

1 Article

# 2 The non-uniform and asymmetric thermal radiation upon 3 the human physiological responses in outdoor 4 environment

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13 **Abstract:** Depending on human body conditions and environmental conditions, it is sometimes difficult to  
14 conduct subject experiments. In such cases, it is effective to use a thermal manikin. There are few studies that  
15 investigate the effect of the non-uniform and asymmetric outdoor thermal environment on the mean skin  
16 temperature. The purpose of this study is to clarify the influence of the non-uniform and asymmetric thermal  
17 radiation of short-wavelength solar radiation in an outdoor environment on the calculation of the mean skin  
18 temperature. The skin temperature of the front of the coronal surface, which was facing the sun and where the  
19 body received direct short-wavelength solar radiation, and the skin temperature of the rear of the coronal  
20 surface, which was in the shadow and did not receive direct short-wavelength solar radiation were respectively  
21 measured. The feet, upper arm, forearm, hand and lower leg, which are susceptible to short-wavelength solar  
22 radiation in a standing posture, had a noticeable difference in skin temperature between sites in the sun and in  
23 shade. The mean skin temperature of sites facing the sun was significantly higher than the mean skin  
24 temperature of those in the shade.

25 **Keywords:** Asymmetry; Mean skin temperature; Non-uniform; Outdoor environment; Physiological  
26 response; Skin temperature; Solar radiation

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## 28 1. Introduction

29 To examine the heat exchange between the human body and the environment, subject  
30 experiments are effective. However, depending on human body conditions and environmental  
31 conditions, it is sometimes difficult to conduct subject experiments. In such cases, it is effective to  
32 use a thermal manikin or a numerical thermal manikin.

33 With these methods using thermal manikins, correspondence between heat generation and  
34 heat dissipation of the human body and of the thermal manikin is not clear. In addition, in the  
35 numerical thermal manikin, human body shape, boundary condition, various coefficient values are  
36 not clear. The thermal manikin is a heat dummy for reproducing the heat transfer characteristics of  
37 human beings. Therefore, it is possible to evaluate the thermal environment without burdening the  
38 human body. The thermal manikin has become an indispensable item to evaluate the thermal  
39 environment.

40 An extremely large number of laboratory experiments on subjects assume the thermal  
41 environment to be in a homogeneous and uniform steady state. However, the ordinary indoor  
42 environment is thermally non-uniform, asymmetrical and nonstationary. In addition, the physical

43 thermal environmental factors fluctuate greatly in the outdoor environment, which is in an  
44 unsteady state. In evaluating the outdoor environment, the psychological reaction of the human  
45 body is made the focus, and research quantitatively dealing with the heat balance of the human  
46 body is rare. The only studies that quantitatively investigate the influence on the human body using  
47 comprehensive thermal environment evaluation indices based on the heat balance of the outdoor  
48 environment as the axis of evaluation are those by Kurazumi et al. [1-8].

49 The outdoor thermal environment, short-wavelength solar radiation, long-wavelength thermal  
50 radiation and the air current are non-uniform and asymmetric evaluation factors. These may  
51 contribute as a local effect on the human body, even if the heat balance in the whole human body is  
52 the same. As pointed out by Kurazumi et al. [4, 7, 8], the influence of these environmental  
53 parameters may cause variation in the response of the human body. The human body may  
54 experience discomfort due to changing environmental factors, and so this experience can be  
55 thought to induce the condition of relative comfort. Accordingly, changes with an effect that  
56 mitigates thermal function are considered to be variables for discomfort with regard to other  
57 environmental factors also. That is, the degree of conscious awareness of thermal environmental  
58 factors may have an influence.

59 Horikoshi et al. [9] and Kurazumi et al. [10], who conducted heterogeneous and asymmetric  
60 subject experiments in an indoor environment, demonstrate that the psychological reactions of the  
61 human body in a heterogeneous and asymmetric thermal radiation environment have directionality  
62 under the effect of local thermal radiation, and that these psychological reactions change. Kurazumi  
63 et al. [11] demonstrate that a parameter exists for the heterogeneous and asymmetric thermal  
64 environmental factors in the thermal environment evaluation index that evaluates the effect on the  
65 human body in a heterogeneous and asymmetric thermal radiation environment. They show that  
66 there is a large spread in the response of the human body due to the effect of this parameter. That is,  
67 the spread in thermal sensory perception becomes large in outdoor spaces due to the influence of  
68 environmental stimuli in addition to the psychological response to thermal action in the outdoor  
69 space.

70 The thermal environment evaluation index based on the heat balance of the human body in the  
71 outdoor environment uses representative values of individual thermal environment factors as  
72 evaluation values. The change factor is handled by using a moving average value, and the  
73 non-uniform factor by using a weighted average value such as mean radiant temperature. However,  
74 although the mean skin temperature of the human body is a representative value of the local  
75 environment, studies investigating the effect of short-wavelength solar radiation in the outdoor  
76 environment are rare.

77 The mean skin temperature, which is the representative value for skin temperature, is used to  
78 calculate the amount of heat exchange between the human body and the environment. Since skin  
79 temperature is not uniform over the whole body surface, it is assumed that it is uniform within a  
80 given site of the body surface and the mean skin temperature is considered to be the skin  
81 temperatures averaged by the area of the surfaces as a proportion of the total surface area of the  
82 body. That is, the mean skin temperature calculation formula has been devised assuming that the  
83 skin temperature is almost uniform on the body surface.

84 Studies on the method for calculating the mean skin temperature deal with the physiological  
85 mean skin temperature and thermal conduction mean skin temperature. There are various

86 measurement points and measurement sites for skin temperature, and considering the relationship  
87 between the human body and the surrounding environment, it is necessary to determine the sites  
88 judged to be affected by the surrounding environment and the distribution of skin temperature.  
89 The more skin temperature measurement scores corresponding to the skin temperature distribution  
90 are used, the smaller the skin temperature distribution within the body surface section becomes.  
91 Therefore, each representative skin temperature approximates the most probable value as the  
92 representative section value, and the accuracy of the mean skin temperature calculation is improved.  
93 However, it is difficult and impractical to actually measure a large number of measurement points.  
94 So far, six types of mean skin temperature calculation method have been proposed as follows.

95 Studies proposing a mean skin temperature calculation method based on the total surface area  
96 weighting of the body surface section divide the distribution of the skin temperature expressed on  
97 the body surface in a certain range and make a weighted average of the section representative skin  
98 temperatures according to the ratio of the section body surface area to the total body surface area  
99 [12-29]. The characteristics of the research vary according to the number of sections and the  
100 selection of the representative skin temperature of the section. However, the skin temperature of  
101 body surfaces in mutual contact and body surfaces in contact with the floor surface are not  
102 considered. That is, the body is assumed to be spread such that there is no contact between body  
103 surfaces and to be standing in a state as if it were floating in air. Depending on the method of  
104 selecting the body surface section and representative skin temperature, these studies can find it  
105 difficult to cope with the local skin temperature distribution.

106 Studies that propose a mean skin temperature calculation method based on the convective heat  
107 transfer area weighting of the body surface section of the human body [30, 31] divide the  
108 distribution of the skin temperature expressed on the body surface by a certain range, and make a  
109 weighted average of the section representative skin temperatures by the ratio of the heat section  
110 transfer area to the total convective heat transfer area. Kurazumi et al. [30] shows a mean skin  
111 temperature calculation formula for the postures of standing position and chair seated position.  
112 Kurazumi et al. [31] shows a mean skin temperature calculation formula for standing, chair seated,  
113 seiza seated, cross-legged seated, sideways seated, both-knees-erect seated, leg-out seated, lateral  
114 and supine positions. Kurazumi et al. [30] investigates the method of calculating the mean skin  
115 temperature by the total surface area weighting of the human body surface section in a uniform  
116 thermal environment where the air temperature and wall temperature are equal, and examines the  
117 difference with the mean skin temperature given by the mean skin temperature calculation method  
118 based on the convective heat transfer area weighting. In a living environment where various  
119 postures are assumed, it is necessary to distinguish the mean skin temperature calculation method  
120 according to the posture. By considering the convective heat transfer area, the study clarifies that  
121 the influence of the skin temperature of a limb can be expressed in terms of the mean skin  
122 temperature in both the standing and chair seated positions. This calculation method focuses on the  
123 heat transfer area based on heat transfer theory and may be considered to cope with a non-uniform  
124 environment.

125 Studies that propose a mean skin temperature calculation method based on the total surface  
126 area weighting of the human body surface section and the conductive heat transfer area weighting  
127 between the body and the floor etc. [32-38] divide the distribution of the skin temperature  
128 expressed on the body surface by a certain range, and make a weighted average of the section

129 representative skin temperatures by the ratio of the section body surface area to the total body  
130 surface area. This calculation method deals with the local skin temperature distribution by contact  
131 heat conduction. Mean skin temperature calculation formulas are given for standing, chair seated,  
132 seiza seated, cross-legged seated, sideways seated, both-knees-erect seated, leg-out seated, and  
133 lateral positions in Kurazumi et al. [37, 38]. This calculation method focuses on the heat transfer  
134 area based on heat transfer theory and may again be considered to cope with a non-uniform  
135 environment.

136 Further research by Kurazumi et al. [39] developed the above concept of a weighting  
137 coefficient for the heat transfer area. A mean skin temperature calculation method is proposed by a  
138 weighting of the convective heat transfer area, the radiative heat transfer area, and the conductive  
139 heat transfer area of the human body surface section. They show a mean skin temperature  
140 calculation formula for standing, chair seated, seiza seated, cross-legged seated, sideways seated,  
141 both-knees-erect seated, leg-out seated, lateral and supine positions. This calculation method  
142 focuses on the heat transfer area based on heat transfer theory and may also be considered to cope  
143 with a non-uniform environment.

144 In studies proposing a mean skin temperature calculation method based on the total surface  
145 area weighting of the human body surface section and the local convective heat transfer coefficient  
146 for the section [40-44], this was obtained from an equation for the body heat balance between the  
147 human body and the surrounding environment. The local convective heat transfer coefficient of  
148 each body surface section is found from a cylindrical model or thermal manikin. In deriving the  
149 body heat balance equation, it is assumed that the entire surface of the body is involved in heat  
150 exchanges through convection, radiation, and evaporation. However, even in a relatively open  
151 standing posture, there is some contact between body surfaces, and these surfaces are not involved  
152 in heat exchange with the environment surrounding the body. Especially in a seated or decubitus  
153 position etc., where there is a lot of contact between the body surface and the floor, the discrepancy  
154 with the actual situation is significant.

155 One study [45] that proposes a mean skin temperature calculation method based on the total  
156 surface area weighting and the skin temperature sensation of the surface section of the human body,  
157 suggests that temperature sensation is related to the expression of skin temperature. In this study, a  
158 perspiration ratio is used for temperature sensation. Representative perspiration amounts and  
159 representative skin temperatures for each body surface section of the body in a supine position  
160 exposed to a high temperature environment of 30 °C or more were measured, and the ratio of the  
161 difference in the perspiration amount of each section and the thigh with respect to the difference  
162 between the mean skin temperature calculated by the skin temperature and body surface area  
163 weighting for each section is regarded as the skin temperature sensation coefficient. The ratio of the  
164 skin temperature sensation coefficient of each section to the skin temperature sensory coefficient of  
165 the thigh is used as the weighting for calculating the mean skin temperature. Since the amount of  
166 perspiration of the human body in a high air temperature environment is the basis of calculation,  
167 the high air temperature environment is considered to be the applicable range. Therefore, caution is  
168 necessary when this method is used under conditions significantly different from the assumed  
169 thermal environment.

170 A study proposing a mean skin temperature calculation method based on the total surface area  
171 weighting of the body surface section and the local convective heat transfer coefficient and the skin

172 temperature sensation for that section of the human body [46] combined the local convective heat  
173 transfer coefficient for the human body obtained from an equation for body heat balance with the  
174 weighting coefficient of Nadel et al. [45]. Since this research has research application limits that are  
175 a factor in deriving the weighting coefficient, attention is necessary when using the method with  
176 postures where the contact surface of the body surface is large or in other than a high air  
177 temperature environment.

178 The mean skin temperature calculation formula must be selected according to the application,  
179 such as whether the calculated mean skin temperature is used as a monitor of physiological  
180 response or applied to the body heat balance equation for the human body. In indoor environments  
181 and shady outdoor environments, there is little influence of short-wavelength solar radiation, so a  
182 strikingly non-uniform and asymmetric environment is not formed. In an outdoor environment,  
183 however, some parts of the body have shaded sites and sites facing the sun, and a remarkable  
184 difference in skin temperature is considered to occur under the influence of the short-wavelength  
185 solar radiation.

186 The thermal manikin body is divided into several sections from the head to the lower limb, so  
187 there is a possibility that the thermal manikin can estimate the heat exchange between the  
188 non-uniform and asymmetric thermal environment and the human body. If we know the heat  
189 transfer characteristics and the sensational and physiological temperature of the thermal  
190 environment for each divided part, we can evaluate the influence of the thermal environment on  
191 the human body in detail.

192 Representative body surface division of the human body and of the thermal manikin body are  
193 head, trunk, upper arm, forearm, hand, thigh, lower leg, and foot. The head and trunk may be  
194 further subdivided. Although, it is possible to study the asymmetric difference between the left and  
195 right thermal radiation stimuli received from the thermal environment targeted at the limbs, it is  
196 difficult to consider other non-uniform and asymmetric thermal environments and other body  
197 surface section to be examined.

198 In indoor environments and outdoor environments, there is strong influence of  
199 short-wavelength solar radiation, so a strikingly non-uniform and asymmetric environment is  
200 formed. However, there are few studies that investigate the effect of the non-uniform and  
201 asymmetric outdoor thermal environment on the mean skin temperature of the human body.  
202 Therefore, the present study aimed to clarify the influence of the non-uniform and asymmetric  
203 thermal radiation of short-wavelength solar radiation in an outdoor environment on the calculation  
204 of the mean skin temperature of the human body and on the classification of the body surface  
205 section.

## 206 **2. Experiment design**

### 207 *2.1. Experimental process and measurement items*

208 Experiments were conducted in Bangkok, Thailand at 13° 44' 20" north latitude during the dry  
209 season. For the measurements, the experiment site was selected with consideration for the condition  
210 that short-wavelength solar radiation should not be shielded during the exposure time. Weather  
211 environment elements in outdoor spaces are in a heterogeneous and unsteady state. Focusing on  
212 the influence of short-wavelength solar radiation, the experiment site chosen for the present study  
213 was a place where fluctuations of other weather environmental factors were minimized. A



214 measurement location surrounded by buildings was selected such that the subjects were in an  
215 enclosed space and the fluctuation of airflow was mitigated. The building and the ground surface  
216 were a concrete material with high heat capacity, so the influence of long-wavelength thermal  
217 radiation was strong, but the exposure time frame of 13:00–14:30, where the solar altitude is high  
218 and fluctuation of the surface temperature decreases, was selected.

219 The thermal environment of outdoor spaces can be harsh to the extent that there are cases of  
220 death by heat stroke. Accordingly, extended periods in hot outdoor spaces under short-wavelength  
221 solar radiation must be avoided. Unlike an indoor space, it is difficult to consider spending  
222 extended periods in an outdoor thermal environment that can become uncomfortable due to  
223 behavioral thermoregulation by means of environmental refuge behavior. Therefore, the actual  
224 measurement of the human body response and the thermal environment was carried out in  
225 consideration of the time the subject spent maintaining the standing posture. Naturally, it can be  
226 conjectured that the human body response will differ the longer the exposure time of the subjects,  
227 but the experimental period was determined with consideration for the safety of the subjects.

228 Subjects remained upright and at rest in an outdoor shady space for about 60 minutes including  
229 the time spent attaching sensors, then moved on foot to the selected site. They were then exposed to  
230 the thermal environment in a standing posture for 15 minutes, positioned such that the front of the  
231 coronal plane directly faced the direction of the solar azimuth in a place where short-wavelength  
232 solar radiation was not obstructed.

233 The thermal environment parameters measured were: air temperature, humidity, air velocity,  
234 globe temperature, and short-wavelength solar heat quantity. Temperature, humidity, air velocity  
235 and globe temperature were measured by a portable PMV meter (Kyoto Electronics Manufacturing:  
236 AM-101, air temperature: 0 to 50.0 °C  $\pm$ 0.5 °C, globe temperature: 0 to 50.0 °C  $\pm$ 0.5 °C, mean radiant  
237 temperature: 0 to 50.0 °C, relative humidity: 0 to 100% RH  $\pm$ 3% RH, air velocity: 0 to 1 m/s  $\pm$ 0.1 m/s;  
238 1 to 5 m/s  $\pm$ 0.5 m/s) at a height of 90 cm above the ground. Concerning the short-wavelength radiant  
239 heat quantity from the visible region to the near-infrared region, amounts of downward and  
240 upward solar radiation were measured by a pyranometer (PREDE: PCM-01NL, sensitivity: 7  
241 mV/W/m<sup>2</sup>, wavelength range: 305 nm to 2800 nm).

242 The skin temperature of the human body was measured by a thermistor thermometer (Nikkiso  
243 THERM N542R data logger, measuring range: -50 to 230 °C, resolution: 0.01 °C, and a Nikkiso  
244 THERM body surface temperature probe: ITP8391). The temperature of skin open to airflow was  
245 measured at the eight positions of the head, upper arm, forearm, hand, trunk, thigh, lower leg, and  
246 foot. The skin temperature of the front of the coronal surface, which was facing the sun and where  
247 the body receives short-wavelength solar radiation, and the skin temperature of the rear of the  
248 coronal surface, which was in the shadow and did not receive short-wavelength solar radiation,  
249 were measured. The subjects were wearing T-shirts and shorts, such that the skin temperature  
250 measurement sites were exposed to the surrounding environment. The T-shirts were turned up to  
251 expose the upper arm, abdomen and lumbar area. In order to prevent burns due to heat conduction  
252 from the ground surface, posture was maintained on sandals with a sole thickness of about 1.0 cm.

## 253 2.2. Subjects

254 The subjects were four healthy young males and females. The subjects were age  $21.0 \pm 0.7$  years,  
255 height  $167.7 \pm 5.8$  cm, body weight  $56.7 \pm 7.5$  kg, body surface area  $1.6 \pm 0.1$  m<sup>2</sup>, and BMI  $20.1 \pm 2.6$ ,

**Table 1.** Physical characteristics of subjects.

Subject	Sex	Age	Height (cm)	Weight (kg)	B-area (m <sup>2</sup> )	Rohrer Index	Native place
1	Male	21	165.3	65.0	1.71	23.79	Bangkok
2	Male	22	177.6	60.0	1.74	19.02	Bangkok
3	Female	20	163.0	44.7	1.47	16.82	Bangkok
4	Female	21	165.0	57.0	1.62	20.94	Bangkok

B-area is the calculated body surface area by Kurazumi's formula [48].

$$S=100.315 W^{0.383} H^{0.693} \times 10^{-4} \text{ (Kurazumi et al., 1994)}$$

S: Body surface area [m<sup>2</sup>], W: Weight [kg], H: Height [cm]

BMI is Body Mass Index.

Native place is life region from birth to 2.5 years old time.

256 and they were not considered to have a unique physique. In addition, the subject's height and  
 257 weight are not significantly different from the average of Thai statistical data [47] (Jordan et al.,  
 258 2012). In calculation of the body surface area of the human body, we used a calculation formula of  
 259 Kurazumi et al. [48]. Table 1 shows the subjects' characteristics.

260 In accordance with the Helsinki Declaration [49], the details of the experiment were explained  
 261 to the subjects in advance and their consent for participation in the experiment was obtained.

262 Experiments with subjects measuring physiological quantities as human body reactions are  
 263 rarely performed using a large number of subjects. In addition, it is difficult to perform experiments  
 264 assuming a statistical population. Therefore, although there are few subjects in this study, they are  
 265 considered meaningful as new data.

266 It is rare to perform a subjective experiment that measures physiological quantities according  
 267 to the response of the human body using a large number of subjects. It is difficult to perform an  
 268 experiment that is hypothesized on a statistical population. Accordingly, as only a small number of  
 269 subjects was used in this study, the new data are a significant addition to the literature.

### 270 3. Experimental results

271 The solar altitude on the experimental days was 72.98–55.81° and the solar azimuth was  
 272 211.01–247.07°. The weather during the exposure time was sunny with the sun occasionally  
 273 obscured by clouds. The experiment was set up with the time of exposure to short-wavelength  
 274 direct solar radiation set to 15 minutes, but weather conditions occurred in which the  
 275 short-wavelength solar radiation was completely shielded. Therefore, in the following discussion,  
 276 the elapsed exposure time in which all meteorological observation times were satisfied was  
 277 analyzed as 13 minutes.

278 The temperature during the experiment was  $34.2 \pm 0.4$  °C, relative humidity was  $48.7 \pm 0.9\%$ ,  
 279 air velocity was  $1.9 \pm 0.8$  m/s, globe temperature was  $42.5 \pm 1.4$  °C, horizontal short-wavelength  
 280 solar radiation was  $766.5 \pm 272.7$  W/m<sup>2</sup>, ground surface reflected solar radiation quantity was  $86.1 \pm$   
 281  $36.1$  W/m<sup>2</sup>. The observation area albedo was 10.7%. There was also an exposure time zone in which  
 282 the temperature around the body was higher than the skin temperature.

283 In a normal posture, the body surfaces are in contact with each other at the armpit and inner  
 284 surface of the thigh. In the standing posture, it is possible to proactively assume an open posture  
 285 with respect to the air current. Also, even in a chair seated position, it is possible to be proactively  
 286 open to the air current to some extent by minimizing the contact area between the human body and  
 287 the chair. However, there is still some of the body surface that is not open to the air flow, such as  
 288 contact between the foot and the floor surface (hereinafter "non-convective heat transfer surface").

289 Non-convective heat transfer surfaces exist in many ordinary postures.

290 A weighted average method based on the ratio of the total surface area of the body is used in  
291 the conventional mean skin temperature calculation method. However, considering the above facts,  
292 the calculation of the heat exchange quantity of the body is inaccurate in this conventional method,  
293 since non-convective heat transfer surfaces are included. In terms of heat transfer, the mean skin  
294 temperature used for accurate calculation of the quantity of convective heat exchange between the  
295 body and the environment should be the weighted average given by the area ratio of the convective  
296 heat transfer surface formed by the same skin temperature expressed on the body surface open to  
297 the air flow (hereinafter “convective heat transfer surface”) with respect to the total convective heat  
298 transfer surface (hereinafter “convective heat transfer area ratio”). That is, it is necessary to use a  
299 mean skin temperature calculation method that considers the convective heat transfer area.  
300 Focusing on this point, Kurazumi et al. [30, 39] propose a mean skin temperature calculation  
301 method based on the convective heat transfer area weighting of the body surface section.

302 The present study assumed the perspective of applying the mean skin temperature to the  
303 evaluation of the heat balance of the body and evaluation of the thermal environment. Accordingly,  
304 to calculate the mean skin temperature, the method based on the convective heat transfer area  
305 weighting of the body surface section proposed by Kurazumi et al. [30, 39] was used.

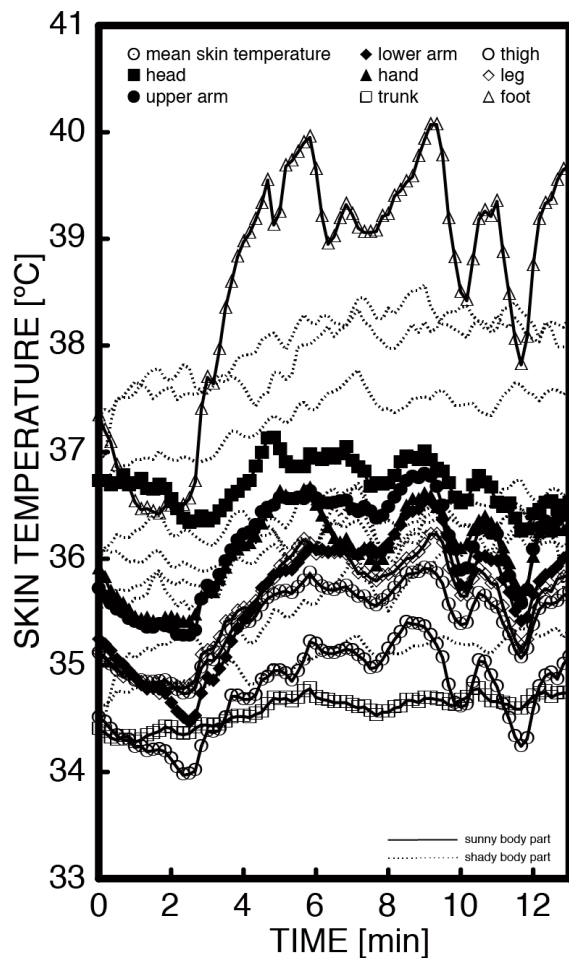
#### 306 4. Discussion

307 Figures 1 and 2 show examples of skin temperature change over time for the same subject  
308 exposed to the outdoor thermal environment for 13 minutes. Figure 1 shows an example of skin  
309 temperature change of the site facing the sun. A fluctuation of skin temperature considered to be  
310 influenced by cooling by perspiration and the influence of changes in air velocity and  
311 short-wavelength solar radiation was observed. Since the altitude of the sun was high and the  
312 subjects were located such that the front of the coronal plane directly faced the direction of the solar  
313 azimuth, the temperature rise is remarkable for the skin of the foot, which is a site susceptible to  
314 solar radiation in the direction normal to the short-wavelength solar radiation. The peak skin  
315 temperature was remarkably high at around 40 °C. Next, the skin temperature of the upper arm,  
316 forearm, hand and lower leg are also considered to be greatly influenced by short-wavelength solar  
317 radiation.

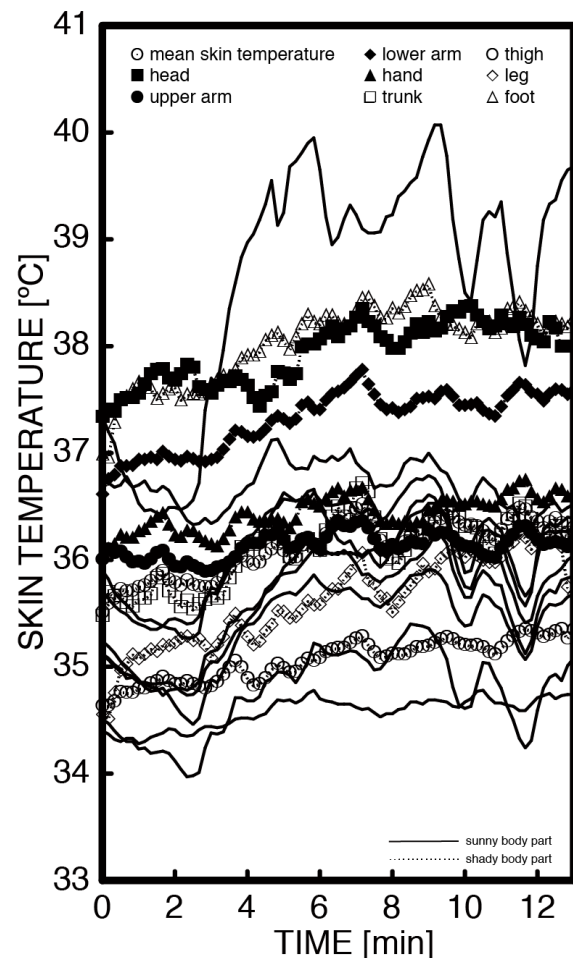
318 Figure 2 shows an example of skin temperature change of the site in the shade. Although this is  
319 for the shaded area of the site shown in Figure 1, a fluctuation of skin temperature considered to be  
320 influenced by cooling by perspiration and the influence of changes in air velocity and  
321 short-wavelength solar radiation was observed in the same way as above. However, it was not a  
322 large fluctuation compared with the skin temperature of sites facing the sun. The skin temperature  
323 of the head, upper arm and foot were extremely high, in excess of 37 °C. The amount of change in  
324 skin temperature of the same site, for which the skin temperature in the part facing the sun was  
325 remarkably high, was increased by about 0.4 °C.

326 Kurazumi et al. [1, 4-8] clarified the influence of reflected solar radiation on the human foot,  
327 and found that both reflected solar radiation and heat conduction from the ground surface  
328 influence the reaction of the human body. However, since the amount of change in the skin  
329 temperature of the foot in the sun and in the shade was significantly different, it is inferred that the  
330 difference in the skin temperature change is strongly influenced by short-wavelength solar





**Figure 1.** Changes of skin temperature exposed to the outdoor thermal environment in the sunny body part.



**Figure 2.** Changes of skin temperature exposed to the outdoor thermal environment in the shady body part.

331 radiation.

332 Figure 3 shows the change in mean skin temperature over time for skin exposed to the outdoor  
 333 thermal environment for 13 minutes. Although there is a slight variation by subject, as described  
 334 above, there was seen to be a fluctuation in the change in mean skin temperature that may have  
 335 been influenced by cooling by perspiration, as well as fluctuations of air velocity and  
 336 short-wavelength solar radiation. However, the overall fluctuation tendency tends to be such that  
 337 the variation in the mean skin temperature of sites facing the sun is higher than the variation at sites  
 338 in the shade, and this variation becomes larger over time. For subjects with the largest difference  
 339 between the fluctuation of mean skin temperature for sites facing the sun 13 minutes after exposure  
 340 and the fluctuation at sites in the shade, this was 1.4 °C. Meanwhile, this was 0.3 °C for the lowest  
 341 subjects.

342 There are very few studies that actually measure the skin temperature of the human body in a  
 343 non-uniform and asymmetric thermal environment. The research of Horikoshi et al. [50] and  
 344 Kurazumi et al. [10, 11] measured the influence on human skin temperature from the perspective of  
 345 a non-uniform and asymmetric thermal environment in an indoor space. The research of Maruyama  
 346 and Tamura [51] measured the influence on human skin temperature from the perspective of sites  
 347 covered by clothing and open to the atmosphere. These studies demonstrate that variations in skin

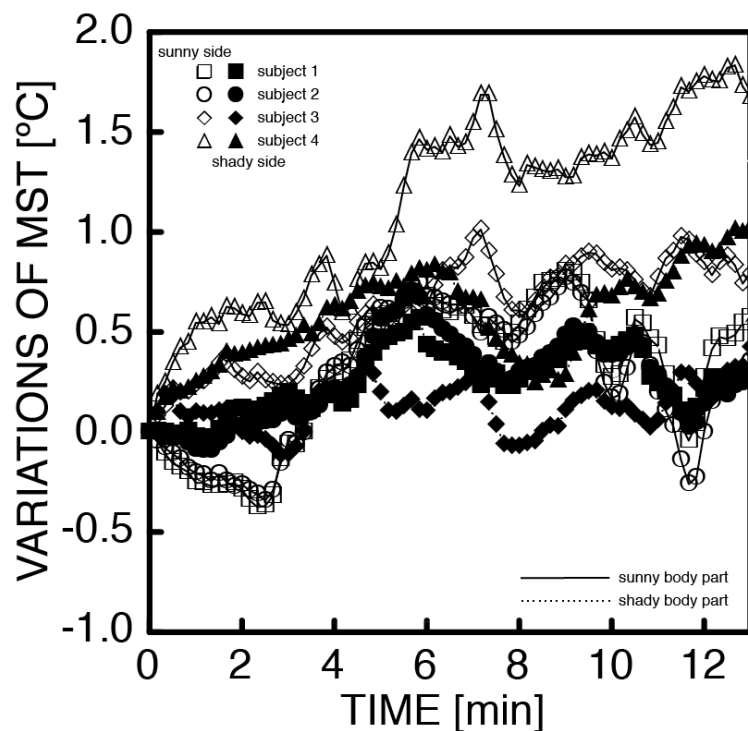


Figure 3. Changes of variation of mean skin temperature.

348 temperature are exhibited in a non-uniform and asymmetric thermal environment according to the  
 349 influence of the local conditions.

350 As a result of investigating the difference between the fluctuation in mean skin temperature in  
 351 sites facing the sun and the fluctuations in sites in the shade, a significant difference of  $p < 0.01$  ( $F =$   
 352 146.1) is shown. Also, as a result of investigating the difference between the fluctuation in mean  
 353 skin temperature in sites facing the sun and the fluctuations in sites in the shade and their  
 354 interaction over exposure time, a significant difference of  $p < 0.01$  ( $F = 51.1$ ) is shown.

355 In an outdoor environment in which the local influence on the human body becomes stronger,  
 356 the tendency for the variation in the skin temperature to become stronger may be more pronounced  
 357 because the thermal radiation environment is more non-uniform and asymmetrical due to short-  
 358 wavelength solar radiation. This suggests that, when clarifying the effect on the human body in an  
 359 outdoor environment, it is necessary to take into account the non-uniformity and asymmetry of the  
 360 skin temperature for sites facing the sun and in the shade. Accordingly, when evaluating the body  
 361 heat balance of the human body and the thermal environment in an outdoor environment, it is  
 362 essential to consider the non-uniformity and asymmetry not only of the physical elements of the  
 363 environment, but also of the skin temperature, which is an element on the side of the human body.

364 In other words, it can be said that the thermal manikin needs to be divided not only in the  
 365 head and trunk but also in the limbs into the anterior part and the posterior part of the coronal  
 366 plane. we can evaluate the influence of the thermal environment on the human body in detail.

## 367 5. Conclusions

368 In an outdoor environment, some parts of the body have shaded sites and sites facing the sun,  
 369 and a remarkable difference in skin temperature is considered to occur under the influence of  
 370 short-wavelength solar radiation. When evaluating the body heat balance of the human body and

371 the thermal environment in an outdoor environment, it is essential to consider the non-uniformity  
372 and asymmetry not only of the physical elements of the environment, but also of the skin  
373 temperature, which is an element on the side of the human body. Therefore, when applying the  
374 mean skin temperature to the body heat balance equation of the human body, it is necessary to  
375 consider the influence of short-wavelength solar radiation.

376 Therefore, the present study aimed to clarify the influence of the non-uniform and asymmetric  
377 thermal radiation of short-wavelength solar radiation in an outdoor environment on the calculation  
378 of the mean skin temperature of the human body and on the classification of the body surface  
379 section.

380 A fluctuation of skin temperature considered to be influenced by cooling through perspiration  
381 and the influence of changes in air velocity and short-wavelength solar radiation was observed. The  
382 temperature of skin when receiving short-wavelength solar radiation due to the positional relation  
383 close to the normal direction was remarkably high at about 40 °C. The feet, upper arm, forearm,  
384 hand and lower leg, which are susceptible to short-wavelength solar radiation in a standing posture,  
385 had a noticeable difference in skin temperature between sites in the sun and in shade. The mean  
386 skin temperature of sites facing the sun was significantly higher than that of those in the shade.  
387 When evaluating the body heat balance of the human body and the thermal environment in an  
388 outdoor environment, it is essential to consider the non-uniformity and asymmetry not only of the  
389 physical elements of the environment, but also of the skin temperature, which is an element on the  
390 side of the human body.

391 The thermal manikin needs to be divided not only in the head and trunk but also in the limbs  
392 into the anterior part and the posterior part of the coronal plane. we can evaluate the influence of the  
393 thermal environment on the human body in detail.

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395 Yoshihito Kurazumi planned the research with Kenta Fukagawa, Tomonori Sakoi, Ariya Aruninta and Ken  
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