

1 *Review*

2 **A Systematic Overview of Soft Actuators for Robotics**

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10 **Abstract:** In this systematic survey, an overview of non-conventional and soft-actuators is
11 presented. The review is performed by using well-defined performance criteria with a direction to
12 identify the exemplary applications in robotics. In addition to this, initial guidelines to measure the
13 performance and applicability of soft actuators are provided. The meta-analysis is restricted to four
14 main types of soft actuators: shape memory alloys (SMA), fluidic elastomer actuators (FEA),
15 dielectric electro-activated polymers (DEAP) and shape morphing polymers (SMP). In exploring
16 and comparing the capabilities of these actuators, the focus was on seven different aspects:
17 compliance, topology, scalability-complexity, energy efficiency, operation range, performance and
18 technological readiness level. The overview presented here provides a state-of-the-art summary of
19 the advancements and can help researchers to select the most convenient soft actuators using the
20 comprehensive comparison of the performance criteria.

21 **Keywords:** soft-actuators, scalability, actuator performance, DEAP, SMP, SMA, FEA

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23 **1. Introduction**

24 In this overview, it is intended to give a broad evaluation of the developments in soft- actuators.
25 These alternative devices or structures either fundamentally differ from the traditional actuators
26 which normally use electro-magneto-mechanical, fluidic and thermal combustion or they present the
27 same operation principles under a complete new design, emphasizing new characteristics that are
28 crucial in soft-robotics. One of the road-blocks in front of designing and realizing efficient and robust
29 yet safer robotic structures is the inherent limitations in the traditional actuation. For example, in
30 robots with serial kinematic chains, the joint closest to the base should be able to cope with all the
31 weight and counter torque requirements of the preceding joints. This requires the base motor to be
32 selected as large as possible, making the robot hefty in turn. In other words, the ratio between the
33 energy supplied by the actuator and the weight of the actuator is a natural limitation. Even this basic
34 fact was a set-back until harmonic drive and light-weight structures offered an intermediate and
35 acceptable solution to robotics community. In addition to energy output/weight, the volumes
36 occupied by the traditional actuators in the robot structure causes the packaging problem. Therefore
37 'energy output/volume' ratio is also an inherent limit in selecting the best actuator for a given
38 application. Considering these two general criteria, the novel/soft actuators can give the researchers
39 the opportunity to design compact, light-weight and compliant actuators to be used in autonomous
40 soft-robots. In the soft robotics field, two recent reviews have been performed one concentrating on
41 design, fabrication and control of soft robots [1] and the other on soft materials used in soft robotics
42 [2]. However, there is no comprehensive review on the soft and novel actuators mapping their
43 properties to possible applications and especially regarding them in a multi-criteria evaluation as
44 presented here. Therefore, in this review, we provide a comprehensive evaluation of the current
45 state-of-art in soft-actuators, focusing on four different type of actuators.

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47 2. Systematical Review Method

48 A systematical review of current developments in soft/novel actuators is needed including the
 49 performance comparison and application-specific selection criteria. Here, we provide seven
 50 selection criteria for four different actuator types namely shape-memory alloys (SMA), fluidic
 51 elastomer actuators (FEA), dielectric/electrically-actuated polymers (DEAP) and shape memory
 52 polymers (SMP). A special importance is given to seven selection criteria, including the aspect of
 53 compliance, topology-geometry, scalability, energy efficiency, technological readiness level, and
 54 operation range of the actuators.

55 To illustrate a systematical evaluation of a soft actuator with the perspective in this review, we
 56 can examine the Pneumatic-Nets which falls under the category of FEA-type actuators. Another
 57 name referring to this type of actuator is 'soft pneumatic actuators' (SPA) as used in [3]. Pneumatic-
 58 nets are devices essentially comprising a series of chambers formed by elastomeric substrates such as
 59 silicone, and supported by an inextensible layer. These devices can be pre-programmed by arranging
 60 their extensible and inextensible parts in a specific geometry to determine the bending and the
 61 orientation of movement in a specific way. Therefore, in terms of design criteria they are topologically
 62 programmable. From the mechanical compliance aspect (2.1), these devices are inherently compliant
 63 however, their structural stiffness can change greatly depending on the internal pressure [3]. The
 64 optimal topology and geometry (2.2) also plays important role in the efficiency of harnessing the full
 65 capacity of the generated power in the actuator. For the FEA-type actuators, especially the chamber
 66 geometry and the connection patterns are important since the pressure build-up regions and the
 67 orientation of the actuation is programmed by this structural parameter. The FEA/SPA type actuators
 68 are highly scalable and less complex to produce (2.3) while the energy efficiency (2.4) depends on the
 69 fluid used in the system. Since the pump, filter and valves already exist for more traditional
 70 pneumatic and hydraulic systems, FEA-type soft actuators can score high in technological readiness
 71 level (2.5). The pneumatic or hydraulic operation principles can be modified to come up with new
 72 FEA devices and the applications (2.6) can range from medical to industrial robotics where inherent
 73 compliance and adjustable stiffness is needed. For example, characteristics such as back-drivability
 74 and the off-axes deformation capability make FEA/SPAs safe for human-robot interaction [4]. Lastly,
 75 the operation range (2.7) of FEA-type soft actuators are determined by the internal pressure and the
 76 environmental settings such as temperature. Although the operational principle of the device is
 77 highly non-linear, control of such devices is relatively easy employing simple on/off control. A table
 78 summarizing the systematical evaluation in this paragraph is given in Table I to illustrate the review
 79 approach of this paper for a selected actuator type (i.e. FEA/SPA) to provide the readers an organized
 80 setting for overview and extracting relevant information.

81 **Table 1.** Systematical evaluation of FEA/SPA¹ for illustrative example of the review methodology

Selection Criteria	Evaluation
Mechanical compliance	Compliant, light structures
Optimal geometry and topology	Depends on the inner chamber size and network
Scalability and complexity	Scalable, easy to manufacture
Amplification/ Energy efficiency	Amplification through structural parameters and snap-through property
Technology readiness level (TRL)	Utilizes existing infrastructure and devices, TRL 7-9
Modality of operation	Pneumatics/hydraulics
Operation range	Force: up to 10 N, Stroke: up to 10 cm, Pressure: up to 0.5 MPa, Watt/Weight: 1W/g [5]

82 ¹FEA: Fluid Elastomer Actuators, SPA: Soft Pneumatic Actuators

83 In the rest of the review, each selection criterion is expanded across all the soft-actuator types
 84 for the sake of brevity, producing a comparison across the actuator types for the criterion in focus. In
 85 the conclusion section, comparing the four types of actuators according to seven criteria to emphasize
 86 the strengths and weaknesses, a list of hybrid solutions is suggested. This table of hybrid solutions is

87 expected to guide the robotic researchers in selection of the actuator type according to their applied
88 field as well as clarifying which one of these actuator types could be used together for a hybrid-
89 actuation solution.

90 *2.1. Mechanical Compliance and Light-weight Structure*

91 With the modern setting of industrial production lines and concepts of smart factory and Industry
92 4.0, the robots used in industry are required to be modular, adaptable, compliant and light-weight.
93 In addition, the mobile robotics also moved towards more compliant and light-weight but robust
94 structures. Another field of robotics where the compliance might be crucial is the medical/surgical
95 applications.

96 *2.1.1. Compliance*

97 The need for compliance is imposed by the human-robot co-operation and interaction scenarios.
98 For example, in industrial robotics a human-robot co-operative team should be able to work together
99 without the danger of robot partners harming humans due to collisions in the task trajectory.
100 Therefore, the industrial robot arm should be inherently compliant, yielding the force control to the
101 human partner in the task when necessary. A similar necessity is brought in minimally invasive
102 robotic catheters where variable stiffness and compliance is desired while passing through torturous
103 channels in human body to prevent tissue damage or rupture.

104 For some soft-actuators, the compliance can be inherent because of the material used. Although
105 difficult, the compliant behavior can be also modeled and numerically represented. The compliance
106 and the mechanical behavior for DEAP type materials was modeled using Timoshenko beam
107 approach [6]. The general material used in lab-based DEAP is acrylic based VHB and the normalized
108 Young modulus for this material is 210 kPa [7]. If the elastomeric dielectric polymers are used the
109 Young modulus can be around 1 MPa while the material can sustain 380% strain in high electric fields
110 [8]. In a non-traditional approach, a novel actuator for soft-robotics using discrete actuation units to
111 form a muscle-like structure uses the compliance as the enabler for discretization of the muscle units
112 [9]. Another polymer group that are used in SMP structures also have attractive properties in terms
113 of high deformation capacity [10].

114 To make the compliance of the structure adjustable and more independent from the selected
115 materials, a hybrid-actuator can be used following the approach in STIFF-FLOP [11], leading to
116 controllable-stiffness. The compliance criterion is examined across all the actuator types and
117 summarized in Table 2.

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119 *2.2. Optimal geometry and topology*

120 In most of the actuator design, even in the traditional motor design, the geometry and topology
121 of the actuator must be optimized to achieve the best energy efficiency, compactness, the most
122 available stable force/torque from the structure. Even in traditional DC motor design the stator/rotor
123 geometry and the air gap between windings are optimized for the best flow of the magnetic field
124 curves. For the novel actuators, the topology and finding the optimal geometry for the specific task
125 is indispensable since it directly effects either the force or the stroke capability or both.

126 In this section we will overview the effect of topology/geometry in SMA, FEA, SMP and DEAP based
127 designs. However, to obtain a comparable base between different actuator modalities we will first
128 describe the main topological features in these actuators which has a definitive effect on the force or
129 stroke amounts.

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Table 2. Evaluation of soft/novel actuators according to compliance criteria

Actuator type	Evaluation according to criteria (2.1)
DC motor (benchmark)	Compliance is based on current control over armature, structural stiffness is high, and the weight increases greatly as the output power requirement gets higher.
SMA (shape memory alloy)	SMA has almost no inherent compliancy. It is not compliant in martensite phase and the austenitic phase lasts only when it is heated. However, when used in spring form or meandering profiles, it can obtain certain compliant features due to form. SMA enables light-weight construction when the circuits are left outside of robotic structure.
FEA (fluidic elastomeric actuator)	FEA platforms are inherently compliant due to the structural elements mostly comprising elastomeric polymers. The fluid also contributes to the compliance however it can be varied by changing the internal pressure of fluidic chambers. FEA is essentially a light-weight structure if compressors and the pneumatic circuit elements are left outside of the robot.
DEAP (dielectric polymer)	DEAP uses a hyper-elastic polymer membrane and compliant/stretchable electrodes, therefore it is inherently compliant. However, the pre-stretching rings or any rigid structure around it may cause the increased stiffness. DEAP supports light-weight structures however the high-voltage circuit should be placed away from the robotic platform.
SMP (shape memory polymers)	SMPs are also inherently compliant because of the polymers used in the structure. However, the thermal actuation can largely affect the state of the polymer and in some states the polymer is more rigid.

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2.2.1. Topology in SMA

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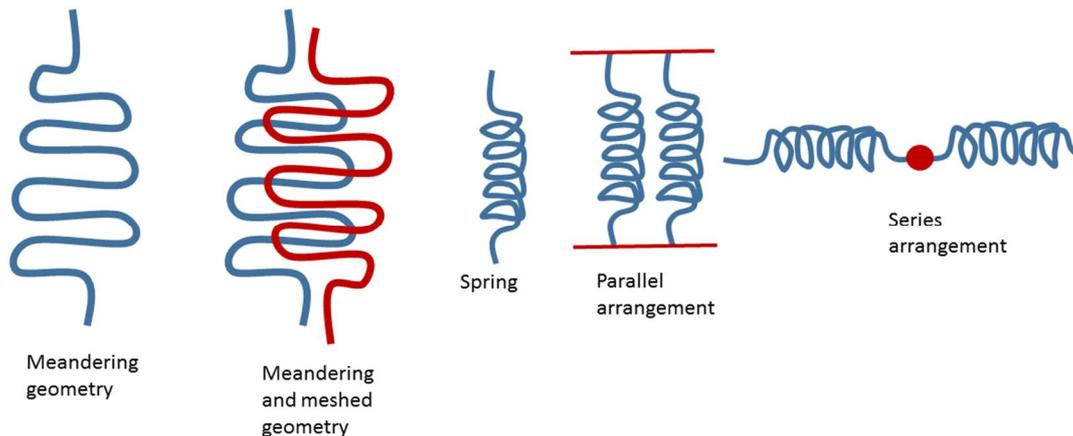
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There are very few studies focusing on the effect of topology/geometry of the actuator on the overall actuator performance. Among the possible geometries, the spring coil is examined [12] including four design parameters, namely wire diameter, the rod diameter, the pitch angle and the number of active coils. The peculiar contribution of this work was in its consideration for the de-twinning phenomenon in shape memory effect together with the geometrical variables. Therefore, the effect of the geometrical design was used efficiently to demonstrate that based on the spring index, a deformation up to 200%-1600% was possible. Using the carefully designed geometry, a two-way antagonistic actuation can also be achieved [13] using simple wire-form SMA elements. This type of design also requires kinematic considerations in addition to basic material properties. Although overlooked in the previous studies, in addition to these obvious geometrical options (i.e. antagonistic couple and spring), meandering shapes on wires, inter-woven wire-meshes and parallel/series assemblies of SMA spring-coils can be examined to further explore the potential of geometrical/topological optimization on actuation performance (see Fig 1).

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161 **Figure 1.** Different geometry/topological arrangements of SMA to increase the stroke or force, with
162 subtle effects on cooling and reaction time

163 2.2.2. Optimal Geometry in FEA

164 Here the effective variables can be listed as the air/fluid chamber geometry and distribution,
165 wall thickness, double polymer designs (to restrict the movement at particular direction), elastomeric
166 fibers and their frequency/angle on the fluidic chambers. As in all other actuator types, the
167 application determines the manipulator geometry and the suitable material, however here the
168 specific emphasis is on the internal pressure and range of motion. In the work [14], finite element
169 analysis is used to simulate the range of motion and hyper-elastic response of the two different type
170 silicones. There, it clearly was indicated that different geometrical ratios and channel designs have
171 affected the generated stress in the structure therefore causing a certain bending angles. The
172 application is found to be appropriate in laparoscopic surgery due to internal tubing and volumetric
173 allowance. Analytical models are also used in [15] to capture the explicit relationship between input
174 pressure, bending angle and output force, by special emphasis on the actuator geometry.

175 Another significant example how the effective use of topology and geometry made it possible to
176 build a macro-scale soft robot can be found in [16], (pp. 1). This soft robot is a 0.65m long, untethered
177 structure able to support the miniature air compressors, battery, valves and controller on itself. The
178 structure was able to operate because of the specific arrangement of the hollow glass spheres. Again,
179 in order to increase the interaction area in the layer-by-layer process and prevent tear, a peg-hole
180 geometry was used.

181 In an interesting work [17], (pp. 2164) using topology/geometry to enhance the response of the device
182 fast-pneu-nets (fPN) was proposed. In contrast to previous and slower motion, the extensible layer
183 of fPN contains gaps between the inside walls of each chamber. The dimensions of chambers here are
184 designed in such a way to have inner wall thinner and greater surface area compared to the outer
185 walls.

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187 2.2.3. Topology in SMP

188 Here the coiling parameter, the self-coiling vs. mandrel coiling, chirality, the number of strands, any
189 patterns of braid in the structure are important. A particular type soft actuator derived from fishing-
190 line or sewing-thread uses thermo-mechanical actuation principle and can be considered in SMP
191 category. In these actuators, the over-twisting and coiling is used before the heat treatment is applied.
192 The geometry is extremely important because inserting the twist can introduce instability. To
193 counter-balance this a counter-balancing braiding structure should be designed [18]. Perhaps one of
194 the most interesting application ideas employing the topological/geometrical optimization is to
195 consider vascularized structures made out of SMP materials using additive manufacturing [19].

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197 2.2.4. Geometry in DEAP

198 The ratio of elastic band/electrode area, the pre-stretching of the polymer (elastic strain),
199 piling/stacking of the material. One of the very early works reporting on electro-active polymers has
200 suggested a two-way working and tubular geometry [20]. A recurring idea to produce useful
201 actuators from DEAP is to use stacking, folding [21, 22] or rolling the elastomer/polymer to increase
202 either the force or the stroke as the main output of the actuator. A rolled elastomer design reported
203 in [23, 24] was able to bend in many directions, therefore presenting a good candidate for surgical or
204 mobile robotics use. Another common approach to manipulate the surface deformation in DEAPs to
205 harvest the stroke/force in the desired orientation is to use fiber strands in various geometrical lay-
206 outs [25]. This fiber surfaces can be arranged in micro-scale and the diamond shape areas can be
207 customized to obtain the better result in actuation output using the angle between intersecting fibers
208 [7].
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210 2.3. Scalability and Complexity

211 A challenging problem in robotic design is the increasing complexity of the actuator as it is produced
212 in larger or smaller scales. In order to better understand this problem and probe into certain
213 limitations, herein the scalability and complexity of each selected actuator type are examined. The
214 scalability can be limited by current manufacturing and assembly methods as well as physical
215 limitations of the modality of the actuator (i.e. saturation, non-linear operation, uncertainty,
216 deterioration of the physical phenomena at a particular scale).
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218 2.3.1. Scalability of SMA

219 Although the studies on SMAs as actuators do not particularly focus on scalability and complexity
220 issues, some applications may be singled out to provide a leading idea on the scalability. In one of
221 those cases, [26] have studied the feasibility of the production of micro-scale structures using the
222 micro-pulling growth technique to obtain thin wires of SMA involving single crystals. This ability of
223 producing single-crystals in micro-scale allowed them to overcome the brittleness of SMA structures
224 when they are produced in small-scales using poly-crystal inner structure. In their work involving
225 the design of a torsional actuator based on SMAs, [27] have used a meso-scale antagonistic structure
226 for bilateral functionality. Despite the disadvantage of difficult heat-transfer in macro-scale, SMA
227 structures as passive super-elastic units in seismic applications is possible as seen in [28].
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229 2.3.2. Scalability of FEA

230 We can see from the work in [16] that the soft lithography is a scalable molding process. In that work,
231 they used this method to produce a robot with length of 15 and 65 cm. Although the manufacturing
232 is scalable without much effort, the operation of the robot does not follow the same trend. The macro-
233 size robot actuated by FEA should use a reduced density material or the actuation pressure should
234 be increased to counter-balance its own weight. In addition to layer-by-layer soft-lithography
235 method, better continuous soft actuators can be molded by a spin production process which is highly
236 scalable [29] to produce monolithic soft-machines. In this scalable casting process, they could control
237 more parameters compared to basic layering such as: (i) viscosity evolution during casting, (ii)
238 rotational speed of the primary axis, (iii) axial speed ratio of the machine and (iv) the internal surface
239 geometry of the two-part molds. This scalable monolithic casting process can be seen in Figure 2.
240 The soft robots actuated by FEA can be assumed to be much simpler than the mechanical ones, since
241 they may be operated without an internal or external skeleton. Although the structural complexity
242 might be low, complex locomotion patterns are possible such as ones including the change in gait [3],
243 (p. 4). A limiting factor for such actuators could be related to the power supply for FEAs. Most fluidic
244 actuators include compressors and bulky supply lines, increasing their complexity level [30], (p. 484).
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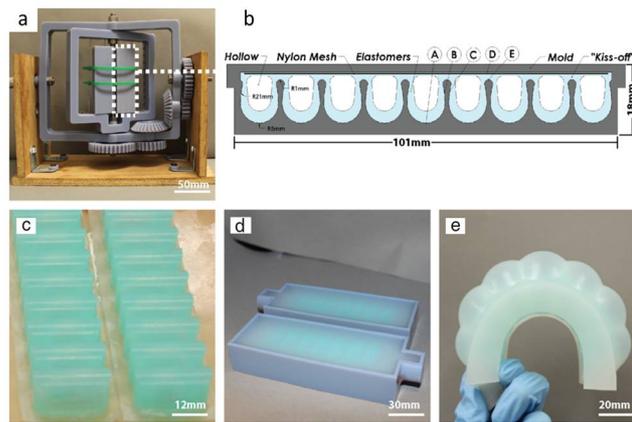
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Figure 2. Rotational casting method (a) machine, (b) interior structure, (c) monoliths, (d) encapsulation, (e) inflation of cuboid actuator [29]

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2.3.3. Scalability of SMP

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2.3.4. Scalability of DEAP

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2.4. Amplification and Energy Efficiency

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SMP In the vascularized SMP blocks, the scalability was determined to be one of the limiting factors [19]. Since SMP structures can usually be actuated only in one direction, to eliminate this a composite containing SMP and SMA is manufactured in [31]. Here the structure is more functional and scalable since the two-way actuation is achieved by the SMA embedded in SMP and the actuation load is not on SMP. Another scalable format for SMPs is to use fiber or yarn based structures [32].

In order to examine the scalability and complexity in DEAP based actuators, a pre-strained circular actuator was modeled in detail [33]. To reduce the complexity and render the DEAP actuator scalable, an automated folding and production procedure was proposed in [22].

The possibility of optimization of the stroke or force obtained from the actuator versus its energetic efficiency is highly linked together in SMA based actuators. In [34], hollow helical springs based on SMAs were proposed to reduce the weight of the actuator and increase the efficiency of the heating-cooling cycle. This work keeps the geometrical advantage of the helical design in amplification of the stroke but also reduces the loss of energetic efficiency by reducing the effective mass with the hollow-structure. In addition, the dimensionless units are employed for a better comparison between the hollow SMA springs and their solid counterparts, demonstrating a significant improvement. In terms of energy efficiency, the smaller the SMA structure, the better the energy conversion dynamics would be handled. An example of this behavior can be seen in SMA ultra-thin films [35]. The energy efficiency and work production is not frequently studied, however, for thermal cycles and work production of special SMAs can be found on a case by case basis as in [36].

In order to operate non-conventional actuators based on smart-materials, we often need to use amplification. In many cases, the energy transformation during actuation is from electrical energy to mechanical energy. For the case of SMP this transformation is thermo-mechanical and for FEAs hydro-mechanical/fluidic to mechanical domain. The need for the amplification and the nature of the energy domain change may bring problems related with efficiency. For this particular problem, we will compare our four selected actuators based on their need for amplification and energy conversion efficiency. It should be although noted that the actuator types with lower efficiencies cannot be considered completely insignificant based on this criterion because low-efficiency type actuators tend to provide compact actuation spaces which might serve as critical solutions especially for medical robotics.

291 The DEAP based actuators is the most disadvantageous option among the soft actuators because
292 of its need for high amplification of the voltage to obtain high electric fields [23]. The high-voltage
293 requirement brings about extra problems such as electrical breakdown. In order to overcome this
294 problem, the dielectric constant of the polymer can be improved by adding silica nanoparticles [37].
295 Although the amplification requirement and high voltage is a drawback, DEAP actuators can convert
296 energy up to 0.4 J/g [38] which is larger than piezoelectric ceramics or electro-magnetic actuators. It
297 is reported that the electro-mechanical coupling is around 60-80% in acrylic and can go up to 90% for
298 silicon based polymers [8].

299 For the SMPs the amplification is not needed however the energy conversion efficiency during
300 contraction is around 1.08-1.32% for Nylon and Polyethylene [18]. Another factor affecting the energy
301 efficiency of SMP based actuators is to change the environment of the heat conduction, such as using
302 water instead of air [32].

303 FEA based actuators can be using the topological optimization for the amplification and their energy
304 efficiency is comparably low because they operate below 0.5MPa. The specific energy is particularly
305 low in that pressure range, however reaching as high as 200 J/g when the pressure is around 5 MPa
306 [39].

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308 2.5. Technology Readiness Level (TRL)

309 This is particularly relevant if these four actuator types are considered to be future solutions for
310 robotics design. Unfortunately, most of the soft-robotics literature reports actuator designs which are
311 not in the adequate TRL, therefore cannot be widely used outside of the laboratory conditions when
312 they are placed in harsher environments with minimum control on the environmental conditions. We
313 will assess the TRL of the selected four actuators based on the manufacturing methods, complexity
314 and available materials.

315 Although being employed in many advanced engineering structures as deformation
316 compensators, shape morphing or surface actuation applications especially in aerospace, the SMA-
317 based actuators cannot be considered in the highest category in terms of technological readiness level
318 (TRL). For example, in order to predict the relations between the variable thermo-mechanical
319 conditions and the behavior of SMA a nonlinear model was formed in [40]. Understanding the
320 underlying mechanism in thermos-mechanical behavior and presenting them in a mathematical
321 model with predictive power is a very important step in terms of increasing the technological
322 readiness level of SMA based actuators. In this way the disadvantages can be leveraged based on the
323 thermos-mechanical conditions for a particular technological application. It is very effortful to reach
324 to high TRL and asses it. In [41], it was demonstrated that for the full assessment of the TRL of SMA
325 mechanical, magnetic, corrosion resistance and biocompatibility were considered.

326 DEAPs are technologically not ready to be used fully in medical and industrial robotics. Some
327 of the challenges are actuation force levels, lifetime and activation voltage levels [23]. An important
328 step to make them more durable and easily manufacturable through an automation process was
329 performed in [22]. There, a fast and automated dry-deposition manufacturing process is
330 demonstrated by producing several multi-layer stack actuators based in roll-to-sheet process. The
331 problem with the DEAP production lies in the fact that, although well-adapted to laboratory
332 experiments, carbon-based compliant electrodes have limitations with patternability, scalability and
333 has no practical aspects for the large volume production [42].

334 For the SMPs, although these materials have been more studied and used in specific applications,
335 their one-way actuation and limited strain endurance limited their potential. In order to alleviate
336 these disadvantages, in [43] a two-way reversible shape memory effect using two types of polymers
337 as the main core and matrix and a double extrusion process. There have been also other works
338 reporting two-way operating SMPs using lamination process [44]. Although the two-way actuation
339 is demonstrated in custom polymer matrix in laboratory conditions, it is not in the level to be used in
340 large quantities or industrial settings. A comparison table for all four actuator types is given in Table
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Table 3. Application oriented TRL comparison of soft and novel

Actuator	TRL	Explanation
SMA	6-8	Adequate research background, some applications in robotics, still needs to be developed into full products. The problems with hysteresis and limited work-range needs attention.
FEA/SPA	7-9	Built on already existing technology and components from pneumatics and hydraulics, closer to be produced for large amounts in an automated manner. Limited range of work.
DEAP	5-8	Very few examples outside of laboratory, still needs improvement on materials, control and electro-mechanical design improvements. Limited due to high voltage requirements.
SMP	5-8	Very few examples outside of laboratory, one-way actuation, limited mechanical recovery.

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2.6. Modality of operation

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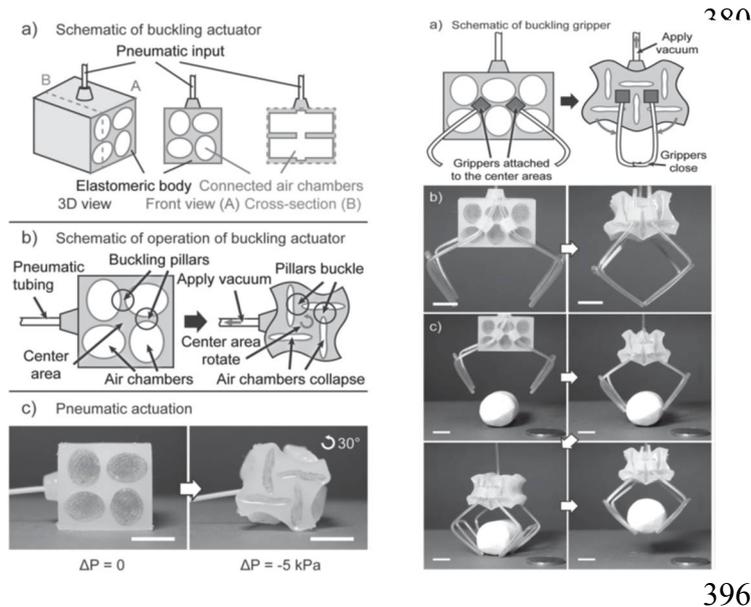
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The modality herein describes the energy domain the actuator mainly works in. For example SMPs are essentially thermo-mechanical actuators because they use the heat energy to relax the bonds between oligomers or re-contract when the heat is taken (cooling). Another case is DEAP which works based on electro-actuation depending on the Maxwell and Coulomb Laws defining electro-restrictive and electro-static forces on a flexible capacitor structure. SMA mainly works electro-mechanically however exploits the heat to transform the micro-structural change. FEA types depend on the fluidic power to obtain mechanical movement. Comparing these four actuation methods, the SMA and SMP are not highly efficient in terms of energy conversion because both of them involves heat-processes. DEAP is relatively efficient however requires amplification of feed-voltage and FEA requires additional complex equipment (compressor, filter and a valve) for the pressured air. Herein leaving aside the efficiency issue, we consider the four actuators in terms of application suitability based on their modality (thermal, fluidic, and electro-mechanical). By this way we clearly can identify which modalities are more appropriate for certain applications, therefore matching the actuators with the best applications to accentuate their significant side/ leverage their usage.

When the application convenience is considered for SMAs, any case where super-elasticity or shape memory is relevant can be thought. It is not uncommon to have SMAs as actuators in aerospace applications for shape-morphing of aero-foils [45] or for the simplification and compactness of UAV actuation [46]. The super-elasticity and shape memory property of SMAs also make them an excellent actuator choice for biomedical applications [47]. Although being not a conventional mechanical application, SMAs can also be used in small-scale thermal engines and pumps [48]. Mainly utilizing their super-elasticity, civil engineering also benefits from SMA materials [49], however, these applications usually benefit from the extra damping feature of SMA and can be considered as passive uses.

SMPs can be used in very specific applications, such as orthopedics, endoscopic surgery, orthodontics, kidney dialysis, neuro-prosthesis and bio-MEM [50]. As a sub-group of SMPs, using the super-coiled Nylon-based yarns, smart-textiles [18] can be produced using nylon as muscles, conductive silver-plated fibers for electro-thermal heating and polyester/cotton mixture for textile functionality.

For the FEA type actuators, it does not always have to be with pressurized air or fluid, a non-conventional prototype uses a system of interconnected chambers and vacuum [51] to achieve gripping force with compliant action. In this type of vacuum-operated actuators, the internal air chamber topology is extremely important since it determines the buckling pattern, please see Figure 3.



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Figure 3. Vacuum-operated buckling FEA actuators, courtesy of [51]

398 Sometimes the pneumatic FEAs have to be integrated with a hybrid actuation as seen in [11]. To
 399 achieve elongation and bending in controlled directions, FEA and tendon drives can be used together.
 400 Regarding the modality or the physical characteristics of the actuators, a particular good example
 401 with the match of the robot function with its environment can be seen in soft jellyfish robot [52] using
 402 DEAP based actuators. This is an application where an underwater robot is designed which can also
 403 handle its own load. It also uses pneumatic principles together with DEAP based actuation to obtain
 404 a specific solution for underwater explorations. In order to widen the application of DEAP based
 405 actuators the flexible and stretchable electrodes are extremely important [42].

406 2.7. Operation range

407 2.7.1 Operation range of SMA

408 The maximum stroke of linear SMA wire actuators lies between 5% and 8% [53, 54]. Higher strains
 409 can be achieved with coil springs made from SMA wire, which represents a trade-off between smaller
 410 forces and larger strokes. The operation range of the SMAs can be increased with material science
 411 engineering studies. Perhaps the most relevant operation range property of SMAs is multi-cycle
 412 performance. Certain types of SMAs are studied to identify their functional performance under multi-
 413 cyclic conditions such as the work in [55].

414 2.7.2. Operation range of FEA

415 The FEA based soft robots are manufactured using siloxanes and elastomers and they are
 416 vulnerable when they meet sharp objects [3]. This property may limit their operation range in high
 417 pressure applications. In a recent work [16], it was demonstrated that robots can be propelled by
 418 pneumatically powered soft actuators with untethered operation underwater, in-land performing
 419 rolling and serpentine movements. Some of these robots had rigid structural components and did not
 420 move in locomotion patterns requiring to work against the gravity. Another performance limitation
 421 also mentioned by [16] is related to reaction time (100 ms) although the actuation itself is rapid
 422 because of the high pressure employed in this work (138 kPa).

423 In 'pneu-net' structures, recently they reduced the amount of the gas needed for actuation thus
 424 accelerating the actuation response [17]. In such structures, a simple actuator can bend from a linear
 425 to a quasi-circular shape in 50 ms when a pressure of 345 kPa is applied. In a normal operation
 426 scenario, pneu-nets can be inflated with pressures as low as 50 kPa and they require a volumetric
 427 change of 20-folds of their initial volume to achieve their full range of bending. Unfortunately, this
 428 volumetric change may also be a disadvantage because of the need of certain workspace and the
 429 transfer of large volumes of gas is a thermodynamically inefficient process. In addition to this,
 430 because of the large strains on the material, the operating life-span of pneu-nets are rather short [17].

431 The other important performance criteria may include the controllability, durability in adverse
432 ambient conditions, and exposure to extreme heat, humidity and light. Some of these criteria is
433 meaningful in the context of medical use since a sterilization might be necessary. While the others,
434 such as controllability could be more important in an industrial setting. The robots with a silicone
435 body are inherently resilient to adverse conditions such as cold weather, water exposure, direct
436 exposure to the flames and high impacts [16]. In the same category with FEA, the pouch-motors
437 proposed by [56] the measured maximum stroke was up to 28% obtaining 100N. In that work, the
438 researchers also demonstrated an easy way to manufacture printable soft-actuators.

439 2.7.3. Operation range of DEAP

440 A general operation requirement for elastomer based DEAPs is an electric field of $100\text{V}/\mu\text{m}$,
441 however in some of the chemically tailored polymers this performance can be greatly improved. For
442 example in [57] a new class of all-organic-field-type EAP composite was derived exhibiting high
443 elastic energy densities that are induced by an electric field as low as $13\text{V}/\mu\text{m}$. In a study exploring
444 the nonlinearity and time-varying properties of DEAP based actuators [58], it was observed that
445 DEAPs display linear dynamic response from approximately 1.5 to 3 kV, after this value a nonlinear
446 actuation mode starts. In the application of DEAP for underwater robots [48] has reported a
447 maximum trust force of 0.15N, which is relatively low for industrial robots however meaningful for
448 the under-water self-sufficient exploration robots. In [33] using acrylic and gold particle-solution for
449 stretchable electrodes, they were able to obtain $200\text{MV}/\text{m}$ for a film thickness of $25\mu\text{m}$ corresponding
450 to $200\text{V}/\mu\text{m}$, applying 5kV source of voltage. In the work by [24], rolled spring actuators based on
451 DEAP were actuated using 5.9 kV for one side and a bending angle of 600 was achieved. The
452 maximum lateral force obtained by this actuator was 1.68N at 7.7 kV. For the repeated and safe
453 operation, the actuator was operated at 6kV obtaining 1.15 N. In order to obtain better performances,
454 using electro-thermal and electro-strictive effects together with the enhanced electro-mechanical
455 coupling, new composite research such as [59] is needed. In that study, titanium oxide nanotubes and
456 carbon nanotubes are used to enhance the properties of candidate membrane materials. Enhancement
457 of polarization and reduction of the stiffness are two parameters in such polymer research to obtain
458 better electromechanical properties. Another work has the focus of eliminating the need for rigid
459 frames in membrane type actuators [60]. In that work, after curing a certain additive, force
460 equilibrium between the polymeric networks was able to preserve part of the pre-stretch, therefore
461 eliminating the need for external rigid frames. Another attempt to reduce the necessary high
462 voltages is to produce thinner elastomeric members as seen in the work by [61]. In the fabrication
463 method described by that paper, the thickness variation was 4% and they were able to fabricate a
464 layer of $5\mu\text{m}$ thickness which in turn making it possible to drive such systems only at 150V. Further
465 performance enhancements can be observed if the snap-through instability of such membranes can
466 be harnessed by controlling the air chamber pressure [62], removing the need of constant voltage
467 application. Sometimes the performance range can be enhanced by utilizing a different geometry and
468 a suitable application. For example, in [63], the tubular form was employed for fluidic control. The
469 system was able to create a rise in pressure by 3.0 kPa when the valve was passive and 0 kPa when it
470 was activated at 2.4kV level.

471 2.7.4. Operation range of SMP

472 Comparing SMP with SMAs, the SMPs have large recovery strains (above 300%) while having low
473 recovery stress (around 1-10 MPa) while SMAs have lower recovery strains (less than 8%) and higher
474 recovery stress (around 1GPa). The other performance related advantages of SMPs come from their
475 biocompatibility, implantable structure and tunable actuation using the glass transition temperature
476 [47]. The super-coiled nylon based SMP actuators have a very encouraging performance when they
477 are used in filament state. For example extreme twisting and spinning of filaments can form artificial
478 muscles that are able to contract by 49% and can generate around 5.3KW of mechanical power per kg
479 of the material [18]. In order to further increase the performance and enhance the energy efficiency
480 of such artificial muscles, passive cooling offers and economical solution to increase the cycle rate.
481 According to the same study, when immersed in water, a two-ply, coiled, silver-plated $180\mu\text{m}$
482 diameter Nylon fiber can be electro-thermally actuated at 5 Hz while producing 10% stroke and

483 lifting 22MPa load. In the work of [64], the focus was to program the SMPs for a sustainable and
 484 repeatable operation of bidirectional actuation. They have achieved at least 250 cyclic thermally
 485 controlled actuations with almost constant performance.

486 3. Conclusion and Discussions

487 In this comprehensive overview of the soft and novel actuators in robotics, we have considered seven
 488 categories of selection criteria over four different type actuators. The overview provides a state-of-
 489 the-art evaluation of the field as well as providing a selection guide for the researchers in applied
 490 robotics field, especially involving soft robotics. It is very difficult to judge if a particular actuation
 491 device is appropriate for the given application without a clear comparison ground. Lastly, as an open
 492 discussion for the research community especially in soft robotics, combinations of these four type of
 493 actuators should be studied to identify the areas we can leverage their short-falls. Early examples of
 494 limited combinations are studied, for example SMA+SMP combination for more effective solutions
 495 have been proposed in [31]. However, a wider exploration space is necessary for the combinations of
 496 the actuator types. A combination table (see Table 4) is prepared here with possible application
 497 domains and improved capabilities.

498 **Table 4.** Soft and novel actuator combination table for hybrid solutions

Combination	Improvement/ Leverage	Application domain
SMA + SMP	Wider bandwidth, removal of the need for external force for SMP, wider cooling window for SMA	Active construction solutions, adaptive and self-healing structures, soft robotics solutions in construction
FEA + SMA	Antagonistic principle can be used, wider time window for SMA to cool down, fast responses with FEA action, increase in compliancy, light-weight, shape morphing and stiffness variation is possible	Spine-like or worm-like structures in surgical robotics
FEA+DEAP	Snap-through property can be used to increase overall stroke or force capability, increased electro-mechanical durability of DEAP, removal of constant need to pressurize a particular system	Active touch-boards and human-machine interfaces
FEA+ SMP	Superb-shape morphing property via thermal or pneumatic actuation, low-weight	Soft surgical robots and exo-skeletons for augmenting human posture and physiotherapy, soft and adaptable prosthesis structures

499

500 As it can be seen in this combination (Table 4), many novel hybrid actuators can be envisioned and
 501 produced to strengthen a particular side of a certain actuator type while allowing the other type to
 502 fill in the gap. The application domains of soft and novel actuators can be widened using multiple
 503 actuator types in a suitable topological and geometrical arrangement or using additive
 504 manufacturing possibilities to obtain a seamless hybrid actuator.

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516 References

- 517 [1] Rus, D., Tolley, M.T., 'Design, fabrication and control of soft robots', *Nature*, vol 521, pp. 467-475, May 2015.
- 518 [2] Elango, N., Faudzi, A. A. M., 'A review article: investigations on soft materials for soft robot manipulations',
519 *Int Jnl Adv Manuf Technol*, vol 80, pp. 1027-1037, 2015.
- 520 [3] Shepherd, R. F.; Ilievski, F.; Choi, W.; Morin, S. A.; Stokes, A. A.; Mazzeo, A. D. et al. (2011): Multigait soft
521 robot. In: *Proceedings of the National Academy of Sciences* 108 (51), S. 20400–20403. DOI: 10.1073/pnas.1116564108.
- 522 [4] Moseley, Philip; Florez, Juan Manuel; Sonar, Harshal Arun; Agarwal, Gunjan; Curtin, William; Paik, Jamie
523 (2015): Modeling, Design, and Development of Soft Pneumatic Actuators with Finite Element Method. In: *Adv.*
524 *Eng. Mater.*, S. n/a. DOI: 10.1002/adem.201500503.
- 525 [5] N. Tsagarakis and D. Caldwell, "Improved modelling and assessment of pneumatic muscle actuators,"
526 *Robotics and Automation*, 2000. Proceedings. ICRA'00. IEEE International Conference on, vol. 4, 2000.
- 527 [6] Mutlu, R., Alici, G., Xiang, X., Li, W., 'Electro-mechanical modelling and identification of electroactive
528 polymer actuators as smart robotic manipulators', *Mechatronics*, vol. 24, pp. 241-251, 2014.
- 529 [7] Lee, K., Tawfick, S., 'Fiber micro-architected Electro-Elasto-Kinematic muscles', *Extreme Mechanic Letters*,
530 <http://dx.doi.org/10.1016/j.eml.2016.03.003>, Online: 4th March 2016.
- 531 [8] Mirfakhrai, T., Madden, J.D.W., Baughman, R.H., 'Polymer artificial muscles', *Materials Today- Elsevier*, vol.
532 10, no 4, pp. 30-38, April 2007.
- 533 [9] Mathijssen, G., Schultz, J., Vanderborght, B., Bicchi, A., 'A muscle-like recruitment actuator with modular
534 redundant actuation units for soft robotics', *Robotics and Autonomous Systems*, vol 74, pp. 40-50, 2015.
- 535 [10] Rodriguez, J.N., Zhu, C., Duoss, E.B., Wilson, T.S., Spadaccini, C.M., Lewicki, J.P., 'Shape-morphing
536 composites with designed micro-architectures', *Nature, Scientific Reports*, vol 6, 27933, pp. 1-10, June 2016.
- 537 [11] Stilli, A., Wurdemann, H.A., Althoefer, K., 'Shrinkable, stiffness-controllable soft manipulator based on a
538 bio-inspired antagonistic actuation principle', *IEEE/RSJ Int. Conf on Intelligent Robots and Systems (IROS)*,
539 September 14-18, 2014, Chicago, IL, USA.
- 540 [12] An, S-M., Ryu, J., Cho, M., Cho, K-J., 'Engineering design framework for a shape memory alloy coil spring
541 actuator using a static two-state model', *Smart materials and Structures*, vol 21, 2012, 16 pp.
- 542 [13] Sofla, A.Y.N., Elzey, D.M., Wadley, H.N.G., 'Two-way antagonistic shape actuation based on the one-way
543 shape memory effect', *Journal of Intelligent Material Systems and Structures*, vol 19, pp. 1017-1027, September
544 2008.
- 545 [14] Elsayed, Y., Lekakou, C., Geng, T., Saaj, C.M., 'Design optimization of soft silicone pneumatic actuators
546 using finite element analysis', *IEEE, Advanced Intelligent Mechatronics (AIM)*, 2014, Besancon, France,
547 10.1109/AIM.2014.6878044.
- 548 [15] Polygerinos, P. et al. 'Modeling of Soft Fiber-Reinforced Bending Actuators' *IEEE Transactions on Robotics* **31**,
549 778–789 (2015).
- 550 [16] Tolley, Michael T.; Shepherd, Robert F.; Mosadegh, Bobak; Galloway, Kevin C.; Wehner, Michael; Karpelson,
551 Michael et al. (2014): A Resilient, Untethered Soft Robot. In: *Soft Robotics* 1 (3), S. 213–223. DOI:
552 10.1089/soro.2014.0008.

- 553 [17] Mosadegh, B.; Polygerinos, P.; Keplinger, C.; Wennstedt, S.; Shepherd, R.; Gupta, U.; Shim, J.; Bertoldi, K.;
554 Walsh, C.; Whitesides, G. Pneumatic networks for soft robotics that actuate rapidly. *Adv. Funct. Mater.* **2014**, *24*,
555 2163–2170.
- 556 [18] Haines, C., Lima, M. D., Li, N., Spinks, G. M., et.al. 'Artificial Muscles from Fishing Line and Sewing
557 Thread', *Science*, 343, (6173), 868 (2014).
- 558 [19] Balasubramanian, A., Bettinger, C.J., 'Shape recovery kinetics in vascularized 3D-printed polymeric
559 actuators', *Advanced Engineering Materials*, vol 17, no 9, pp. 1287-1293, 2015.
- 560 [20] Pelrine, R., Kornbluh, R., Joseph, J., 1998. Electrostriction of polymer dielectrics with compliant electrodes
561 as a means of actuations. *Sensor and Actuators A: Physical* 64 (1), 77–85.
- 562 [21] Carpi, F., Salaris, C., De Rossi, D., 'Folded dielectric elastomer actuators', *Smart Materials and Structures*,
563 vol. 16, pp. 300-305, 2007.
- 564 [22] Maas, J., Tepel, D., Hoffstadt, T., 'Actuator design and automated manufacturing process for DEAP-based
565 multilayer stack actuators', *Meccanica, Soft Mechatronics*, vol 50, pp. 2839-2854, 2015.
- 566 [23] Bar-Cohen, Y., 'Electroactive Polymers as Actuators', chapter 8, Jet Propulsion Lab, Woodhead Publishing
567 Limited, 2010.
- 568 [24] Pei, Q., Rosenthal, M., Pelrine, R., Stanford, S., Kornbluh, R., 'Multifunctional electroelastomer roll actuators
569 and their application for biomimetic walking robots', *Proc. SPIE 5051, Smart Structures and Materials 2003:*
570 *Electroactive Polymer Actuators and Devices (EAPAD)*, 28 July 2003.
- 571 [25] Shian, S., Bertoldi, K., Clarke, D.R., 'Dielectric elastomer based grippers for soft robotics', *Advanced*
572 *materials*, vol 27, pp. 6814-6819, 2015.
- 573 [26] Lopez-Ferreno, I., San Juan, J., 'Micro pulling growth of very thin shape memory alloys single crystals',
574 *Functional Materials Letters*, vol.10, no:1, 1740003, pp.1-6, 2017.
- 575 [27] Sheng, J., Gandhi, D., Gullapalli, R., Simard, J.M., Desai, J.P., 'Development of a Meso-scale SMA-based
576 Torsion Actuator for Image-Guided Procedures', *IEEE Trans on Robotics*, vol.33, no 1, pp. 240-248, February
577 2017.
- 578 [28] Wang, W., Fang, C., Liu, J., 'Large size superelastic SMA bars: heat treatment strategy, mechanical property
579 and seismic application', *Smart. Mater. Struct.*, vol 25, 075001, pp 1-17, 2016.
- 580 [29] Zhao, H., Li, Y., Elsamadisi, A., Shepherd, R., 'Scalable manufacturing of high force wearable soft actuators',
581 *Extreme Mechanics Letters*, vol 3, pp. 89-104, 2015.
- 582 [30] Shapiro, Yoel; Wolf, Alon; Gabor, Kosa (2011): Bi-bellows: Pneumatic bending actuator. In: *Sensors and*
583 *Actuators A: Physical* 167 (2), S. 484–494. DOI: 10.1016/j.sna.2011.03.008.
- 584 [31] Lelieveld, C., Jansen, K., Teuffel, P., 'Mechanical characterization of a shape morphing smart composite with
585 embedded shape memory alloys in a shape memory polymer matrix', *Journal of Intelligent Material systems*
586 *and Structures*, vol 27, no 15, pp. 1-11, 2015.
- 587 [32] Yip, M.C., Niemeyer, G., 'High-performance robotic muscles from conductive nylon sewing thread', *IEEE*
588 *Int. Conf. on Robotics and Automation (ICRA)*, Seattle, Washington, pp. 2313-2318, May 26-30, 2015.
- 589 [33] Wissler, M., Mazza, E., 'Modeling of a pre-strained circulator actuator made of dielectric elastomers', *Sensors*
590 *and Actuators A*, vol. 120, pp. 184-192, 2005.
- 591 [34] Spinella, I., Dragoni, E., 'Analysis and design of hollow helical springs for shape memory alloys', *Journal of*
592 *Intelligent Material Systems and Structures*, vol 21., pp. 185-199, January 2010.
- 593 [35] Zong, H., Ni, Z., Ding, X., Lookman, T., Sun, J., 'Origin of low thermal hysteresis in shape memory alloy
594 ultrathin films', *Acta Materialia*, vol. 103, pp. 407-415, 2016.

- 595 [36] Belyaev, S., Resnina, N., Zhuravlev, R., 'Work production and variation in shape memory effects during
596 thermal cycling of equiatomic TiNi Alloy', *Journal of Materials Engineering and Performance*, vol. 23 (7), pp.
597 2343-2346, July 2014.
- 598 [37] Roy, M., Nelson, J.K., MacCrone, R.K., Schadler, L.S., Reed, C.W., Keefe, R., 'Polymer nanocomposite
599 dielectric-the role of the interface', *IEEE Trans. on Dielectrics and electrical Insulation*, vol 12, issue 4, pp. 629-
600 643 Aug 2005.
- 601 [38] Koh, S.J.A., Zhao, X., Suo, Z., 'Maximal energy that can be converted by a dielectric elastomer generator',
602 *Applied Physics Letters*, vol 94, 262902, pp. 1-3, 2009.
- 603 [39] Wehner, M., Tolley, M. T., Menguc, Y., Park, Y-L., Mozeika, A., Ding, Y., Onal, C., Shepherd, R.F.,
604 Whitesides, G. M., Wood, R.J., 'Pneumatic Energy Sources for Autonomous and Wearable Soft Robotics', *Soft*
605 *Robotics*, vol 2, no 00, pp. 1-12, 2014.
- 606 [40] Jani, J.M., Huang, S., Leary, M., Subic, A., 'Numerical modeling of shape memory alloy linear actuator',
607 *Computational Mechanics*, vol. 56, pp. 443-461, 2015.
- 608 [41] Feng, Y. P., Blanquer, A., Fornell, J., Zhang, H., Solsona, P., Baro, M.D., Surinach, S., Ibanez, E., Garcia-
609 Lecina, E., Wei, X., Li, R., Barrios, L., Pellicer, E., Nogues, C., Sort, J., 'Novel Fe-Mn-Si-Pd alloys: insights into
610 mechanical, magnetic, corrosion resistance and biocompatibility performances', *Jornal of Materials Chemistry*
611 *B*, vol.4, pp. 6402-6412, 2016.
- 612 [42] Rosset, S., Shea, H.R., 'Flexible and stretchable electrodes for dielectric elastomer actuators', *Applied Physics*
613 *A*, February 2013, vol. 110, issue 2, pp 281-307.
- 614 [43] Westbrook, K.K., Mather, P.T., et al, 'Two-way reversible shape memory effects in a free-standing polymer
615 composite', *Smart Materials and Structures*, vol 20, no: 6, 2011.
- 616 [44] Chen, S., Hu, J., Zhuo, H., Zhu, Y., 'Two-way shape memory effect in polymer laminates', *Materials Letters*,
617 vol. 62, pp. 4088-4090, 2008.
- 618 [45] Karagiannis, D., Stamatelos, D., Kappatos, V., Spathopoulos, T., 'An investigation of shape memory alloys
619 as actuating elements in aerospace morphing applications', *Mechanics of Advanced Materials and Structures*,
620 vol. 24, no 8, pp. 647-657, 2017.
- 621 [46] Ameduri, S., Concilio, A., Favaloro, N., Pellone, L., 'A shape memory alloy application for compact
622 unmanned aerial vehicles', *Aerospace*, vol. 3, 16, pp. 1-18, 2016.
- 623 [47] Zainal, M.A., Sahlan, S., Ali, M. S. M., 'Micromachined Shape-Memory-Alloy Microactuators and Their
624 Application in Biomedical Devices', *Micromachines*, vol 6., pp. 879-901, 2015.
- 625 [48] Ossmer, H., Wendler, F., Gueltig, M., Lambrecht, F., Miyazaki, S., Kohl, M., 'Energy-efficient miniature-scale
626 heat pumping based on shape memory alloys', *Smart Material Structure*, vol. 25, 13 pp. 2016.
- 627 [49] Chang, W-S., Araki, Y., 'Use of shape-memory alloys in construction: a critical interview', *Proceedings of*
628 *the Institution of Civil Engineers, Civil Engineering*, vol. 169, issue CE2, pp. 87-95, 2016.
- 629 [50] Small IV, W., Singhal, P., Wilson, T.S., Maitland, D.J., 'Biomedical Applications of Thermally Activated
630 Shape Memory Polymers', *Journal of Materials Chemistry*, LLNL-JRNL-412712, May 2009.
- 631 [51] Yang, D., Mosadegh, B., Ainla, A., Lee, B., et al, 'Buckling of elastomeric beams enables actuation of soft
632 machines', *Advanced Materials*, vol. 27, pp. 6323-6327, 2016.
- 633 [52] Godaba, H., Li, J., Wang, Y., Zhu, J. "A soft jellyfish robot driven by a dielectric elastomer actuator", *IEEE*
634 *Robot. Autom. Lett.*, vol. 1, no. 2, pp. 624-631, Jul. 2016.

- 635 [53] Coral, W. , Rossi, C. , Colorado, J. , Lemus, D. and Barrientos, A., 'SMA Based Muscle-Like Actuation in
636 Biologically Inspired-Robots: A Stateof the Art Review, in Smart Actuation and Sensing Systems – Recent
637 Advances and Future Challenges', G. Berselli, Ed., InTech, 2012, pp.5382.
- 638 [54] Follador, M., Cianchetti, M. , Arienti, A. and Laschi, C., 'A general method for the design and fabrication
639 of shape memory alloy active spring actuators', in Smart Materials and Structures, vol 21, no 11, 115029,
640 November 2012.
- 641 [55] Sehitoglu, H., Wu, Y., Patriarca, L., ,Shape memory functionality under multi-cycles in NiTiHf', Scripta
642 Materialia, vol. 129, pp. 11-15, 2017.
- 643 [56] Niyajama, R., Sun, X., Sung, C., An, B., Rus, D., Kim, S., 'Pouch motors: Printable Soft Actuators Integrated
644 with Computational Design', Soft Robotics, Vol 2, No 2, pp. 59-70, 2015.
- 645 [57] Zhang, Q.M., Li, H., Poh, M., Xia, F., Cheng, Z.Y., Xu, H., Huang, C., 'An all-organic composite actuator
646 material with a high dielectric constant', Nature, vol 149, pp. 284-287, 2002.
- 647 [58] Jacobs, W.R., Wilson, E. D., Assaf, T., et al, 'Control-focused, nonlinear and time-varying modelling of
648 dielectric elastomer actuators with frequency response analysis', Smart Materials and Structures, vol 24, 11 p,
649 2015.
- 650 [59] Ignat, M., Ovezza, D., Hamciuc, E., Hamciuc, C., Dimitrov, L., 'Study on the electromechanical properties
651 of polyimide composites containing TiO₂ nanotubes and carbon nanotubes', Jrnal Polym Res, vol 21, pp. 536, 2014.
- 652 [60] Lotz, P., Matysek, M., Schlaak, H.F., 'Fabrication and Application of Miniaturized Dielectric Elastomer Stack
653 Actuators', IEEE/ASME Trans. on Mechatronics, vol. 16, no.1, February 2011.
- 654 [61] Schmidt, A., Bergamini, A.E., Kovacs, G., Mazza, E., 'Experimental characterization and modeling of circular
655 actuators made of interpenetrating polymer network-reinforced acrylic elastomer', Jrnal of Intelligent Material
656 Systems and Structures, vol 24 (10), pp. 1257-1265, 2013.
- 657 [62] Keplinger, C., Li, T., Baumgartner, R., Suo, Z., Bauer, S., 'Harnessing snap-through instability in soft
658 dielectrics to achieve giant voltage-triggered deformation', Soft Matter, vol 8, no 2, pp. 285-288, 2012.
- 659 [63] McCoul, D., Pei, Q., 'Tubular dielectric actuator for active fluidic control', Smart Materials and Structures,
660 vol. 24, issue: 10, pp. 105016, 2015.
- 661 [64] M. Behl, K. Kratz, U. Nöchel, T. Sauter, A. Lendlein, Temperature-Memory Polymer Actuators, P Natl Acad
662 Sci USA, 110 (31), 12555-12559 (2013)