

Application of Numerical Tools to Investigate a Leaky Aquitard beneath Urban Well Fields

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Abstract

Memphis aquifer is the primary drinking water source in Shelby County (Tennessee, USA) and supplies industrial, commercial, and residential water. Memphis aquifer is separated from the Shallow aquifer by a clayey layer known as Upper Claiborne Confining Unit (UCCU). All of the production wells in the Memphis area are screened in the Memphis aquifer or even deeper in the Fort Pillow aquifer. Traditionally, it was assumed that the UCCU could fully protect the Memphis aquifer from the contaminated Shallow aquifer groundwater. However, recent studies show that at some locations the UCCU is thin or absent which possibly leads to the contribution of Shallow aquifer to the Memphis aquifer. Accurately locating the breaches demands expensive and difficult geological or geochemical investigations, especially within an urban area. Hence, a pre-field investigation to identify the locations where the presence of breaches is likely can significantly reduce the cost of field investigations and improve their results. In this study, to identify the locations where the presence of breaches in the UCCU is likely we use three different analyses: (1) pilot point calibration (PPC), (2) velocity and flow budget (VFB), and (3) particle tracking (PT) to post-process the developed groundwater results. These pre-field numerical investigations provide relevant and defensible explanations for groundwater flow anomalies in an aquifer system for informed decision-making and future field investigations. In this study, we identify five specific zones within the broad study area which are reasonable candidates for the future field investigations. Finally, we test the results of each analysis against other evidence for breaches to demonstrate that the results of the numerical analyses are reliable and supported by previous studies.

Key words: Groundwater model, well field, pre-field investigation, aquitard breach

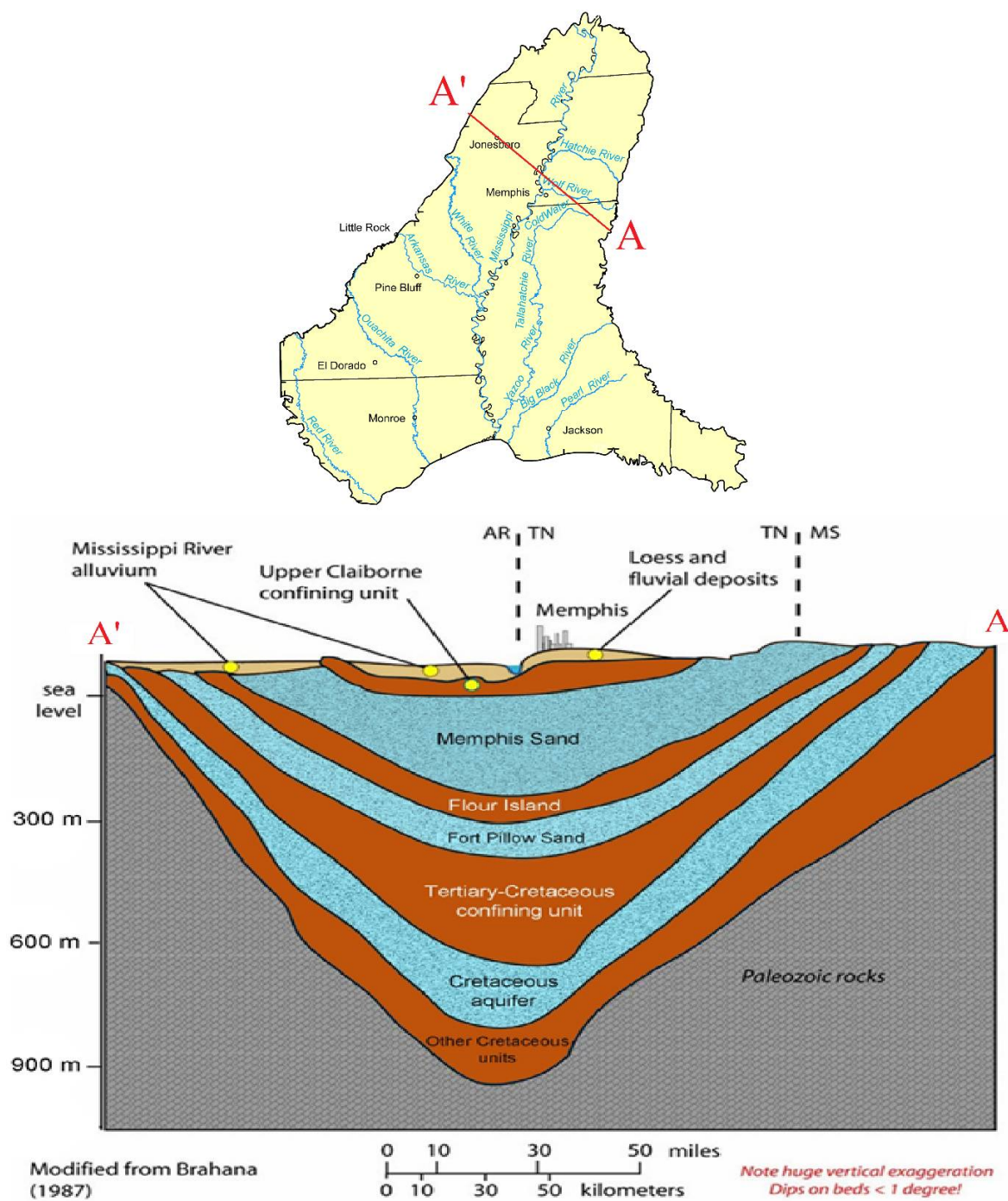
1 **1 Introduction**

2 The City of Memphis (Shelby County, Tennessee, USA) has undergone significant urban
3 development from 1950 to 2000, partially due to the availability of inexpensive, high-quality water
4 from Memphis aquifer, a regional groundwater resource. Local utilities and industries in Shelby
5 County, Tennessee extract more than 680 thousand cubic meter per day of groundwater that
6 requires minimal treatment for municipal use (Dieter et al., 2018). The groundwater quality of
7 Memphis is not only crucial for the general consumption but also for the economy of the region
8 (Staff, 2015). After decades of continues extraction, water quality degradation and contamination
9 of the Memphis aquifer has become a concern leading to local utilities and citizen groups taking a
10 more proactive approach to address these issues rather than the traditional reactive approach.

11 Memphis is within the Mississippi embayment aquifer system and underlain by
12 approximately one kilometer of unconsolidated sediments (Figure-1). The subsurface is divided
13 into a series of alternating sand and clay layers grouped into hydrostratigraphic units that include
14 several water-bearing units. As shown in Figure-1, four sand aquifers beneath Shelby County,
15 Tennessee include the Shallow aquifer, the Memphis aquifer, the Fort Pillow aquifer, and the
16 Cretaceous aquifer, each of which is separated from adjacent aquifers by aquitard units, known as
17 Upper Claiborne confining unit (UCCU), Flour Island, Tertiary-Cretaceous confining unit, and
18 other Cretaceous units (Brahana and Broshears, 2001; Clark and Hart, 2009). The Shallow aquifer
19 consists of the Mississippi River Valley alluvial (MRVA) aquifer and the Gulf Coastal Plain (GCP)
20 fluvial and alluvial aquifer. The MRVA aquifer serves as a water source for industrial, domestic,
21 and irrigation wells in the Mississippi alluvial valley and typically is not utilized in urban settings.
22 Water from the Shallow aquifer is of poorer quality than that in the underlying Memphis and Fort
23 Pillow aquifers due to the absence of an overlying aquitard; thus, it is locally contaminated in
24 places. The Memphis aquifer serves as the primary source of drinking water in Shelby County,
25 Tennessee with minor withdrawals coming from the deeper Fort Pillow aquifer. The Cretaceous
26 aquifer is not utilized in Shelby County due to the depth and poorer water quality.

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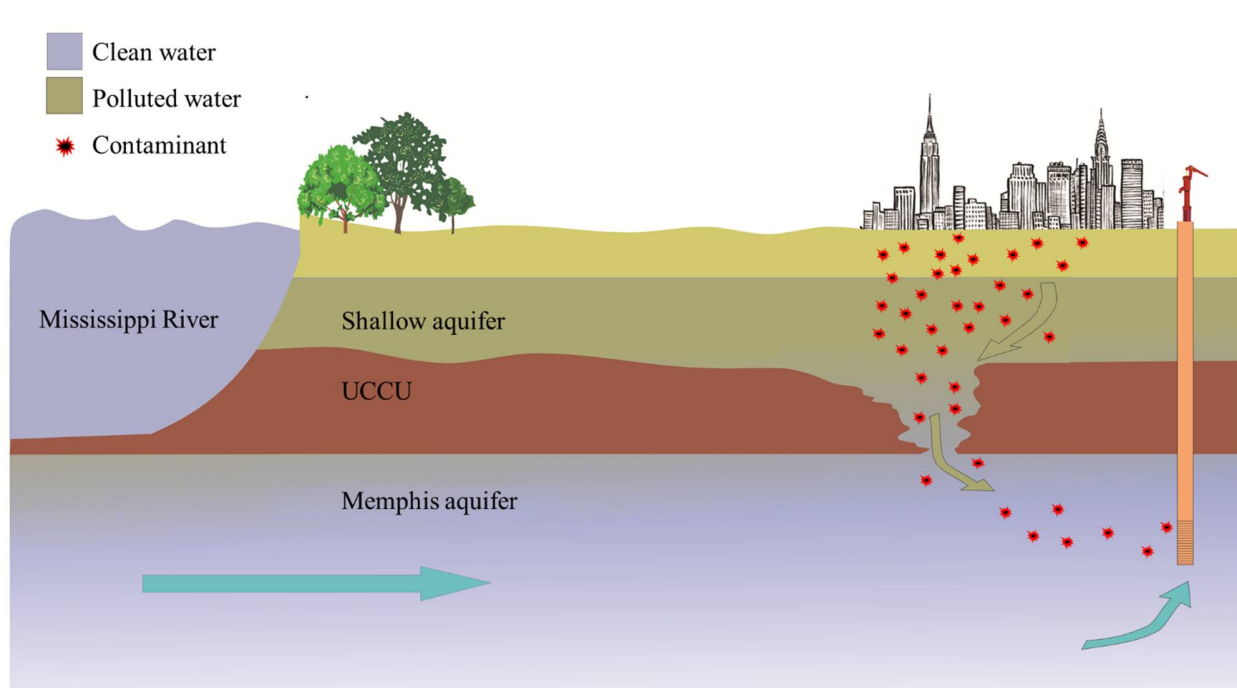
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1
2 Figure-1 A-A' hydrogeological section of the Memphis groundwater system, through the Mississippi embayment. It represents
3 four aquifers and four confining units. Note that the vertical axis is dramatically exaggerated for visualization purposes.

4 The UCCU layer separates the Shallow and the Memphis aquifers throughout most of the
5 Shelby County acting as an upper protective layer to the Memphis aquifer. However,
6 hydrogeologic breaches, also termed windows, within the UCCU locally create hydraulic

1 connections between these aquifers (Parks, 1990). The quantity of water passing through these
 2 hydraulic connections increases with greater groundwater withdrawal and groundwater head
 3 depression within the Memphis aquifer (Kingsbury and Parks, 1993). Hence, through these
 4 breaches the Shallow aquifer is recharging the Memphis aquifer through the leaky hydrogeologic
 5 breaches where the hydraulic conductance is relatively high comparative to the rest of the UCCU.
 6 Figure-2 demonstrates a schematic of a breach in the aquitard layer that acts as a preferential flow
 7 path from the Shallow aquifer to a screened production well in the Memphis aquifer.



8
 9 *Figure-2 shows how pollution can be transferred from urban activities to the Shallow aquifer, and finally to the Memphis aquifer*
 10 *through a breach.*

11 Breaches in the UCCU aquitard threaten the water quality of the City of Memphis;
 12 therefore, identifying locations of the breaches are essential for source-water protection, and the
 13 development and implementation of wellhead protection plans. However, the seemingly
 14 straightforward question is --Where are the breaches? So far, two different approaches are
 15 employed to answer this question. The first approach is the “geochemical investigation”
 16 (Neretnieks, 1981; Busenberg et al., 1993; Larsen et al., 2003, 2013, 2016; Ivey et al., 2008;
 17 Majidzadeh et al., 2017) where groundwater samples are analyzed to identify geochemical
 18 signatures attributed to surface water within the Memphis aquifer water. Within the Memphis
 19 area, age-dating of groundwater using tritium-helium-3 and sulfur hexafluoride support

1 geochemical data and reflects the influence of modern water (< 50 years) in the Memphis aquifer.
2 Subsequent studies have shown that modern water contributes up to 40% of groundwater
3 withdrawn from production wells – in one case production water contains as much as 75% modern
4 water (Larsen et al., 2003, 2013, 2016). The second approach is the “geological investigation” in
5 which techniques such as surveying stratigraphic thickness and water table elevation, electrical
6 resistivity surveys, shear-wave seismic reflection, and other geophysical analyses are used to
7 identify gaps in impermeable layers (Parks, 1990; Sutinen, 1992; Besson et al., 2004; Waldron et
8 al., 2009; Schoefnacker, 2018). Geological investigations show how hydrogeologic units are
9 connected in the subsurface and where preferential leakage pathways may exist. Parks (1990)
10 created an isopach map of the UCCU throughout Shelby County and identified several areas where
11 clay layers within the UCCU are thin or absent. Parks (1990) also prepared a water-table elevation
12 map for Shelby County and showed that several areas with anomalous water-table depressions also
13 had thin or absent confining unit clay, consistent with vertical leakage through a breach in the
14 UCCU. Waldron et al. (2009) used an S-wave seismic reflection survey to map the size and the
15 orientation of localized breaches in the UCCU near an unlined landfill.

16 The abovementioned approaches have several limitations. First, mapping breaches are
17 complicated, costly and time-consuming owing to their depth, unknown location and randomness
18 of origin causality. Second, mapping studies with geophysical methods are technically limited to
19 the small study area and their measuring accuracy dissipates as the study area extends. Third,
20 approaches involving extensive drilling and geophysical studies are inapplicable or prohibitive in
21 urban areas due to infrastructure, and compact residential and commercial areas. Therefore, when
22 the presence of a breach in the aquitard layer is likely, numerical investigations conducted prior to
23 field studies (pre-field investigation) can be extremely helpful to identify locations where a breach
24 is likely to exist. Pre-field numerical investigations provide relevant and defensible explanations
25 for groundwater flow anomalies in an aquifer system for informed decision-making.

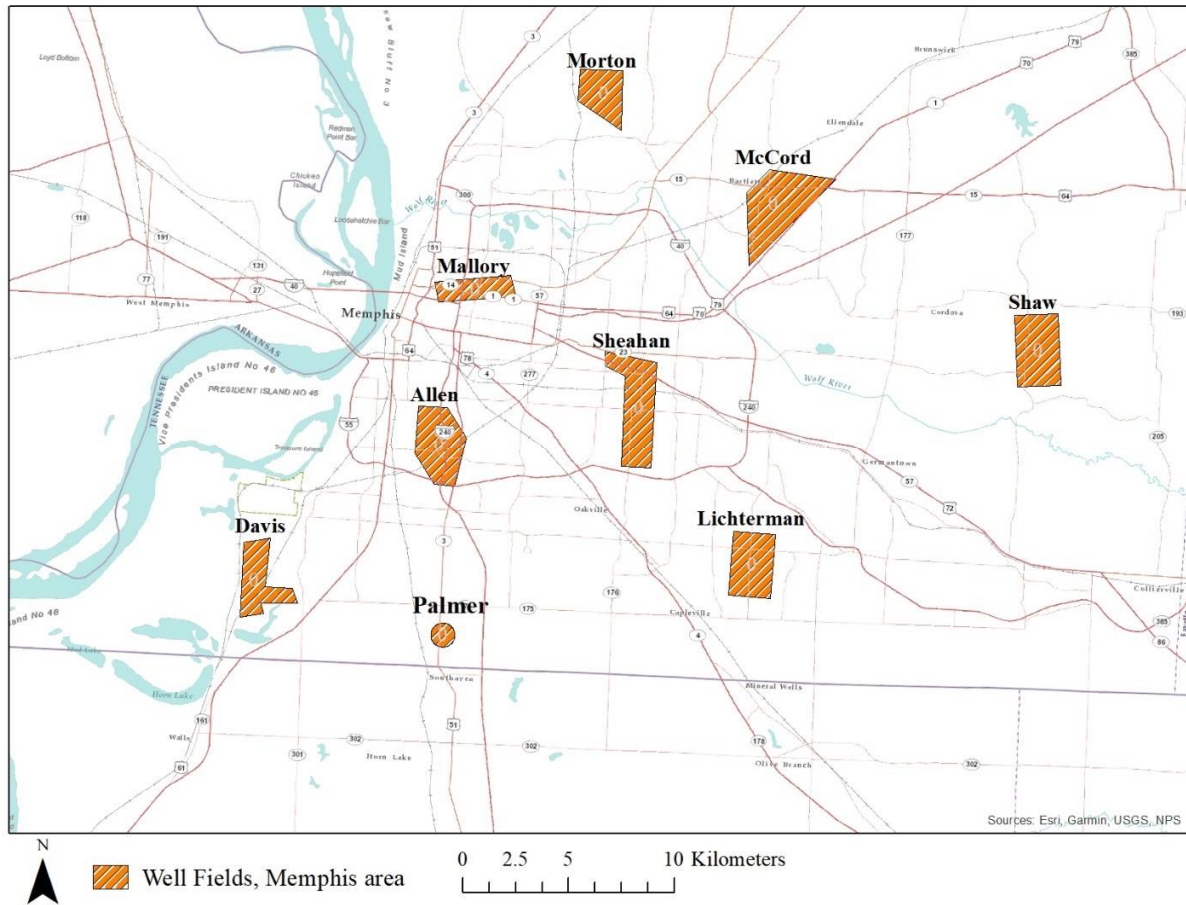
26 Several numerical tools are developed to simulate the groundwater flow within the system.
27 Groundwater models provide invaluable information about what cannot be adequately measured
28 or observed, in both space and time domains (e.g., geological conceptualization, flow rates and
29 flow pathways). Such numerical tools apply mathematical equations to calculate aquifer system
30 responses to forcing conditions such as pumping, stream-stage variation, and rainfall events

1 (Anderson et al., 2015). Beside the groundwater models, several other numerical tools and
2 techniques are developed to post-process the flow equations and results of numerical models to
3 improve our understanding of the studying groundwater system (Pollock, 1994; Owen et al., 1996;
4 Zimmerman et al., 1998; Van Dam and Feddes, 2000; Guha, 2008; Simpson et al., 2013; Jazaei et
5 al., 2014, 2016, 2017).

6 In this work, we show how a combination of forward and backward numerical modeling,
7 and post-processing numerical tools can be used to produce a more satisfactory representation of
8 the groundwater system to make informed field investigation decisions. Herein, three numerical
9 analyses are utilized: (1) pilot point calibration analysis (PPC); (2) velocity and flow budget
10 analyses (VFB); and (3) particle tracking analysis (PT), to reasonably identify the locations where
11 the presence of breaches is likely. Finally, we test the results of each analysis against other
12 evidence for breaches to demonstrate that the results of the numerical analyses are reliable and
13 supported by previous studies.

14 **2 Methodology**

15 This study incorporates multiple Memphis Light, Gas and Water (MLGW) well fields
16 including the Allen, Davis, and Palmer well fields. These three well fields are located east of the
17 Mississippi River bluff line in southwestern Shelby County (Figure-3) that include 49 production
18 wells (26 wells in Allen; 19 wells in Davis, and 4 wells in Palmer) and collectively produce more
19 than 50 million cubic meter per year over 2005 to 2016 (TDEC Dataviewers, n.d.). Herein, we
20 consider only the upper three geological units: (1) Shallow aquifer, (2) UCCU, and (3) Memphis
21 aquifer (Figure-1). This approach is justified because all the production wells within these well
22 fields are screened in the upper and middle Memphis aquifer and little evidence exists for upward
23 flow of water from deeper hydrogeologic units (Brahana and Broshears, 2001). Therefore, we
24 neglect the interaction between the lower Memphis aquifer and the Flour Island aquitard by
25 assuming a no-flow boundary condition at the base of the Memphis aquifer (Figure-1).



1

2

Figure-3 shows all active well fields in the Memphis area.

3 **2.1 Extent of the study area**

4 In this study, we first assemble and analyze existing relevant hydrogeological field data to

5 define a proper extent for the study area, and build an advisory conceptual model. In groundwater

6 studies, the delineation of the extent of the study area is quite critical and challenging. To evaluate

7 a proper extent for this study, we use available potentiometric data of the Memphis aquifer in 2005,

8 2007, 2010 and 2015 (“USGS Water Data for the Nation,” n.d.; Kingsbury, 2018). Figure-4 shows

9 the types and locations of boundary conditions which encompass Allen, Davis, and Palmer well

10 fields. The purple, blue, green, and orange lines are associated with the years of 2005, 2007, 2010

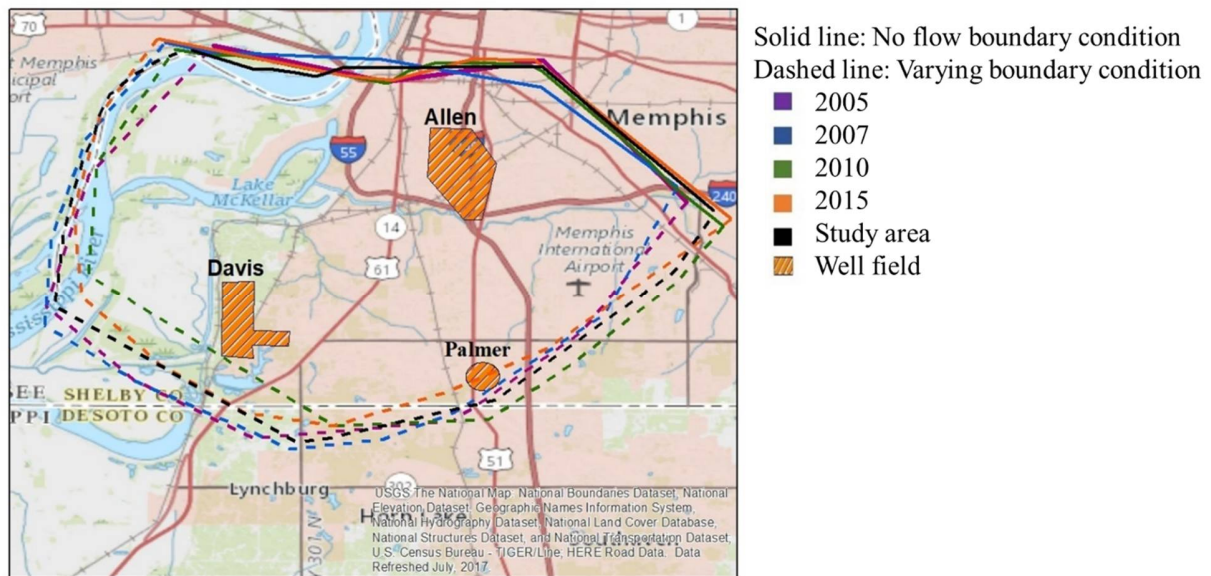
11 and 2015, respectively. Dashed lines symbolize temporally varying boundary conditions in the

12 Memphis aquifer (i.e., the groundwater heads along the dashed lines are spatially constant while

13 their magnitudes vary with time). The solid line symbolizes the no-flow boundary condition at the

14 groundwater divides between Allen, Sheahan and Mallory well fields (Figure-3 and 4). As shown

1 in Figure-4, locations of both no-flow and temporarily varying boundary conditions remain nearly
 2 consistent from 2005 to 2015. Hence, we estimate the study area to encompass the average extent
 3 of the boundary conditions in different years, which is shown in black in Figure-4. The same
 4 extent is delineated for the Shallow aquifer and UCCU; however, with relevant spatially and
 5 temporally varying boundary conditions.



6

7 *Figure-4 shows the no-flow boundary condition (solid lines) and temporarily varying boundary conditions (dashed lines) of the*
 8 *Memphis aquifer for the years of 2005, 2007, 2010, and 2015. The black line shows the estimated extent of the study area.*

9 **2.2 Conceptual model**

10 Figure-5 shows the conceptual model for the site-specific hydrogeological setting. In the
 11 conceptual model, we simplify the system conditions and capture the essential features of the site.
 12 Figure-5(a) shows a plan view of the conceptual model. A bluff line of 15 to 45 m high separates
 13 alluvial and fluvial Shallow aquifers. Consequently, the hydraulic characteristics of the Shallow
 14 aquifer vary significantly on either side of the bluff line. Figure-5(b) shows a side view of the
 15 conceptual model which is made up of three layers: Shallow aquifer, UCCU, and the Memphis
 16 aquifer. Stratigraphic unit elevations were derived from Clark and Hart (2009). Production well
 17 screen intervals are illustrated in Figure-5(b), taking note that they vary in depth. This aquifer
 18 system conceptualization was very helpful in developing the numerical model.

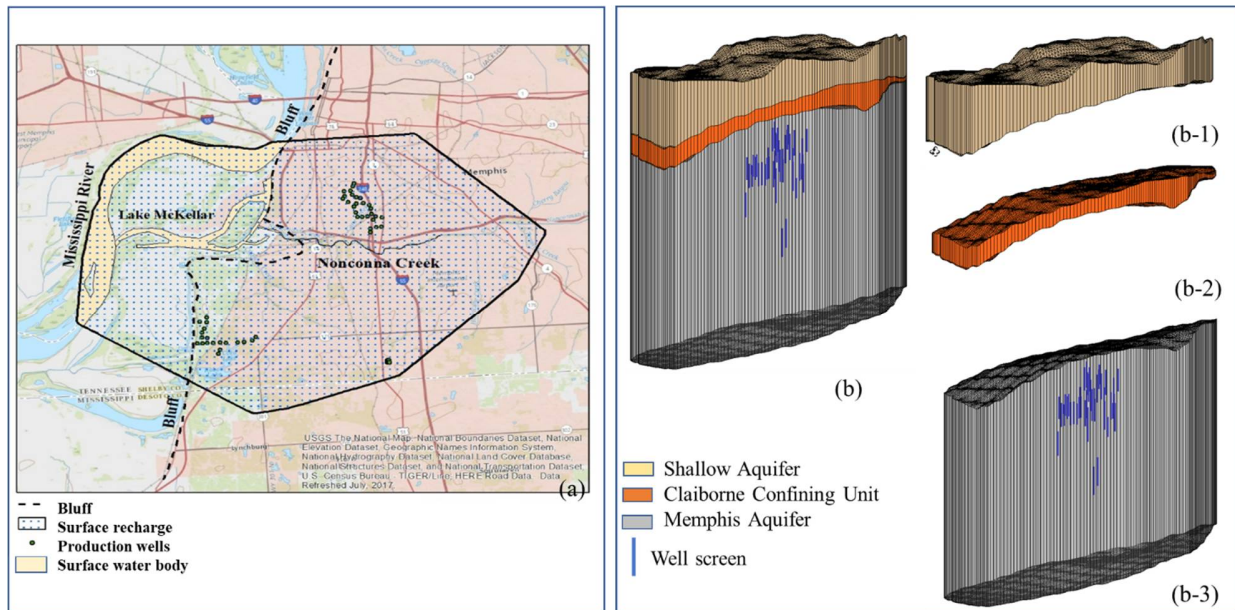


Figure-5 (a) shows a plan view of the conceptual model which includes a part of the Mississippi River, Lake McKellar, Nonconna Creek, production wells and surface recharge. (b) shows a side view of the conceptual model and the location of production well screens. (b-1), (b-2) and (b-3) separately show the Shallow aquifer, UCCU, and the Memphis aquifer, respectively.

2.3 Groundwater model

To describe the transient groundwater flow in the study area, we develop a high resolution three-dimensional numerical model using (Bear, 2012):

$$S \frac{\partial h}{\partial t} = \frac{\partial}{\partial x} \left(K_x \frac{\partial h}{\partial x} \right) + \frac{\partial}{\partial y} \left(K_y \frac{\partial h}{\partial y} \right) + \frac{\partial}{\partial z} \left(K_z \frac{\partial h}{\partial z} \right) + w, \quad (1)$$

where h [L] is groundwater head, K_x , K_y , and K_z [L/T] are hydraulic conductivity in x , y and z directions, respectively; t is time [T]; S [1/L] is the storage coefficient of the aquifer and w [1/T] is a source and sink parameter (volumetric flux per unit volume). We use MODFLOW-NWT to solve Eq. (1) (Niswonger et al., 2011). The numerical model has 6 layers with a uniform 250×250 m² cells, totaling 20,773 active cells. The first and second numerical layers represent the Shallow aquifer and UCCU, respectively. Other four numerical layers uniformly divide the Memphis aquifer. The time domain of the model begins from 2005 to 2015, a span we have relatively sufficient data for Shallow and Memphis aquifer groundwater head within the study

1 area. This duration is discretized into 121 monthly stress periods. Each stress period has 5 time
2 steps.

3 **2.4 Initial conditions and boundary conditions**

4 In this study, the initial head conditions of the Shallow aquifer are set to the water-table
5 surface (Shallow aquifer) measured in 2005. There are no information regarding the groundwater
6 head in UCCU. Therefore, we assume the same initial condition within the UCCU in 2005
7 (Narsimha, 2007). The initial head conditions for the Memphis aquifer are derived from the 2005
8 Memphis aquifer potentiometric surface (Kingsbury, 2018). Boundary conditions of the Shallow,
9 UCCU, and Memphis aquifer are estimated using available potentiometric surfaces during 2005
10 to 2015. The boundary condition of the Shallow aquifer is assumed to be spatially and temporally
11 varying during 2005-2015 except beneath the Mississippi River where it is controlled by the river
12 stage variations. Therefore, the boundary condition under the Mississippi River is estimated
13 according to the monthly measurements of river stage at the nearby Beale Street gage during the
14 period of 2005 to 2015 (“Rivergages.com: Providing River Gage Data for Rivers, Streams and
15 Tributaries,” n.d.). We neglect the horizontal inflow and outflow at the UCCU boundary condition;
16 therefore, the boundary condition of the UCCU is assumed to be a no-flow boundary condition.
17 Two boundary conditions are applied to the Memphis aquifer: no-flow (boundary is perpendicular
18 to equipotential lines) and temporarily varying boundary conditions (Figure-3). The Memphis
19 aquifer head variation at the varying boundary condition, at many points, remains in relatively
20 small range of fluctuation during 2005 to 2015. Therefore, the temporally varying boundary
21 condition of the Memphis aquifer is estimated by interpolating available 2005 to 2015 Memphis
22 aquifer heads (Kingsbury, 2018).

23 **2.5 Internal forcing conditions**

24 Internal forcing conditions within the study area include McKellar Lake, Nonconnah
25 Creek, production wells, and surface recharge. Since McKellar Lake has an open connection to the
26 Mississippi River, lake stage follows Mississippi River stages. The Nonconnah Creek stage
27 variation is modeled using monthly mean stages measured at an upstream and downstream
28 stations, Farris View Drive stage and Riverport stage, during the period 2011 to 2017 when the
29 stage data were recorded (“Rivergages.com: Providing River Gage Data for Rivers, Streams and
30 Tributaries,” n.d.). The exact withdrawal rates of the production wells are unavailable. Therefore,

1 monthly production for the entire well field is uniformly distributed to each active well during that
2 month (Tennessee Department of Environment and Conservation (TDEC) “Upon request: TDEC
3 Dataviewers,” n.d.). Precipitation recharge is applied to the upper layer representing the Shallow
4 aquifer surface recharge. Unfortunately, recharge rates are unknown and must be inferred from
5 available precipitation records. However, since precipitation events occur almost in all months of
6 each year we assume a constant but spatially varying recharge rate over the study area (See
7 Appendix-3).

8 **3 Numerical analysis results**

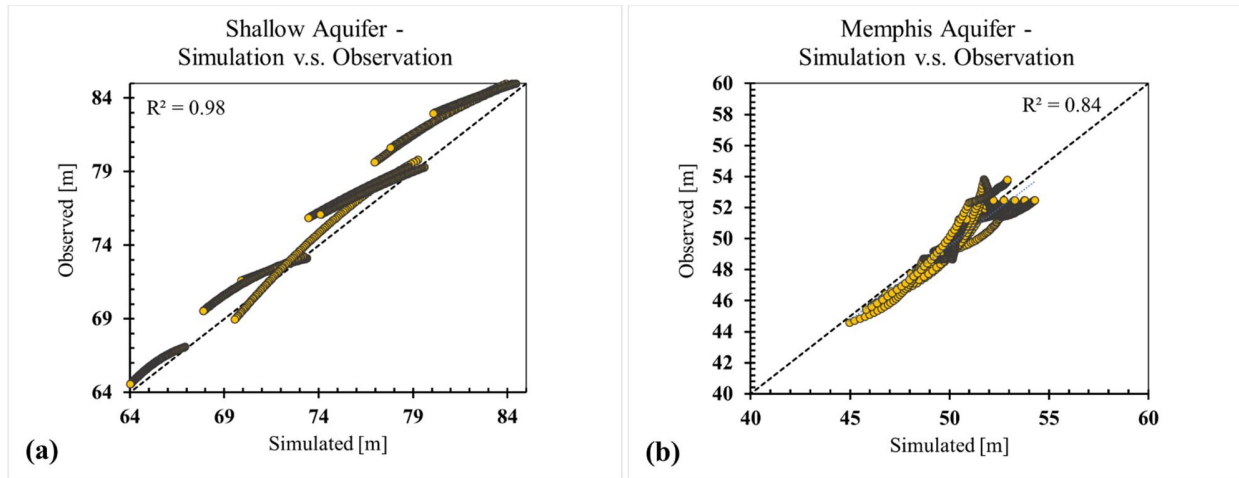
9 In this study, we locate zones where the presence of leaky aquitard (UCCU) breaches is
10 likely by applying three numerical analyses: (1) pilot point calibration (PPC) performed against
11 horizontal and vertical hydraulic conductivities, (2) velocity and flow budget (VFB), and (3)
12 particle tracking (PT). As it pertains the identifying plausible aquitard breach locations, the
13 following observances are assumed: (1) hydraulic conductivities at breaches are expected to be
14 locally high, (2) convergence of flow to a specific area is a sign of the presence of a breach, and
15 (3) vertical flow at breaches is expectedly high compared with other parts of the study area. These
16 conditions will be derived from the PPC and VFB. In contrast, PT should show that groundwater
17 particles at the breaches vertically transport further than in the surrounding area.

18 **3.1 Pilot point calibration analyses (PPC)**

19 Although the boundary conditions and withdrawal rates are estimated, several required
20 parameters for groundwater modeling including horizontal and vertical hydraulic conductivities,
21 storage coefficients, surface recharge, and the conductance of the hyporheic zone at Nonconnah
22 Creek bed are remained unknown. To estimate the unknowns we use an advanced nonlinear
23 method of spatial parameter characterization to develop an inverse groundwater model (Doherty,
24 2003). We first use uniform properties for each layer to estimate proper starting calibration values
25 within a meaningful range of parameters reported in previous studies conducted in the Mississippi
26 embayment area (Moore, 1965; Brahana and Broshears, 2001). In the groundwater literature, this
27 approach is known as zonal calibration (Park et al., 2014; Jiménez et al., 2016). We consider two
28 zones at the east and west of the bluff for Shallow aquifer. Similarly, we consider two zones at
29 either side of the bluff for UCCU. Finally, we consider one zone for each numerical layer (four
30 layers) of the Memphis aquifer. Parameters used for this pre-calibration process are horizontal and

1 vertical hydraulic conductivities, storage coefficients, the Nonconnah Creek bed conductance, and
2 surface recharge. To describe the heterogeneity in hydraulic conductivity and surface recharge
3 within each zone we use "pilot points" accompanied by advanced regularization functionality
4 available through PEST (Doherty, 2003, 2002). This model includes 69 pilot points distributed in
5 all layers. The inverse distance weighted method is used to spatially distribute pilot points values
6 to each cell of the model. We use PEST to estimate a new set of the model parameters (i.e.,
7 horizontal and vertical hydraulic conductivities, storage coefficients, the Nonconnah Creek bed
8 conductance, and surface recharge) using a robust mathematical technique by comparing
9 simulation results to a set of observations (Doherty, 2003, 2002). Observation points are derived
10 from the available Shallow and Memphis aquifers potentiometric surfaces maps (Narsimha, 2007;
11 Kingsbury, 2018). To evaluate the calibration results, we compare the simulated transient
12 groundwater head with the observed data at 31 observation points within the Shallow and Memphis
13 aquifers. Shallow aquifer observation data include water levels collected in 2005 and 2015. The
14 Memphis aquifer observation data include groundwater heads collected during 2005 to 2015.
15 Groundwater head fluctuation in each observation point was not high; therefore, the monthly
16 varying head at each observation point is estimated by linear interpolation between years when the
17 observation data are available. The observed versus simulated groundwater heads are shown in
18 Figure-6. The goodness of fit coefficients between the simulated and calibrated results of the model
19 are computed for all observation points within the Shallow and the Memphis aquifers (Glantz and
20 Slinker, 1990). R^2 values of Shallow and Memphis aquifers are estimated 0.98 and 0.84,
21 respectively, which indicate a satisfactory goodness of fit.

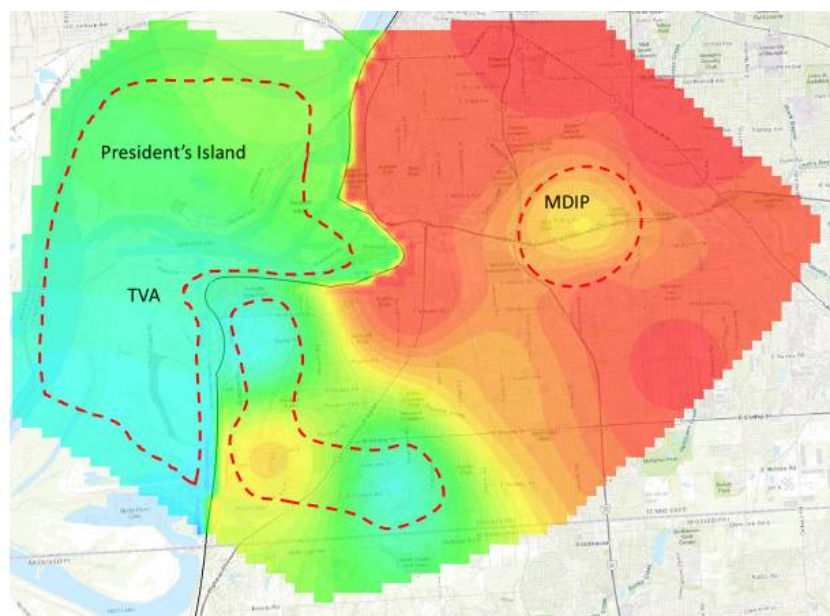
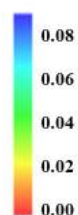
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2 Figure-6 (a) and (b) show observed vs simulated results of the model for the Shallow and Memphis aquifers, respectively. The
 3 goodness of fit coefficients for the Shallow and Memphis aquifers are estimated as 0.98 and 0.84, respectively.

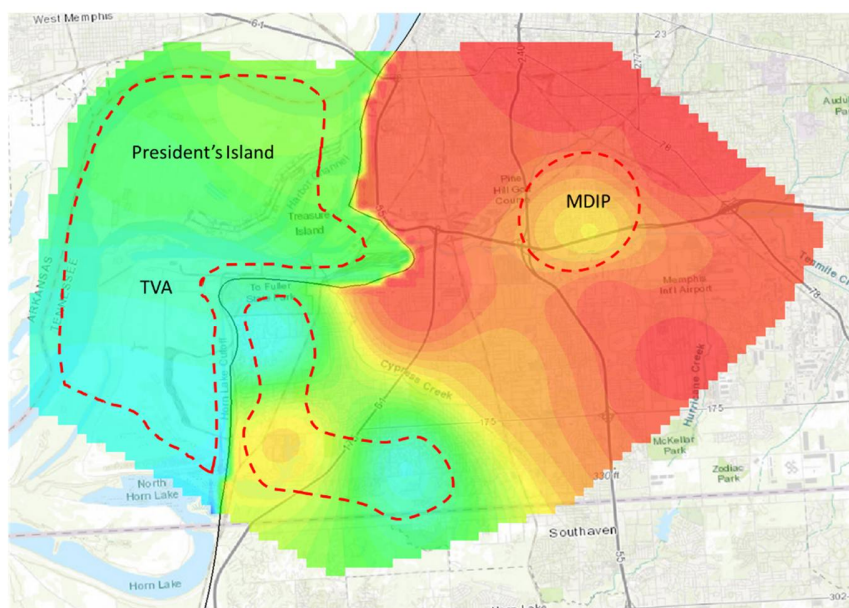
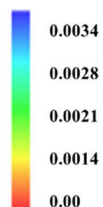
4 The calibrated horizontal and vertical hydraulic conductivities of the UCCU are shown in
 5 Figure-7(a) and (b), respectively. Figure-7 shows that the patterns of the distribution of horizontal
 6 and vertical hydraulic conductivities are quite similar however with different values (see
 7 Appendix-1, 2 and 3 which summarize all six numerical layers' calibrated hydraulic
 8 conductivities, storage coefficients and surface recharge, respectively). As shown in Figure-7, PPC
 9 reveals three major zones (dashed lines) in which the vertical and horizontal hydraulic
 10 conductivities of the UCCU are relatively high. Since we expect locally high hydraulic
 11 conductivity at the breaches, we concluded that the presence of breaches at these three zones is
 12 more probable than other parts of the study area.

Horizontal Hydraulic Conductivity of UCCU [m/d]



(a)

Vertical Hydraulic Conductivity of UCCU [m/d]



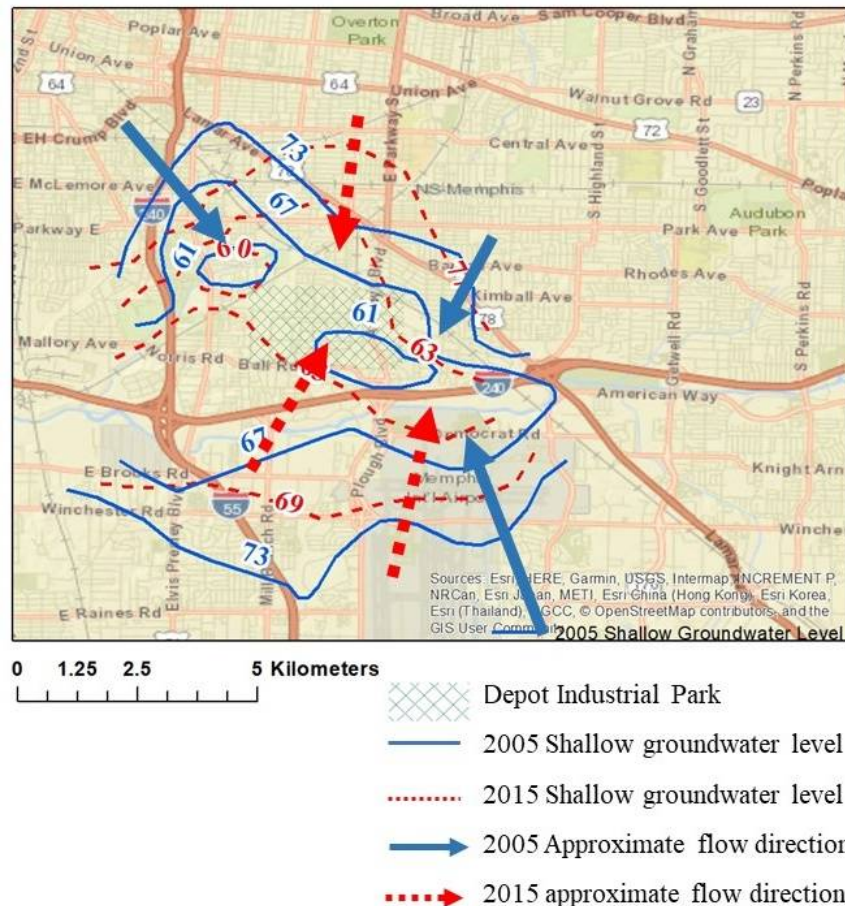
(b)

Figures-7(a) and (b) maps show calibrated horizontal and vertical hydraulic conductivities of UCCU, respectively. They show relatively higher hydraulic conductivities in three zones: Memphis Depot Industrial Park (MDIP), Tennessee Valley Authority (TVA) and President's Island, and the south of the study area.

3.1.1 Validation of PPC results

The increase of hydraulic conductivities represented within the three identified zones (Figure-7) likely exist due to lithologic variation or erosion of the UCCU with an increase of coarser grained sediments (Ebina et al., 2004; Alakayleh et al., 2018). The first identified area by PPC is located in the Memphis Depot Industrial Park (MDIP) (Figure-7). Recent investigations

1 have already indicated that the Shallow groundwater level in this area is locally lower than that in
 2 the surrounding areas (Bradshaw, 2011; Narsimha, 2007). Figure-8 shows the approximate flow
 3 directions of Shallow aquifer in 2005 and 2015, which converge from the surrounding areas toward
 4 the MDIP. There are no pumping wells in this area which otherwise would have resulted in such
 5 local cone of depression.



6

7 *Figure-8 map shows Shallow aquifer groundwater level and approximate flow directions in 2005 (blue arrow) and 2015 (red*
 8 *arrow) at the MDIP area*

9 The second zone is located on President's Island (Figure-7). Previous study and field
 10 investigation in this area have indicated that the thickness of the UCCU beneath President's Island
 11 significantly thins (Parks, 1990). Calibration results in the President's Island area affirm the
 12 suspicion of the thinning or absence of the UCCU. Moreover, in the area immediately south of
 13 President's Island that includes the Tennessee Valley Authority (TVA) combined cycle plant a

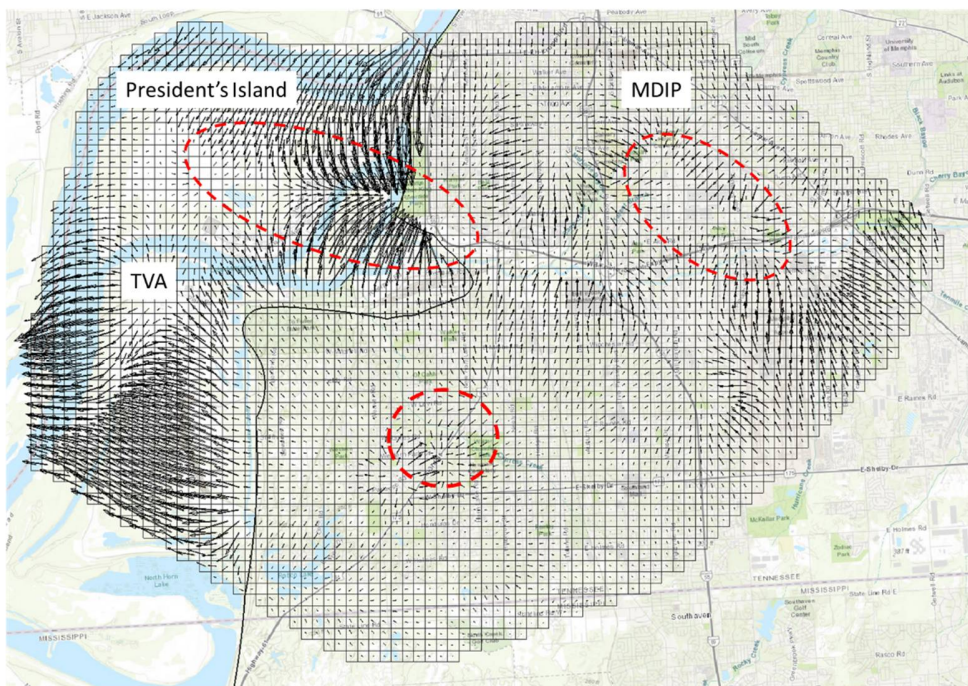
1 hydraulic connection of the Shallow and Memphis aquifer is identified (Carmichael et al., 2018)
2 (Figure-7). This recent study supports the likely presence of a breach in that area.

3 The third identified zone is located at the southern part of the study area adjacent to the
4 bluff line. This area is an undiscovered zone where field investigations are lacking. Therefore, this
5 area is considered an area of interest where further investigations are required to validate the PPC
6 results.

7 **3.2 Velocity and flow budget analyses (VFB)**

8 High hydraulic conductivity alone at a breach does not necessarily lead to a vertical flow
9 and needs sufficient vertical gradient to create flow. Determining the velocity and flow directions
10 of the Shallow aquifer can provide valuable information regarding the likely presence of a breach.
11 Figures-9(a-c) show the horizontal velocity vector of the Shallow aquifer in the study area in 2005,
12 2010 and 2015 derived from the developed numerical model. The magnitude of the velocity is
13 proportional to the arrows lengths. A longer arrow refers to a higher horizontal velocity. As shown
14 in Figure-9(a-c), the VFB approach identifies three zones where the velocity vectors converge to
15 specific areas. The horizontal velocity of groundwater decreases inside the convergence zones,
16 suggesting downward flow (assuming upward flow is negligible due to the regional downward
17 vertical gradient). As shown in Figure-10(a-c), VFB analyses also show vertical downward flow
18 budgets at the bottom of the Shallow aquifer in 2005, 2010, and 2015, respectively. Negative
19 values refer to an upward flow and positive value refers to a downward flow. As shown, the vertical
20 flows in all three identified zones by VFB are locally high. The main difference between the results
21 of the PPC and VFB analyses is that VFB does not show any local flow convergence and an
22 increase in vertical flow budget at the TVA area. Using this approach, we can conclude that the
23 presence of breaches at the three identified zones is more likely than other parts of the study area.

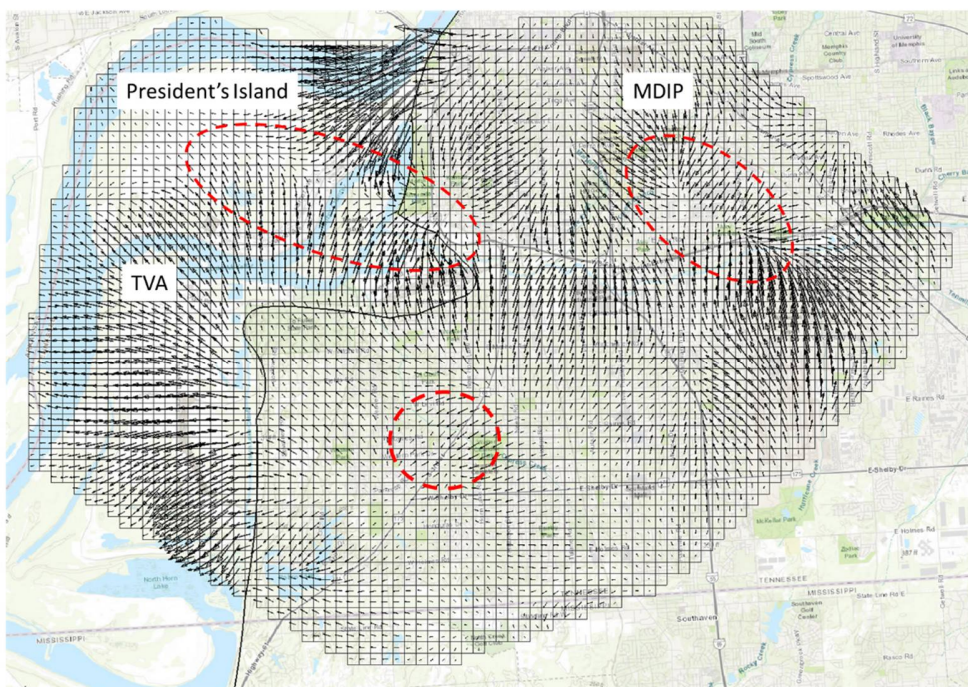
2005



(a)

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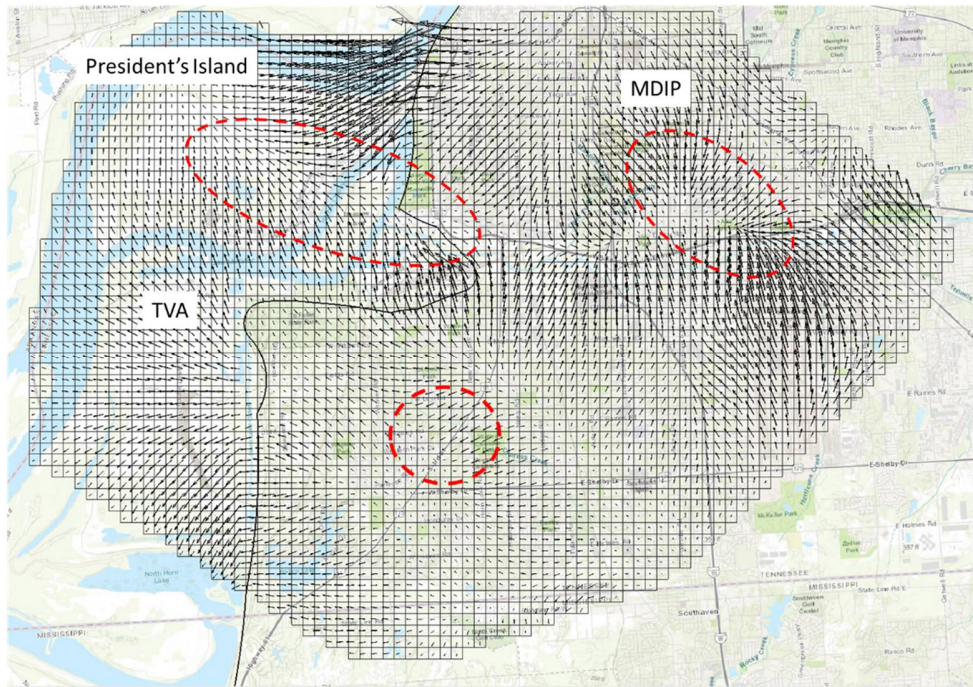
2010



(b)

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2015

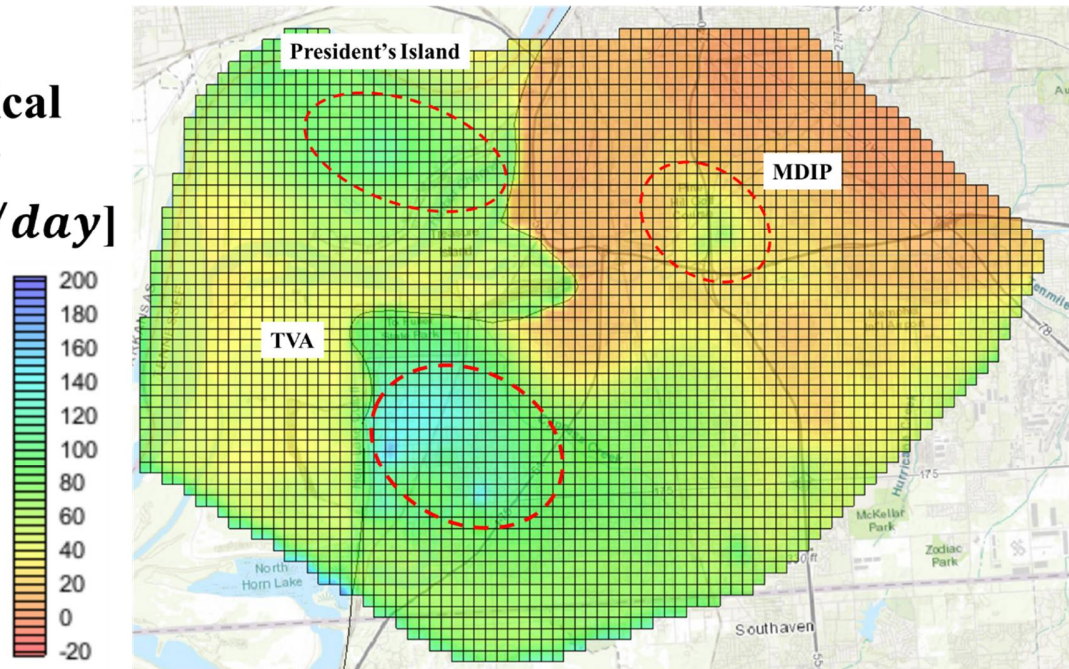


(c)

1

2 Figure-9(a-c) maps show the Shallow aquifer groundwater velocity vectors for 2005, 2010 and 2015, respectively. Magnitude of
 3 velocities are proportional to the length of arrows. Three zones where the groundwater velocity vectors are converged are
 4 shown. The probability of the presence of a breach in these zones are more probable than that of the surrounding areas.

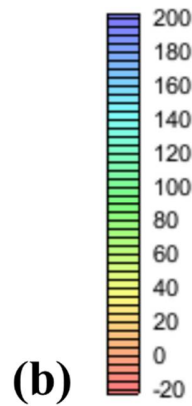
2005
 Vertical
 Flow
 [m^3/day]



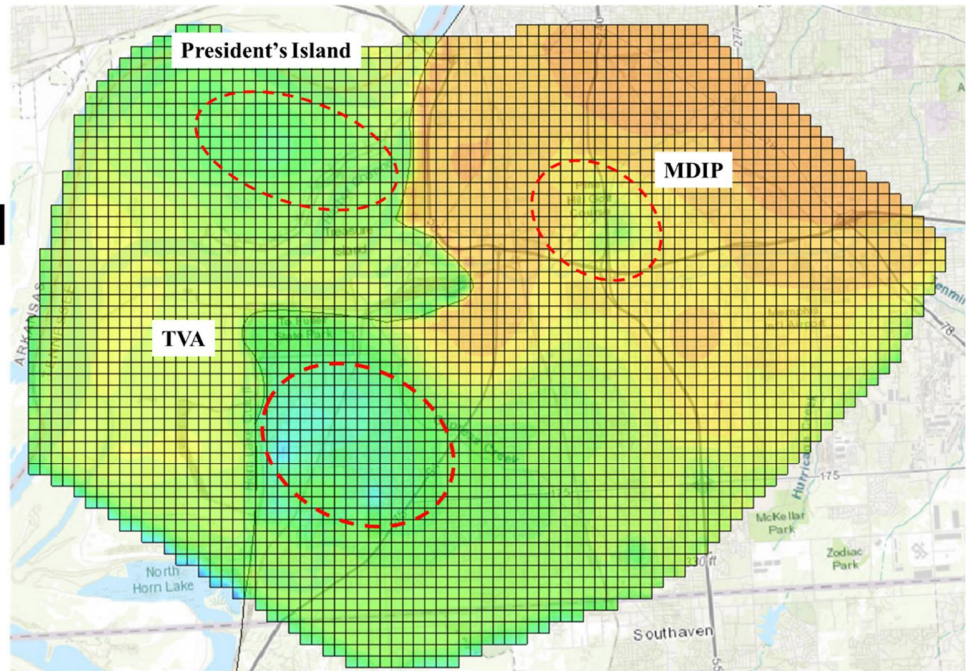
(a)

5

**2010
Vertical
Flow
[m³/day]**

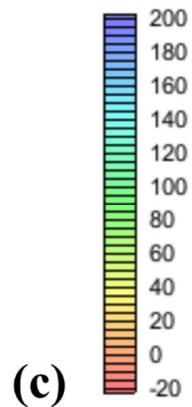


(b)

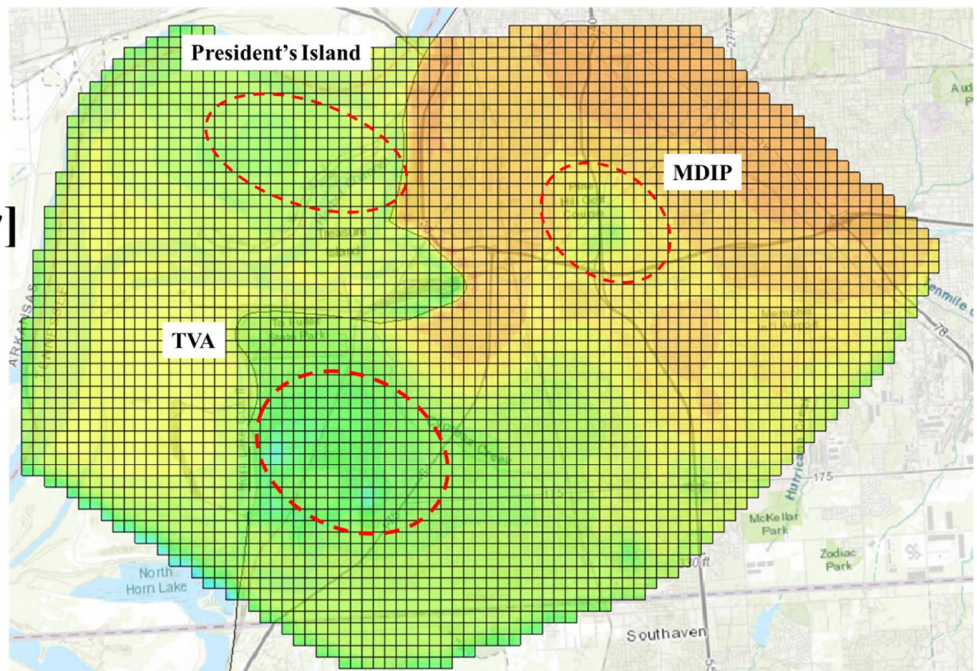


1

**2015
Vertical
Flow
[m³/day]**



(c)



2

3

4

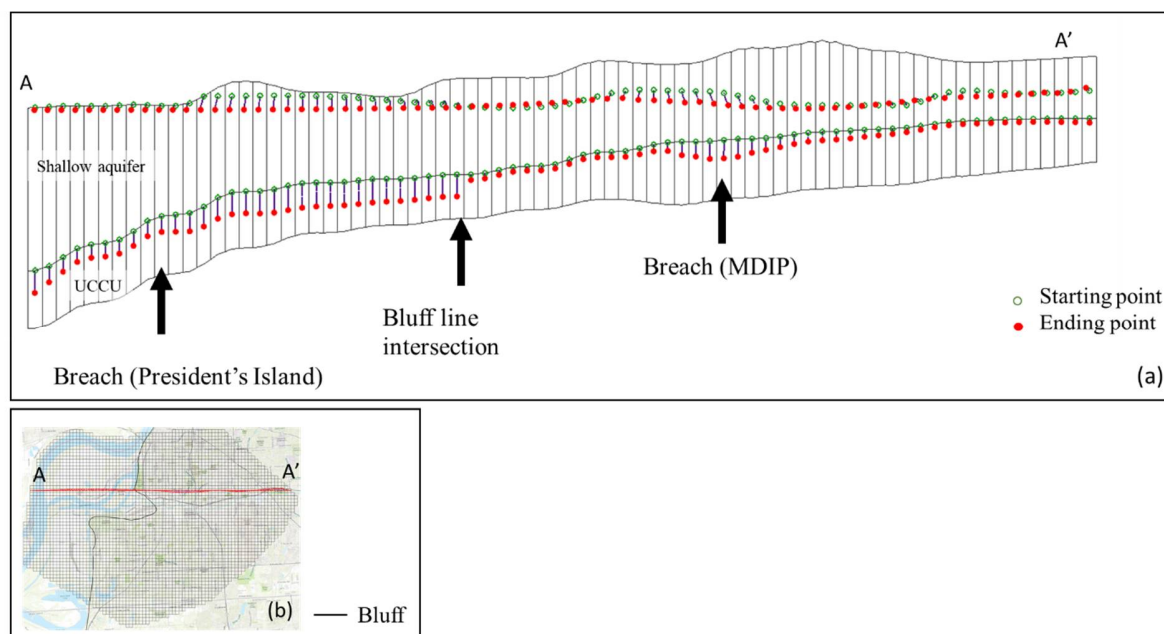
Figure-10(a-c) maps show vertical flow budgets at the bottom of the Shallow aquifer in 2005, 2010, and 2015, respectively. Negative values refer to upward flow and positive values refer to downward flows.

1 **3.2.1 Validation of VFB results**

2 As shown in Figure-9, the velocity vectors converge and focalize to three specific zones.
3 These zones are almost the same as the three zones identified by PPC analysis except in the TVA
4 area; therefore, VFB analysis only verifies the previous findings in the MDIP and President's
5 Island. However, it should be noted that VFB identifies smaller breach areas compared with PPC.
6 The third identified zone at the southern part of the study area is an undiscovered zone where
7 further local and detailed investigations are required for verification. It should be noted that the
8 convergence of the flow near the Nonconnah Creek is not necessarily because of the presence of
9 a breach in this area. Flow budget analysis shows that the convergence of the flow in this area is
10 mainly because of the drainage of the Shallow aquifer to the creek.

11 **3.3 Particle tracking analyses (PT)**

12 In this approach, we use the numerical tool, MODPATH (Pollock, 1994), to conduct
13 forward particle tracking. Figure-11(a) shows cross-section A-A' of the Shallow aquifer and
14 UCCU, an east to west transect of the study area that is shown in context in Figure-11(b). Forward
15 particle tracking represents the location of imaginary particles at the Shallow aquifer surface and
16 top of the UCCU from 2005 (green marks) to 2015 (red marks). Figure-11(a) shows vertical
17 downward flow transport from the Shallow aquifer and UCCU to the Memphis aquifer. A sudden
18 change is observed at the bluff line due to differences in alluvial (west of the bluff) and fluvial
19 (east of the bluff) deposits characteristics. The particles in the MDIP area also locally penetrate
20 further from 2005 to 2015. As shown, particles west of the bluff within the President's Island move
21 downward significantly faster than the east of the bluff, consistent with higher hydraulic
22 conductivity of the MRVA and fluvial deposits at either side of the bluff line.



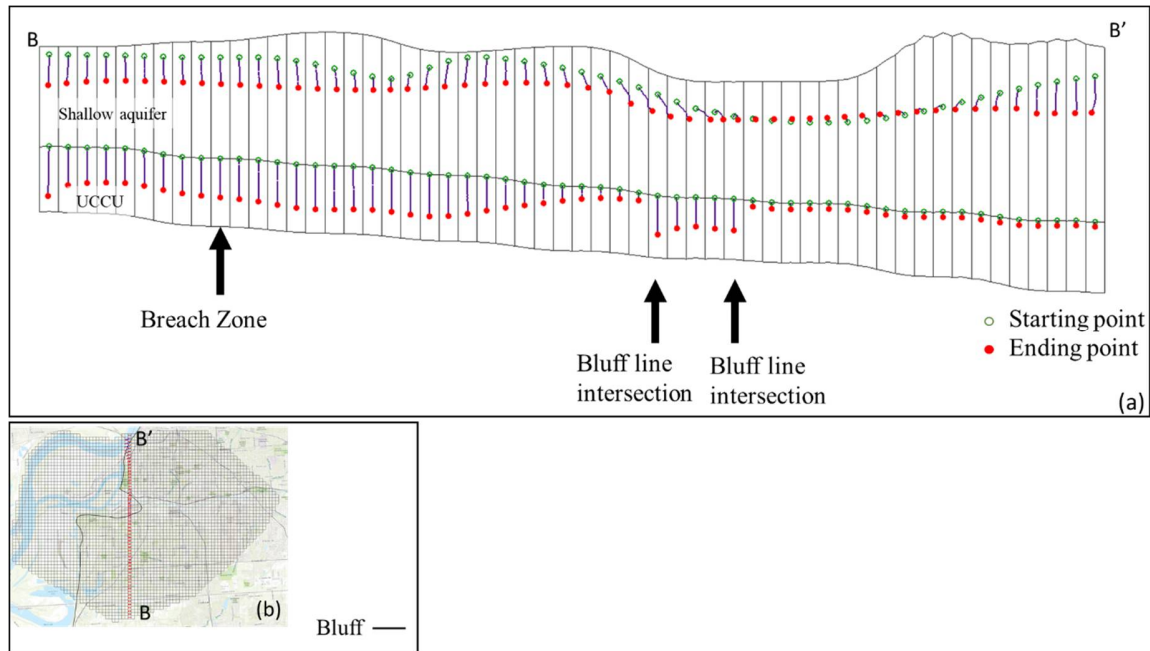
1

2 *Figure-11 shows the A-A' cross section of the Shallow aquifer and the UCCU used for particle tracking. (a) shows the Shallow*
 3 *aquifer and the UCCU at the cross section. (b) shows the plan view of the cross section. Particles are placed on top of the*
 4 *groundwater in the shallow aquifer and top of the UCCU in 2005 (Green mark). Forward particle tracking shows the transport*
 5 *of the particles within the layers (blue line) and the position of each particle at the end of simulation in 2015 (Red mark).*

6 Figure-12(a) shows placement of north-south cross-section B-B' of the Shallow aquifer
 7 and UCCU that is shown in context in Figure-12(b). Cross-section B-B' intersects the bluff at
 8 three points. Figure-12(a) shows a sudden change in particle migration proximal to the bluff due
 9 to hydraulic characteristics differences in alluvial and fluvial deposits at either side of the bluff
 10 line. Particles at the southern part of the cross-section B-B' transport further at depth from 2005
 11 to 2015, compared with particles at the northern part of the cross-section.

12

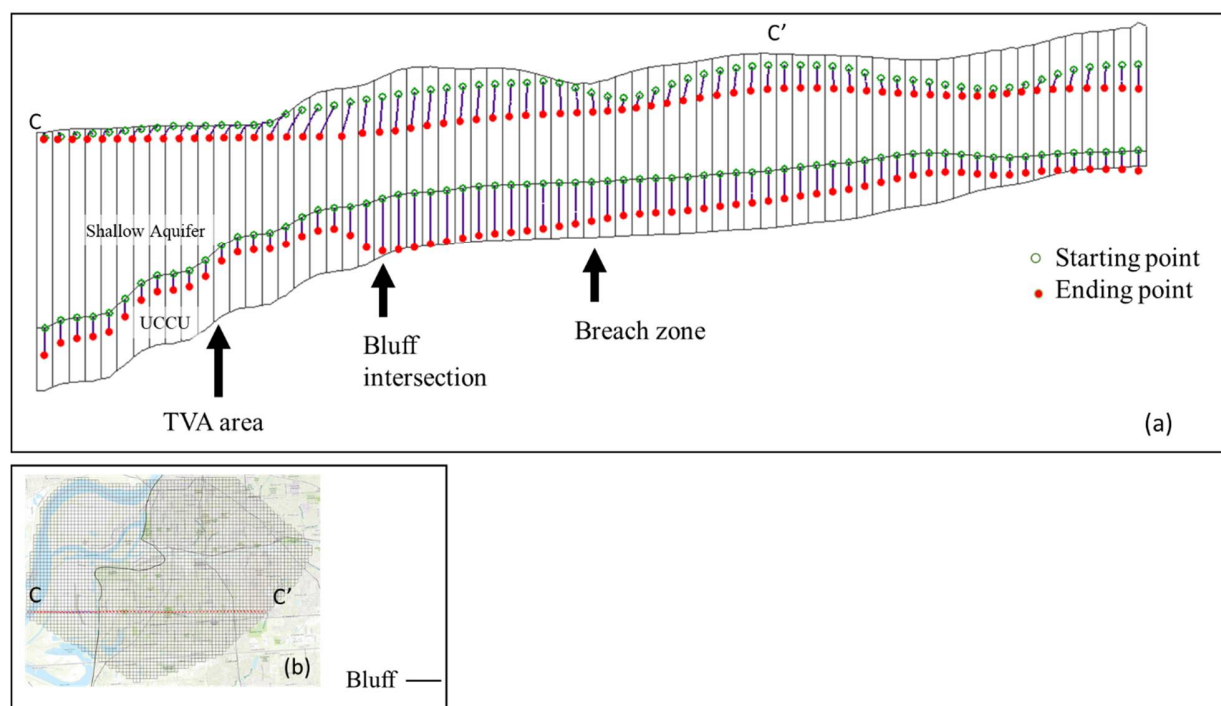
13



1

2 *Figure-12 B-B' cross section of the shallow aquifer and the UCCU showing particle tracking results. (a) Cross-section of the*
 3 *shallow aquifer and the UCCU along B-B'. Particles are placed on top of the groundwater in the shallow aquifer and top of the*
 4 *UCCU in the year of 2005 (Green mark). Forward particle tracking shows the transport of the particles within the layers (blue*
 5 *line) and the position of each particle at the end of the simulation in 2015 (Red mark).*

6 Figure-13(a) shows cross-section C-C' of the Shallow aquifer and UCCU, an east to west
 7 transect of the study area that is shown in context in Figure-13(b). The cross-section intersects the
 8 bluff at one point. Similarly, we place imaginary particles on the Shallow aquifer and top of UCCU
 9 in the year of 2005 (green marks). Forward particle tracking represents the location of each particle
 10 in 2015 (red marks). Same as cross-section A-A', an abrupt change is observed at the bluff;
 11 however, PPT results show a relatively high interaction between layers adjacent the bluff line. As
 12 shown in Figure-13(a), PPT shows no sign of a breach at the TVA area. However, there is a broad
 13 area east of the bluff where particles transport paths are relatively long. Therefore, there is a high
 14 possibility for the presence of a breach in this area.



1

2 *Figure-13 C-C' cross section of the shallow aquifer and the UCCU showing particle tracking results. (a) Cross-section of the*
 3 *shallow aquifer and the UCCU along C-C'. Particles are placed on top of the groundwater in the shallow aquifer and top of the*
 4 *UCCU in the year of 2005 (Green mark). Forward particle tracking shows the transport of the particles in the layers (blue line)*
 5 *and the position of each particle at the end of simulation in 2015 (Red mark).*

6 **3.3.1 Validation of PT results**

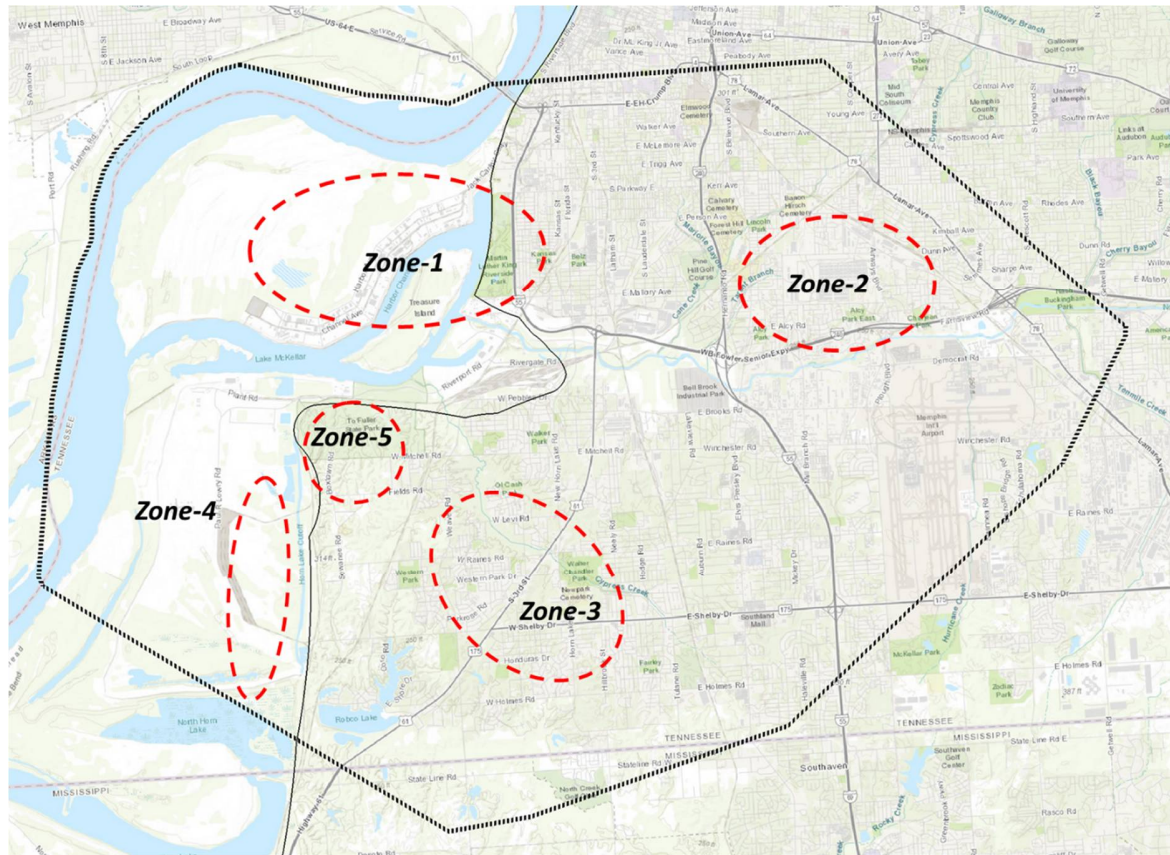
7 PT results confirm all the zones identified by PPC and VFB analyses. The results show that
 8 the particles in the President's Island and MDIP transport locally further which is consistent with
 9 previous studies (Parks, 1990; Narsimha, 2007; Bradshaw, 2011) in these areas. PT shows that
 10 particles in the TVA area transport slowly downward except adjacent the bluff line. This finding is
 11 consistent with a recent study (Carmichael et al., 2018). However, similar to PPC analysis, there
 12 is an undiscovered area in the southern part of the study area where PT identifies it as the locations
 13 where the presence of breaches is likely.

14 **4 Summary and Conclusion**

15 The Memphis aquifer is the primary drinking water source in the Shelby County
 16 (Tennessee, USA), and supplies industrial, commercial, and residential water. Memphis aquifer is
 17 one of several deep sand aquifers separated from the Shallow aquifer by a clayey confining layer,
 18 UCCU. All of the production wells in the Memphis area are screened in the Memphis aquifer or
 19 even deeper in Fort Pillow aquifer to avoid Shallow aquifer contamination. Traditionally, the

1 public water supply authority in the Memphis area assumed that the UCCU could fully protect the
2 water in the Memphis aquifer from downward leakage of the contaminated or poor-quality
3 groundwater from overlying Shallow aquifer. However, recent studies show that at some locations
4 the UCCU is thin or absent which leads to the contribution of water from the Shallow aquifer to
5 the Memphis aquifer (Parks, 1990; Larsen et al., 2003, 2013, 2016). Hence, sustainable water
6 management in the Memphis area requires locations of breaches in the UCCU to ensure protection
7 of water pumped from the production wells. Locating breaches demands expensive geological or
8 geochemical investigations. These studies are even more costly and complicated in densely
9 developed urban areas. Therefore, other techniques are desired that can help determine the
10 locations of breaches so that complicated and costly field investigations can be focused in limited
11 areas.

12 In this study, to identify the locations where the presence of breaches in the UCCU is likely
13 we use three different analyses: (1) pilot point calibration (PPC), (2) velocity and flow budget
14 (VFB), and (3) particle tracking (PT). As shown in Figure-14, these approaches identify five zones
15 where the presence of breaches is expected. As summarized in Table-1, all three approaches
16 distinguish Zone-1, 2, and 3 from other parts of the study area. However, VFB does not identify
17 Zone-4 and 5 as the locations of possible breaches. Previous investigations results are concurrent
18 with this study in that the presence of breaches in Zone 1, 2, and 4 is likely. These findings validate
19 the reliability of the numerical model. However, the presence of breaches in Zone 3 and 5 have
20 never been explored and need further investigation. Five zones identified in this study are
21 reasonable candidates for the future field investigations based on the current understanding of the
22 study area. The results of this study can reduce the cost and increase the efficiency of investigations
23 all over the broad study area, by directing future studies.



1
2 Figure 14 shows five zones identified by PPC, VFB and PT where further field investigations are required.

3 Table-1 summarizes the PPC, VFB and PT analyses identified zones.

	Typ of analysis			Is it consistent with previous investigations?
	PPC	VFB	PT	
Zone-1	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	Yes
Zone-2	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	Yes
Zone-3	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	N/A (no previous study)
Zone-4	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>	Yes
Zone-5	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>	N/A (no previous study)

4
5 **5 Acknowledgment**

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7 under the title of Allen Wellfield Evaluation (Contract#11783).

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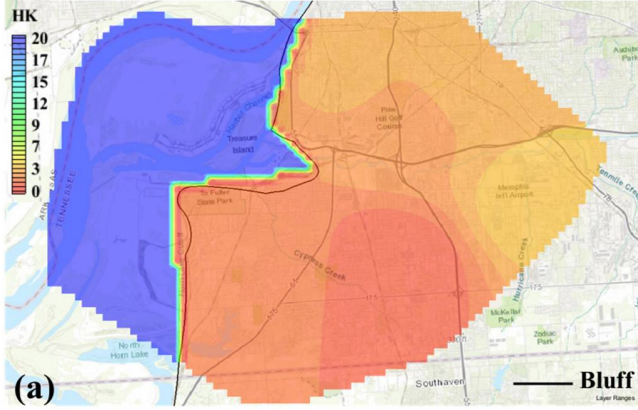
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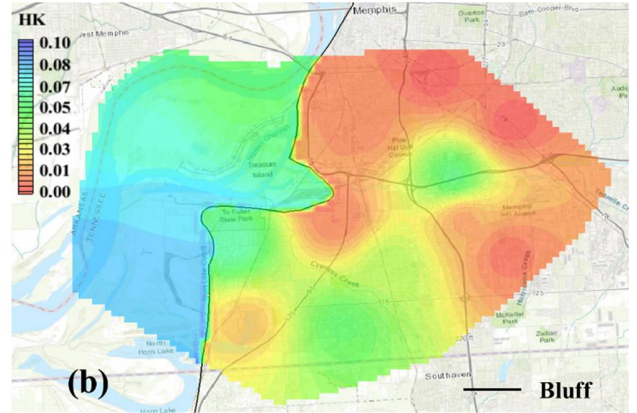
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1 Appendix-1

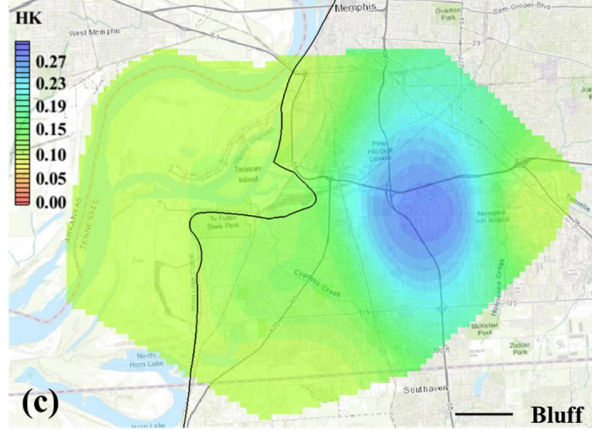
Horizontal Hydraulic Conductivity [m/d] – *Shallow aquifer*



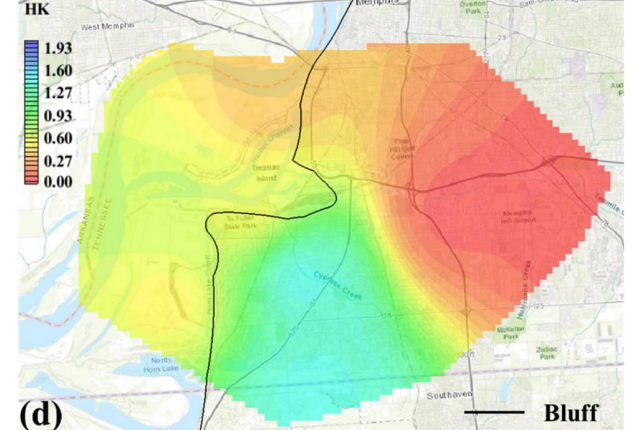
Horizontal Hydraulic Conductivity [m/d] - *UCCU*



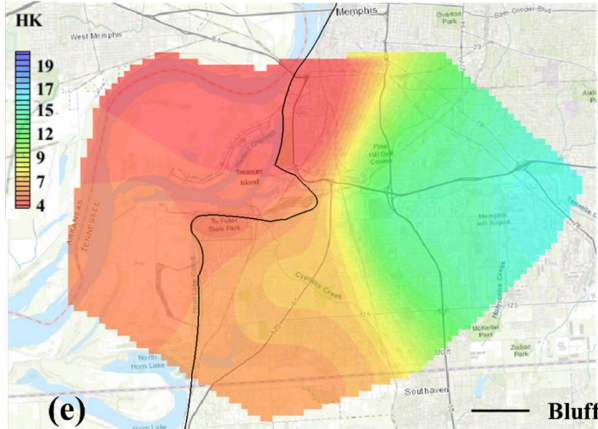
Horizontal Hydraulic Conductivity [m/d]- *Memphis aquifer-layer 1*



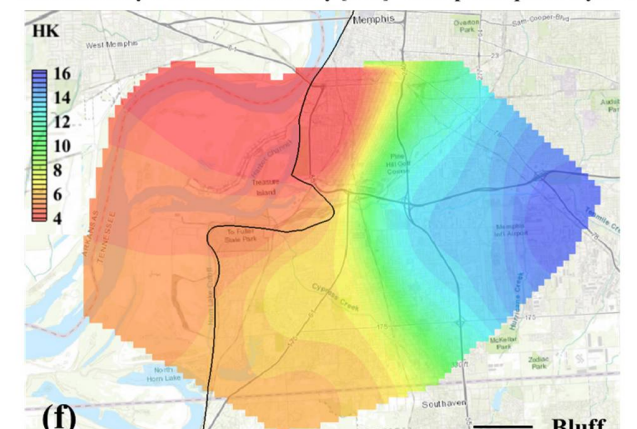
Horizontal Hydraulic Conductivity [m/d] - *Memphis aquifer-layer 2*



Horizontal Hydraulic Conductivity [m/d] - *Memphis aquifer-layer 3*



Horizontal Hydraulic Conductivity [m/d] - *Memphis aquifer-layer 4*



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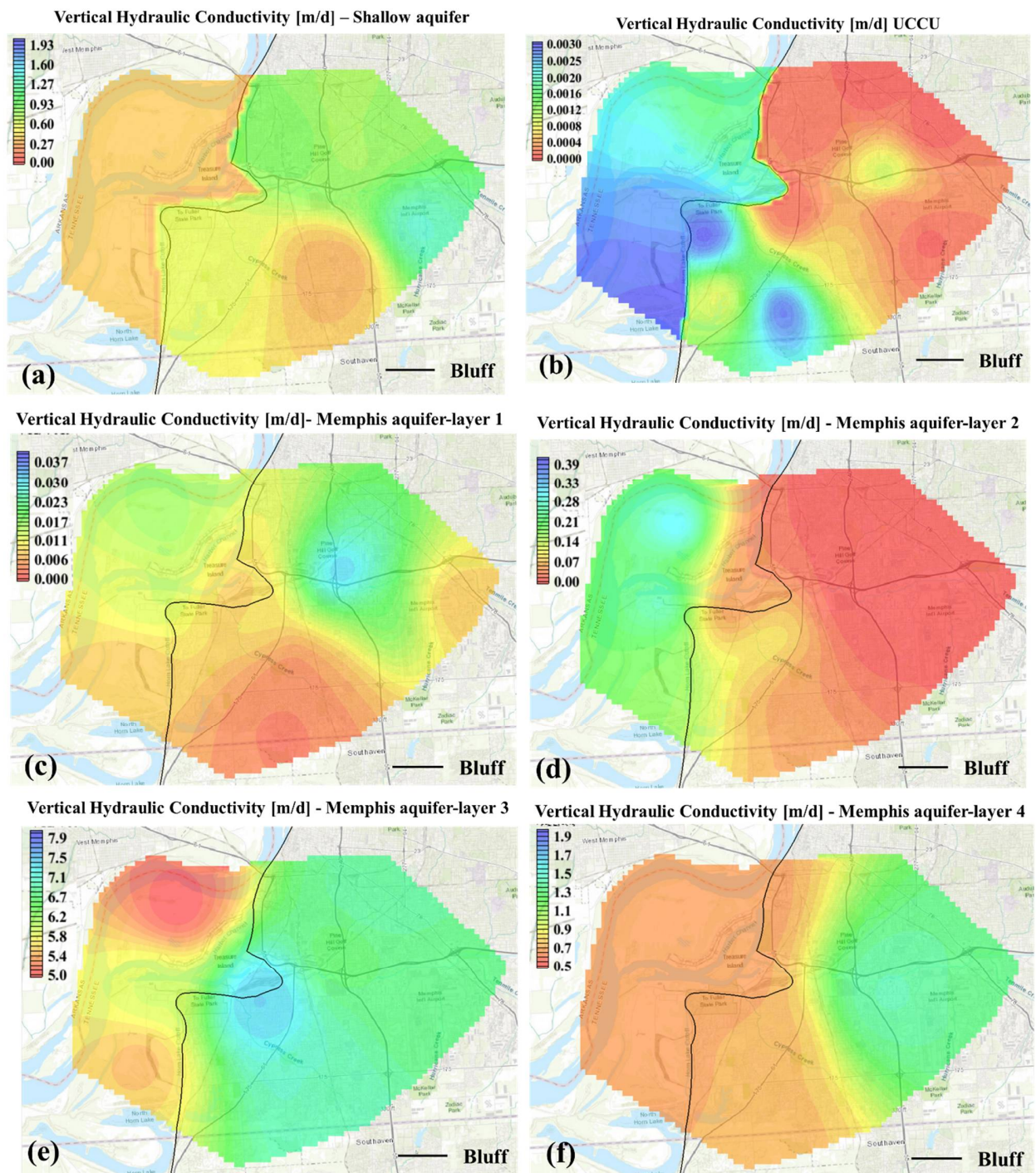
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Figure 15- Figures (a-f) shows the horizontal hydraulic conductivity of each numerical layer.

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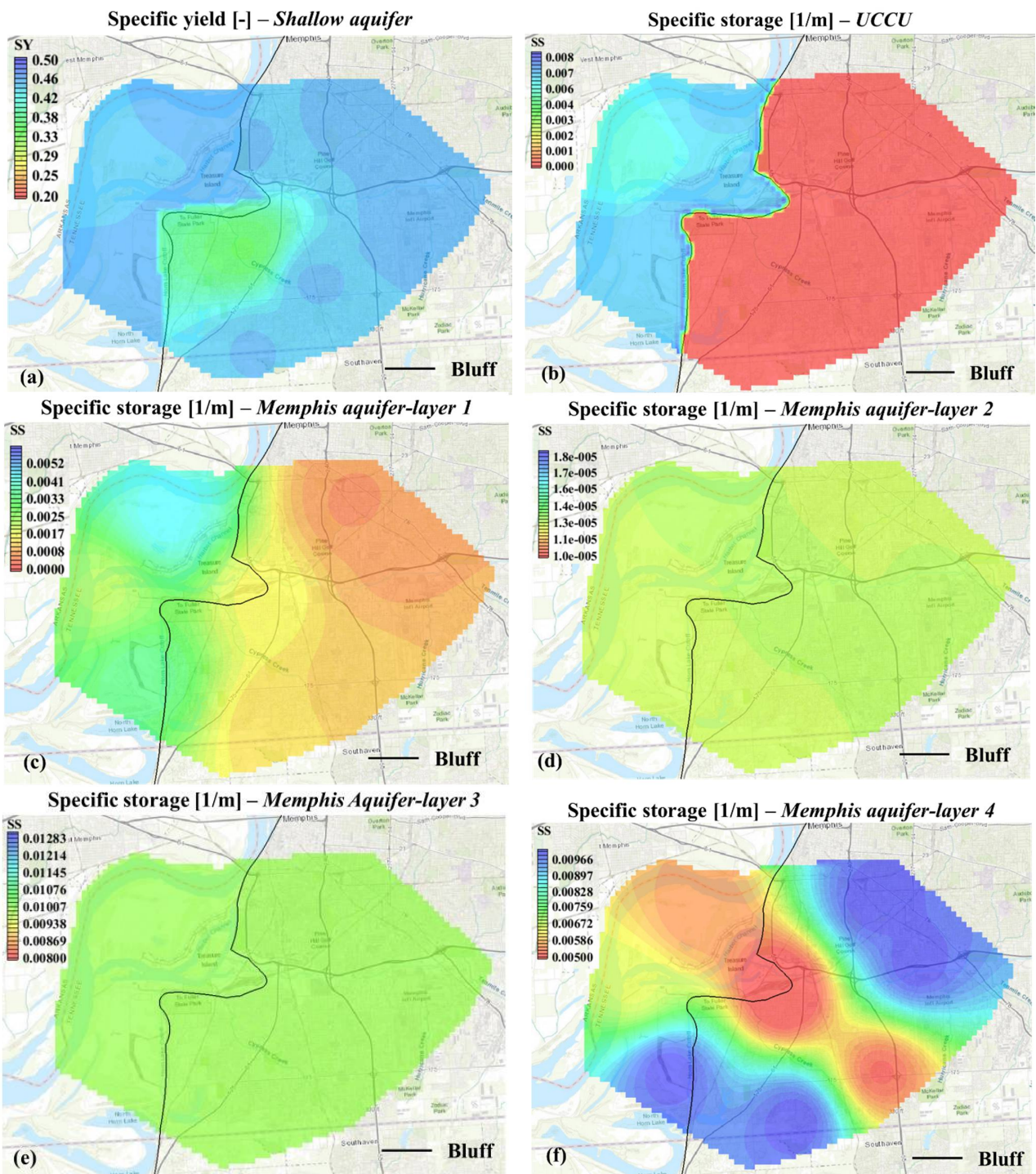


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Figure-16 (a-f) show the vertical hydraulic conductivity of each numerical layer.

1 Appendix-2

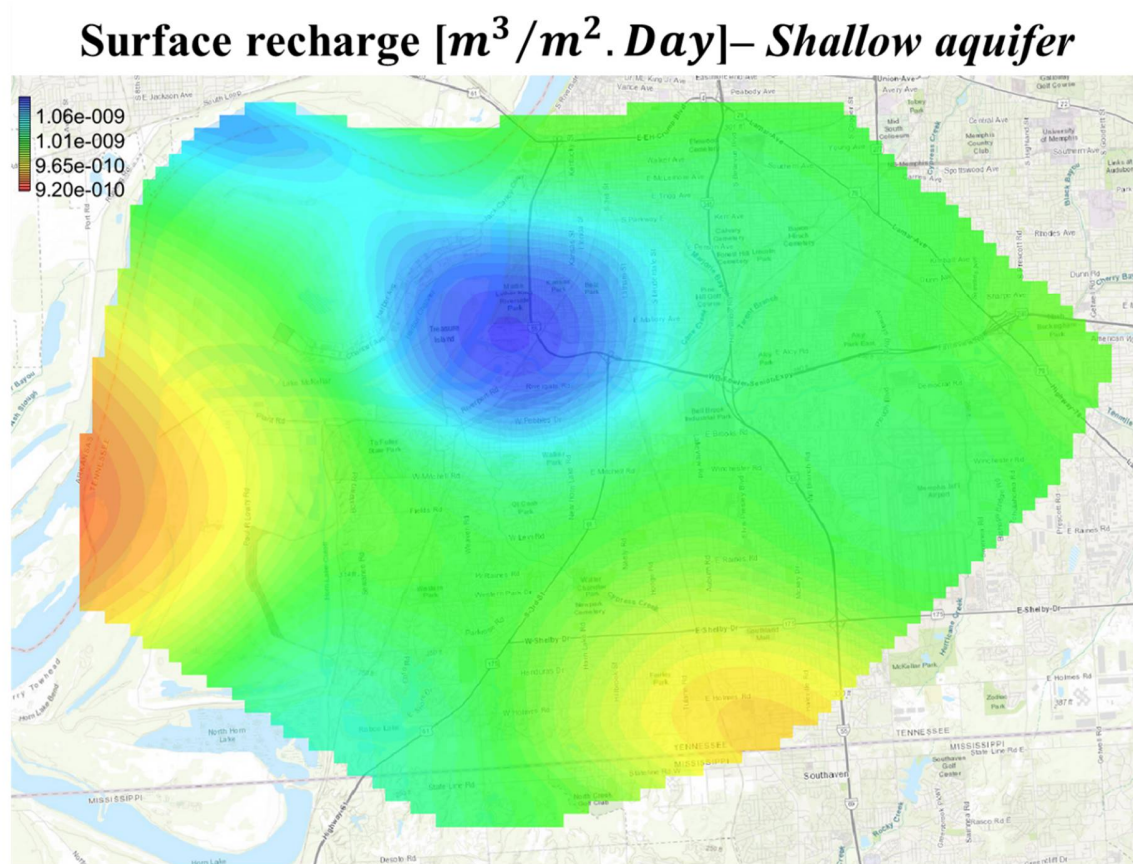


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3 *Figure-17 (a) shows the specific yield coefficient of the Shallow aquifer. Figures-17(b-f) shoes specific storage of UCCU and*
 4 *Memphis aquifer, respectively.*

5

1 Appendix-3



2

3

Figure-18 shows the calibrated surface recharge to the Shallow aquifer.