## Article

# Geometry of chalcogenide negative curvature fibers for CO<sub>2</sub> laser transmission

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- \* Correspondence: jonathan\_hu@baylor.edu; Tel.: +1-254-710-1853
- Abstract: We study impact of geometry on leakage loss in negative curvature fibers made with
- <sup>2</sup> As<sub>2</sub>Se<sub>3</sub> chalcogenide and As<sub>2</sub>S<sub>3</sub> chalcogenide glasses for carbon dioxide (CO<sub>2</sub>) laser transmission.
- <sup>3</sup> The minimum leakage loss decreases when the core diameter increases both for fibers with six and
- 4 for fibers with eight cladding tubes. The optimum gap corresponding to the minimum loss increases
- <sup>5</sup> when the core diameter increases for negative curvature fibers with six cladding tubes. For negative
- 6 curvature fibers with eight cladding tubes, the optimum gap is always less than 20  $\mu$ m when the core
- <sup>7</sup> diameter ranges from 300  $\mu$ m to 500  $\mu$ m. The influence of material loss on fiber loss is also studied.
- 8 When material loss exceeds 10<sup>2</sup> dB/m, it dominates the fiber leakage loss for negative curvature fiber
- at a wavelength of 10.6  $\mu$ m.
- <sup>10</sup> Keywords: CO<sub>2</sub> lasers; negative curvature fibers; chalcogenide glass; fiber loss; mid-IR

#### 11 1. Introduction

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Carbon dioxide  $(CO_2)$  lasers have been widely used in surgery, medicine, and material 12 processing [1-3]. Step index fibers are commonly used to transmit CO<sub>2</sub> laser light. The nonlinearity 13 in the silica glass limits the transmitted power. Hollow-core fibers have low nonlinearity, because 14 the light is mostly transmitted in air, which does not contribute to the nonlinearity. In addition, it is 15 possible in principle to obtain a lower loss in hollow-core fiber than in step-index fiber because air 16 does not contribute to material loss [4,5]. Recently, hollow-core negative curvature fibers have drawn a 17 large amount of attention due to their attractive properties including low loss, broad bandwidth, and a 18 high damage threshold [6–12]. The delivery of mid-infrared radiation has also been successfully 19 demonstrated using chalcogenide negative curvature fibers for a CO<sub>2</sub> laser at a wavelength of 20 10.6  $\mu$ m [13–15]. Previous study shows that chalcogenide glass should be used for wavelength larger 21 than 4.5  $\mu$ m [16]. The relative simplicity of the negative curvature structure could enable the fabrication 22 of fiber devices for mid-IR applications using non-silica glasses, such as chalcogenide [13–15]. 23

The guiding mechanism in negative curvature fibers is inhibited coupling [10,17,18]. A large 24 amount of research [10,19] has been carried out to determine the impact of the fiber parameters on 25 the leakage loss [20] in negative curvature fibers and then optimize these parameters to minimize 26 the loss. These parameters include the curvature of the core boundary, the number of cladding 27 tubes, the thickness of the tubes, and the nested cladding tubes [17,18,21–24]. By introducing a gap between cladding tubes, the loss can be decreased in negative curvature fibers [24,25]. When the tubes 29 touch, modes exist in the localized node area. A separation between the cladding tubes removes the 30 additional resonances due to the localized node. Fibers with a gap between tubes are also expected to 31 be easier to fabricate, since surface tension would naturally assist to maintain the circular shape of the 32 tubes [22]. On the other hand, when the gap is too big, the core mode can leak through the gaps, which 33 increases the loss in negative curvature fibers [26]. Therefore, an optimum gap exists. The optimal 34 gap corresponding to the minimum loss in a fiber with six cladding tubes is three times as large as 35

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Figure 1. Schematic illustration of negative curvature fibers with (a) six and (b) eight cladding tubes.

the optimal gap in fibers with eight or ten cladding tubes [26]. A larger gap is required to remove the

<sup>37</sup> weak coupling between the core mode and tube modes in a fiber with six cladding tubes [26].

In this paper, we find optimal structures of chalcogenide negative curvature fibers for  $CO_2$  laser

transmission, in which we minimize the loss in the two-dimensional parameter space that consists
of the core diameter and the gap size. In previous studies, the optimum gap was found in negative

<sup>41</sup> curvature fibers with a fixed core diameter [26]. We find that the minimum leakage loss decreases

<sup>42</sup> when the core diameter increases both for fibers with six and for fibers with eight cladding tubes.

<sup>43</sup> The optimum gap increases when the core diameter increases for negative curvature fibers with six

cladding tubes. The optimum gap is always less than 20  $\mu$ m when the core diameter increases for

<sup>45</sup> negative curvature fibers with eight cladding tubes when the core diameter ranges from 300  $\mu$ m to <sup>46</sup> 500  $\mu$ m.

#### 47 2. Geometry

<sup>48</sup> Negative curvature fibers with six and eight cladding tubes have been fabricated by several <sup>49</sup> research groups [17,25,27,28]. Figure 1 shows schematic illustrations of negative curvature fibers with <sup>50</sup> six and eight cladding tubes. The gray regions represent glass, and the white regions represent air. <sup>51</sup> The inner tube diameter,  $d_{tube}$ , the core diameter,  $D_{core}$ , the tube wall thickness, t, the minimum gap <sup>52</sup> between the cladding tubes, g, and the number of tubes, p, are related by the expression:  $D_{core} =$ <sup>53</sup>  $(d_{tube} + 2t + g)\sin(\pi/p) - (d_{tube} + 2t)$  [29]. The wavelength of 10.6  $\mu$ m for a CO<sub>2</sub> laser is used in our <sup>54</sup> simulation.

#### **3.** As<sub>2</sub>Se<sub>3</sub> chalcogenide glass

In this section, we study the loss in negative curvature fibers made with As<sub>2</sub>Se<sub>3</sub> chalcogenide 56 glass. The material loss of 10.6 dB/m for As<sub>2</sub>Se<sub>3</sub> chalcogenide glass is included in the simulation [30]. 57 The tube thickness, t, is fixed at 5.2  $\mu$ m corresponding to the third antiresonance. A glass thickness 58 corresponding to the third antiresonance has been drawn in the past [15]. We first study negative 59 curvature fibers with six cladding tubes. We define  $d_{6max}$  as the maximum possible tube diameter for 60 the fiber with 6 cladding tubes, which equals  $D_{core} - 2t$ . Figure 2(a) shows the contour plot of loss as a 61 function of core diameter,  $D_{\text{core}}$ , and normalized tube diameter,  $d_{\text{tube}}/d_{\text{6max}}$ . For a fixed  $D_{\text{core}}$ , the loss 62 decreases and then increases when  $d_{tube}/d_{6max}$  increases from 0.2 to 1.0. The minimum loss occurs 63 when  $d_{\text{tube}}/d_{6\text{max}} = 0.62$ , and it does not change when  $D_{\text{core}}$  increases from 300  $\mu$ m to 500  $\mu$ m. The loss 64 decreases when  $D_{core}$  increases. In addition, we show the loss as a function of the core diameter,  $D_{core}$ , 65 and the gap, g, in Fig. 2(b). The loss first decreases and then increases as the gap, g, increases. When 66 there is no gap, a mode exists in the node that is created by the two touching tubes [25]. When the gap 67 is too large, core mode leaks through the gap [17,26]. We also plot the loss as a function of gap, g, for 68



**Figure 2.** (a) Contour plot of loss as a function of core diameter and normalized tube diameter. (b) Contour plot of loss as a function of core diameter and gap. The number of cladding tube is six.



**Figure 3.** (a) Loss as a function of gap in fibers with different core diameters. (b) Minimum loss and the corresponding optimum gap in fibers with different core diameters. The number of cladding tube is six.

different core diameters in Fig. 3(a). In order to quantify the minimum loss and the corresponding 69 optimum gap for different core diameters, we also plot the minimum loss and the corresponding 70 optimum gap, g, using blue solid curve and red dashed curves, respectively, in Fig. 3(b). When the 71 core diameter increases from 300  $\mu$ m to 500  $\mu$ m, the minimum loss decreases by more than one order 72 of magnitude and the corresponding optimum gap, g, increases from 60  $\mu$ m to 90  $\mu$ m. Hence, a larger 73 gap is needed for a fiber with a larger core diameter to lower the loss in negative curvature fibers with 74 six cladding tubes. 75 We next carry out the same loss analysis on negative curvature fibers with eight cladding tubes. 76 Figure 4(a) shows the contour plot of loss as a function of core diameter, D<sub>core</sub>, and normalized tube 77 diameter,  $d_{tube}/d_{8max}$ , where  $d_{8max}$  is defined as the maximum possible tube diameter for the fiber 78 with 8 cladding tubes, which is  $\{D_{core}\sin(\pi/8) - 2t[1 - \sin(\pi/8)]\}/[1 - \sin(\pi/8)]$  [31]. Figure 4(b) 79

shows the contour plot of loss as a function of core diameter,  $D_{core}$ , and gap, g. The minimum loss

occurs at a larger value of  $d_{tube}/d_{8max}$ , or a smaller value of g, than is the case for negative curvature

<sup>82</sup> fibers with six cladding tubes. In Fig. 5(a), we show the loss as a function of the gap, g, for different



**Figure 4.** (a) Contour plot of loss as a function of core diameter and normalized tube diameter. (b) Contour plot of loss as a function of the core diameter and gap. The number of cladding tube is eight.



**Figure 5.** (a) Loss as a function of the gap in fibers with different core diameters. (b) Minimum loss and the corresponding gap in fibers with different core diameters. The number of cladding tubes is eight.

core diameters. The optimum gap corresponding to the minimum loss is less than 20  $\mu$ m for fibers with 83 different core diameters and the loss increases slowly when gap further increases. The minimum loss 84 and the corresponding gap, g, are plotted using blue solid curve and red dashed curves, respectively, 85 in Fig. 5(b). The minimum loss decreases by around one order of magnitude when the core diameter 86 increases from 300  $\mu$ m to 500  $\mu$ m. Different from fibers with six cladding tubes, the corresponding 87 optimum gap, g, is much smaller and is always less than 20  $\mu$ m when the core diameter increases from 88 300  $\mu$ m to 500  $\mu$ m in fibers with eight cladding tubes. There is a wide range of gaps that realize low 89 loss in the fibers with eight cladding tubes, as shown in Fig. 5(a). The loss is less sensitive to the gap in 90 the region between 10  $\mu$ m and 50  $\mu$ m. Since the tube diameter is much smaller than the diameter of 91 core, the coupling between the core mode and tube modes is weak. A larger gap is needed for fibers 92 with six cladding tubes to remove the weak coupling between the core mode and cladding tube modes 93 in negative curvature fibers with six cladding tubes. 94

eer-reviewed version available at Fibers 2018, 6, 74; doi:10.3390/fib60400

#### **4.** As<sub>2</sub>S<sub>3</sub> chalcogenide glass

In this section, we carried out the same loss analysis in negative curvature fibers made with  $As_2S_3$ 96 chalcogenide glass. The material loss of 500 dB/m for As<sub>2</sub>S<sub>3</sub> chalcogenide glass is included in the 97 simulation [15,16]. The tube thickness, t, is fixed at 6.1  $\mu$ m corresponding to the third antiresonance. 98 Figure 6(a) shows the loss as a function of gap, g, when the core diameter increases from 300  $\mu$ m to 99 500  $\mu$ m in As<sub>2</sub>S<sub>3</sub> chalcogenide fiber with six cladding tubes. Compared with the loss in Fig. 3(a), the 100 losses in the fiber using  $As_2S_3$  chalcogenide glass, shown in Fig. 6(a), are higher and have a flatter 101 minimum. In Fig. 6(b), we show the minimum loss and the corresponding gap, g, as blue solid curve 102 and red dashed curve, respectively. We also study the fiber leakage loss with and without material loss 103 in an  $As_2S_3$  chalcogenide fiber with six cladding tubes. In Fig. 7(a), we show the results in order to 104 explain the broad, low-loss region in Fig. 6(a). The core diameter is fixed at 300  $\mu$ m. The solid curve 105 shows the fiber loss with material loss of 500 dB/m for  $As_2S_3$  chalcogenide glass, which is the same as 106 the blue solid curve in Fig. 6(a). The dashed curve shows the fiber loss without material loss, which 107 is similar to the curve in Fig. 3(a). The high material loss of As<sub>2</sub>S<sub>3</sub> chalcogenide glass dominates and 108 leads to a flat minimum in the fiber loss curve, as shown by the blue solid curve in Fig. 7(a). 109

In order to better illustrate the influence of the material loss on the total fiber loss, we study the 110 fiber loss as a function of material loss both for As<sub>2</sub>S<sub>3</sub> chalcogenide glass and As<sub>2</sub>Se<sub>3</sub> chalcogenide 111 glass, shown in Fig. 7(b) as the red dashed and blue solid curves, respectively. The core diameter 112 is 300  $\mu$ m and the gap is 60  $\mu$ m. The fiber loss changes little when the material loss increases from 113 0.1 dB/m to 10 dB/m, and the fiber loss is dominated by the confinement loss in the blue region for 114 both curves. The loss of fiber that is made with As<sub>2</sub>Se<sub>3</sub> chalcogenide glass is located in the blue region, 115 which is marked with the blue circle on the blue solid curve. The fiber loss begins to increase when 116 the material loss increases from 10 dB/m to  $10^2 \text{ dB/m}$ , and the influence of the material loss becomes 117 visible. When the material loss further increases, the fiber loss increases sharply, and the fiber loss is 118 dominated by the material loss in the red region for both curves, when the material loss is higher than  $10^2$  dB/m. The loss of fiber made with As<sub>2</sub>S<sub>3</sub> chalcogenide glass is located in the red region, which is 120 marked with the red triangle on the red dashed curve. 121

Figure 8(a) shows the loss as a function of gap, g, in As<sub>2</sub>S<sub>3</sub> chalcogenide fiber with eight cladding tubes. In Fig. 8(b), we show the minimum loss and the corresponding gap, g, using a blue solid curve and a red dashed curve, respectively. The minimum loss decreases by less than one order of magnitude and the corresponding optimum gap, g, is always less than 20  $\mu$ m, which agrees with the results in the



**Figure 6.** (a) Loss as a function of gap in fibers with different core diameters. (b) Minimum loss and corresponding optimum gap in fibers with different core diameters. There are six cladding tubes.



**Figure 7.** (a) Loss as a function of gap in fibers with and without material loss. (b) Fiber loss as a function of material loss in  $As_2Se_3$  chalcogenide glass fiber and  $As_2S_3$  chalcogenide glass fiber with six cladding tubes, a core diameter of 300  $\mu$ m, and a gap of 60  $\mu$ m.



**Figure 8.** (a) Loss as a function of gap in fibers with different core diameters. (b) Minimum loss and corresponding gap in fibers with different core diameters. The number of cladding tube is eight.

As<sub>2</sub>Se<sub>3</sub> chalcogenide fiber with 8 cladding tubes. Small loss variation near zero gap occurs due to the
 glass modes existed near the node area between two tubes in Fig. 8(a).

### 128 5. Conclusions

In this paper, we optimize the structure of negative curvature fibers for CO<sub>2</sub> laser transmission. We 129 investigate the impact of the size of the gap between cladding tubes on the loss of negative curvature 130 fibers made with As<sub>2</sub>Se<sub>3</sub> and As<sub>2</sub>S<sub>3</sub> chalcogenide glasses. For As<sub>2</sub>Se<sub>3</sub> chalcogenide fibers with six 131 cladding tubes, the minimum loss decreases by an order of magnitude and the corresponding optimum 132 gap, g, increases from 60  $\mu$ m to 90  $\mu$ m when the core diameter increases from 300  $\mu$ m to 500  $\mu$ m. A 133 greater gap is needed for a fiber with greater core diameter to reduce the coupling between the core 134 mode and tube mode. For a fiber with eight cladding tubes, the optimum gap, g, that corresponds to 135 the minimum loss is always less than 20  $\mu$ m when the core diameter ranges from 300  $\mu$ m to 500  $\mu$ m. We 136 also study As<sub>2</sub>S<sub>3</sub> chalcogenide fibers, which has a higher material loss at a wavelength of 10.6  $\mu$ m. It is 137

Peer-reviewed version available at Fibers 2018, 6, 74; doi:10.3390/fib60400

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found that material loss dominates the fiber leakage loss. The fiber loss is dominated by the material loss, when the material absorption loss is higher than  $10^2$  dB/m.

Author Contributions: Supervision, Curtis Menyuk and Jonathan Hu; Validation, Curtis Menyuk and Jonathan
 Hu; Writing – original draft, Chengli Wei; Writing – review & editing, Chengli Wei, Curtis Menyuk and Jonathan
 Hu.

- **Conflicts of Interest:** The authors declare no conflict of interest.
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