

## Article

# La-Ni based Alloys Preparation for Hydrogen Reversible Sorption and their Application for Renewable Energy Storage

Artem Chesalkin<sup>1\*</sup>, Petr Moldrik<sup>2</sup>, Alexandr Martaus<sup>3</sup>

<sup>1</sup> ENET Centre – Research Centre of Energy Units for Utilization of Non Traditional Energy Sources, VSB-TUO Technical University of Ostrava, Ostrava, Czech Republic; artem.chesalkin@vsb.cz

<sup>2</sup> ENET Centre – Research Centre of Energy Units for Utilization of Non Traditional Energy Sources, VSB-TUO Technical University of Ostrava, Ostrava, Czech Republic; petr.moldrik@vsb.cz

<sup>3</sup> CET- Centre for Environmental Technology, VSB-TUO Technical University of Ostrava, Ostrava, Czech Republic; alexandr.martaus@vsb.cz

\* Correspondence: chez47@gmail.com ; artem.chesalkin@vsb.cz Tel.: +420-774-269-863

**Abstract:** Metal hydrides are one of the types of functional materials that allow safe and compact storage of a large amount of hydrogen, which is increasingly used today as an alternate fuel or energy source. The possibility of obtaining the initial energy necessary for the production of hydrogen by electrolysis process from renewable energy sources, such as solar panels and wind generators, makes hydrogen energetic quite attractive and rapidly developing industry sector. Solid form of hydrogen storage with the possibility of reversible sorption, gives opportunity for creation autonomous energy storage systems. La-Ni based alloys allow hydrogen storing at ambient temperatures and pressure not higher than 15 bar, which makes the application of these alloys quite practical, interesting and prospects for analysis and modifications on the ways of stored hydrogen capacity increasing, alloys price reducing and application for renewable energy storage.

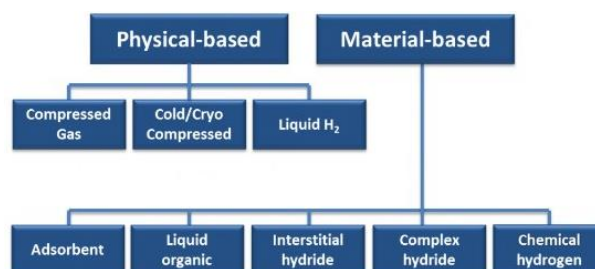
**Keywords:** metal hydrides; hydrogen storage; La-Ni based alloys; alloy modification and analysis; renewable energy storage

## 1. Introduction

The study of hydrogen sorption and desorption processes is of interest for various fundamental and practical problems. In the field of hydrogen energy, it is necessary to study hydrogen storage materials [1]. Hydrogen accumulators are investigated for maximum storage capacity [2], the conditions for the introduction and withdrawal of hydrogen and the number of such cycles are studied [3]. In nuclear power engineering and in those industries where such hydride-forming materials as zirconium alloys [4], various grades of steel [5], titanium alloys [6] are subjected to hydrogenation

The most important energetic process is the combustion of hydrogen, which is accompanied by the release of large amounts of energy and water without any harmful emissions. Among all the kinds of fuel, hydrogen has the highest gravimetric calorific value  $120 \text{ MJ/kg} = 33.33 \text{ kWh/kg}$  which is higher than many of liquid hydrocarbons  $\sim 45 \text{ MJ/kg}$  [7,8].

One of the best metal for hydrogen storage is palladium (Pd) and its alloys, but the price of this material does not allow its use widely [9,10]. Complex hydrides have a biggest storage hydrogen density in comparison with other types of hydrides, but most of them are not relevant for reversible hydrogen sorption. The micro-porous adsorbents and interstitial hydrides have similar hydrogen capacity, but intermetallic hydrides can operate at ambient temperatures. The aim of hydrogen storage technologies is to reduce the volume that hydrogen naturally occupies in its thermodynamically stable state under ambient conditions. Different ways of hydrogen storage are shown in Figure 1.



**Figure 1.** Different ways of hydrogen storage [11,12]

Most of metal hydrides formed by direct reaction with gaseous hydrogen, the thermodynamics of metal–hydrogen formation can be found in the literature [13, 15–19]. Because the La-Ni based metal hydride formation reaction requires rearrangement of metal atoms while in the hydride reaction the motion of atoms is minimal, the hydride formation goes at low temperature [14].

Analysis of scientific works in the field of LaNi<sub>5</sub> based alloys production and modification shows the existing problems on the way of widespread using these materials for hydrogen storage.

In the works of A. Apostolov, L. Bozukov, N. Stanev, P.Tcholackov devoted to hydrogen absorption in mishmetal-nickel-chromium-iron intermetallic compounds and hydrogen absorption in MmNi<sub>5</sub> type pseudo-binaries compounds, done by team of researchers from company «LabTech Int. Ltd.» Sofia and from personal working experience with (LaCe)Ni<sub>5</sub> based storage system HBond-1500, made also by LabTech company, few problematic aspects of alloy practical using were determined. First of all, it is a problematic of full system charging or complete hydrogen sorption in (LaCe)Ni<sub>5</sub> alloy. Completeness of hydrogen sorption depends on the accurate thermoregulation of ongoing hydride formation process. In addition, maximal hydrogen weight capacity of unmodified LaNi<sub>5</sub> and (LaCe)Ni<sub>5</sub> alloys is not more than 1.8% wt. The second problematic aspect is a complexity of alloys producing. This issue has become a significant obstacle for the project realization. The classic method of alloy production is a direct fusion from the pure bulk metals in the oven.

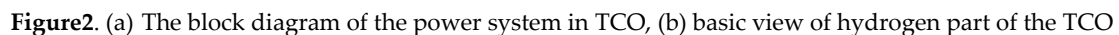
The same method is used by «LabTech» company. Alloys synthesis, by carrying out joint chemical and heat treatment transformations and using metal oxides and chlorides, instead of bulk metals, is not typical and common method of production. In this regard, lack of equipment for the synthesis of LaNi<sub>5</sub> based alloys was appeared. To perform the alloys synthesis, the new system was assembled. Quartz or graphite crucible with reagents and covered by cap should be placed to the oven. The crucible lid has two holes for gas pipes connection. One end of the tube is connected to a source of inert gas cylinder with argon. The second tube is used for gas byproducts removal from the reaction zone. Further analysis of the practical works of other authors shows that the chemical method of LaNi<sub>5</sub> alloy production from metal oxides and chlorides is applicable in practice. In the work of G.Giresan, S.R. Sankaranarayanan, L.J. Berchman was described an example of LaNi<sub>5</sub> alloy production by thermo-chemical synthesis and using magnesium (Mg) as a reducing agent:  $\text{La}_2\text{O}_3 + 10\text{Ni} + 3\text{Mg} \rightarrow 2\text{LaNi}_5 + 3\text{MgO}$  [20].

Moreover, in the work of S. Kamasaki, Y. Misaki, T.Kanayama, M.Yamada method of alloy modification by additional metal powders of Co and Al for alloy lifetime increasing during operation was described [21].

## 2. La-Ni based alloys application in Laboratory of Hydrogen Technologies in TCO

For the private sector and small production areas the pressure of hydrogen production and storage should not be very high for safety and regulation reasons. Working pressure in metal hydride storage tanks could not be more than 1.0 -1.5 MPa. Low storage pressure with big amount of stored hydrogen together with the small physical volume of storage vessels provides a big advantage for hydride systems application.

Private houses and industrial facilities, which identify independent from any vendor and external energy sources, always attracted people in the whole world. The main task is an integration of all presented technologies into a single power system adapted for home and industrial applications. Solar and wind power systems and autonomous backup power supply as well as fuel



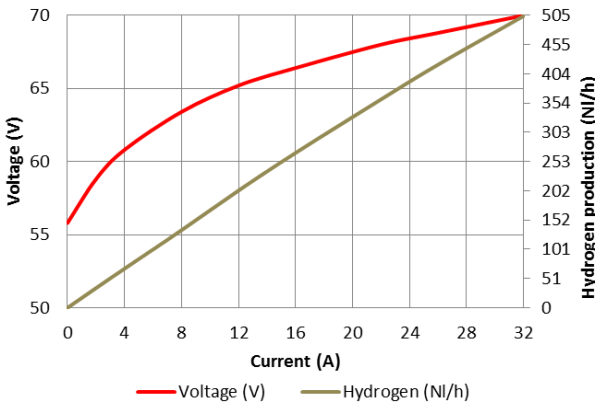
The TCO further has the battery room formed by the main and auxiliary battery blocks. The first block is made of lead traction batteries with the total capacity of 930 Ah. The second block is formed by LiFePO batteries with the total capacity of 200 Ah. The primary purpose of this block is to ensure a link to the photovoltaic power plant and to adjust the fluctuation of power consumption among electrolysis (hydrogen generation). The main storage bloc (lead batteries) allows for storage of approximately 550 kWh of electric power. The auxiliary storage block (LiFePO battery) then holds further 80 kWh of electric power. Semi-conductor power converters are linked to coupling transformers in order to ensure a connection between the DC Bus and both AC Buses. Their management enables modification of their functioning into various operating modes for transfer of electric power or its active filtration. These converters ensure two-way transfer of electric power with respect to the power distribution grid rated 50 Hz at the connection point. They may also ensure power supply to a designated local power grid in an off-grid mode, to cater for potential disconnection of TCO from the power distribution grid.

The hydrogen technologies subject to our research are included within the electric power storage system of TCO. These are based on the closed hydrogen cycle principle, where the electric power supplied from the photovoltaic power plant is transformed into chemical energy of hydrogen gas via electrolysis of water using AEM (Anion-Exchange Membrane) type electrolyzers. The hydrogen is

then stored in the gas - compressed form and in the solid form by forming metal hydrides in La-Ni based alloys and re-used to generate electric power using low-temperature fuel cells of PEM (Proton exchange membrane) type. The hydrogen storage system installed comprises eight electrolyzers with the total electric input of 17 kW and the total hydrogen production capacity of 4 m<sup>3</sup>/h. Basic parameters of one AES500 electrolyzer are shown in Table 1. The hydrogen storage system further includes five modules of hydrogen fuel cells with the total electric output of 40 kW. These are used for reverse conversion of the hydrogen gas into electric power and heat energy. Measured operation characteristics of this electrolyzer are shown in Figure 3.

**Table 1.** Basic parameters of electrolyzer [26]

Chracteristic	Value
Cell number	38 (2 blocks x 19 cells)
Maximum H <sub>2</sub> production	504 NI/h
Operating current	30 A
Operating voltage	34.6–35.5 V (each block)
Power consumption	2075–2132 W
Efficiency	85 %



**Figure3.** Basic characteristics of electrolyzer

The daytime operation with the photovoltaic plant in full pace delivering sufficient power involves operation of electrolyzers producing hydrogen gas that is collected into high-capacity pressure vessels and in metal hydrides storage system. Any fluctuations of electric power delivered by the photovoltaic power plant (due to the proportion of cloud-covered skies) are balanced using the LiFePO batteries. This feature then ensures reliable operation of electrolyzers. The electric power produced by fuel cells is primarily used by the TCO on its own; any potential surplus can be then supplied into the power distribution grid.

2. La-Ni based alloys preparation

Materials and Methods

Mixing of the initial components was conducted under inert atmosphere in glow-box to prevent oxidation and saturation of air moisture.

Reagents weights for samples preparation of La-Ni based alloys from metal chlorides are shown in Table 4, from pure powder metals are shown in Table 5. In practice, synthesis was performed for obtain 5-10 g of each of the La-Ni based alloy samples.

La-Ni based alloys were prepared in reaction chamber of induction furnace, shown in Figure 4. Table 3 described the main working characteristics of the furnace.

**Table 3.** The main working parameters of the furnace used for alloys preparation [27]

Furnace type	T max, °C	Working volume, l	Power nom., kW
LAC VP20/17	1700	20	7



**Figure 4.** General view of induction furnace used for alloys preparation

### 2.1. La-Ni based alloys preparation from metal chlorides

Crucibles with different samples were placed to the reaction zone of the induction furnace:

- Sample (A) – LaNi<sub>5</sub> prepared at 750 °C, holding time 80 minutes
- Sample (B) - LaNi<sub>5</sub> prepared at 900 °C, holding time 80 minutes
- Sample (C) - LaNi<sub>5</sub> prepared at 900 °C holding time 90 minutes

Temperature program of alloy synthesis:

- Step 1: heating up to 750-900 °C during 80 minutes
- Step 2: 750-900 °C temperature holding during 80-90 minutes
- Step 3: cooling till 200 °C

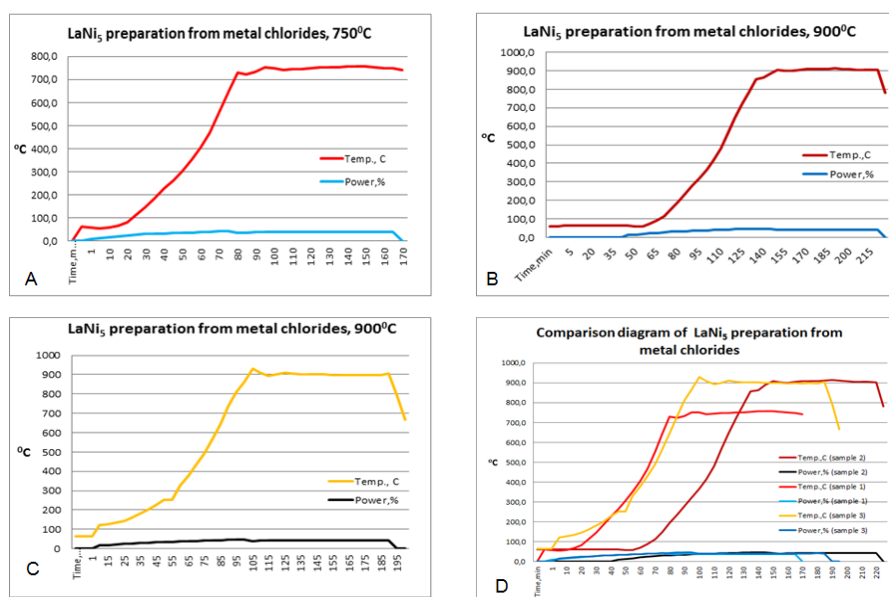
Step 1-3 should be carried out at inert atmosphere to prevent alloy oxidation and saturation by air moisture

- Step 4: transfer of alloy samples to a desiccator for subsequent analysis

All temperature profiles of the samples synthesis and their comparison diagram are shown in Figure 5.

**Table 4.** Reagents calculation for alloy preparation from metal chlorides

Reagent	LaNi <sub>5</sub> , g	(LaCe)Ni <sub>5</sub> , g	(LaMm)Ni <sub>5</sub> ,g
LaCl <sub>3</sub>	566,55	429,20	431,66
CeCl <sub>3</sub>		431,34	
NiCl <sub>2</sub>	1496,42	1133,65	1140,13
Mm			241,30
LiH	238,44	222,60	181,90



**Figure 5.** Temperature profile of alloys preparation in induction oven from metal chlorides

## 2.2. La-Ni based alloys preparation from pure powder metals

Crucibles with samples were placed to the reaction zone of the induction furnace:

- Sample (A) – LaNi<sub>5</sub>; Sample (B) - (LaCe)Ni<sub>5</sub>; Sample (C) - (LaMm)Ni<sub>5</sub>

Temperature program of alloy synthesis:

- Step 1: heating up to 1500 °C during 90 minutes
- Step 2: 1500 °C temperature holding during 180 minutes
- Step 3: cooling till 200 °C

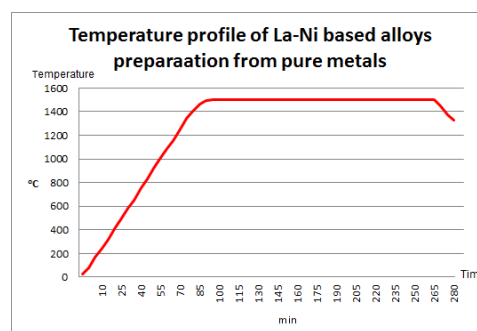
Step 1-3 should be carried out at inert atmosphere to prevent alloy oxidation and saturation by air moisture

- Step 4: transfer of alloy samples to a desiccator for subsequent analysis

Temperature profile of the samples synthesis is shown in Figure 6.

**Table 5.** Reagents calculation for alloy preparation from pure metals

Reagent	LaNi <sub>5</sub> , g	(LaCe)Ni <sub>5</sub> , g	(LaMm)Ni <sub>5</sub> , g
La	320,86	243,07	244,46
Ce		245,19	
Ni	677,87	513,54	516,47
Mm			241,30



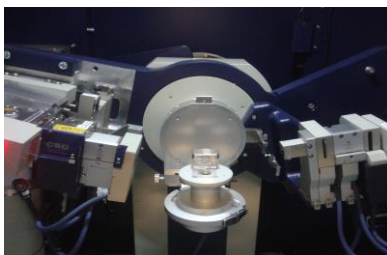
**Figure 6.** Temperature profile of alloys preparation in induction oven from pure powder metals

## 2.3. XRD analysis of La-Ni based alloys



Data about chemical composition and structure of prepared alloys were obtained from XRD analysis of relevant samples. Measured samples were evaluated using appropriate software and compared with ICDD database. Measured sample was not stable under the ambient conditions. From this reason sample was gently grinded under flow of nitrogen and covered with 6  $\mu\text{m}$  thick Mylar foil to eliminate exhibition of air humidity. Process of sample scanning is shown in Figure 7. Broad diffraction at positions 16.0, 19.3 and 30.0° 2theta corresponds to the Mylar foil.

XRD measurement conditions: diffractometer Rigaku SmartLab; goniometer geometry – Bragg-Brentano theta-2theta; lamp –  $\text{CoK}\alpha$  ( $\lambda_1=0.178892$  nm,  $\lambda_2=0.179278$  nm); detector – D/teX Ultra 250; range of the measurement - 5 – 90° 2theta; sample holder – glass holder with cavity depth 0.5 mm.

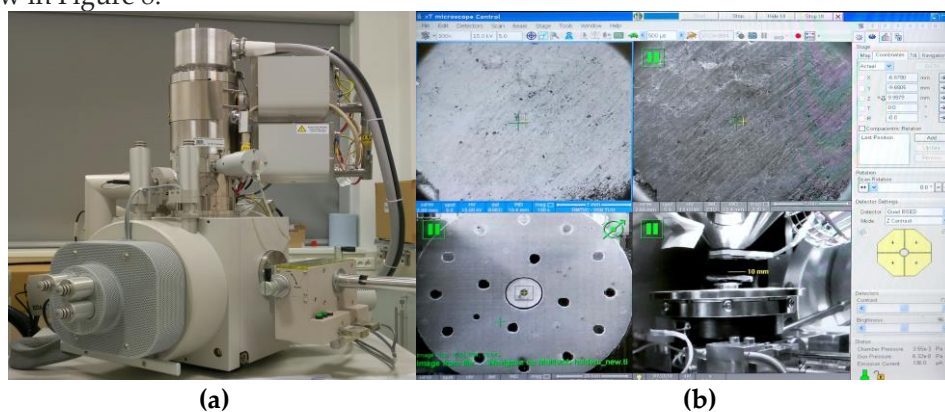


**Figure 7.** XRD analysis of the samples: La-Ni based alloy sample under X-ray scanning

Unfortunately the XRD analysis results were not sufficiently clear and informative to determine the composition of the alloys, because of similar nature and as a consequence of the identity of peaks of rare-earth components used for the preparation of alloys. This situation was however solved with the aid of the electronic microscopy analysis use.

#### 2.4. SEM analysis of La-Ni based alloys

The scanning electron microscope Quanta FEG 450 (FEI) with EDS microprobe analysis OCTANE (EDAX) was used for characterization of the morphology of the studied samples. Images were taken by use of secondary electrons and backscattered electron detectors at 15-20 kV. Microprobe analysis was performed with an EDAX detector and processed with the EDAX software, shown below in Figure 8.



**Figure 8.** The basic view during analysis (a) scanning electron microscope (b) SEM analysis software

### 3. Results of prepared La-Ni based alloys analysis

#### 3.1. Analysis results of La-Ni based alloys prepared from metal chlorides

##### 3.1.1. LaNi<sub>5</sub> alloy analysis results

The results of electron microscopy gave good information about alloys composition, distribution of phases and alloy homogeneity. Tables 6,7 show composition of the LaNi<sub>5</sub> sample, prepared at 1100°C. Figures 9,10 show the SEM analysis images and spectrum of the prepared alloy.

Table 6. Sample LaNi<sub>5</sub> prepared at 1100 °C (La-Ni-O composition).

Element	Wt, %	At, %	Z	A	F
O	9,51	39,66	1,2538	0,3364	1,0002
Cl	3,30	6,21	1,1731	0,6545	1,0114
La	72,26	34,69	0,9146	1,0174	1,0047
Ni	13,06	14,83	1,1204	0,8991	1,0000
Total	100,00	100,00			

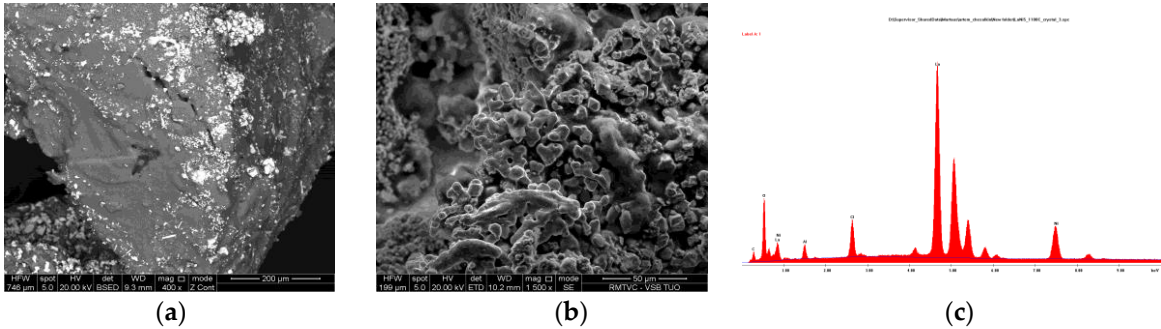


Figure 9. LaNi<sub>5</sub> sample prepared at 1100 °C : (a) sample view at 400 x zoom SEM analysis ; (b) sample view at 1500 x zoom SEM analysis ; (c) SEM spectrum

Table 7. Sample LaNi<sub>5</sub> prepared at 1100 °C (Ni crystal).

Element	Wt, %	At, %	Z	A	F
O	3,17	10,66	1,1376	0,3362	1,0039
Cl	1,18	1,79	1,0452	0,6990	1,0043
Ni	96,65	87,55	0,9934	1,0002	1,0000
Total	100,00	100,00			

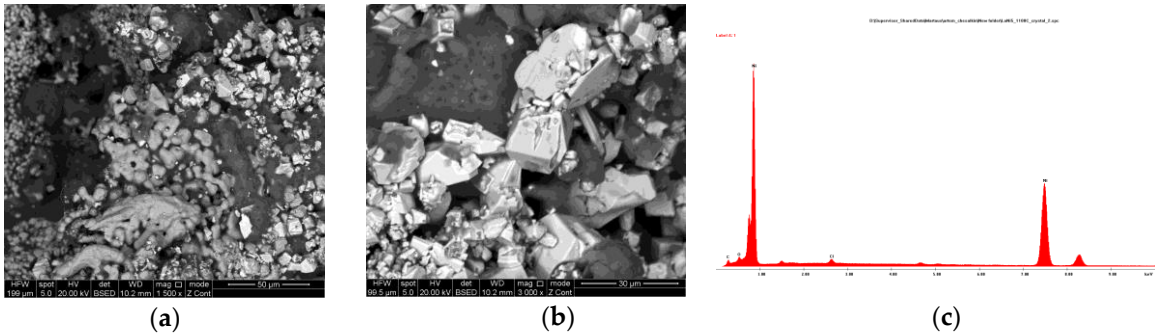


Figure 10. LaNi<sub>5</sub> sample prepared at 1100 °C : (a) sample view at 1500 x zoom SEM analysis ; (b) sample view at 3000 x zoom SEM analysis ; (c) SEM spectrum

3.1.2. (LaCe)Ni<sub>5</sub> alloy analysis results

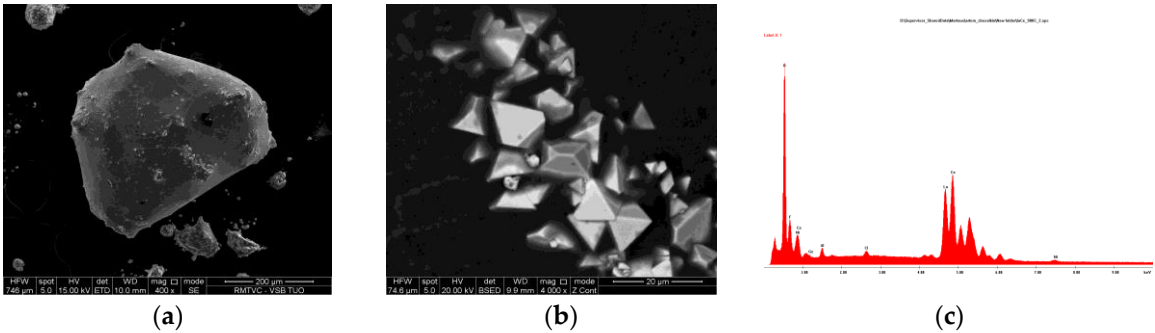
Tables 8,9 show composition of the (LaCe)Ni<sub>5</sub> sample, prepared at 900°C. Figures 11,12 show the SEM analysis images and spectrum of the prepared alloy.

Table 8. Sample (LaCe)Ni<sub>5</sub> prepared at 900 °C (La-Ce-O composition).

Element	Wt, %	At, %	Z	A	F
O	25,79	63,67	1,1872	0,4125	1,0003
Cl	0,56	0,62	1,1018	0,6892	1,0103



La	27,66	7,87	0,8626	1,0374	1,0002
Ce	36,58	10,31	0,8687	1,0421	1,0003
Ni	0,56	0,38	1,0525	0,9109	1,0002
other	8,85	17,15			
Total	100,00	100,00			



**Figure 11.** (LaCe)Ni<sub>5</sub> sample prepared at 900 °C : (a) sample view at 400 x zoom SEM analysis ; (b) sample view at 4000 x zoom SEM analysis ; (c) SEM spectrum

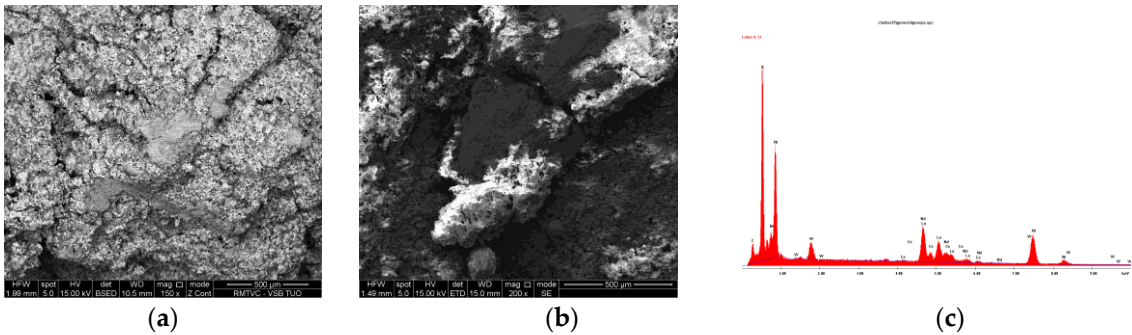
3.2. Analysis results of La-Ni based alloys prepared from pure powder metals

3.2.1. LaNi<sub>5</sub> alloy analysis results

Tables 9-11 show composition of the LaNi<sub>5</sub> sample, prepared at 1500°C. Figures 12,13 show the SEM analysis images and spectrum of the prepared alloy.

**Table 9.** Sample LaNi<sub>5</sub> prepared at 1500 °C (La-Ni-O composition).

Element	Wt, %	At, %	Z	A	F
O	22,88	49,25	1,1632	0,4157	1,0005
La	23,59	5,85	0,8079	1,0239	1,0102
Ni	25,42	14,91	1,0132	0,9729	1,0051
other	28,11	29,99			
Total	100,00	100,00			



**Figure 12.** LaNi<sub>5</sub> sample prepared at 1500 °C : (a) sample view at 150 x zoom SEM analysis ; (b) sample view at 200 x zoom SEM analysis ; (c) SEM spectrum

**Table 10.** Sample LaNi<sub>5</sub> prepared at 1500 °C (La-Ni-O composition, La-phase).

Element	Wt, %	At, %	Z	A	F
---------	-------	-------	---	---	---

O	6,60	32,62	1,3119	0,4569	1,0004
La	74,13	42,19	0,9227	1,0096	1,0062
Ni	13,41	18,05	1,1703	0,9452	1,0007
other	5,86	7,14			
Total	100,00	100,00			

Table 11. Sample LaNi<sub>5</sub> prepared at 1500 °C (La-Ni-O composition, Ni-phase).

Element	Wt, %	At, %	Z	A	F
O	8,74	23,81	1,1702	0,4254	1,0014
La	16,14	5,07	0,8098	1,0239	1,0312
Ni	50,20	37,27	1,0117	0,9889	1,0000
other	24,92	33,85			
Total	100,00	100,00			

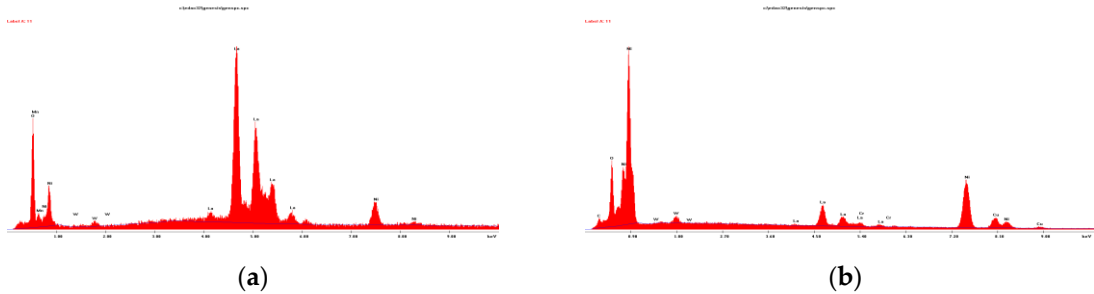


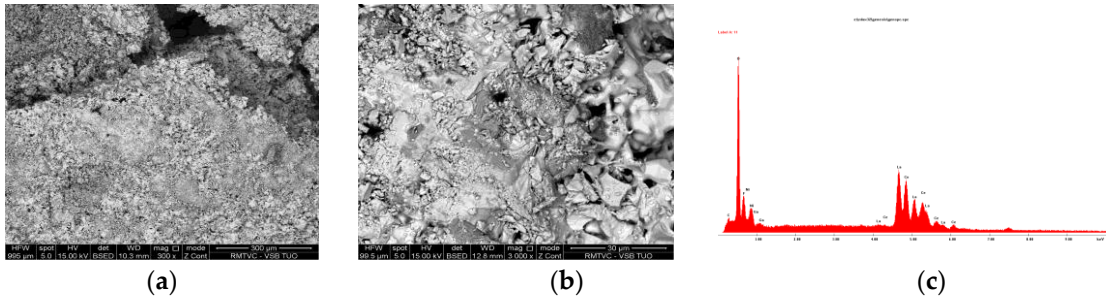
Figure 13. LaNi<sub>5</sub> sample prepared at 1500 °C: (a) SEM spectrum La dominant phase ; (b) SEM spectrum Ni dominant phase

3.2.2. (LaCe)Ni<sub>5</sub> alloy analysis results

Tables 12 shows composition of the (LaCe)Ni<sub>5</sub> sample, prepared at 1500°C. Figures 14 shows the SEM analysis images and spectrum of the prepared alloy.

Table 12. Sample (LaCe)Ni<sub>5</sub> prepared at 1500 °C (La-Ce-Ni-O composition).

Element	Wt, %	At, %	Z	A	F
O	17,14	47,61	1,2319	0,4578	1,0003
Ce	32,53	10,32	0,8671	1,0219	1,0025
La	34,83	11,14	0,8619	1,0193	1,0020
Ni	6,88	5,21	1,0585	0,4101	1,0000
other	8,62	25,72			
Total	100,00	100,00			



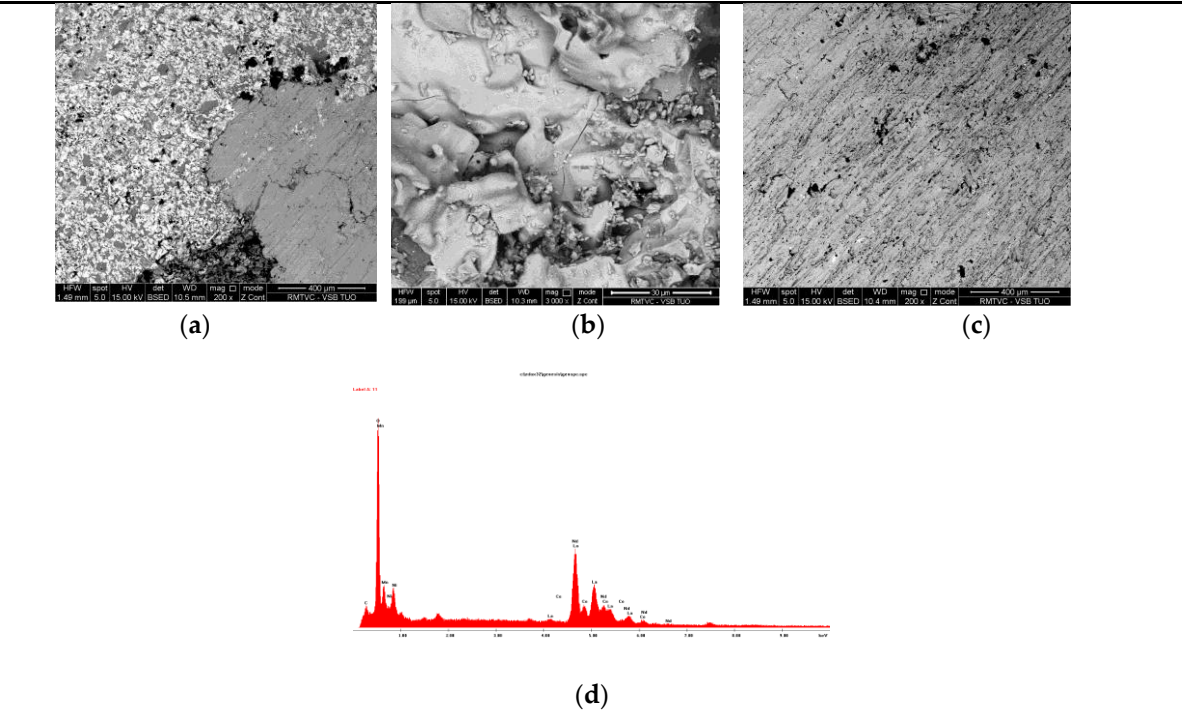
**Figure 14.** (LaCe)Ni<sub>5</sub> sample prepared at 1500 °C : (a) sample view at 300 x zoom SEM analysis ; (b) sample view at 3000 x zoom SEM analysis ; (c) SEM spectrum

3.2.2. (LaMm)Ni<sub>5</sub> alloy SEM and XRD analysis results

Tables 13 shows composition of the (LaMm)Ni<sub>5</sub> sample, prepared at 1500°C. Figures 15 shows the SEM analysis images and spectrum of the prepared alloy.

**Table 13.** Sample (LaMm)Ni<sub>5</sub> prepared at 1500 °C (La-Ce-Fe-Nd-O composition).

Element	Wt, %	At, %	Z	A	F
O	15,84	42,31	1,2112	0,4423	1,0008
Fe	17,65	13,73	1,0022	0,5499	1,0002
La	34,00	10,46	0,8438	1,0249	1,0164
Ce	9,45	2,88	0,8486	1,0272	1,0156
Nd	5,49	1,63	0,8473	1,0301	1,0056
other	17,57	28,99			
Total	100,00	100,00			



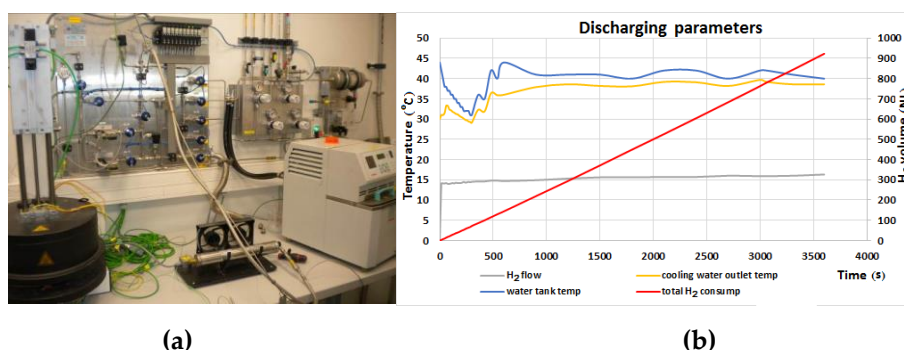
**Figure 15.** (LaMm)Ni<sub>5</sub> sample prepared at 1500 °C : (a) sample view with phase separation at 200 x zoom SEM analysis ; (b) sample view at 3000 x zoom SEM analysis ; (c) sample view phase – Ni at 200 x zoom SEM analysis (d) SEM spectrum.

4. Discussion

As can be seen from the results of the qualitative analysis of alloys, most samples were susceptible to oxidation during alloys preparation or subsequent analysis. Nevertheless, the least oxidized samples were confirmed by further analysis of the possibility of hydrogen sorption. In this paper, careful results of hydrogen adsorption on each of the samples will not be described. The following describes the hydrogen desorption parameters in (LaCe)Ni<sub>5</sub> alloy as on one of the most successful prepared samples.

For discharging of the alloy was used a fuel cell type “Nexa Ballard System” like device with stable and easy to controlled and if necessary, easily variable hydrogen consumption. Constant hydrogen flow is a most important parameter for user or hydrogen consumer (in that case consumer

is a fuel cell) and thanks to integrated in a fuel cell mass flow meter was possible to control and regulate the discharge flow. In other way free discharge flow without regulation provide very sharp temperature decreasing on a metal hydride side.



**Figure 16.** Hydrogen desorption from the metal hydride storage based on (LaCe)Ni<sub>5</sub> alloy (a) basic view of the discharging process (b) discharging parameters

Figure 16 shows the metal hydride discharging process and main discharging parameters. Presence of fuel cell together with the hydrogen storage can be used like the energy storage system and gives possibility to use hydrogen like a source of electrical energy. The connection of fuel cell to the electric load instead of the any grid could provide the effective regulation of discharging flow depends on the fuel cell consumption profile – the regulation of thermal impact during hydrogen desorption cycles. Future works on the synthesis of alloys will be carried out with careful protection of the alloy components and the subsequent products from oxidation. Analysis of alloys not exposed to oxidation will give a complete picture of the possibilities of future La-Ni based alloys modification and the ways of final product cost reducing and hydrogen sorption capacity increasing.

## 5. Conclusions

Results of chemical composition analysis of La-Ni based alloy samples gave useful information about exist problem with alloys synthesis from metal chlorides such as a choosing of optimal time-temperature working parameters of synthesis, which from one side should be enough for creation desired LaNi<sub>5</sub> phase during synthesis, and from other side should be as shorter as possible for energy and time consumption reducing of the synthesis process. Cost of the reagents, which should be used for alloy preparation and respectively cost of the final alloy is the second important issue and the reason why the La-Ni alloys in this job were synthesized from metal chlorides. Next synthesis should be carried out at increased temperature sample holding stage for fully LaNi<sub>5</sub> phase creation.

Studies of properties, kinetics of different alloys based on metals like La, Ce, Ni or another metals together with polymers, modification of traditional alloys and creation of totally new artificial materials will provide a development of new energy area – hydrogen energetics and hydrogen mobility. Low storage pressure with big amount of stored hydrogen together with a small physical volume of storage vessels provides a big advantage for final user of that system in comparison with classic hydrogen storage methods.

Next researching and modifications of La-Ni based alloys could provide increasing of hydrogen storage capacity and material costs decreasing, that allows to use these storage systems not only in laboratory scale.

**Acknowledgments:** This work was supported by ENET Centre – Research Centre of Energy Units for Utilization of Non Traditional Energy Sources, Ostrava, CZ., and CET- Centre for Environmental Technology, Ostrava, CZ, supported by the project LO1404: Sustainable development of ENET Centre and project CZ.1.05/2.1.00/19.0389: Development of the research infrastructure of the ENET Centre.

**Author Contributions:** Artem Chesalkin conceived, designed and performed the experiments, contributed reagents/materials. Petr Modrik provided the TCO and alloys application description. Alexandr Martaus performed the XRD and SEM analysis of prepared alloys. All authors contributed to the writing of the paper.



**Conflicts of Interest:** The authors declare no conflict of interest.

## References

1. Rather S., Mehraj-ud-din N., Zacharia R., Hwang S.W., Kim A.R., Nahm K.S. Hydrogen storage of nanostructured TiO<sub>2</sub>-impregnated carbon Nanotubes, *International Journal of Hydrogen Energy* 34 (2009) 961–966.
2. Zacharia R., Kim K.Y., Hwang S.W., Nahm K.S. Intrinsic linear scaling of hydrogen storage capacity of carbon Nanotubes with the specific surface area, *Catalysis Today* 120 (2007) 426–431.
3. Srinivas G., Sankaranarayanan V., Ramaprabhu S. Kinetics of hydrogen absorption in Ho<sub>1-x</sub>MmxCo<sub>2</sub> alloys, *Journal of Alloys and Compounds* 448 (2008) 159–165.
4. McRae G.A., Coleman C.E., Leitch B.W. The first step for delayed hydride cracking in zirconium alloys, *Journal of Nuclear Materials* 396 (2010) 130–143.
5. Dong C.F., Liu Z.Y., Li X.G., Cheng Y.F. Effects of hydrogen-charging on the susceptibility of X100 pipeline steel to hydrogen-induced cracking, *International Journal of Hydrogen Energy* 34 (2009) 9879–9884.
6. Madina V., Azkarate I. Compatibility of materials with hydrogen. Particular case: hydrogen embrittlement of titanium alloys, *International Journal of Hydrogen Energy* 34 (2009) 5976–5980.
7. J. Huot, *Metal Hydrides*, in *Handbook of Hydrogen Storage*, M. Hirscher, Wiley-VCH Verlag GmbH & Co. KGaA, Weinheim, Germany, 2010.
8. John B. Heywood, *Internal Combustion Engine Fundamentals*, table D.4 page 915
9. L. Zaluski, A. Zaluska, P. Tessier, J.O. Ström-Olsen, R. Schulz, Catalytic effect of Pd on hydrogen absorption in mechanically alloyed Mg<sub>2</sub>Ni, LaNi<sub>5</sub> and FeTi, *Journal of Alloys and Compounds*, Volume 217, Issue 2, 1 February 1995, Pages 295-300 (296).
10. B. Sakintuna, F. Lamari-Darkrim, M. Hirscher, Metal hydride materials for solid hydrogen storage: A review, *International Journal of Hydrogen Energy*, Volume 32, Issue 9, June 2007, Pages 1121-1140 (1128)
11. <http://energy.gov/eere/fuelcells/hydrogen-storage> Office of Energy Efficiency and Renewable Energy
12. G. Sandrock, A panoramic overview of hydrogen storage alloys from a gas reaction point of view, *J. Alloys and Compounds*, 293-295 (1999) p. 877-888.
13. Schlapbach, L., Anderson, I., and Burger, J.P. (1994) Hydrogen in metals, in *Electronic and Magnetic Properties of Metals and Ceramics Part II*, vol. 3B (ed. K.H. Jurgen Buschow), VCH, Weinheim, p. 271.
14. Libowitz, G.G. (1991) presented at the Hydrogen Storage Materials, Batteries, and Electrochemistry, Phoenix, Arizona, *Electrochemical Society Proceedings* (eds D.A. Corrigan and S. Srinivasan), 92-5, 3.
15. Flanagan, T.B. (1977) presented at the Hydrides for Energy Storage, Geilo, Norway, Pergamon (eds A.F. Andresen and A.J. Maeland).
16. Flanagan, T.B. and Oates, W.A. (1988) Thermodynamics of Intermetallic Compound-Hydrogen Systems, in *Hydrogen in Intermetallic Compounds I* (ed. L. Schlapbach), Springer Verlag, Berlin, p. 49.
17. Griessen, R. and Riesterer, T. (1988) Heat of formation models, in *Hydrogen in Intermetallic Compounds I* (ed. L. Schlapbach), Springer-Verlag, Berlin, pp. 219.
18. Yamaguchi, M. and Akiba, E. (1994) Ternary hydrides, in *Electronic and Magnetic Properties of Metals and Ceramics Part II*, vol. 3 (ed. K.H. Jurgen Buschow), VCH, Weinheim, p. 333.
19. 44 Fukai, Y. and Okuma, N. (1993) *Jpn. J. Appl. Phys.*, 32, L1256.
20. G.Giresan, S.R. Sankaranarayanan, L.J. Berchman, Investigation on the thermodynamic analysis, preparation and characterization of LaNi<sub>5</sub> – hydrogen storage alloy by magnesiothermic reduction diffusion process, Tamilnadu, India.
21. S. Kamasaki, Y. Misaki, T. Kanayama, M. Yamada, Surface modification of hydrogen storage alloy LaNi<sub>5</sub> by milling with Al and Co powders, *Hyomen Gijutsu Kyokai*, Tokyo, (1989)
22. A. Ursua, I. San Martin, E.L. Barrios, P. Sanchis, Stand-alone operation of an alkaline water electrolyser fed by wind and photovoltaic systems. *International Journal of Hydrogen Energy*, 2013, vol. 38, no. 35, pp. 14952–14967.
23. F. Barbir, PEM electrolysis for production of hydrogen from renewable energy sources. *Solar Energy*, 2005, vol. 78, no. 5, pp. 661–669.
24. A. Yilanci, I. Dinger, H.K. Ozturk, A review on solar-hydrogen/fuel cell hybrid energy systems for stationary applications. *Progress in Energy and Combustion Science*, 2009, vol. 35, no. 3, pp. 231–244.
25. D. Minarik, B. Horak, P. Moldrik, Z. Slanina, An experimental study of laboratory hybrid power system with the hydrogen technologies. *AEEE Advances in Electrical and Electronic Engineering*, 2014, vol. 12, no. 5, pp. 518-528.



26. <http://www.actaspa.com/products/aes250/>,<http://www.actaspa.com/wp-content/uploads/2013/08/AES500-1000.pdf> "ACTA AES500-1000 technical data sheet.
27. <http://www.lac.cz/en/furnaces-and-dryers/vp-high-temperature-furnace> "LAC VP20/17 technical parameters".