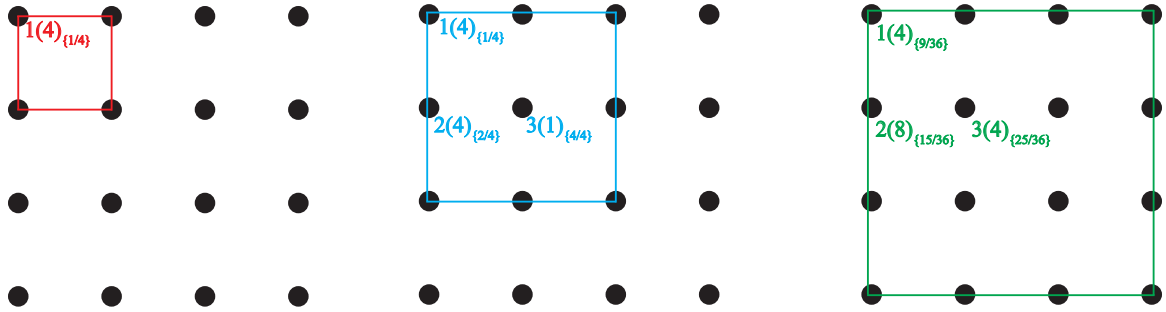

Figure 4. Numbering scheme for all possible origins of SAWs restricted to a tube of square cross section on the cubic P (SC) lattice, for three tube cross section sizes. In all panels, black circles represent lattice points, squares are the tube cross sections: 1×1, 2×2 and 3×3 from left to right. The view is along the tube axis in direction $[100]$. Numbers on the left correspond to the label of each distinct origin (*type*). Numbers in parentheses correspond to the cardinality (multiplicity) of each subset. Subindices in braces correspond to area ratios (overlaps), r_i.

Figs.4 and 5 schematically show the definition of tube size and the numbering/labeling scheme for the SC and FCC restricted lattices, respectively. Thus, an $n\times n$ tube has a cross section of the same size as $n\times n$ conventional cubic unit cells arranged in a square array, and its side measures $L=n$ units of length (SAW step) for the SC lattice, and $L=n\sqrt{2}$ for the FCC lattice. In these figures, a number placed at selected lattice points is their label, corresponding to the notation *types* in Tables A1 through A9. Each different type corresponds to a different origin for the SAW. The number in parenthesis corresponds to the multiplicity of that *type* (number of crystallographically equivalent restricted lattice points) while the subindex in braces refers to the overlap, to be defined and discussed in Section 4.

As the size of the tube cross section grows, the number of distinct origins (i.e. of different types) increases. The value of c_N reported below is given separately for all possible distinct (crystallographically non-equivalent) origins: the values of c_N in Tables A1 through A9 correspond to the number of SAWs starting from only one of all equivalent lattice sites of a given type. The value of the multiplicity is a useful piece of information for situations in which the $I4_1/acd$ symmetry of the tube is possibly further reduced by other geometrical considerations. For example, a flat, comb-like array of equidistant, identical parallel tubes joined at one end by a common channel loses (among others) all fourfold rotation and screw axes of symmetry, which lowers its space group symmetry to orthorhombic *Imma*. For the estimation of the entropy of polymers confined to such a nanostructure, origins belonging to the same subset for the isolated tube are, at least in principle, no longer equivalent.

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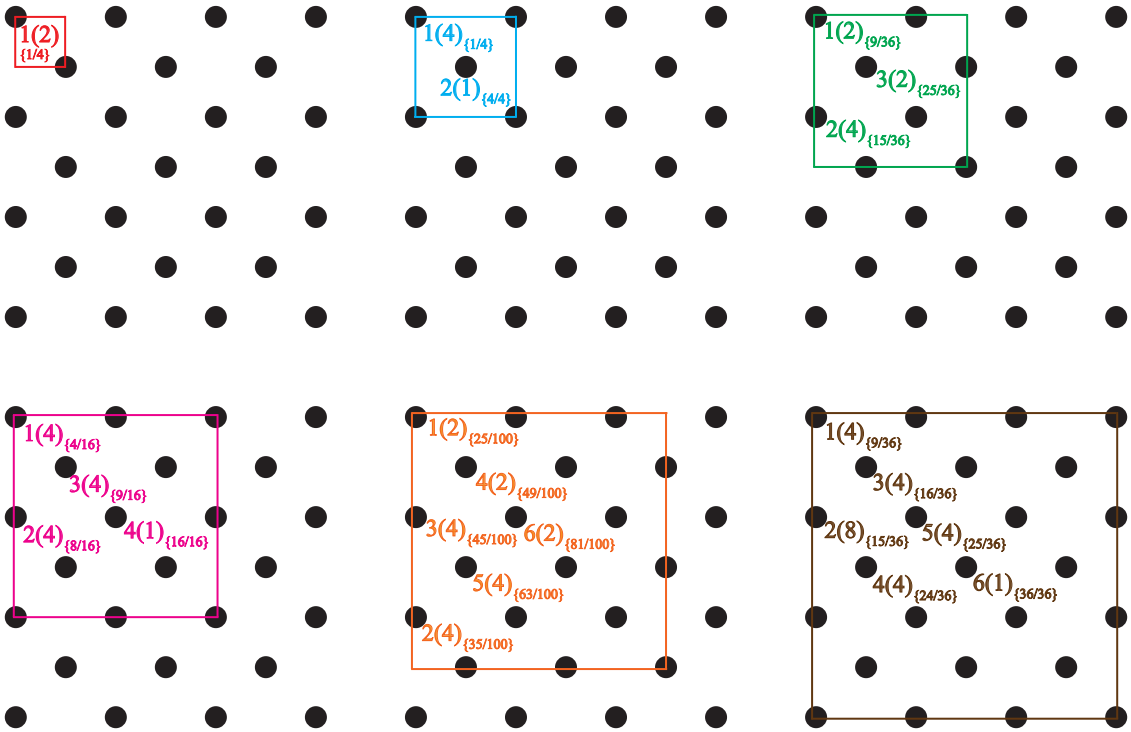

Figure 5. Numbering scheme for all possible origins of SAWs restricted to a tube of square cross section on the cubic F (FCC) lattice, for six tube cross section sizes. In all panels, black circles represent lattice points, squares are the tube cross sections: $0.5\sqrt{2}\times 0.5\sqrt{2}$, $1\sqrt{2}\times 1\sqrt{2}$, $1.5\sqrt{2}\times 1.5\sqrt{2}$, $2\sqrt{2}\times 2\sqrt{2}$, $2.5\sqrt{2}\times 2.5\sqrt{2}$, and $3\sqrt{2}\times 3\sqrt{2}$ from left to right, and top to bottom. The view is along the tube axis in direction [100]. Numbers on the left correspond to the label of each distinct origin (*type*). Numbers in parentheses correspond to the cardinality (multiplicity) of each subset. Subindices in braces correspond to area ratios (overlaps), r_i.

For the calculation of c_N for SAWs of the moderate lengths considered in this work, simple enumeration was more than adequate: c_N was obtained by exhaustively testing all possible SAWs of length N for self-intersections or for violation of the geometrical restrictions, and discarding those that fail to fulfill self-avoidance or geometrical constraint. Computations were carried out on Intel i7-8700K CPUs with 16 Gb of memory. For benchmark purposes in the case of unconstrained SAWs the computational (CPU) time required for the full enumeration of a $N = 17$-SAW in the SC lattice and of a $N = 13$-SAW in the FCC lattice reaches approximately 108 and 928 h, respectively.

It must be emphasized that the goal of this work is not to achieve high-accuracy values [27,82,83,86,93,94] in the calculation of the critical exponents or the leading or sub-leading correction-to-scaling exponents, but to obtain correlations for c_N for chains of moderate length to be used in the understanding of the entropic mechanisms of phase transitions observed in the off-lattice (continium) simulations of confined and densely-packed polymers.

3. Results

The values of c_N for SAWs on lattices restricted to a tube of cross section $L\times L$ oriented along the $\langle 100\rangle$ direction are presented in Tables A1 through A3 for the SC lattice, together with their average squared end-to-end distance. The corresponding results for the FCC lattice can be found in Tables A4 through A9. SAW origin *types* correspond to the labeling schemes of Figs.4 and 5. The coefficients of best fit of the scaling laws in Eqs. (1) and (2) to the data of Tables A1 through A9 are shown in Tables 1 and 2. As expected, the values of all coefficients are specific for each lattice type, tube size and type of origin. Within a given tube size, restricted SAWs starting at more confined lattice sites (lower *type*) have systematically lower values of c_N than those further removed from the boundaries. Thus, for SAWs of $N = 17$ restricted to a 3×3 tube in the SC lattice, $c_N = 9\,239\,393\,494$ for the more confined, in the corner of the tube, type 1 (of multiplicity 4), $c_N = 12\,003\,817\,994$ for the less confined type 2 (on the side wall with multiplicity 8) and $c_N = 14\,972\,474\,238$ for the least confined type 3 (with

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multiplicity 4). For comparison, using the same number of steps the number of different SAW configurations is ($N = 17$) $c_N = 473\,730\,252\,102$ for the unrestricted SC lattice.

Table 1. Calculated coefficients in scaling laws (Eqs. (1) and (2)) for SC lattice restricted to a tube oriented along [100]. Universal exponents for unrestricted SAWs are marked with an asterisk *.

Tube size	Type	A	μ	γ	D	ν
1×1	1	1.634	2.410	1.417	0.151	1.039
2×2	1	1.171	3.354	1.202	0.399	0.750
	2	1.519	3.262	1.289	0.315	0.794
	3	1.926	3.133	1.430	0.259	0.834
3×3	1	0.993	3.975	0.923	1.610	0.477
	2	1.303	3.806	1.133	1.052	0.543
	3	1.661	3.606	1.393	0.656	0.620
unrestricted SC lattice:		1.269	4.719	1.102*	1.046	0.603*

Table 2. Calculated coefficients in scaling laws (1) and (2) for FCC lattice restricted to a tube oriented along [100]. Universal exponents for unrestricted SAWs are marked with an asterisk *.

Tube size	Type	A	μ	γ	D	ν
$0.5\sqrt{2}\times0.5\sqrt{2}$	1	1.876	2.674	1.564	0.187	1.047
$1\sqrt{2}\times1\sqrt{2}$	1	1.063	4.696	1.745	0.203	0.899
	2	2.430	4.928	1.296	0.171	0.952
$1.5\sqrt{2}\times1.5\sqrt{2}$	1	0.747	6.615	1.352	0.710	0.597
	2	1.213	6.540	1.331	0.477	0.671
	3	1.917	6.267	1.410	0.314	0.756
$2\sqrt{2}\times2\sqrt{2}$	1	0.622	7.987	1.030	1.914	0.404
	2	1.062	7.512	1.282	1.163	0.480
	3	1.586	7.532	1.207	0.910	0.520
	4	1.764	6.843	1.634	0.521	0.624
$2.5\sqrt{2}\times2.5\sqrt{2}$	1	0.568	8.790	0.844	2.420	0.384
	2	0.911	8.740	0.873	1.916	0.408
	3	0.957	8.347	1.128	1.687	0.421
	4	1.413	8.477	1.004	1.421	0.444
	5	1.494	8.023	1.279	1.182	0.467
	6	1.577	7.606	1.544	0.910	0.505
$3\sqrt{2}\times3\sqrt{2}$	1	0.544	9.200	0.749	2.515	0.403
	2	0.906	8.827	1.028	1.849	0.425
	3	1.335	8.995	0.889	1.578	0.448
	4	1.396	8.575	1.200	1.318	0.460
	5	1.460	8.224	1.415	1.262	0.454
	6	1.456	8.172	1.505	1.062	0.474
unrestricted cubic F lattice:		1.190	10.06	1.135*	0.934	0.598*

Based on the results presented in Tables A1 through A9 Fig.6 shows the log-log plot of the number of distinct SAWs, c_N, versus the number of SAW steps, N, for all SC (left panel) and selected FCC (right panel) lattices for different SAW origins (types) and sizes of the confining tube. Also shown for comparison purposes are the corresponding results for the unrestricted cases. It can be clearly seen that for a given tube size the closer

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to the tube surface the lower the total number of distinct SAWS; for origin types residing in the corner of the tube the larger the tube size the larger the SAW population. Compared to the unrestricted case, type 1 (corner) of the smallest tube shows always the largest difference while the type of highest value (farthest from the corner) of the largest tube shows the closest similarity, independently of lattice type.

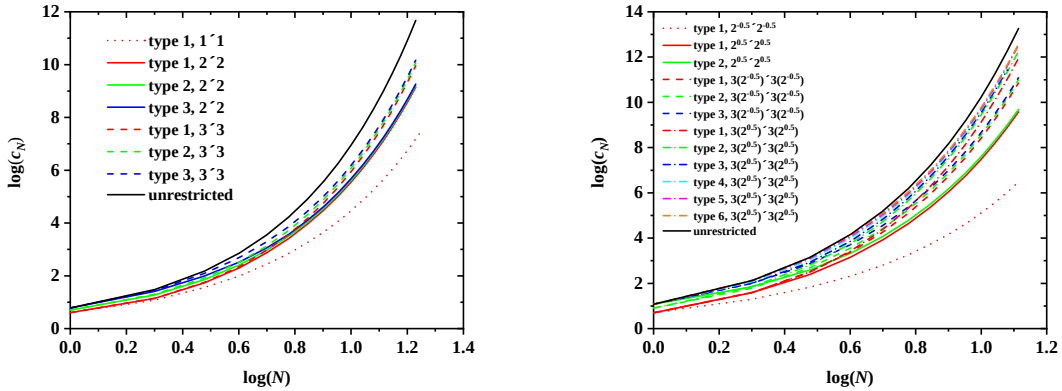

Figure 6. Log-log plot of the number of distinct SAW configurations, c_N, versus the number of SAW steps, N, for the SC (left panel) and the FCC (right panel) lattices. Tube cross-sections correspond to 1×1, 2×2 and 3×3 for SC and to $0.5\sqrt{2}\times0.5\sqrt{2}$, $1\sqrt{2}\times1\sqrt{2}$, $1.5\sqrt{2}\times1.5\sqrt{2}$ and $3\sqrt{2}\times3\sqrt{2}$ for FCC. For a given lattice and confining tube results are shown for every possible distinct SAW origin (type). Also shown for comparison are the corresponding curves for the unrestricted lattices (solid black lines).

We should note here that Eq. 1, quantifying the dependence of c_N on N is manifestly valid for the whole range of studied systems, independently of lattice type, tube confinement and SAW origin. However, the same is not true for Eq. 2 which relates SAW size, as quantified by the average square end-to-end distance, with number of SAW steps. For the unrestricted lattice Eq. 2 remains accurate in the whole N-range. In sharp contrast, for the confined lattices, especially for SAW origins near the confining tube, anomalous behavior is clearly observed for small-N SAWs. This is particularly evident in the results shown in Fig.7 showing log-log plots of $\left\langle \left|\omega^N\right|^2 \right\rangle$ versus N for SC (filled symbols) and FCC (open symbols) unrestricted (black color) and confined (red or green color) lattices. For the latter we differentiate between SAW origins corresponding to the most (SC: type 1 in 1×1 tube; FCC: type 1 in $0.5\sqrt{2}\times0.5\sqrt{2}$) and least (SC: type 3 in 3×3 tube; FCC: type 6 in $3\sqrt{2}\times3\sqrt{2}$) confined cases. The combination of spatial restrictions along with the anisotropy in cell size leads to this anomalous scaling for early-N SAWs. Thus, all D and ν coefficients reported in Tables 1 and 2, correspond to fittings applied on data covering the late-N SAW regime.

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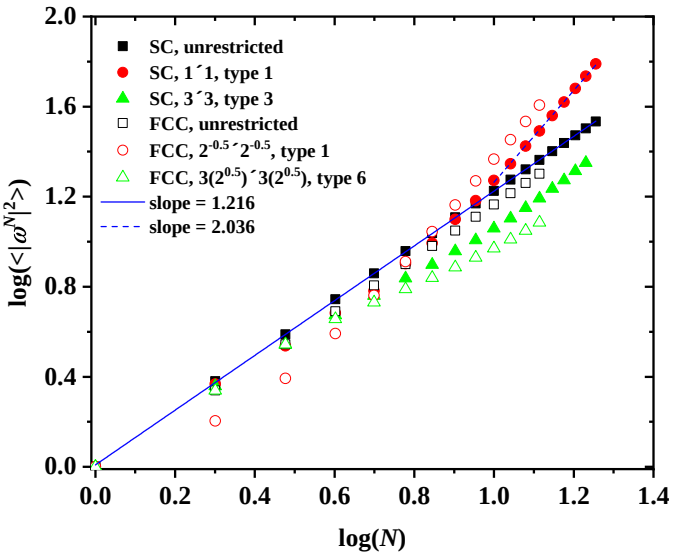

Figure 7. Log-log plot of the average squared end-to-end distance, $\left\langle \left|\omega^N\right|^2 \right\rangle$, versus the number of SAW steps, N, for the SC (filled symbols) and the FCC (open symbols) lattices. Black color corresponds to unrestricted lattices, while red and green to confined ones. Solid blue line corresponds to best linear fit on the whole range of SAW data for unrestricted SC lattice. Dashed blue line corresponds to best linear fit on the late-N SAW range for the most confined SC case (type 1 in 1×1 tube).

In addition to c_N and $\left\langle \left|\omega^N\right|^2 \right\rangle$, the discrete probability distribution functions of $\left|\omega^N\right|^2$ were also collected. In Figs.8 and 9 the effects of tube size (left panel), for a fixed SAW origin, and of origin type (right panel), for a fixed tube cross section, on the distribution for SAWs of length $N = 16$ are presented for the SC and FCC lattices, respectively. As expected, higher confinement (i.e. smaller tube cross section) leads to more stretched SAWs and a distribution shifted to higher values of $\left|\omega^{16}\right|^2$ (remarkably higher histogram values above $\left|\omega^{16}\right|^2$ at and above 50). This shift is particularly evident in the cumulative distributions (left panels of Figs.10 and 11). The strong confinement induced by the small tube 1×1 definitely leads to significantly more stretched SAWs.

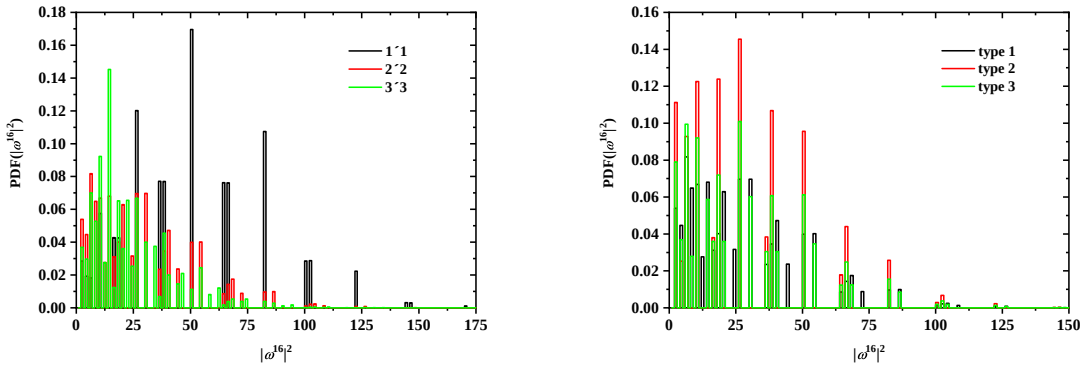

Figure 8. Probability distribution function for $\left|\omega^{16}\right|^2$ for SAWs of fixed length $N = 16$ on restricted SC lattices. Left panel shows the effect of tube cross section for a fixed SAW origin (type 1); right panel depicts the effect of SAW origin (type) for a fixed tube cross section (2×2).

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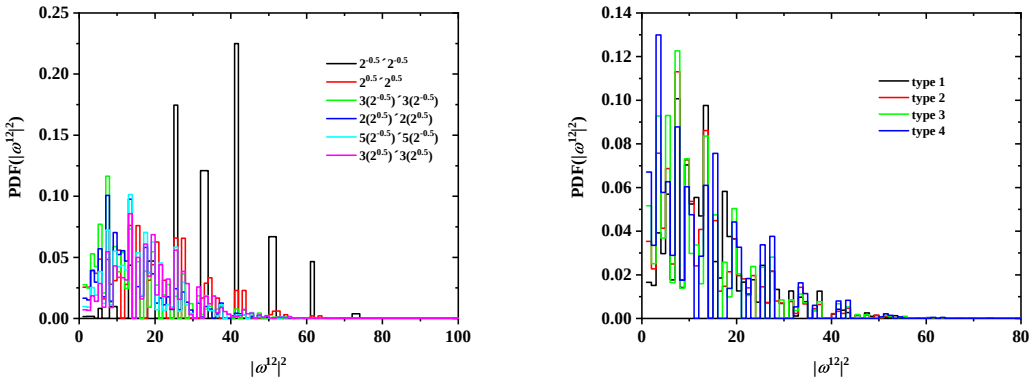

Figure 9. Probability distribution function for $\left|\omega^{12}\right|^2$ for SAWs of fixed length $N = 12$ on restricted FCC lattices. Left panel shows the effect of tube cross section for a fixed SAW origin (type 1); right panel depicts the effect of SAW origin (type) for a fixed tube cross section ($2\sqrt{2} \times 2\sqrt{2}$).

On the other hand, the SAW origin type has little influence on the spread of the distribution, but it does increase or reduce the probability of certain SAW extensions (see for example the higher red bars in the right panel of Fig.8). It is also remarkable that for a given N and tube cross section, the most confined SAWs (type 1 in this case) show non-vanishing probabilities for values of $\left|\omega^{16}\right|^2$ for which the probability for types 2 and 3 is zero (isolated black bars in the plot of Fig.8 at $\left|\omega^{16}\right|^2 = 12, 24, 44, 73$). Identical conclusions can be drawn for the effect of origin type and tube length for SAWS on FCC lattices according to the probability distributions presented in Fig.9. As can be seen in the right panels of Figs.10 and 11, there is virtually no difference in the cumulative distributions for the different types of SAW origins.

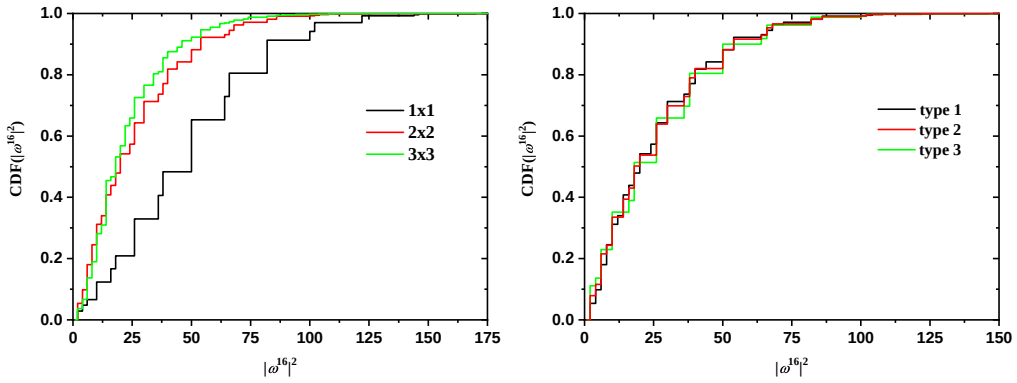

Figure 10. Cumulative probabilities for the distribution functions of $\left|\omega^{16}\right|^2$ for SAWs of fixed length $N = 16$ on restricted SC lattices of Fig.8.

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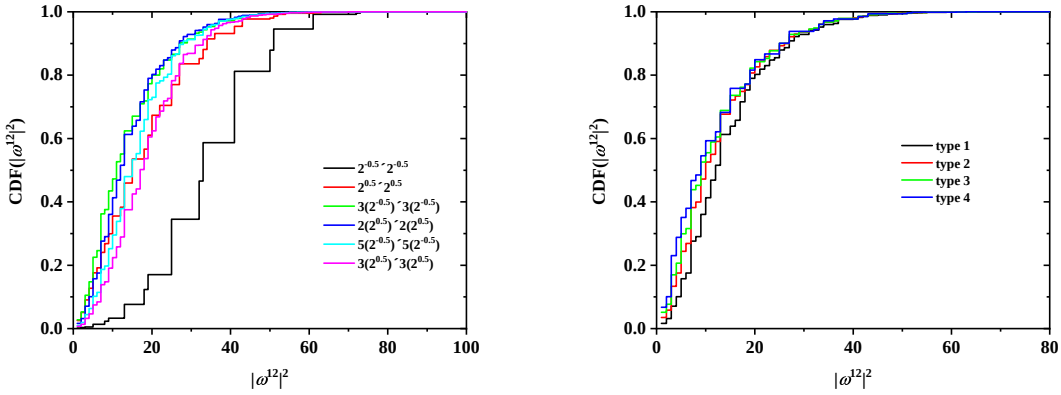

Figure 11. Cumulative probabilities for the distribution functions of $\left|\omega^{12}\right|^2$ for SAWs of fixed length $N = 12$ on restricted FCC lattices of Fig.9.

The effect of chain length on the cumulative distribution of $\left|\omega^{N}\right|^2$ is shown in Figs.12 and 13 for the SC and FCC lattices, respectively. With respect to SC, according to the data in Fig.12 the four curves corresponding to $N = 11, 13, 15, 17$ (left panel) are noticeably different, as they should be for different values of N. However, they come much closer together when scaled by $1/N$ (right panel of the same figure). In other words, the characteristic ratio of the SAWs is fairly constant in this range of N, with a median value of approx. 1.25. Very similar conclusion can be drawn for the FCC case (Fig.13), where the characteristic ratio shows little variation with the number of SAW steps.

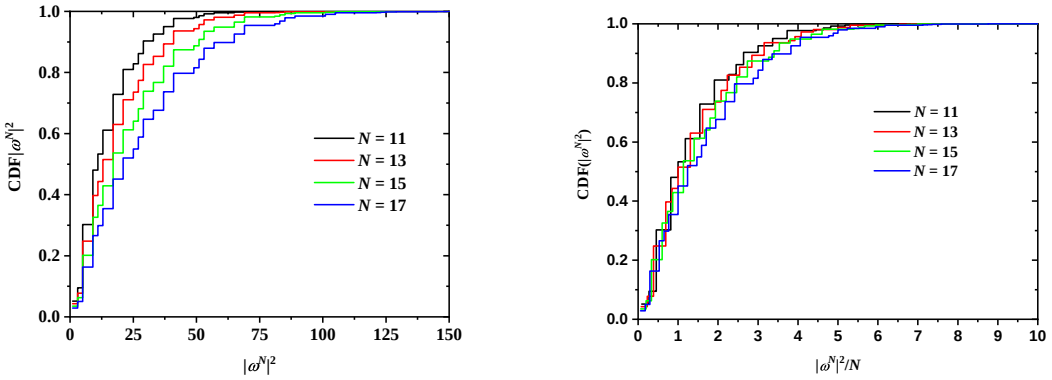

Figure 12. Cumulative probability distribution function for $\left|\omega^{N}\right|^2$ for SAWs of different length in a 2×2 tube and for SAW origin of type 1 (left panel) on restricted SC lattices. The right panel shows the same distributions, scaled by $1/N$, which for a step length of 1 is numerically equivalent to the characteristic ratio of the SAW [95].

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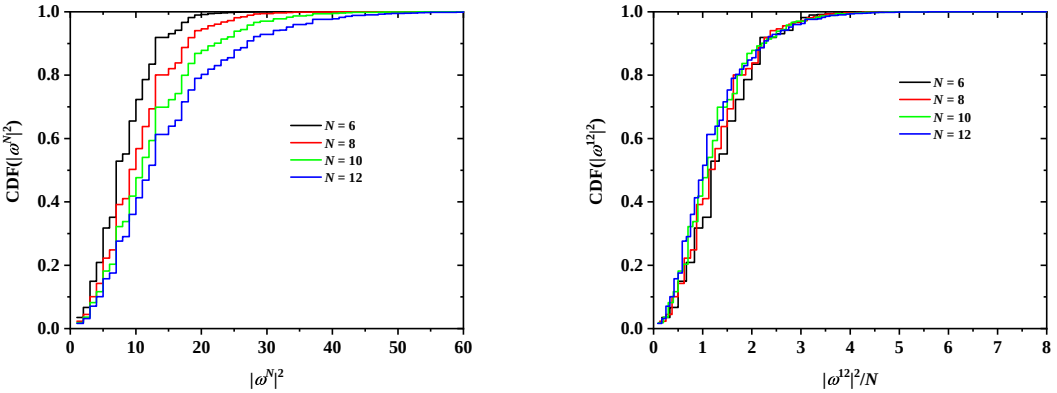

Figure 13. Cumulative probability distribution function for $\left|\omega^N\right|^2$ for SAWs of different length in a $2\sqrt{2}\times 2\sqrt{2}$ tube and for SAW origin of type 1 (left panel) on restricted FCC lattices. The right panel shows the same distributions, scaled by $1/N$, which for a step length of 1 is numerically equivalent to the characteristic ratio of the SAW [95].

4. Discussion

An inspection of the tables shows that c_N is, as expected, lower for the restricted lattices than for the unrestricted ones, the more so, the smaller the restricting tube. The black, solid line in both panels of Fig.6 represents in log-log scale the growth of c_N with SAW length N for the unrestricted case, while all other lines correspond to the value of c_N for SAWs restricted on confining tubes of specific sizes for all possible different origins, both on the cubic P (left panel) and F (right panel) lattices.

The faster growth of c_N for unrestricted SAWs is also reflected in the larger values of the connective constant μ, which is the dominant term in Eq. 1 for large values of N: $\mu^{SC} = 4.719$ for the unrestricted SC lattice, against $\mu_r^{SC} = 3.798$ (multiplicity-based, weighted average over all three types of origin) for the restricted 3×3 SC lattice, while the corresponding value drops to just $\mu^{SC} = 2.410$ for the 1×1 tube, a decrease of approximately 50% with respect to the bulk case. For the FCC lattice the analogous numbers are: $\mu^{FCC} = 10.06$ (unrestricted), $\mu_r^{FCC} = 8.751$ (weighted average over all six types of origin for the restricted $3\sqrt{2}\times 3\sqrt{2}$ FCC lattice) and $\mu^{FCC} = 2.674$ for the most confined $0.5\sqrt{2}\times 0.5\sqrt{2}$ FCC case, the latter being around 75% less than the value of the unrestricted FCC SAW. This behavior is in agreement with the geometrical meaning of connectivity: restricted SAWs that start close to one of the boundaries have, on average, fewer neighbors than those that start close to the confining tube.

In addition, the average (weighted by the multiplicity of the type of starting lattice point) connectivity constants in Tables 1 and 2 reflect this trend very clearly: as tube size increases, the values of the average connectivity constant increase and approach the unrestricted values. For FCC lattices of sizes $0.5\sqrt{2}\times 0.5\sqrt{2}$, $1\sqrt{2}\times 1\sqrt{2}$, $1.5\sqrt{2}\times 1.5\sqrt{2}$, $2\sqrt{2}\times 2\sqrt{2}$, $2.5\sqrt{2}\times 2.5\sqrt{2}$ and $3\sqrt{2}\times 3\sqrt{2}$ the multiplicity-weighted average values of μ are 2.674 (73.4%), 4.742 (52.9%), 6.491 (35.5%), 7.613 (24.3%), 8.344 (17.2%) and 8.751 (13.1%), where numbers in parentheses denote percentage reduction with respect to the connectivity constant of the bulk FCC lattice.

Furthermore, for a given size of the tube the values of c_N for different origins tend to converge as N grows. This is most clearly observed in the left panel of Fig.6: the curves for the three origin types are already quite close for the moderate value $N = 17$ for all restricted SC lattices. The same true for the SAWs of length $N = 12$ on confined FCC lattices as seen in the right panel of Fig.6. For a given lattice type (FCC or SC) and a given spatial restriction (tube cross section), the value of c_N must approach a common limit as $N\to\infty$, independently of the particular type of SAW origin: sufficiently long SAWs lose the "memory" of their starting point so that:

$$\lim_{N\to\infty}\frac{\log c_N^i}{\log c_N^j} = 1 \quad i\in O_i,\ j\in O_j \quad i\neq j$$

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must hold, where O_k is one of the sets of equivalent SAW origins for a restricted lattice, and c_N^i is the number of restricted SAWs of length N starting at an origin of type $i \in O_i$. The rate at which c_N^i approaches this common $N \to \infty$ limit is of course dependent on the lattice. As can be seen in Fig.6, SAWs on the restricted FCC lattice tend to this limit more slowly than SAWs on the SC one.

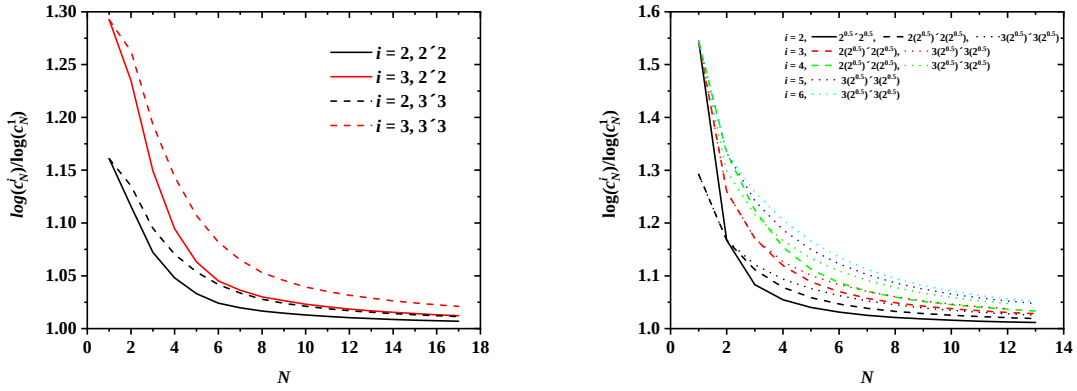

Figure 14. Ratio $\dfrac{\log c_N^i}{\log c_N^1}$ as a function of SAW steps, N, for different SAW origins $i = 2, \ldots, |O_k|$ on (left): 2×2 (solid lines) and 3×3 (dashed lines) SC and (right): $1\sqrt{2} \times 1\sqrt{2}$ (solid line), $2\sqrt{2} \times 2\sqrt{2}$ (dashed lines) and $3\sqrt{2} \times 3\sqrt{2}$ (dotted lines) FCC lattices.

In Fig.14 the ratio $\dfrac{c_N^i}{c_N^1}$ for different SAW origins (i.e. the ratio of the curves represented in Fig.6 divided by the curve for c_N of SAW origin of type 1, taken arbitrarily as reference) is seen to indeed approach unity as N increases for both SC (left panel) and FCC (right panel) lattices. Systematically, the ratio tends faster to unity for SAW origins that lie close in space and for smaller tube cross sections. For example, for a SAW of length $N = 13$ on the $3\sqrt{2} \times 3\sqrt{2}$ FCC lattice for type of origin $i = 2$, 4 and 6 the corresponding ratios are 1.026, 1.048 and 1.051. In parallel, for a SAW of $N = 17$ steps on a SC lattice with origin type 2 the ratio increases from 1.007 for a 2×2 tube to 1.011 for a 3×3 one.

The dependence of c_N on SAW origin (type) for given N and tube size can be explained, at least approximately, by a simple geometric argument. Since a higher degree of confinement leads to a greater reduction in c_N, it seems natural to attempt a scaling of c_N^i by means of the following area ratio or *overlap*:

$$r_i = \frac{A_i \cap A^{tube}}{A^{tube}} \leq 1$$

where $A_i \cap A^{tube}$ is the area common to a tube cross section (a square in the present work) centered at the SAW origin of type i (square in dotted line in Fig.15), and the tube cross section. The overlap r_i is the ratio of this area (small square in Fig.15) to the entire tube cross section. More highly confined SAW origins (i.e. a corner, like type 1 in the 3×3 restricted SC lattice) have lower values of r^i, while those close to the center of the tube have higher r^i. Taking the SC lattice restricted by a 3×3 tube (rightmost panel in Fig.4) as an illustrative example, the values of the overlap for the three distinct types of origin are:

$$r_1 = \frac{1}{4} \qquad r_2 = \frac{5}{12} \qquad r_3 = \frac{25}{36}$$

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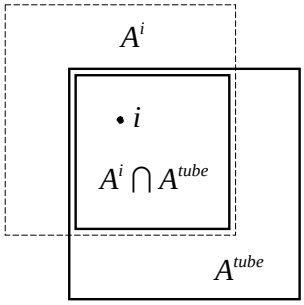

Figure 15. The overlap r_i is defined as the area (small square) common to a tube cross section centered at the origin of type i (dashed line) and the tube cross section (solid line), divided by the complete tube cross section.

The overlap values for all SAW origin types in the SC and FCC lattices used in the present work are reported in braces in the schemes of Figs. 4 and 5. In fact, going back to the sketches the labeling of the distinct types of SAW origins is in fact based on the overlap value of a given site: the lower the overlap value the lower the origin index. According to the definition, overlap values for the SC and FCC lattices, confined in tube with direction type $\langle 100 \rangle$, are bounded between 0.25 (assigned always to origin type 1) and 1. As can be seen in the reported area ratios of Figs. 4 and 5 for a given tube size no two distinct origin types have the same overlap value. With respect to the confined $3\sqrt{2} \times 3\sqrt{2}$ FCC lattice origin types 1, 2, 3, 4, 5 and 6 are characterized by area ratios (overlaps) of $9/36$, $15/36$, $16/36$, $24/36$, $25/36$ and $36/36$, respectively.

Based on the above it is tempting to study the behavior of the curves $\frac{c_N^i}{r_i}$ (log-log plots in Fig.16) versus N, where now the number of distinct SAW configurations for a given origin type is divided by the corresponding overlap of that type. The comparison of the left panel of Fig.6 with Fig.16 strongly suggests that this simple geometric argument does indeed successfully explain to first order the dependence of c_N on the type of SAW origin. Curves corresponding to different tube cross-sections and origin types seem to be brought closer together when they are scaled by the proper overlap values.

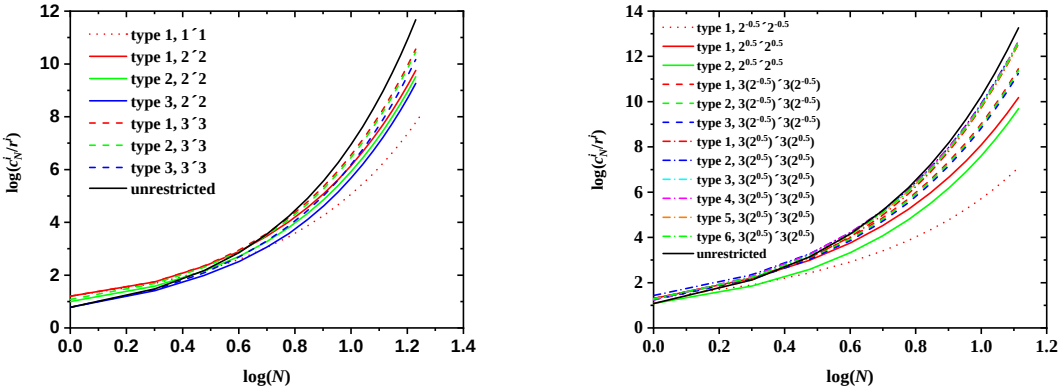

Figure 16. Log-log plot of the number of distinct SAW configurations scaled by the inverse overlap, c_N^i/r^i, as a function of SAW steps, N, on confined SC (left panel) and FCC lattices (right panel) for various origin types and tube cross-sections. Also shown for comparison are the corresponding results for the unrestricted SAW (solid black line).

Author Contributions: conceptualization, ML; methodology, NK, ML, JB; software, JB; writing—original draft preparation, ML; writing—review and editing, NK, JB; visualization, NK; funding acquisition, NK.

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Abbreviations

The following abbreviations are used in this manuscript:

FCC	Face Centered Cubic
MC	Monte Carlo
MD	Molecular Dynamics
SAW	Self-Avoiding Walk
SC	Simple Cubic
CCE	Characteristic Crystallographic Element (norm)
BCC	Body Centered Cubic

Appendix A

Table A1. SC lattice, tube cross section 1.0×1.0. The second column of the first table is the value of c_N for SAWs on the unrestricted SC lattice, included for comparison purposes.

		Type 1 multiplicity $\lvert O_1 \rvert = 4$	
N	c_N unrestricted	c_N	$\left\langle \lvert \omega^N \rvert^2 \right\rangle$
1	6	4	1.000
2	30	12	2.333
3	150	36	3.444
4	726	98	4.816
5	3 534	274	6.051
6	16 926	702	7.977
7	81 390	1 854	9.846
8	387 966	4 614	12.56
9	1 853 886	11 778	15.20
10	8 809 878	28 914	18.73
11	41 934 150	72 394	22.19
12	198 842 742	176 310	26.59
13	943 974 510	435 346	30.98
14	4 468 911 678	1 055 730	36.29
15	21 175 146 054	2 584 026	41.66
16	100 121 875 974	6 249 358	47.94
17	473 730 252 102	15 208 438	54.34
18	2 237 723 684 094	36 724 294	61.60

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Table A2. SC lattice, tube cross section 2.0×2.0.

	Type 1	multiplicity $\lvert O_1\rvert = 4$		Type 2	multiplicity $\lvert O_2\rvert = 4$
N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$	N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$
1	4	1.000	1	5	1.000
2	14	2.571	2	19	2.316
3	54	3.963	3	72	3.556
4	200	5.420	4	258	4.853
5	744	6.634	5	926	5.916
6	2 626	7.925	6	3 176	7.146
7	9 186	9.051	7	11 000	8.276
8	31 122	10.37	8	36 988	9.670
9	105 766	11.63	9	125 302	11.01
10	351798	13.18	10	414 518	12.68
11	1 175 726	14.71	11	1 381 390	14.31
12	3 859 350	16.59	12	4 515 022	16.31
13	12 729 142	18.46	13	14 853 462	18.30
14	41 355 642	20.71	14	48 105 654	20.67
15	134 970 238	22.96	15	156 694 796	23.03
16	435 124 318	25.60	16	504 010 840	25.80
17	1 408 619 206	28.25	17	1 629 120 330	28.56

	Type 3	multiplicity $\lvert O_3\rvert = 1$
N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$
1	6	1.000
2	26	2.154
3	98	3.122
4	330	4.170
5	1 130	5.120
6	3 746	6.388
7	12 802	7.581
8	42 498	9.120
9	143 610	10.58
10	472 242	12.42
11	1 570 714	14.19
12	5 110 426	16.36
13	16 779 354	18.46
14	54 148 874	21.00
15	176 058 234	23.49
16	564 679 330	26.43
17	1 822 489 530	29.34

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Table A3. SC lattice, tube cross section 3.0×3.0.

	Type 1	multiplicity $\lvert O_1\rvert = 4$		Type 2	multiplicity $\lvert O_2\rvert = 8$
N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$	N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$
1	4	1.000	1	5	1.000
2	14	2.571	2	20	2.400
3	56	4.143	3	82	3.780
4	224	5.911	4	328	5.311
5	926	7.505	5	1 336	6.683
6	3 738	9.179	6	5 273	8.107
7	15 056	10.64	7	20 813	9.331
8	59 092	12.09	8	80 282	10.61
9	230 254	13.36	9	309 654	11.76
10	881 850	14.65	10	1 175 480	13.02
11	3 367 124	15.84	11	4 466 712	14.20
12	12 712 194	17.13	12	16 770 216	15.54
13	47 952 018	18.38	13	63 066 644	16.85
14	179 317 400	19.77	14	234 827 439	18.33
15	670 507 498	21.17	15	875 986 779	19.80
16	2 488 658 374	22.73	16	3 239 657 890	21.47
17	9 239 393 494	24.31	17	12 003 817 994	23.13

	Type 3	multiplicity $\lvert O_3\rvert = 4$
N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$
1	6	1.000
2	28	2.286
3	122	3.492
4	488	4.721
5	1 926	5.760
6	7 328	6.885
7	28 132	7.896
8	106 004	9.068
9	403 470	10.17
10	1 512 774	11.46
11	5 715 168	12.70
12	21 299 430	14.15
13	79 832 758	15.55
14	295 630 770	17.18
15	1 099 932 734	18.77
16	4 049 793 742	20.60
17	14 972 474 238	22.38

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Table A4. FCC lattice, tube cross section $0.5\sqrt{2} \times 0.5\sqrt{2}$. The second column of the first table is the value of c_N for SAWs on the unrestricted FCC lattice, included for comparison purposes.

		Type 1	multiplicity $\lvert O_1 \rvert = 2$	
N	c_N unrestricted		c_N	$\left\langle \lvert \omega^N \rvert^2 \right\rangle$
1	12		5	1.000
2	132		20	1.600
3	1 404		68	2.471
4	14 700		208	3.904
5	152 532		624	5.776
6	1 573 716		1 840	8.157
7	16 172 148		5 360	11.07
8	165 697 044		15 488	14.56
9	1 693 773 924		44 608	18.61
10	17 281 929 564		128 192	23.22
11	176 064 704 412		368 064	28.39
12	1 791 455 071 068		1 056 000	34.13
13	18 208 650 297 396		3 028 992	40.43

Table A5. FCC lattice, tube cross section $1.0\sqrt{2} \times 1.0\sqrt{2}$.

	Type 1	multiplicity $\lvert O_1 \rvert = 4$		Type 2	multiplicity $\lvert O_2 \rvert = 4$
N	c_N	$\left\langle \lvert \omega^N \rvert^2 \right\rangle$	N	c_N	$\left\langle \lvert \omega^N \rvert^2 \right\rangle$
1	5	1.000	1	12	1.000
2	39	2.256	2	72	1.556
3	248	3.113	3	392	2.265
4	1 460	3.907	4	2 176	3.199
5	8 132	4.756	5	11 680	4.286
6	43 860	5.816	6	61 136	5.633
7	230 476	7.106	7	314 416	7.226
8	1 190 588	8.657	8	1 600 960	9.073
9	6 072 572	10.47	9	8 070 448	11.20
10	30 677 292	12.57	10	40 350 672	13.63
11	153 744 188	14.97	11	200 495 840	16.38
12	765 753 696	17.68	12	992 030 176	19.45
13	3 796 189 560	20.70	13	4 893 578 576	22.85

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Table A6. FCC lattice, tube cross section $1.5\sqrt{2} \times 1.5\sqrt{2}$.

	Type 1	multiplicity $\lvert O_1\rvert = 2$		Type 2	multiplicity $\lvert O_2\rvert = 4$
N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$	N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$
1	5	1.000	1	8	1.000
2	39	2.256	2	62	2.097
3	317	3.738	3	487	3.234
4	2 456	4.927	4	3 643	4.223
5	18 028	5.920	5	26 106	5.096
6	127 242	6.813	6	181 783	5.960
7	876 392	7.705	7	1 240 790	6.878
8	5 934 196	8.661	8	8 342 670	7.894
9	39 648 964	9.725	9	55 415 928	9.034
10	261 993 600	10.92	10	364 364 782	10.32
11	1 715 097 328	12.27	11	2 375 202 602	11.76
12	11 139 357 984	13.79	12	15 371 509 668	13.36
13	71 869 479 512	15.47	13	98 873 697 150	15.14

	Type 3	multiplicity $\lvert O_3\rvert = 2$
N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$
1	12	1.000
2	101	1.941
3	736	2.707
4	5 152	3.468
5	35 522	4.299
6	241 888	5.216
7	1 627 468	6.236
8	10 825 480	7.377
9	71 271 844	8.656
10	465 099 616	10.08
11	3 012 465 424	11.67
12	19 389 036 972	13.43
13	124 130 404 052	15.36

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Table A7. FCC lattice, tube cross section $2.0\sqrt{2} \times 2.0\sqrt{2}$.

	Type 1	multiplicity $\lvert O_1 \rvert = 4$		Type 2	multiplicity $\lvert O_2 \rvert = 4$
N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$	N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$
1	5	1.000	1	8	1.000
2	39	2.256	2	72	2.222
3	317	3.738	3	602	3.326
4	2 707	5.402	4	5 018	4.556
5	22 778	6.887	5	41 050	5.692
6	186 798	8.169	6	328 378	6.703
7	1 493 410	9.278	7	2 577 480	7.640
8	11 705 520	10.28	8	19 944 688	8.557
9	90 414 004	11.23	9	152 636 704	9.491
10	690 737 504	12.19	10	1 157 776 248	10.47
11	5 231 407 492	13.18	11	8 716 517 832	11.52
12	39 334 158 792	14.23	12	65 200 437 688	12.65
13	293 889 553 284	15.37	13	484 934 433 160	13.88

	Type 3	multiplicity $\lvert O_3 \rvert = 4$		Type 4	multiplicity $\lvert O_4 \rvert = 1$
N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$	N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$
1	12	1.000	1	12	1.000
2	101	1.941	2	132	2.182
3	847	3.116	3	1 152	2.958
4	6 946	4.152	4	9 144	3.636
5	55 498	5.088	5	70 400	4.353
6	435 926	5.985	6	536 376	5.144
7	3 379 684	6.879	7	4 071 072	6.012
8	25 926 400	7.797	8	30 796 856	6.961
9	197 133 924	8.763	9	231 952 920	7.991
10	1 487 560 076	9.795	10	1 738 210 872	9.107
11	11 150 268 460	10.91	11	12 958 623 176	10.31
12	83 085 654 372	12.11	12	96 129 954 888	11.61
13	615 859 395 980	13.41	13	709 838 117 576	13.02

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Table A8. FCC lattice, tube cross section $2.5\sqrt{2} \times 2.5\sqrt{2}$.

	Type 1	multiplicity $\lvert O_1 \rvert = 2$		Type 2	multiplicity $\lvert O_2 \rvert = 4$
N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$	N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$
1	5	1.000	1	8	1.000
2	39	2.256	2	62	2.097
3	317	3.738	3	522	3.421
4	2 707	5.402	4	4 508	4.922
5	23 701	7.209	5	39 468	6.465
6	208 144	8.941	6	344 215	7.922
7	1 810 302	10.50	7	2 966 304	9.241
8	15 526 912	11.89	8	25 216 726	10.43
9	131 356 780	13.18	9	211 725 485	11.52
10	1 098 163 378	14.24	10	1 759 351 811	12.54
11	9 092 485 480	15.28	11	14 497 192 414	13.54
12	74 701 087 430	16.29	12	118 646 116 612	14.52
13	609 855 297 956	17.29	13	965 528 829 603	15.53

	Type 3	multiplicity $\lvert O_3 \rvert = 4$		Type 4	multiplicity $\lvert O_4 \rvert = 2$
N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$	N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$
1	8	1.000	1	12	1.000
2	72	2.222	2	101	1.941
3	637	3.474	3	847	3.116
4	5 557	4.763	4	7 365	4.472
5	48 366	6.108	5	63 980	5.751
6	418 016	7.410	6	549 602	6.915
7	3 570 910	8.604	7	4 663 884	7.987
8	30 133 676	9.693	8	39 130 524	8.997
9	251 551 004	10.71	9	325 115 970	9.971
10	2 081 126 958	11.69	10	2 679 470 380	10.93
11	17 091 369 920	12.66	11	21 936 104 286	11.90
12	139 509 610 898	13.64	12	178 579 440 256	12.90
13	1 132 860 537 091	14.66	13	1 446 780 259 612	13.94

	Type 5	multiplicity $\lvert O_5 \rvert = 4$		Type 6	multiplicity $\lvert O_6 \rvert = 2$
N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$	N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$
1	12	1.000	1	12	1.000
2	116	2.069	2	132	2.182
3	1 044	3.176	3	1 277	3.249
4	9 138	4.292	4	11 348	4.143
5	78 471	5.355	5	96 462	4.951
6	664 057	6.347	6	802 244	5.743
7	5 558 369	7.293	7	6 601 488	6.553
8	46 127 001	8.218	8	54 022 204	7.400
9	380 120 277	9.144	9	440 478 598	8.292
10	3 113 966 985	10.09	10	3 580 119 048	9.236
11	25 377 886 728	11.06	11	29 005 342 540	10.24
12	205 863 958 205	12.08	12	234 222 195 762	11.29
13	1 662 935 723 189	13.14	13	1 885 131 153 122	12.41

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Table A9. FCC lattice, tube cross section $3.0\sqrt{2} \times 3.0\sqrt{2}$.

	Type 1	multiplicity $\lvert O_1\rvert = 4$		Type 2	multiplicity $\lvert O_2\rvert = 8$
N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$	N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$
1	5	1.000	1	8	1.000
2	39	2.256	2	72	2.222
3	317	3.738	3	637	3.474
4	2 707	5.402	4	5 683	4.881
5	23 701	7.209	5	50 802	6.330
6	211 575	9.140	6	455 104	7.820
7	1 903 598	11.06	7	4 070 009	9.286
8	17 110 652	12.87	8	36 207 759	10.67
9	152 867 156	14.52	9	319 799 348	11.95
10	1 354 729 516	16.02	10	2 803 337 706	13.14
11	11 906 603 784	17.38	11	24 402 025 435	14.26
12	103 849 402 452	18.63	12	211 104 465 801	15.32
13	899 747 181 304	19.79	13	1 816 626 021 973	16.35

	Type 3	multiplicity $\lvert O_3\rvert = 4$		Type 4	multiplicity $\lvert O_4\rvert = 4$
N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$	N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$
1	12	1.000	1	12	1.000
2	101	1.941	2	116	2.069
3	847	3.116	3	1 100	3.313
4	7 365	4.472	4	10 076	4.478
5	65 563	5.968	5	90 588	5.648
6	587 910	7.447	6	806 164	6.802
7	5 257 852	8.837	7	7 114 248	7.907
8	46 707 884	10.13	8	62 314 664	8.960
9	411 696 828	11.33	9	542 275 908	9.972
10	3 601 355 396	12.46	10	4 692 529 524	10.96
11	31 287 972 228	13.53	11	40 409 930 416	11.93
12	270 207 494 804	14.57	12	346 527 771 156	12.90
13	2 321 640 993 718	15.59	13	2 960 543 277 900	13.89

	Type 5	multiplicity $\lvert O_5\rvert = 4$		Type 6	multiplicity $\lvert O_6\rvert = 1$
N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$	N	c_N	$\left\langle \lvert\omega^N\rvert^2 \right\rangle$
1	12	1.000	1	12	1.000
2	132	2.182	2	132	2.182
3	1 277	3.249	3	1 404	3.496
4	11 839	4.380	4	13 680	4.530
5	107 062	5.466	5	125 376	5.383
6	950 202	6.476	6	1 109 776	6.157
7	8 326 206	7.429	7	9 637 976	6.915
8	72 328 430	8.352	8	82 849 936	7.690
9	624 508 830	9.265	9	708 279 448	8.499
10	5 368 075 614	10.18	10	6 035 931 488	9.350
11	45 975 770 236	11.12	11	51 329 173 080	10.25
12	392 534 289 628	12.07	12	435 731 432 064	11.19
13	3 341 824 209 214	13.06	13	3 692 543 313 752	12.19

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