

Article

Two-Level Evolutionary Multi-Objective Optimization of a District Heating System with Distributed Cogeneration

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Abstract: The paper deals with the modelization and optimization of an integrated multi-component energy system. On-off operation and presence-absence of components must be described by means of binary decision variables, besides equality and inequality constraints; furthermore, the synthesis and the operation of the energy system should be optimized at the same time. In this paper a hierarchical optimization strategy is used, adopting a genetic algorithm in the higher optimization level, to choose the main binary decision variables, whilst a MILP algorithm is used in the lower level, to choose the optimal operation of the system and to supply the merit function to the genetic algorithm. The method is then applied to a distributed generation system, which has to be designed for a set of users located in the center of a small town in the North-East of Italy. The results show the advantage of distributed cogeneration, when the optimal synthesis and operation of the whole system are adopted, and significant reduction in the computing time by using the proposed two-level optimization procedure.

Keywords: District Heating; multi-objective evolutionary optimization; distributed cogeneration; optimal operation.

1. Introduction

A more thorough integration among energy systems is expected to significantly contribute to reducing primary energy consumption, as well as global pollutant emissions and energy costs for final users. Integrated District Heating (DHN) networks and Combined Heat and Power (CHP) are of particular interest for the object of defining an efficient system for distributed energy generation and are widely discussed in Literature, i.e. in terms of role and opportunities in a country like Denmark [1] or United Kingdom [2], or considering a review of the different technology opportunities [3] and of the energy sources [4] also for Combined Heat, Cooling and Power systems (CHCP). The expected advantages of energy integration can, in fact, be obtained in real world applications only if the structure (synthesis) and the management of the whole system are carefully optimized. For instance, in [5] a computational framework is proposed to face the problem at city districts level, in [6] a Mixed Integer Linear Programming (MILP) model is used to determine the type, number and capacity of equipment in CHCP systems installed in a tertiary sector building, in [7] a modelling and optimization method is developed for planning and operating a CHP-DH system with a solar thermal plant and a thermal energy storage, in [8] a detailed optimization model is presented for planning the short-term operation of combined cooling, heat and power (CCHP) energy systems, for a single user in [9] an algorithm for the minimization of a suitable cost function is applied to optimize CHP commercial and domestic systems with variable heat demand.

Synthesis and operation optimization of integrated multi-component energy systems generally require a binary variable set to be introduced to describe the existence/absence and the on/off operation status of components and energy connections inside the model. Besides these, other

continuous variables have to be introduced for modelling the energy and material flows exchanged among components, as well as other possible design options [6, 10, 11].

In addition to this complex variable set, the variation of the thermal demands of the final users has also to be taken into account. Thus, a Mixed Integer Non Linear Programming (MINLP) problem has generally to be solved for obtaining the optimal synthesis and operation of the integrated system, with a high computational effort. A general introduction to MILP, MINLP and other possible approaches to the design and synthesis optimization of energy systems can be found in [12]. Recently, the MINLP approach has been used, for instance in [13, 14] to optimize the CCHP systems of different buildings with solar energy integration.

The computational effort can be reduced if the whole problem is faced by defining two (or more) levels, which can be solved dealing with a reduced number of independent variables [15], or if it is decomposed into many sub-problems, which have to be solved with an iterative procedure [16–18]. In both cases the solution could be more easily obtained if the problem were described with sufficient precision by means of a linear model (MILP), even if additional variables are introduced for considering strong non-linear relations among flows of both energy and mass [10, 11].

Unfortunately, when there is a high number of binary variables present in almost all sub-problems, the coupling variables, which allow each sub-problem to be solved consistently with the optimal solution of the whole system [19, 20], become too changeable to allow the convergence of the optimization process toward the actual optimum. This is highlighted, for instance, in [21], where the Mixed Integer Linearized Exergoeconomic (MILE) method is presented and the thermoeconomic costs are used as coupling variables.

In the present paper, such difficulties are overcome by using a novel approach, characterized by a two-level hierarchical optimization strategy which does not require an explicit system decomposition. In the proposed method a genetic algorithm is used in the higher optimization level, to choose the main binary decision variables, whilst a MILP algorithm is used in the lower level, to choose the optimal operation of the system and to supply the merit function to the genetic algorithm.

The proposed system model is intended for district-level implementation and is concerned with the optimal layout and operation of CHP units, deployed in different buildings, as well as with the optimal configuration of one, or more micro-district heating grids. A central CHP plant, besides a set of micro-CHP gas turbines distributed among the involved buildings, along with the installation of thermal collectors and photovoltaic (PV) panels have been considered to further improve the energy efficiency and sustainability of the whole system.

The main optimization was aimed at minimizing the total annual cost for owning, maintaining and operating of the whole system. Furthermore, the optimal solution, beside satisfying the electric energy and heating demands of each building throughout the year, should allow a minimum environmental impact. Therefore, a multi-objective optimization has been performed, by considering, as a second objective of the optimization, the avoided CO₂ compared to the conventional energy supply.

In summary, the method allows the identification of the optimal configuration of the micro-district heating grids, of the design of the CHP units in each building and the optimal operation of the whole energy system inside a unique optimization procedure, satisfying the energy demands of multiple users.

The focus of this paper does not lie so much in the numerical solution of the case study, but rather in the performance of the hierarchical optimization algorithm and on the option of easily performing a multi-objective optimization. The expectation is that the developed optimization strategy highlights a reduction in the computing time compared with the direct implementation of the whole problem in a single level MILP solver. Therefore, the presented method could be applied to distributed cogeneration systems with a number of energy users and district heating branches much higher than those considered in the case study.

2. Model of a cogeneration system with District Heating

In the following, a distributed cogeneration and district heating system is considered, whose model includes both a set of micro-cogeneration gas turbines (TG), a centralized cogeneration system based on an Internal Combustion Engine (ICE), photovoltaic panels (PV), solar thermal collectors (ST) and various district heating pipelines, potentially connecting the users.

The mathematical problem of optimizing the layout and operation of such a distributed cogeneration plant can be generally formulated as a MINLP problem, because the optimization variables expressing partial load operation of each CHP engine are involved in non-linear relations. However, a realistic description of the system may be formulated as a MILP problem by properly discretizing the load curves, so that in each time interval the thermal and electrical demands can be assumed as constants, and approximating the performance maps of energy producing components with a set of linear functions (see, for instance, [22, 23] for a single energy user and [24, 25] for multiple energy users). Notice that, in the discretized problem, each time interval is solved as the power and heat demand of each building were constant, therefore neglecting also the effect of dynamic load variation on the performance of the energy supplying components, but considering only their performance evaluated at different level of constant load. In other words, the dynamic response of engine and microturbines are considered much faster than the dynamic variations in the demand of the users. Notice also that this does not mean that each time interval could be optimized individually, because of the decision variables describing the existence/absence of components and connections inside the model, which link together all time intervals. In this work, discrete time intervals of one hour have been considered.

The problem cannot be solved separately for each cogeneration unit installed at a specific building because each of them is connected with the district heating network through a node where income and outcome thermal energy flows can be potentially exchanged with any other node of the network (Fig. 1). Consequently, the heat demand faced by each unit is not defined “in advance”, and the optimal operation has to be defined jointly with the optimal synthesis of the district heating micro-grids and with the number and position of CHP engines.

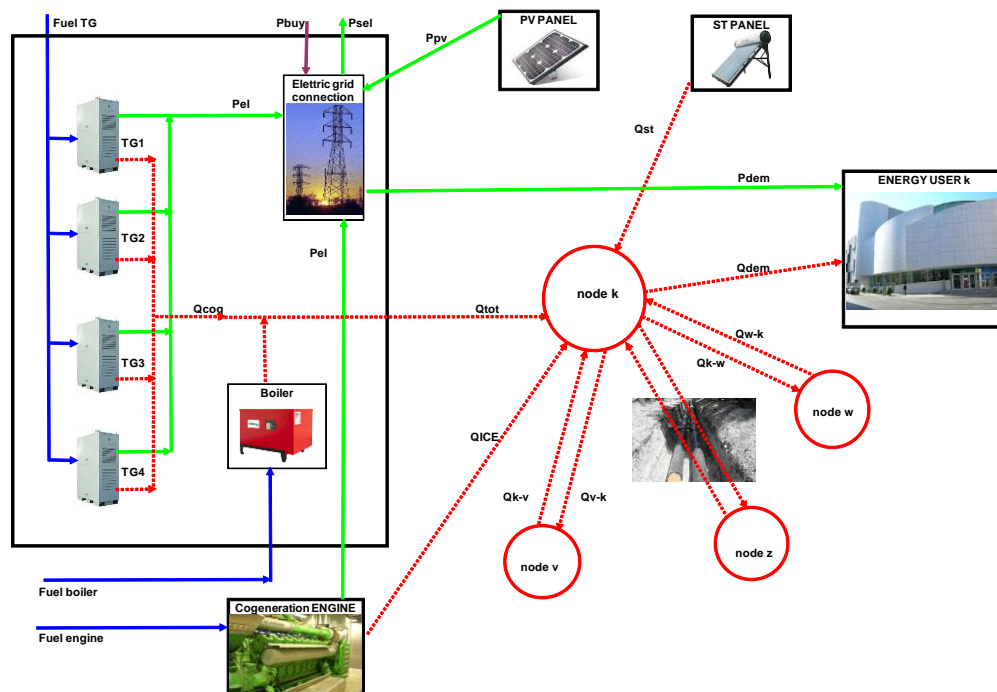


Figure 1. A cogeneration unit with its connections with the nodes of the district heating network.

In each time interval, the energy system is described by means of the amount of every exchanged energy flow and by two sets of binary optimization variables expressing the existence/not-existence of the components and their on/off operation. Other design binary variables and continuous operating variables can also be used to describe the district heating network to be optimized, without

violating the model linearity. In the following, the equations of the MILP model used in the presented optimization procedure are summarized.

The objective function is the Total Annual Cost for owning, maintaining and operating the whole system (Equation 1). The operating costs mainly consist in the sum of the sustained costs for the purchase of the external fuel energy flows, minus profits from the optional selling of electricity to another grid, for the whole year, while the owning costs are simply obtained by multiplying the total capital cost of each kind of component by the corresponding capital cost recovery factor, and the maintaining costs are regarded as proportional to the electric energy produced all the yearlong.

Variables $X(j,k)$ represent the existence/not-existence of CHP engine (TG or ICE) “j” inside building “k”, while variables $y(i,j,k) \leq X(j,k)$ represent the on/off operation of the same CHP engine at the time interval “i”.

Variables $r(k,v)$ express the existence/not-existence of the pipeline from node “v” to node “k” into the district heating network, while variables $D_{HN}(k,v)$ express the maximum nominal heat flow of the same pipeline and $Q(i,k,v)$ express the actual heat flow, sent from node “k” to node “v” through the district heating network, at the time interval “i” (Figure 1).

$$\text{cost}_{\text{TOT}} = \sum \text{Fuel}_{\text{CHP}}(i,j,k) * C_{\text{FuelCHP}}(i) + \sum [\text{Fuel}_{\text{boil}}(i,k) * C_{\text{Fuelboil}}(i) + P_{\text{buy}}(i,k) * C_{\text{BUY}}(i,k) - \text{P}_{\text{sel}}(i,k) * C_{\text{SEL}}(i)] + f_{\text{aCHP}} * \text{cost}_{\text{CHP}} + f_{\text{aHN}} * \text{cost}_{\text{HN}} + f_{\text{aPV}} * \text{cost}_{\text{PV}} + f_{\text{aST}} * \text{cost}_{\text{ST}} + \text{cost}_{\text{man}} \quad (1)$$

where:

$$\text{cost}_{\text{PV}} = \sum C_{\text{PV}} * A_{\text{PV}}(k) \quad (2)$$

is the total capital cost of PV panels

$$\text{cost}_{\text{ST}} = \sum C_{\text{ST}} * A_{\text{ST}}(k) \quad (3)$$

is the total capital cost of ST collectors

$$\text{cost}_{\text{CHP}} = \sum C_{\text{CHP}}(j,k) * X(j,k) \quad (4)$$

is the total capital cost of CHP components

$$\text{cost}_{\text{HN}} = \sum [D_{\text{HN}}(k,v) * E + r(k,v) * F] * l(k,v) \quad (5)$$

is the total capital cost of the district heating networks

$$\text{cost}_{\text{man}} = \sum C_{\text{man}} * P_{\text{el}}(i,j,k) \quad (6)$$

is the maintenance cost of the whole system.

The cost of each pipeline (branch) per unit length, can be considered as a linear function of the maximum nominal heat flow of the same pipeline [24], whilst the efficiency of the integration boilers can be regarded as a constant.

Note that the existence of TG, ICE and branches of the DHN are described by (binary) decision variables whilst the extensions of PV and ST panel surfaces (A_{PV} and A_{ST} , respectively) are continuous decision variables, but none of them depend on the specific time interval. On the contrary, the on/off operation of the same components and the thermal and electrical energy flows, exchanged inside the system, are also decision variables (binary and continuous, respectively) but they can change by switching from one time interval to the next one. A first set of constraints represents the performance maps of the components which have been linearized, with negligible approximation:

$$\text{Fuel}_{\text{CHP}}(i,j,k) = A(j,k) * P_{\text{el}}(i,j,k) + B(j,k) * y(i,j,k) \quad (7)$$

$$Q_{\text{cog}}(i,j,k) = M(j,k) * P_{\text{el}}(i,j,k) + N(j,k) * y(i,j,k) \quad (8)$$

$$P_{\text{min}}(j,k) * y(i,j,k) \leq P_{\text{el}}(i,j,k) \leq P_{\text{max}}(j,k) * y(i,j,k) \quad (9)$$

In this paper, the coefficients of the linearized performance maps of the components have been regarded as time dependent, because they are affected by temperature variations.

In addition, the maximum nominal heat flow and the heat flow direction of each pipeline has to be respected:

$$D_{HN}(k,v) \geq Q(i,k,v) \geq 0 \quad (10)$$

$$D_{HNmin}(k,v) \cdot r(k,v) \leq D_{HN}(k,v) \leq D_{HNmax}(k,v) \cdot r(k,v) \quad (11)$$

$$r(k,v) + r(v,k) \leq 1 \quad (12)$$

The thermal demand has to be satisfied by cogeneration equipment, auxiliary boilers and solar thermal integration. At the same time the electricity demand has to be satisfied by cogeneration equipment, PV production and by electricity external purchase:

$$Q_{int}(i,k) = Q_{dem}(i,k) - \sum Q_{cog}(i,j,k) + Q_{diss}(i,k) + \sum Q(i,k,v) - \sum Q(i,v,k) \cdot (1-d(v,k)) - Q_{ST}(i,k) \quad (13)$$

$$P_{sel}(i,k) = \sum P_{el}(i,j,k) - P_{dem}(i,k) + P_{buy}(i,k) + P_{PV}(i,k) \quad (14)$$

Thermal losses along the district heating network have been taken into account through constant factor ϕ , expressing the fraction of Q that is expected to be lost, per unit length:

$$d(v,k) = (\phi/100) \cdot l(v,k) \quad (15)$$

The energy efficiency of both solar thermal and photovoltaic panels can be regarded as linear vs. the temperature difference between the fluid collector average temperature and the outside ambient [26, 27]:

$$\eta_{ST} = -7.5 (t-t^\circ)/G + 0.7 \quad (16)$$

$$\eta_{PV} = -0.0009 (t^\circ - t) + 0.1987 \quad (17)$$

where t is the fluid collector average temperature, t° is the ambient temperature and G [W/m²] is the solar radiation. Available data for G and t° have to be introduced into the model from [24]. In this case study, an average energy efficiency of solar thermal panels equal to about 42% has been obtained. Eq. 17 is valid for South oriented panels, having an inclination equal to 30° with respect to the horizontal plane.

The CO₂ emissions as a result of the operation of the whole CHP and DHN can be calculated by introducing the Carbon Intensity (CI) of fuels and purchased/sold electricity to the grid. Then, the avoided CO₂ emissions can be easily calculated as the difference between the conventional and the CHP and DHN energy production, to supply the same users.

3. Case study

The optimization model has been applied to a distributed cogeneration system with district heating, taking as a reference for the supplying of thermal energy and electricity the consumptions of six public buildings in the centre of the city of Pordenone (Italy) [28] considering this as representative of generic commercial building systems [29].

The conventional power supply, for the six buildings considered, involves an annual cost of 796,064 €/ year, for the purchase of 2959 MWh of electrical energy and for the production of 4846 MWh of thermal energy by conventional boilers, fed with natural gas [30].

In Figure 2 it is shown the city center map with the location of the six buildings and a possible pipeline network of the district heating system. To reduce the overall number of variables, the whole year can be modeled by taking into account a small number of “typical days” for energy demand and rates. In the case study, 24 typical days have been considered (one working day and one public holiday, for each month). In this way the energy demand of the whole year is adequately approximated by repeating a proper number of times each typical day. This approach is widely accepted in literature (see, for instance, [13, 14, 31]). Recently, Pfenninger presented a systematic

analysis of the different techniques to reduce the computational effort for energy models resolution [32], including time slices and typical days or weeks identification. In [33] the approach of identifying a set of proper typical days is used in the optimal design of a multi-energy system with seasonal thermal storage, while in [34] an improved adaptive genetic algorithm is proposed to model the typical day load sequence for multi-objective optimization of a distributed generation system.

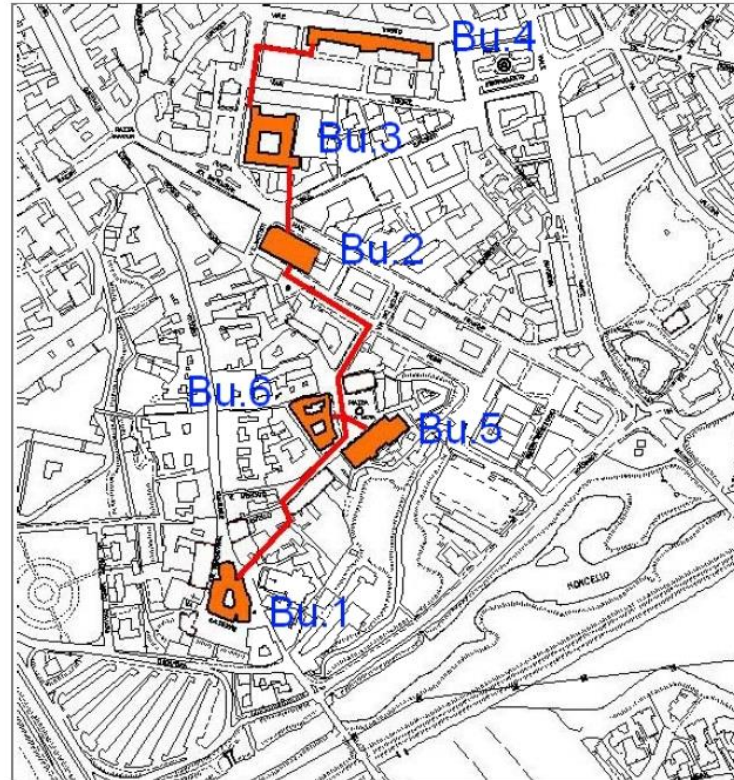


Figure 2. Plan of buildings and path of district heating network in the Pordenone city center: 1) Town Hall, 2) Theatre, 3) Library, 4) Primary school, 5) Retirement home, 6) Ex-monastery.

In Figures 3a and 3b, the energy demands of the 6 buildings are shown for a winter working day, as an example. In Figure 4 the total monthly energy demands are shown for all the year. Notice that the thermal demand shows strong seasonal variations, as it is common for civil buildings in the central European region.

In each building a local cogeneration unit may be installed, with a maximum number of microturbines equal to 4, jointly with an integration boiler; all buildings are also connected to the external electric grid. In addition, a 600 kWe cogeneration ICE may be located near the buildings (Figure 1). This size has been chosen to avoid the adoption of a too big ICE in an urban context, whilst the choice of its location is obtained from the optimization procedure. Only one ICE can be chosen in the optimal solution, to compare a fully distributed cogeneration system with a more concentrated one. Each cogeneration unit can produce electrical energy for both the grid and the building where it is placed, as well as thermal energy for both the district heating network and the building.

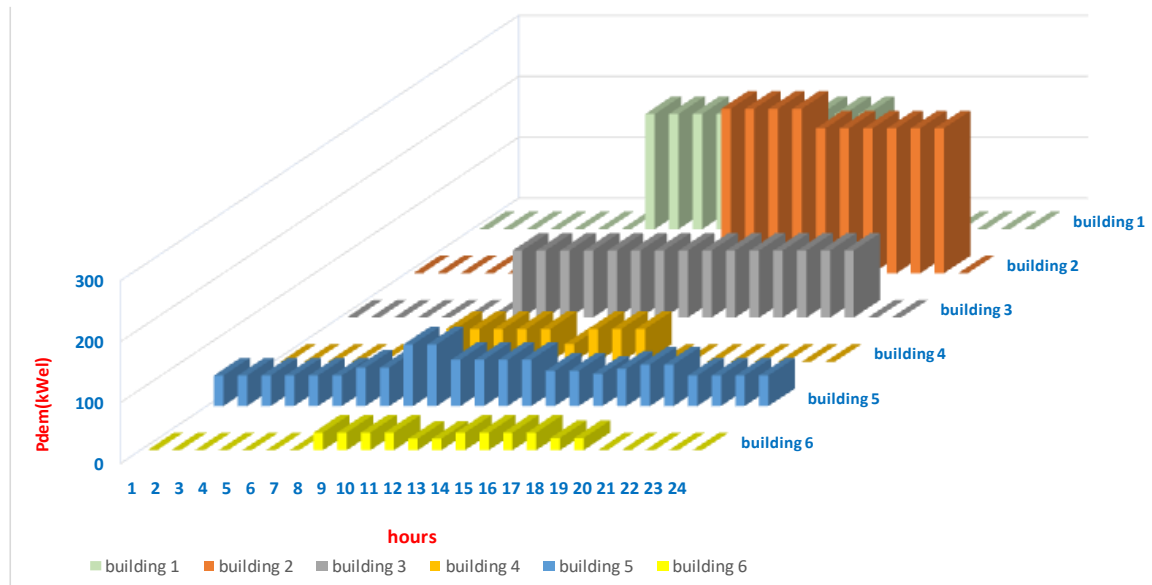


Figure 3a. Electrical energy demand (P_{dem}) for a typical January working day (24 hours), for the 6 buildings considered.

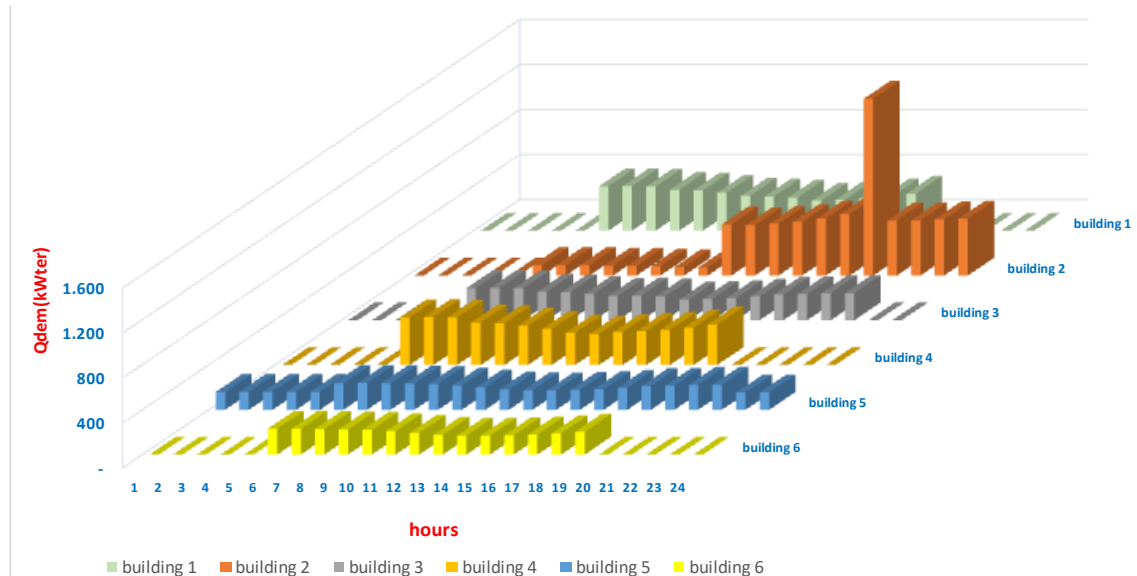


Figure 3b. Thermal energy demand (Q_{dem}) for a typical January working day (24 hours), for the 6 buildings considered.

To improve the thermal and electrical energy production, a set of thermal and photovoltaic panels can be installed on the buildings with a maximum area of 100 m² each, except on the buildings 2 (theater) and 4 (primary school), because of their architectural constraints.

Capstone C60 has been considered as the microturbine reference model, consistently with the modular approach adopted for each local cogeneration unit (see Fig. 1) and with the characteristic of this kind of components in term of noise and pollutant emissions, which allow easily their adoption in an urban context. Full and partial load performances have been evaluated on the basis of experimental data available in literature [35]. Linear approximations have been introduced to express natural gas consumption (Fuel [kW]) and cogenerated heat (Q_{cog} [kW]) vs. net electric power (P_{el} [kW]). Different electrical and thermal efficiencies of GT have been taken into account depending on the ambient temperature, varying with time inside each typical day considered.

A similar procedure has been followed to evaluate ICE performance [36], considering for the central unit a Jenbacher – GE JMS 312 GS-NL. In the ICE case, ambient temperature effect has been ignored, for reasons of simplicity. Nominal and partial load performances, at standard temperature

conditions, are summarized in Table 1. The linear approximations of engine performance curves, in terms of energy flows, have to be regarded as adequate [10, 37, 38], without the need of introducing multi-linear approximations. Natural gas is considered as the fuel of both integration boilers and cogeneration systems. A constant thermal efficiency equal to 90% has been introduced for integration boilers, as an average value.

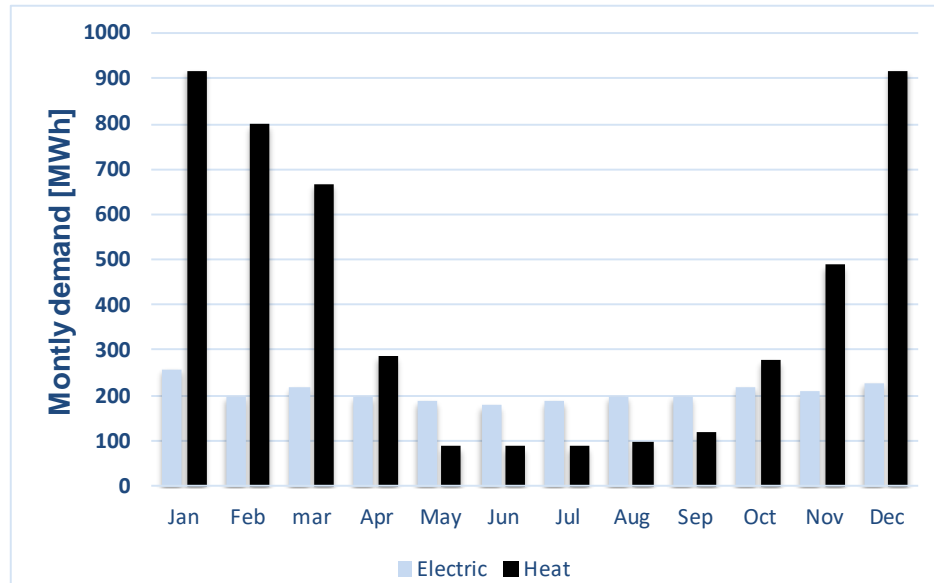


Figure 4. Annual distribution of energy demands for all the 6 buildings considered.

Table 1. Nominal and partial load performance of micro turbine and cogeneration ICE, at standard temperature.

P_{el} [kW]	η_{el} [%]	η_{th} [%]	Fuel [kW]	Q_{cog} [kW]
Microturbine Capstone C 60				
54.9	26.2	52.2	209.5	109.4
39.9	24.2	56.4	164.9	93.0
24.8	20.0	56.7	124.0	70.3
Jenbacher – GE JMS 312 GS-NLC				
601	38.9	47.4	1544	732
449	37.7	48.4	1191	576
310	37.0	49.9	838	418

A prudent value of $\delta = 10\%$ per km has been introduced for the constant value of losses per unit length, in the district heating pipelines.

The objective function of the optimization procedure is the total annual cost for owning, maintaining and operating the whole cogeneration system, as shown in Eq. 1. This total cost depends on the cost rates of gas and electricity (sold and/or purchased) for each considered time interval, on the capital cost of cogeneration equipment and on the fixed and variable costs for pipelines in the district heating network; the values used in the calculations are shown in Table 2 and refer to the present Italian market situation.

In particular, the PV panel cost includes auxiliary and grid connection components [10], while the ST panel cost includes piping for the CHP unit integration. Cost of the fuel for boilers and cogeneration engines is different because, adopting cogeneration engines, the taxation value applied changes from civil user to industrial self-producer. All capital costs are converted into a cost rate by

means of capital recovery factors (fa). Values equal to 0.15, 0.11 and 0.09 are used in the calculation for cogeneration engines, solar panels and district heating pipelines, respectively, to take into account the different expected life time for each kind of component (8 years for cogeneration engines, 12 years for solar panels and 16 years for pipelines).

In this case study, the total CO₂ emissions are associated with the carbon intensity (CI) of both natural gas and electricity, because they are the only input fuels at the system boundary. While the natural gas has similar CI all around the world, the electricity CI is widely variable, depending on the electricity mix of the network to which the system is connected and also on the boundary considered for the evaluation of indirect emissions [39]. In this work a value equal to 0.22 kg/kWh has been used for CI of natural gas [40, 41], while the greenhouse emissions of the electricity have been assumed equal to the specific emission factor of the main thermoelectric plant of the region where the users are located, which is a coal-fired power plant (0.79 kg/kWh) [42].

Table 2. Cost rate of electricity and capital cost of microturbines, cogeneration ICE, district heating pipelines and PV / ST panels (E and F refer to the coefficients used in Equation 5).

1 st - 4 th μ TG capital cost	65,000-100,000	[€]
ICE capital cost	500,000	[€]
PV capital cost	200	[€/m ²]
ST capital cost	580	[€/m ²]
Bought electric energy	0.160	[€/kWh]
Sold electric energy	0.026 -0.078	[€/kWh]
TG maintenance cost	0.010	[€/kWh]
ICE maintenance cost	0.020	[€/kWh]
Boiler fuel cost	0.56	[€/m ³]
TG and ICE fuel cost	0.37	[€/m ³]
Fixed cost of excavation (F)	270.63	[€/m]
Cost proportional to D _{HN} (E)	0.179	[€/kWm]

4. Two-level optimization strategy

The objective of this project is the optimization of a complex CHP and DHN system. The proposed model is intended for district-level implementation and is concerned with the optimal layout and operation of CHP units deployed in different buildings and with the optimal configuration of heating grids connecting multiple sites in the district. The implementation of a central CHP plant and micro-CHP gas turbines distributed among the involved buildings, along with the installation of thermal collectors and photovoltaic (PV) cells, have been considered to further improve the energy efficiency and sustainability of this system, as introduced in § 2.

The original single-objective formulation of the problem was aimed at minimizing the total annual cost of ownership, maintenance and operation of the described system. To reach this objective we sought the best system configuration. This required us to identify the optimal number of CHP units and their position and the heating grid layout to minimize energy loss. Furthermore, we had to determine the optimal number of thermal collectors and PV panels for each site to satisfy energy and heating demands of each building throughout the year. The optimal solution should have also considered the environmental pollution in terms of CO₂ emissions.

Complex energy systems of this kind can be optimized with different approaches known in literature [12]. A mixed integer linear programming approach (MILP) can be directly applied if the

number of binary decision variables is low enough, as shown by the authors in [24, 25, 43, 44]. Otherwise, the computational effort becomes unacceptable. For instance, the first optimization of the case study was performed with this approach by using the commercial software FICO® Xpress Optimization Suite [45] and a desktop computer with an Intel Core i7-4770 processor at 3.40 GHz, 16 Gb RAM and a solid-state disk. The computational time increased from a few seconds for only three buildings to 26 minutes for six buildings. This meant that the problem complexity caused by the number of the independent variables was too great to obtain a solution covering an entire town district instead of a limited number of buildings. In other words, this approach is not feasible for large scale instances. To solve problems of this kind, different approaches based on problem decomposition can be found in literature [12, 16-18]. For instance, a physical decomposition could be considered, by dividing the whole system into the heating network and the different thermal energy suppliers, but this approach is advisable if the binary variables affect only one of the sub-systems obtained by the decomposition [21].

In this case study, there are many binary variables in all sub-systems, not in only one of them, therefore a mere physically based decomposition of the problem cannot be usefully applied. To overcome this difficulty, in this study the problem has been modeled as a hierarchical problem which involves two levels: an outer and an inner level.

The outer level is concerned with the general configuration of the CHP system in terms of the number of branches of the heating grid (i.e. pipeline connections between buildings), the position of the central CHP plant, the location and the number of micro-CHP plants. The scheduling of the CHP units throughout the year, as well as the surface of thermal collectors and PV cells, are inner level variables instead. The objective of the inner level is to find the optimal operation which satisfies the constraints expressed by thermal and power demands of each final user and minimizes the operational costs of the whole system.

The problem has been formulated as a two-level problem with the commercial optimization software modeFRONTIER® [46], integrated with FICO® Xpress Optimization Suite. The outer level configuration has been optimized with a genetic algorithm, whereas the inner level has been solved with the Xpress exact solver.

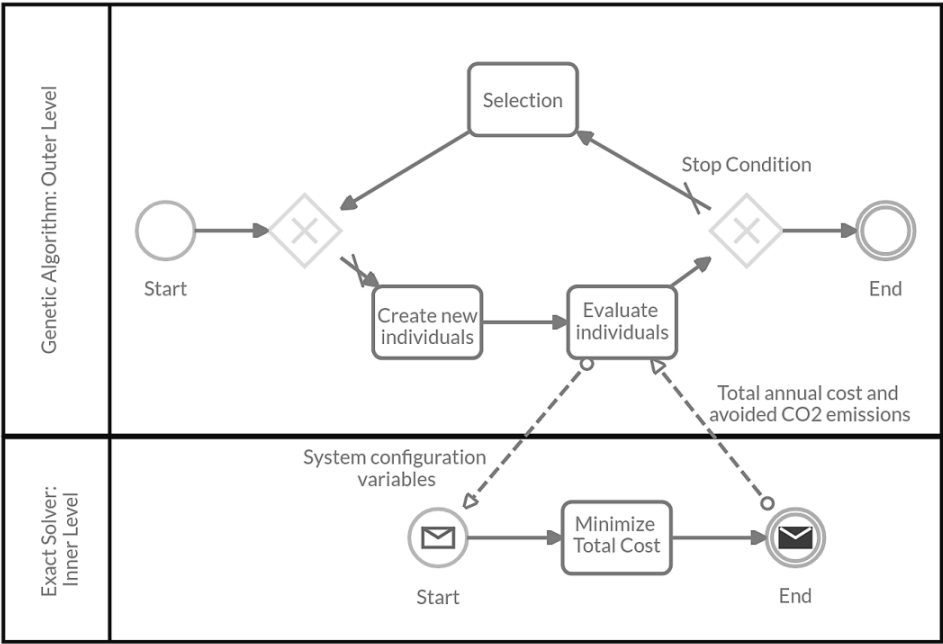


Figure 5. Interaction of the Outer and Inner levels in the Bi-level optimization algorithm.

As shown in Figure 5, a simple iteration loop has been defined. During its optimization loop the genetic algorithm assigns the values to the system configuration variables defining the current generation of individuals (i.e. variables $X(j,k)$ and $r(k,v)$ introduced in § 2). The problem has been set

with 40 individuals per generation and 25 generations. The individual evaluation phase is made on the basis of the results of exact solver at the inner level. The latter receives the configuration variables of each individual and, for each of them, it performs the operation optimization using the total annual cost ($Cost_{TOT}$, Equation 1) as objective function. The optimal solution contains not only the minimum total annual cost allowed by the configuration variables introduced for each individual, but also the equivalent CO_2 emissions and therefore the avoided emissions, with respect to the conventional solution for energy supply. The optimized variable assignment in the inner level is sent back to the outer level to allow the genetic algorithm to determine whether a solution is suitable for guiding the creation of the next generation of solutions, as well as the quantitative indexes of each solution (these indexes are then summarized in the Scatter Matrix and in the Probability Density Function charts, presented in the following § 5). The entire loop is repeated until the termination criterion is reached, i.e. when a further evolution of the population does not obtain any appreciable performance improvement, indicated as Stop Condition in Figure 5. It is worth noting that more than one objective function can be used to evaluate the individual performance, allowing to highlight different convergence stories and to identify the Pareto front. In this case study one second objective function (besides the total annual cost) have been considered: the avoided CO_2 emissions during the year (to be maximized), in order of measuring the environmental impact of the modeled system.

By applying this two-level approach to the case study, i.e. the optimization of the CHP system with district heating for 6 buildings, the computational times for each solution provided to the inner level were reduced to a mere 3 seconds compared to the previous 26 minutes required by the direct MILP approach. This means that we could perform 520 design evaluations in the same time without using any parallel computing functionalities of the workstation.

The modeFRONTIER® software enabled us not only to keep the original MILP model used in the direct approach, but also to integrate it in a hierarchical optimization workflow. After an exploration of different optimization algorithms, we decided to use the genetic algorithm NSGA-II, widely discussed in literature [47]. We considered it the most suitable approach for tackling the outer level of this problem in terms of result accuracy and convergence rate. Furthermore, this approach enabled us to use the multi-core processor of the computer and thus perform in parallel multiple inner level runs, which significantly sped up the optimization process. Repeated optimization test runs resulted in the optimal problem solution in less than 15 minutes with an accurate exploration of the design space.

Given these results, a sub-set of the inner level parameters was transferred to the outer level, i.e. the surfaces of thermal collectors ($A_{ST}(k)$) and PV panels ($A_{PV}(k)$). In this way the computations at the inner level were further streamlined without this having a negative impact on the outer level, and all design variables have been put in the outer decision level, allowing the genetic algorithm to manage directly the surfaces of thermal collectors and PV panels, in view of both objective functions.

It is worth noting that an easy implementation of the multi-objective approach has been possible because the choice of the objective as the merit function of the genetic algorithm affects only the decision variables of the outer level, not the inner level.

The presence of two objectives in the outer level and only one of those objectives, i.e. cost minimization, at the inner level, may throw the search off balance in favor of this objective. In spite of this apparent drawback, the NSGA-II algorithm is able to maintain the uniformity of the Pareto front. However, we can expect a different quality of exploration between the two tails of the front corresponding to the best values of each of the objectives. The tail of the avoided CO_2 emissions objective will be less explored, but this is not an issue because the most expensive solutions lead to a rather small additional environmental benefit in terms of CO_2 emissions and has thus poor industrial appeal.

5. Results

Figures 6 and 7 show the convergence history of the hierarchical optimization of both objectives, i.e. avoided CO_2 emissions and total annual cost. In particular, Figure 6 shows that the maximum CO_2 savings of 3314 t/year has been obtained at iteration number 964 (Design ID), but this solution implies

an unacceptable annual cost of 30,383,000 €/year. At this point we performed result post processing to exclude unfeasible solutions from a practical point of view. This consisted in limiting the maximum annual cost to 1,000,000 €/year. With this constraint the new optimal design has been obtained at iteration number 905 (Design ID) with 3241 t/year CO₂ saving.

Figure 7 shows that the minimum annual cost of 742,705 €/year has been obtained at iteration number 714 (Design ID). However, the genetic algorithm had already found a value very similar to this after only about 150 iterations.

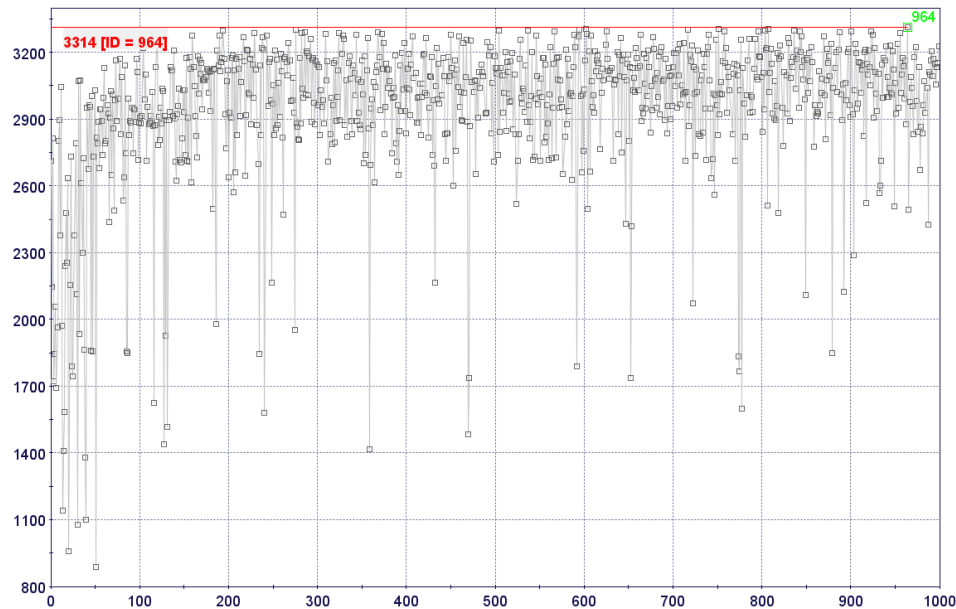


Figure 6. History of the convergence process for the objective of the avoided CO₂ emissions.

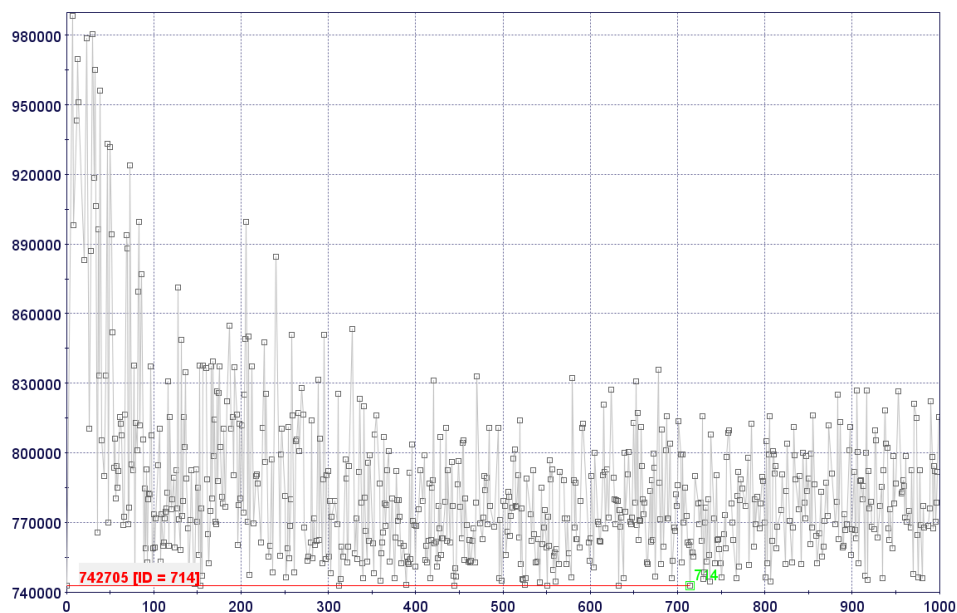


Figure 7. of the convergence process for the objective of the Total annual cost.

The two optimal solutions (ID 714 and 905) are shown in Table 3. The cheapest solution (ID 714) includes 4 micro-gas turbines and the ICE CHP installed near building number 2, three pipeline connections and the maximum allowed area of PV panels. The contribution of the solar thermal collectors in this case is negligible. The monetary saving amounts to about 53,000 €/year compared to the reference solution.

Table 3. Main results for the optimal total annual cost and for the optimal avoided CO₂ emissions.

Design ID	0 - Reference conventional energy supply	714	905	419
Total number of TG	0	4	11	9
Position of ICE at building	-	2	2	2
Total number of pipelines in the DHN	0	3	5	4
Total amount of PV panels [m ²]	0	600	600	594
Total amount of ST collectors [m ²]	0	2	4	10
Total cost [€/year]	796,064	742,705	826,940	788,265
Total cost reduction [€/year]	0	53,359	-30,876	7,799
Avoided CO ₂ emissions [t/year]	0	2714	3241	3186

One of the main advantages of multi-objective optimization methods is the generation of many feasible trade-off solutions, so the designer can easily identify the best compromise. Approximately 1000 evaluations with NSGA-II have been performed in 8 minutes and a set of Pareto solutions representing equally valid CHP system configuration alternatives have been identified.

The final Pareto front obtained for the case study is shown on the Scatter Chart in Figure 8. The Cost objective (to be minimized) is plotted on the x axis whereas the avoided CO₂ emissions (to be maximized) are plotted on the y axis. The Pareto solutions, displayed as green circles, are well distributed in the design space. The reference solution is represented as a red dot at the bottom of the chart with cost value of 796,064 €/year. However, for the sake of clarity of the comparison it was placed on the x axis even though the CO₂ saving is actually 0 t/year. The solution with ID 905 brings about a CO₂ saving of approximately 3241 t/year with a cost of 826,940 €/year, which is only 30,876 €/year more than the reference solution. For this reason this solution is regarded as the most environmentally friendly (see Table 3). This optimal solution includes the ICE and the maximum number of micro-gas turbine (11) and pipelines (5) among all solutions of the Pareto front.

The Scatter Matrix chart available in modeFRONTIER® (Figure 9) deals in detail with the solutions on the Pareto front and helps us understand the behavior of outer level variables, how they influence each other and how their values are distributed. The chart uses the Pearson coefficient for correlations and the Probability Density Function for variable distribution [48]. All input variables of the outer level and the two objectives are plotted on both axes: each colored square shows the strength and the type of correlation (positive or negative) between a variable pair (one plotted on the x axis and the other on the y axis).

The two objectives (total annual cost and avoided CO₂ emissions) are strongly positively correlated, as expected, but even more so with the number of micro-CHP units. It is perfectly plausible that the more the CHP components in the plant to be purchased and maintained, the higher the cost, but on the other hand this helps to reduce the CO₂ emissions. These three variables (total cost in particular) are also highly positively correlated with the number of branches (pipelines) of the DHN, but with a lower value of the Pearson coefficient.

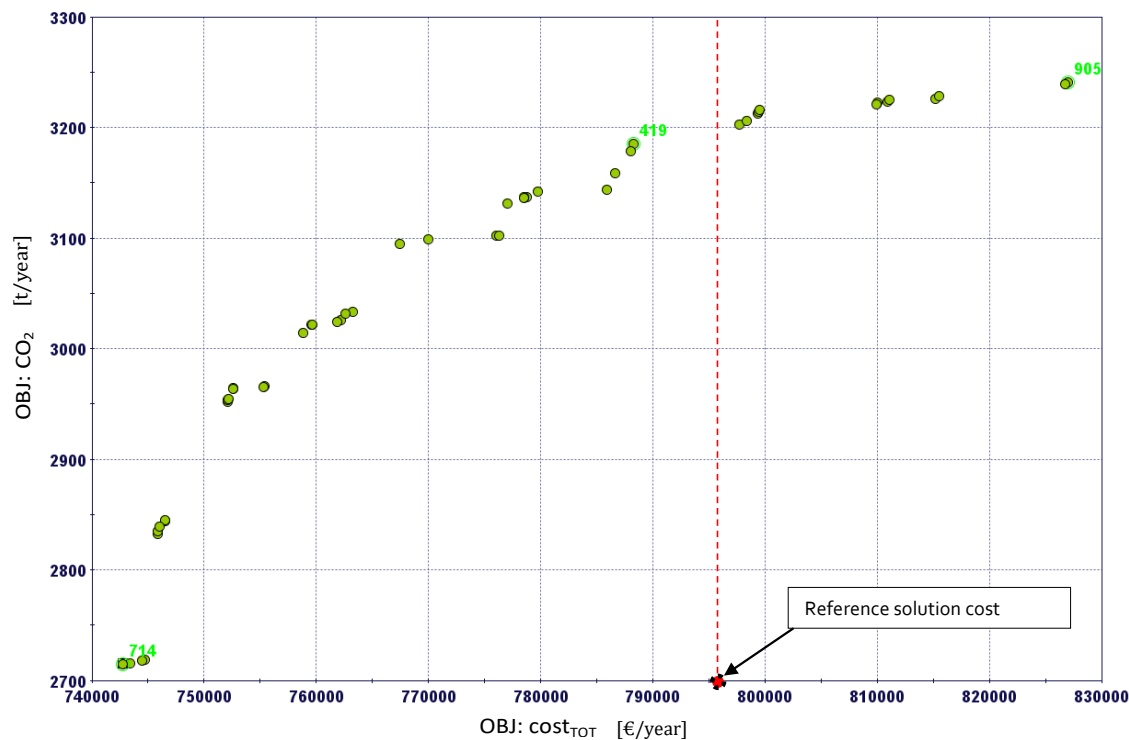


Figure 8. Pareto front of the multi-objective optimization.

A moderate inverse correlation can be observed between the thermal collector surface (A_{st}) and all the above mentioned variables. In fact, the more the branches and CHP units in the plant, the less the usefulness of the thermal collectors to satisfy the energy demand of the buildings. On the other hand, the use of solar energy implies a reduction of CHP units and therefore a lower total cost, but also less avoided CO₂ emissions because additional power has to be purchased from the grid.

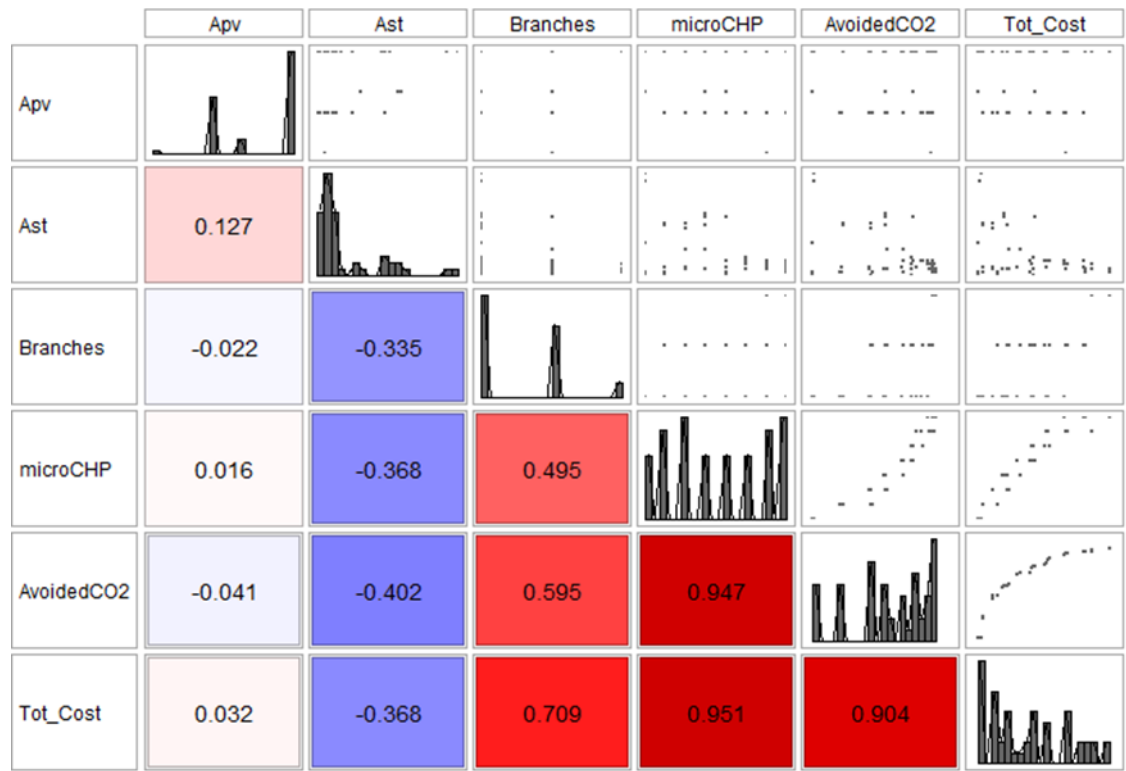


Figure 9. Scatter Matrix chart of the variables in the outer level.

The Probability Density Function charts (Figure 10) reveal that the number of branches is in most cases limited to two mid values, i.e. 3 and 4. In no case has an optimal solution been found for the minimum (i.e. 0) and the maximum (i.e. 8) number of branches.

A significant variability can be observed in the total surface of thermal collectors A_{ST} (between 0 and 70 m²), although the majority of solutions have the lowest values. Few solar thermal collectors are installed in all optimal solutions because of the high investment costs.

On the contrary, the PV panel range of values is quite restricted: between 590 and 600 m², with more than half optimal configurations having the highest value, because of the strong reduction of costs occurred in recent years for this kind of components.

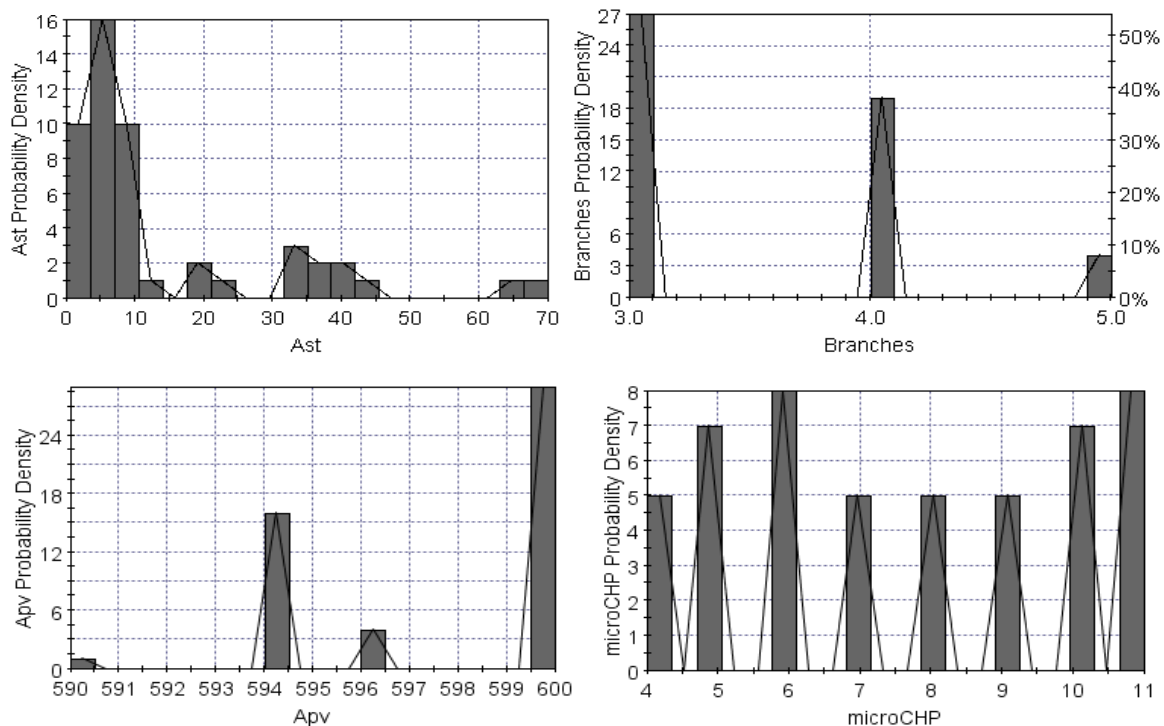


Figure 10. Probability Density Function charts for the outer level variables.

The PV panel range of values is quite restricted, i.e. between 590 and 600 m², with more than half optimal configurations with the highest value because of low investment costs.

Finally, we can consider the number of micro-CHP units as the most relevant outer level variable due to their rather uniform distribution on the Pareto front, as shown in Figure 10. From the Pareto front (Fig. 8) it can be noted that the solution allowing the maximum CO₂ saving and, at the same time, a reduction of the total cost compared to the reference solution, is ID 419. The main results for this compromise solution are shown in Table 3.

Once one solution has been identified in the Pareto front, the output of the optimization model contains complete information about the optimal structure and operation of the energy system. As an example, Fig. 11 shows the electricity, heat and pipelines optimal hourly schedules in 4 typical working days, for the compromise optimal solution ID 419.

Notice that the electrical and thermal energy values have been aggregated at global system level, even if the solution contains the values of all energy flows exchanged by each building and produced by each cogeneration unit. In Fig. 12 the detailed hourly schedules of heat flows through the pipelines and electric energy exchanged with the grid is shown for a typical January working day.

By analyzing the electric energy balance in Fig. 11, it can be noted that the whole system produces an excess of energy compared to the electric demand, especially during the winter time; nevertheless, some buildings need, at the same time, to buy electric energy from the grid. Fig. 12 shows that this happens in buildings 1 and 6 (during the typical January working day).

Looking at the heat balances, it can be noted that the cogeneration units satisfy almost the whole heat demand; in summer time the ICE is operated at partial load for about 10 hours per day and the excess heat is dissipated. The optimal solutions also contain the position of the mGTs and of the pipelines, so that the path of the micro district heating grids can be easily inferred. In particular, for the solution considered, there is only one micro district heating grid and one isolated building (Fig. 12). The purpose of the grid is to distribute the heat produced by the ICE in building 2 also to buildings 3, 4 and 6, so that a grid bifurcation is required in site 3. Building 6 is connected to the micro district heating grid, so that it can take advantage of the cogenerated heat even if there are no cogeneration units inside it.

The micro district heating grid is operated all the time, except in the summer time. This detailed information can be obtained for each identified solution and for each typical day, providing a basis for knowledge for the design of the complex energy system, taking into account in advance the peculiarities of its optimal management.

6. Conclusions

The design and operation optimization of integrated multi-component energy systems generally require a binary variable set to be introduced to describe the existence/absence and the on/off operation status of components and energy connections inside the model. Besides these, other continuous variables have to be introduced for modelling the energy and material flows exchanged among components, as well as other possible design options. In these kinds of optimization problems the decomposition approach, often suggested in literature [13, 17, 18], may be not best suited, because the discontinuous nature of variables present in many sub-problems can prevent the convergence of the whole problem.

In the case study there are many binary variables in all sub-systems. It is a distributed cogeneration and district heating system, including a set of micro-cogeneration gas turbines (to be located at the energy user sites), a centralized cogeneration system, photovoltaic panels, solar thermal collectors and various district heating pipelines, potentially connecting the users. The existence of each one of these components is related to a binary variable in the optimization problem.

In this paper an innovative approach is presented that allows to exploit the essential positive characteristics of decomposition, overcoming its difficulties by using a bi-level optimization strategy, which involves an outer and an inner level. The outer level configuration was optimized with a genetic algorithm of the commercial optimization software modeFRONTIER®, whereas the inner level was solved with FICO® Xpress Optimization Suite. The outer is concerned with all the structural variables of the whole system, including the distribution of the micro CHP units, at the energy user sites, the district heating pipelines of the network and the surface of thermal collectors and PV panels, leaving at the inner level only the MILP problem of the optimal operation of the whole system. In this approach, a multi objective optimization can be easily performed, by introducing a second objective in the outer level only, and the Pareto front can be obtained. The avoided CO₂ emissions have been introduced as a second, environmental objective, besides the minimum annual cost.

Anyhow, the solutions obtained confirm that CHP systems, optimized for the minimum annual cost, can be favorable from both the economic and environmental standpoints. In the case study, the minimum cost solution allows a monetary saving of about 53,000 €/year and a CO₂ saving of about 2700 t/year. A possible environmental-friendly alternative on the Pareto front allows a maximum CO₂ saving of about 3240 t/year, with an additional cost of only 31,000 €/year, compared to the conventional solution.

The presented optimization strategy highlights an important reduction in the computing time compared to the direct implementation of the whole problem in a single level MILP solver; therefore, the expectation is that it could be applied also to more complex systems, in particular to distributed cogeneration systems with far more users and pipelines in the district heating.

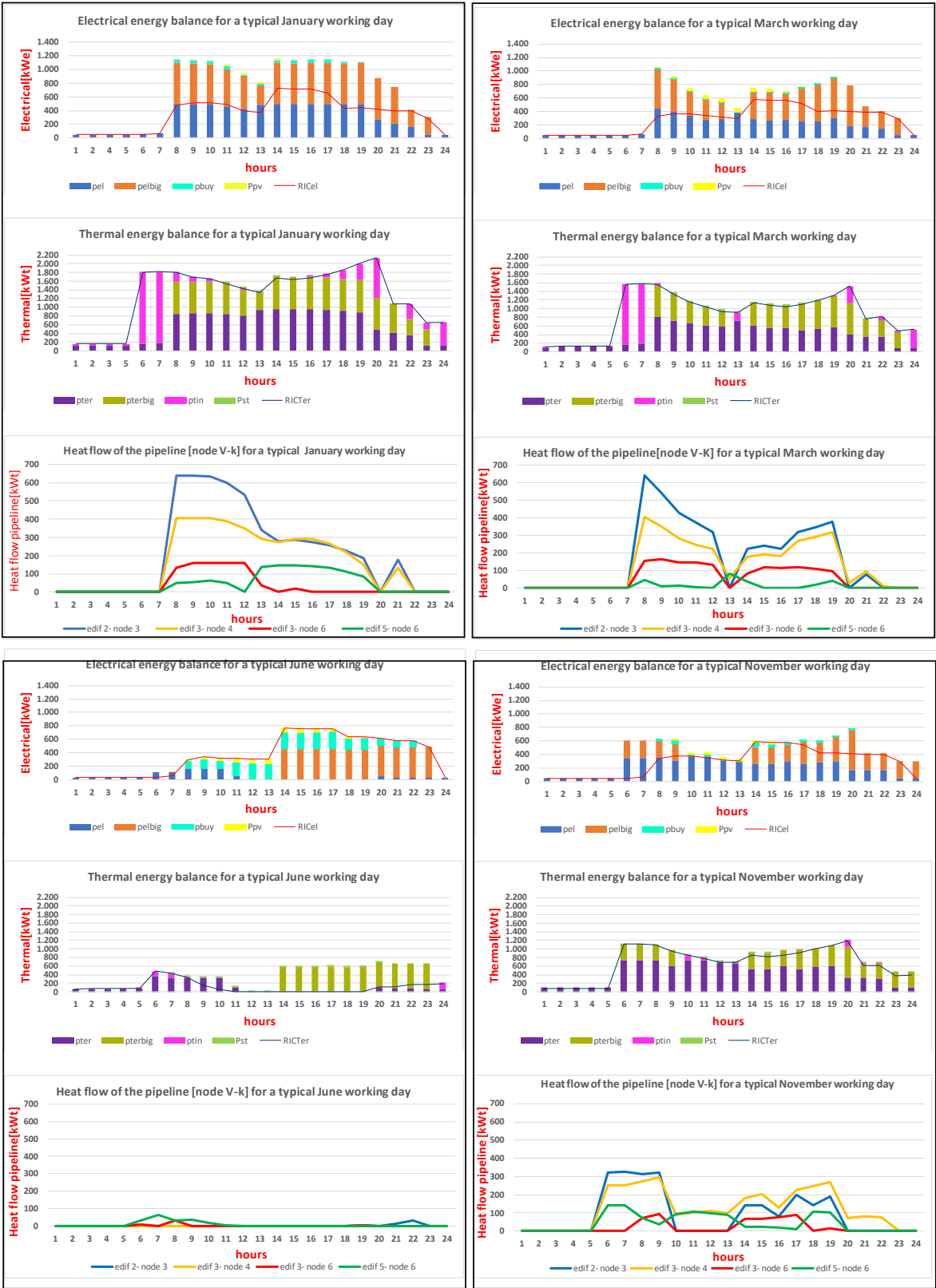


Figure 11. Global electricity, heat and pipelines hourly schedules in 4 typical working days, for the compromise optimal solution ID 419.

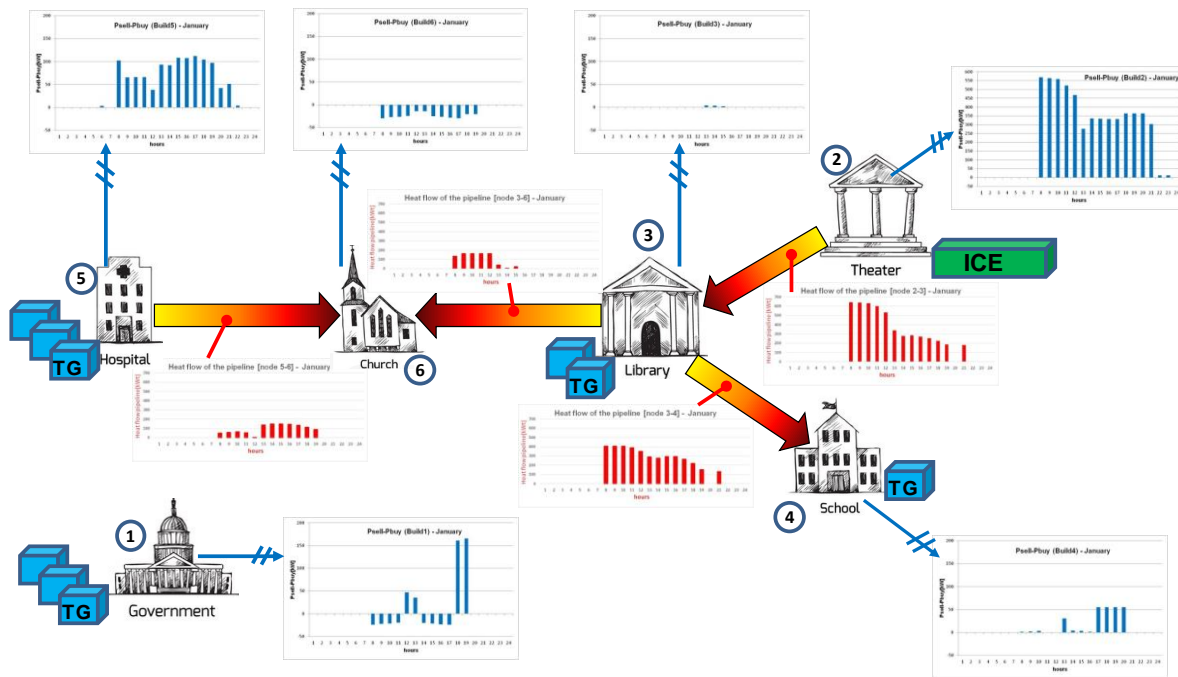


Figure 12. Detailed hourly schedules of heat flows in the pipelines and electric energy exchanged with the grid, in a typical January working day, for the compromise optimal solution ID 419.

From the data analysis, it can be observed that the evolutionary strategy, implemented in the outer optimization level, allows us to obtain a value very close to the actual optimum after a limited number of iterations. The two objectives are strongly positively correlated and they are mostly influenced (even though to different extents) mainly by the number of micro CHPs, and also by the number of pipelines in the district heating network. This fact highlights how the dislocation of the CHP units is the most critical choice, in order to really obtain the economic and environmental advantages which are expected by the cogeneration technology.

In addition, detailed information can be obtained for each identified solution and for each typical day, providing a knowledge basis for the design of the complex energy system, taking into account in advance the peculiarities of its optimal management.

In summary, the proposed method allows the simultaneous optimization of the distributed cogeneration system and the configuration of micro-district heating networks with multiple users, with an innovative approach, applicable to complex systems, allowing a significant reduction of computing time thanks to the proposed two-level optimization procedure.

Nomenclature

A, \dots, L	generic coefficients of linear approximation [consistent dim.];
A_{PV}	PV panel surface [m ²];
A_{ST}	ST panel surface [m ²];
$cost_{CHP}$	capital cost of CHP system [€];
$cost_{HN}$	total capital cost of district heating network [€];
$cost_{man}$	maintenance cost [€/year];
$cost_{PV}$	total capital cost of PV panels [€];
$cost_{ST}$	total capital cost of ST panels [€];
$cost_{TOT}$	owning, maintaining and operating total costs [€/year];
C	specific cost [€/kW];

CI	carbon intensity [kg/kWh];
$d(v,k)$	thermal losses fraction along the district heating pipeline from node v to node k;
D_{HN}	nominal heat flow of a district heating pipeline [kW];
E	cost coefficient of the DHN proportional to D_{HN} [€/Kw m];
fa	capital cost recovery factor [year ⁻¹];
F	fixed cost coefficient of the DHN [€/m];
Fuel _{boil}	fuel for integration boiler [kW];
Fuel _{CHP}	fuel for CHP system [kW];
G	solar radiation [W/m ²];
$l(v,k)$	length of the pipeline district heating from node v to k [m];
P	power
P _{buy}	purchased electrical energy [kW];
P _{dem}	electrical energy demand [kW];
P _{el}	cogenerated electrical energy [kW];
P _{sel}	sold electrical energy by CHP system [kW];
Q	generic heat flow inside the district heating network [kW];
Q _{ST}	heat flow produced by solar thermal panels [kW];
Q _{cog}	cogenerated thermal energy [kW];
Q _{dem}	thermal energy demand [kW];
Q _{diss}	dissipated thermal energy [kW];
Q _{int}	thermal integration [kW];
t	fluid collector average temperature [°C];
t°	ambient temperature [°C];
X, y, r	generic binary variables;

Acronyms

CHP	Combined Heat and Power;
CHCP	Combined Heat, Cooling and Power;
DHN	District Heating Network;
HN	Heating Network;
ICE	Internal Combustion Engine;
MILE	Mixed Integer Linear Exergoeconomic;
MINLP	Mixed Integer Non-Linear Programming;
MILP	Mixed Integer Linear Programming;
OBJ	Objective function;
PV	Photovoltaic;
ST	Solar thermal;
TG	Gas Turbine;

Greek symbols

δ	percentage thermal losses along district heating pipeline per unit length [km ⁻¹];
η	efficiency;

Subscripts and superscripts

el	electric;
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th	thermal;
i	generic time interval;
j	generic CHP system;
k	generic building or node;
v, w, z	generic node of the district heating network;

References

1. H. Lund, B. Moller, B.V. Mathiesen, A. Dyrelund, The role of district heating in future renewable energy systems, *Energy* **2010**, 35, 1381–1390.
2. S. Kelly, M. Pollitt, An assessment of the present and future opportunities for combined heat and power with district heating (CHP-DH) in the United Kingdom, *Energy Policy* **2010**, 38, 6936–45.
3. B. Rezaie, M.A. Rosen, District heating and cooling: review of technology and Potential enhancements, *Applied Energy* **2012**, 93, 2–10.
4. A. Lake, B. Rezaie, S. Beyerlein, Review of district heating and cooling systems for a sustainable future, *Renewable and Sustainable Energy Reviews* **2017**, 67, 417–425.
5. J. A. Fonseca, T. Nguyen, A. Schlueter, F. Marechal, City Energy Analyst (CEA): Integrated framework for analysis and optimization of building energy systems in neighborhoods and city districts, *Energy and Buildings* **2016**, 113, 202–226.
6. M.A. Lozano, J.C. Ramos, M. Carvalho M, L. Serra, Structure optimization of energy supply systems in tertiary sector buildings, *Energy and Buildings* **2009**, 41, 1063–1065.
7. H. Wang, W. Yin, E. Abdollahi, R. Lahdelma, W. Jiao, Modelling and optimization of CHP based district heating system with renewable energy production and energy storage, *Applied Energy* **2015**, 159, 401–421.
8. A. Bisch, L. Taccari, E. Martelli, E. Amaldi, G. Manzolini, P. Silva, S. Campanari, E. Macchi, A detailed MILP optimization model for combined cooling, heat and power system operation planning, *Energy* **2014**, 74, 12–26.
9. A. Reverberi, A. Del Borghi, V. Dovì, Optimal design of cogeneration systems in industrial plants combined with district heating/cooling and underground thermal energy storage, *Energies*, **2011**, 4, 2151–2165.
10. M.A. Lozano, Planteamiento optimo de sistemas de cogeneración (in Spanish). Proceedings of the 2nd Congreso Iberoamericano de Ingeniería Mecánica, Belo Horizonte (Brazil), december 12–15 1995.
11. D. Buoro, M. Casisi, P. Pinamonti, M. Reini, Optimization of distributed trigeneration system integrated with district heating and cooling micro-grids, *Distributed generation and alternative energy journal* **2011**, 26, 7–33.
12. C.A. Frangopoulos, M. R. von Spakovsky, E. Sciubba, A Brief Review of Methods for the Design and Synthesis Optimization of Energy Systems, *International Journal of Applied Thermodynamics* **2002**, 5, 151–160.
13. L.F. Fuentes-Cortès, A. Flores-Tlacuahuac, Integration of distributed generation technologies on suitable buildings, *Applied Energy* **2018**, 224, 582–601.
14. X. Zheng, G. Wu, Y. Qiu, X. Zhan, N. Shah, N. Li, Y. Zhao, A MINLP multi-objective optimization model for operational planning of a case study CCHP system in urban China, *Applied Energy* **2018**, 210, 1126–1140.
15. J.F. Marquanta, R. Evinsa, L.A. Bollinger, J. Carmelieth, A holarchic approach for multi-scale distributed energy system optimization, *Applied Energy* **2017**, 208, 935–953.
16. J.R. Muñoz, M.R. von Spakovsky, A Decomposition Approach for the Large Scale Synthesis/Design Optimization of Highly Coupled, Highly Dynamic Energy Systems, *International Journal of Applied Thermodynamics* **4** (2001) 19–33.
17. J.R. Muñoz, M.R. von Spakovsky, The Application of Decomposition to the Large Scale Synthesis/Design Optimization of Aircraft Energy Systems, *International Journal of Applied Thermodynamics* **2001**, 4, 61–76.
18. B. Oyarzabal, M.R. von Spakovsky, W. Ellis, Optimal Synthesis/Design of a PEM Fuel Cell Cogeneration System for Multi-Unit Residential Applications—Application of a Decomposition Strategy, *Journal of Energy Resources Technology* **2004**, 126, 30–39.
19. C. A. Frangopoulos, Thermoeconomic Functional Analysis and Optimization, *Energy* **1987**, 7, 563–571.
20. M.R. von Spakovsky, R.B. Evans, *The Optimal Design and Performance of Thermal System and their Components, In Analysis and Design of Advanced Energy System Fundamentals*, A.E.S. vol.3-1, A.S.M.E. ed. N.Y (USA), 1987, pp. 1–18.

21. M. Reini, D. Buoro, Mixed Integer Linearized Exergoeconomic (MILE) method for energy system synthesis and optimization, Proceedings of the 23th International Conference on Efficiency, Cost, Optimization, Simulation and Environmental Impact of Energy Systems - ECOS 2010, , Lausanne (CH), June 14-17 2010.
22. K. Ito, S. Akagi, An optimal planning method for a marine heat and power generation plant by considering its operational problem, *International Journal of Energy Research* **1986**, 10, 75-85.
23. R. Yokoyama, K. Ito, K. Kamimura, F. Miyasaja, Development of a General purpose optimal operational planning system for energy supply plants, *Journal of Energy Resources Technology* **1994**, 116 290-296.
24. M. Casisi, P. Pinamonti, M. Reini, Optimal lay-out and operation of CHP distributed generation systems, *Energy* **2009**, 34, 2175-2183.
25. M. Casisi, A. De Nardi, P. Pinamonti, M. Reini, Effect of different economic support policies on the optimal synthesis and operation of a distributed energy supply system with renewable energy sources for an industrial area, *Energy Conversion and Management* **2015**, 95, 131-139.
26. B.Y.H. Liu, R.C. Jordan, The long-term average performance of flat-plate solar energy collectors, *Solar Energy* **1963**, 7, 53-74.
27. IFA-CNR, Climate data of the Italian Energy Finalized Project (Progetto Finalizzato Energetica), 1979 (in Italian).
28. G. Di Prampero, Technical-economic comparison between distributed generation and DH for a cogeneration urban system, Bachelor Thesis, University of Trieste, Italy, 2005 (in Italian).
29. M. Medrano, J. Brouwer, V. McDonell, J. Mauzey, S. Samuelsen, Integration of distributed generation systems into generic types of commercial buildings in California, *Energy and Buildings* **2008**, 40 537-548.
30. M. Casisi, L. Castelli, P. Pinamonti, M. Reini, Effect of different economic support policies on the optimal definition and operation of a CHP and RES distributed generation systems, Proceedings of the ASME TURBO EXPO 2008, Berlin (D), June 9-13 2008.
31. M. Ameri, Z. Besharati, Optimal design and operation of district heating and cooling networks with CCHP systems in a residential complex, *Energy and Buildings* **2016**, 110, 135-148.
32. S. Pfenninger, Dealing with multiple decades of hourly wind and PV time series in energy models: A comparison of methods to reduce time resolution and the planning implications of inter-annual variability, *Applied Energy* **2015**, 152, 83-93.
33. P. Gabrielli, M. Gazzani, E. Martelli, M. Mazzotti, Optimal design of multi-energy systems with seasonal storage, *Applied Energy* **2018**, 219, 408-424.
34. Y. Gao, J. Liu, J. Yang, H. Liang, J. Zhang, Multi-objective of multi-type distributed generation considering timing characteristics and environmental benefits, *Energies* **2014**, 7, 6242-6257.
35. Greenhouse Gas Technology Center – Southern Research Institute, Environmental Technology Verification Report - Combined Heat and Power at a Commercial Supermarket - Capstone 60 kW Microturbine CHP System, Report SRI/USEPA-GHG-VR-27, Sept. 2003.
36. Jenbacher , GE Technical description of cogeneration plant, JMS 312 GS-NLC.
37. S. Consonni, G. Lozza, E. Macchi, Optimization of a cogeneration systems operation Part A: Prime movers modelization, Proceedings of ASME Cogen-Turbo '89, Nice (F), august 30 – September 1 1989
38. M. Reini, R. Taccani, A. Giadrossi, Optimal Operation of a Diesel Engine Cogeneration System Including Thermal and Mechanical Energy Storage, Proc. of ECOS 2001, A. Ozturk and Y. A. Gogus eds., Istanbul (Turkey), July 4-6 2001.
39. L. Ji et al., Greenhouse gas emission factors of purchased electricity from interconnected grids, *Applied Energy* **2016**, 184, 751-758.
40. Eurostat, Environment, transport and energy indicators, ISSN-1725-4566; Eurostat Pocketbooks 2009, <http://epp.eurostat.ec.europa.eu/>.
41. IPCC Guidelines 2006, Revised 1996 IPCC Guidelines for National Greenhouse Gas Inventories – Reference manual.
42. ENDESA Italia, Sustainability Report 2003 (In Italian).
43. D. Buoro, P. Pinamonti, M. Reini, Optimization of a Distributed Cogeneration System with solar district heating, *Applied Energy* **2014**, 124, 298-308.
44. D. Buoro , M. Casisi, A. De Nardi, P. Pinamonti, M. Reini, Multicriteria Optimization of a Distributed Energy Supply System for an Industrial Area, *Energy* **2013**, 58, 128-137.
45. <http://www.fico.com/en/products/fico-xpress-optimization-suite>
46. <http://www.esteco.com/modelfrontier>

47. K. Deb, A. Pratap, S. Agarwal, T. Meyarivan, A fast and elitist multiobjective genetic algorithm: NSGA-II, *IEEE Transactions on Evolutionary Computation*, **2002**, 6, 182-197.