

The Mechanical Properties Enhancement of Biodegradable Aminofunctional Starch/Carboxylate Nitrile Butadiene Rubber Latex Films

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Abstract

The Aminofunctional starch/Carboxylated nitrile butadiene rubber (ANS/XNBR) latex films were prepared with control (0), 5, 10, 15, and 20 phr of ANS loadings. The films were subjected to soil burial test for 8 weeks, which recovered every two weeks to quantify the degraded properties. The control (week 0) and biodegraded films were subjected to physical tests (crosslink density, tensile, and tear strength tests) and biodegradation quantification (mass loss retention, and water vapor transmission rates). The optimum physical properties of ANS/XNBR films were subjected to further assessment of its degradation properties which include morphological (optical and scanning electron microscopes (SEM)), Fourier transform infrared (FTIR) analysis, and thermogravimetric analysis (TGA) respectively. Overall, mechanical properties of biodegraded ANS/XNBR latex films decreased as biodegradation period elapses. The biodegradation assessment via water vapor transmission rates and mass loss analyses indicates the high degree of biodegradation rates were observed with higher loading of ANS/XNBR latex films. Morphological analyses via optical microscope shows the transformation of the films surface opacity during biodegradation test. SEM images depicted the microorganism remains on the film surfaces. For FTIR analysis, the most significant changes in the spectras of the films appeared in the region of 790–3000 cm⁻¹. TGA thermograph shows the thermal retention of the materials decreased, as the biodegradation period elapses for optimum ANS/XNBR latex films. From the results obtained, ANS/XNBR latex films shows optimum degradation and mechanical properties at 10 phr filler loading.

Keywords: - Aminofunctional starch (ANS), biodegradation, carboxylated nitrile butadiene rubber (XNBR) latex films.

1. Introduction

Carboxylated nitrile butadiene rubber (XNBR) latex is a colloidal dispersion of acrylonitrile-butadiene-carboxylate terpolymer in a water based medium [1]. The latex is used as a substitute material for nitrile butadiene rubber latex in the production of latex-dip articles. The material has the ability to form an ionic crosslinking, providing an alternative rubber curing system with the absence of an accelerator [2]. Accelerator free latex compound or products provides a less potential of encountering type IV hypoallergenic problem which occurs due to the delay reaction of nitrosamine and nitrosatable compounds [3]. Thus, medical devices which made from the XNBR latex provide better hypoallergenic retention.

However, synthetic latex films are difficult to degrade when disposed [4]. This is due to the lack of an organic substance, such as proteins, lipids, or carbohydrates on the surface of rubber particles and its dispersing medium to be consumed by the microorganism. Thus, attempts were made by introducing a bio-filler such as starch into XNBR latex compound. Starch granules consist of polysaccharide macromolecules of branched amylopectin and straight chain of amylose [5]. They are closely packed with a multiple layer of crystal and amorphous structure of its polymeric chain within the starch granules [6]. As the glucopyranosyl group of starch consist of 3 three hydroxyl groups attached to the main chain, the starch tends to form strong hydrogen bonding among their molecules which resulting in the formation of filler agglomeration during XNBR latex compounding [7]. Thus, modification of its functional group was done by grafting with the acrylonitrile monomer to produce aminofunctional starch (ANS). The similar functional group of ANS with XNBR increases the homogeneity of the filler dispersion in the latex compound [8].

Conventionally, for materials which are enriched with bio fillers, two types of degradation may occur during biodegradation test. First, the ability to degrade is due to the interaction of the materials with surrounding environment such as the soil pH, humidity, and thermo-mechanical induced environment. This type of degradation which takes place on the surface of the materials up to the molecular level refers to the environmental induced degradation.

As for microorganism induced degradation (biodegradation), the process involves an enzymatic reaction which secreted by potential degrading microorganisms that resides on the surface of the polymeric materials [9]. At first, the microorganism will secrete an enzyme which could solubilize the surface of the polymeric materials and convert the polymers into water soluble extract. The extract would then be consumed by the microorganism as their

source of nutrients [9]. These complex processes actually could be quantified by examining the formation of microorganisms' colony on the surface of polymer substrate and the progress could easily be quantified by observing the behavior of the microorganisms' colony under microscope. However, to further quantify the progress, several techniques also could be employed. In contrast to the environmental induced degradation, biodegradation usually unnoticed at an early stage and could only occur selectively [10].

In previous research, the ability for ANS/XNBR latex films to biodegrade after 8 weeks of soil burial is confirmed by observing the degraded film surface morphology. The formation of microorganism colonies was detected on the 2nd week of biodegradation assessment. The microorganisms' colonies number and size were increased as the biodegradation period elapses. Even though the biodegradability of ANS/XNBR latex is promising, the results also indicate that, mixing the ANS with XNBR latex compound, it decreased the latex films green strength [8]. The reduction is related to the thermoplastic properties of the starch that lower the films modulus contribute to failure at low stress [11]. Apart from that, it is postulated that the reduction of crosslinking formation between rubber macromolecules also contributes towards the properties decrement. Thus, in order to leverage the physical properties decrement with biodegradability of latex films, a study on the optimum loading was conducted to determine the optimum ANS filler loading that could be admixed during latex compounding.

2. Materials and methods

2.1. Preparation of amino functional starch (ANS)

Sago starch was gelatinized at 80°C with sodium hydroxide (NaOH) by heating mantle in a reaction flask together with five round-neck stoppers. Nitrogen gas was purged in and out to provide an inert environment during the reaction. After the starch gelatinized, the paste was cooled down to 60°C. An initiator reagent (mixture of Ceric (V) ammonium nitrate and 70% Nitric acid) was added and mixed for 10 minutes. Purified acrylonitrile was added and the paste was stirred for 2 hours at 600 rpm. Table 1 indicates the formulations for preparation of amino functional starch. The ANS degree of substitution as reported is 0.464 [8].

Table 1: The formulations for preparation of amino functional starch

Ingredients	Value	Unit
Sago starch	50.0	g
10 % potassium hydroxide	12.3	g
Initiator reagent	16.5	g
Purified acrylonitrile	3.0	Mol/AGU*
DI Water	250.0	g

*mol/AGU = mol per one anhydroglucose unit of starch

2.2. Compounding and latex film preparation process.

Prior addition of ANS paste, the pH was adjusted with aqueous potassium hydroxide (KOH) to the pH of XNBR latex compound. The ingredient to prepare the ANS/XNBR latex was indicated in Table 2. ANS/XNBR latex compound were prepared with control (0), 5, 10, 15, and 20 phr loading of ANS in XNBR latex compound. XNBR latex was first mixed with KOH to stabilize the latex and stirred at 270 rpm. Subsequently, the others chemical ingredients were added, followed by the addition of ANS paste and the compound was stirred for an hour. The compound was pre – vulcanized for 1 hour at a temperature of 80°C followed by maturation process for 24 hours under room temperature.

The latex films were prepared through the coagulant dipping process. Clean aluminium plate was dipped into coagulant (10% calcium nitrate) for 10 seconds and dried in a convection oven for 15 minutes at a temperature of 100°C. The plate was taken out and recondition under room temperature until the plate temperature reduced to 50C. The plate was dipped into ANS/XNBR latex compound for 17 seconds and cured in convection oven for 1 hour at a temperature of 100°C. The ANS/XNBR latex films were designated as ANS/XNBR *x*, where *x* = loading of phr (e.g. ANS/XNBR 5).

115 Table 2: Compounding formulation for production of amino functional starch (ANS) /
116 carboxylated nitrile butadiene rubber latex film.

Ingredients	Dry weight, phr	Wet weight, g
44.80 % XNBR latex	100.00	223.21
10.00 % KOH	1.00	0.10
42.15 % MBT	0.15	0.36
30.80 % TMTD	0.15	0.49
55.40 % ZnO	1.50	2.71
27.65 % ZDEC	0.70	2.53
26.70 % AnO	0.50	1.87
36.10 % S	0.50	1.39
10.00 % ANS dispersion	*	**

117 * The ANS concentration were varied from 5, 10,15, and 20 phr.

118 **2.3. Biodegradation procedure and testing**

119 The biodegradation test was conducted for 8 weeks. The control and ANS/XNBR latex films
120 were divided into 5 sub series according to the week of recovery. All the films were buried in
121 a controlled soil. The soil pH and moisture were monitored by 3 in 1 soil tester and were kept
122 at 80% RH throughout the biodegradation test. The samples were taken out every two weeks.
123 The samples were then leached in distill water at room temperature for 15 minutes and dried
124 in an open air for 18 hours.

125 **2.4. Swelling test**

126 Small samples of the dried XNBR latex films were cut (2 x 2 cm), weighed and placed in
127 glass vials which were filled with chloroform. The vials were stored at 21°C for 48 h. The
128 samples were taken out of the solvent, placed in the air for 30 s to ensure that the solvent was
129 evaporated from the surface and were weighed again. The network density was calculated
130 using Equation 1,

$$V = \frac{-\ln(1-V_p) + V_p + \chi V_p^2}{V_s(V_p^{1/2} - \frac{V_p}{2})} \quad (1)$$

Where; V_P is the volume fraction of the polymer in the swollen state, V_S the molar volume of the solvent, and χ the Flory-Huggins interaction parameter. The Flory-Huggins interaction parameter was calculated with the following equation, $\chi = 0.487 + 0.228 \times V_P$ [12].

The density of the XNBR latex films ($\rho_{polymer}$) was determined by the hydrostatic weighing method using a Sartorius balance (Goettingen, Germany) with a resolution of ± 0.1 mg. The apparent weight of the post-cured XNBR films was measured in air and n-heptane and the density was calculated according to Equation 2.

$$\rho_{polymer} = \frac{(G_{n-heptane} \times \rho_{air})}{(G_{air} - G_{n-heptane})} \quad (2)$$

Where; $\rho_{n-heptane}$ and ρ_{air} were the densities of air and n-heptane at 20°C. G_{air} corresponds to the weight determined in atmosphere and $G_{n-heptane}$ was the weight determined in n-heptane. Ten samples were measured and the resulting means value of the density of cross linked XNBR films was $\rho_{XNBR} = 1.013 \text{ g/cm}^3$. For biodegraded sample, after the samples had recovered, the samples were washed with distilled water before subjected to swelling test.

2.5. Tensile test

Tensile test was conducted by using Instron 3366, Machine (Norwood, MA, US) according to ASTM D 412-06. The specimens were cut into dumbbell shape and the thickness of each test piece was recorded. The crosshead speed was set at 600 mm/min. Five samples were prepared and the average values were calculated. For biodegraded sample, after sample recovery, the samples were washed with distilled water and sanitized with ethanol before subjected to tensile test.

2.6. Tear test

Tear test was conducted by using Instron 3366 Machine (Norwood, MA, US) according to ASTM D 624-00. The specimens were cut into crescent shape (Die C) and the thickness of each test piece was recorded. The crosshead speed was set at 200 mm/min. Five samples were prepared and the average values were calculated. For biodegraded sample, after the samples had recovered, the samples were washed with distilled water and sanitized with ethanol before subjecting to tear test.

2.7. Fourier transform infrared (FTIR) analysis

FTIR analysis was carried out with Perkin Elmer Spectrum One spectrometer (Shelton, USA), with wave number ranging from 550 to 4000 cm^{-1} with resolution of 0.5 cm^{-1} . The surface of the samples was screened by DinoliteTM digital microscope and the most severe parts were subjected to FTIR analysis.

2.8. Optical microscope analysis

The surface of latex films was captured by Meiji digital microscope (San Jose, CA, US) with 10 times magnification. The control and biodegraded samples were washed with distill water and dried in a desiccator to remove any stain or dirt.

2.9. Scanning electron microscope (SEM) analysis

SEM analysis was carried out using a Zeiss Supra 35 VP SEM (Oberkochen, Germany) machine with magnification of 5000, and 25000 X. The voltage acceleration was set at 5 KV. The sample was mounted on aluminium specimen stubs and coated with a plasma ion before analysis. For biodegraded samples, the films were sanitized with chloroform before coating to eliminate foreign substances which may interrupt the coating process. For biodegraded sample, the films were sanitized by ethanol before SEM analysis were conducted. The samples were screened thoroughly by DinoliteTM digital microscope to qualitatively assess the biodegradation process of the films. After the most biodegraded part of the film was determined, the sample was cut into small piece and the desired part was subjected to the SEM analysis.

2.10. Thermo-gravimetric analysis (TGA)

Thermo gravimetric analysis (TGA) was carried by Perkin Elmer Pyris 6 (Waltham, USA) machine in a nitrogen environment. 7 mg of sample was transferred into an aluminum pan and placed in the designated sample chamber. The temperature was set from 30°C to 600°C at heating rates of 10°C/min. For biodegraded sample, the samples were washed with distill water and sanitized with ethanol before subjecting to TGA test.

2.11. Water vapor transmission (WVT) analysis

WVT analysis was done according to ASTM E96. Biodegraded control and ANS/XNBR latex films were cut into 15 x 15 cm. A cup was filled with silica gel and ANS/XNBR latex films were used to cover the top of the cup. The cups were then being inserted into

desiccators with a bowl of water at the bottom to ensure a high humidity environment. The desiccator was then sealed to prevent vapor loss except through the test sample. An initial weight was taken and then periodically weighed every day until constant weight was obtained. The increment of weight was monitored until constant weight was achieved. Graph of weight gain against the period of testing was plotted and the best straight line was drawn to obtain the respective gradient. The gradient obtained was divided with the open area of the tested samples. ANS/XNBR latex films WVT rates were calculated by using Equation 3.

$$\text{Water vapor transmission rates, g day}^{-1} \text{ cm}^{-2} = \frac{\left(\frac{\text{Final mass, g} - \text{Initial mass, g}}{\text{week, days}} \right)}{\text{Film's open area, cm}^2} \quad (3)$$

For biodegraded sample, after the samples were recovered, and washed with distill water before the WVT rate measurement.

2.12. Mass loss analysis

Biodegraded control and ANS/XNBR latex films were taken out every two weeks. The weight of the films was measured after the films were leached with distill water and dried at room temperature for 18 hours. The films mass retention was calculated according to Equation 4.

$$\text{Mass retention} = \frac{(\text{Initial mass, g} - \text{final mass, g})}{\text{Initial mass}} \times 100 \quad (4)$$

3. Results and discussion

3.1. Mechanical properties

3.1.1. Crosslink density.

From Figure 1 (a), as the biodegradation weeks progressed, the crosslink density of both control and ANS/XNBR latex films reduced with ANS/XNBR latex films undergoes a higher degradation process compared to control films.

216

217 Table 3: Percentage of mechanical properties retentions for biodegraded ANS/XNBR latex
218 films.

Week of recovery	2	4	6	8
(a) Percentage of crosslink density retention, %				
Control	87.7	28.3	17.6	13.1
ANS/XNBR 5	117	57.6	49.3	32.8
ANS/XNBR 10	153.3	74.3	53.7	30
ANS/XNBR 15	105.3	52.1	44.7	31.3
ANS/XNBR 20	-	60	45	20.7
(b) Percentage of tensile strength retention, %				
Control	100	94	84	72
ANS/XNBR 5	106	93	74	66
ANS/XNBR 10	112	109	85	65
ANS/XNBR 15	105	79	74	59
ANS/XNBR 20	106	81	76	63
(c) Percentage of elongation at break retention, %				
Control	99	98	98	94
ANS/XNBR 5	95	92	91	86
ANS/XNBR 10	94	93	88	87
ANS/XNBR 15	87	86	85	81
ANS/XNBR 20	96	89	89	85
(d) Percentage of tear strength retention, %				
Control	96	81	74	72
ANS/XNBR 5	111	80	74	69
ANS/XNBR 10	94	75	71	62
ANS/XNBR 15	93	71	71	53
ANS/XNBR 20	79	56	43	40

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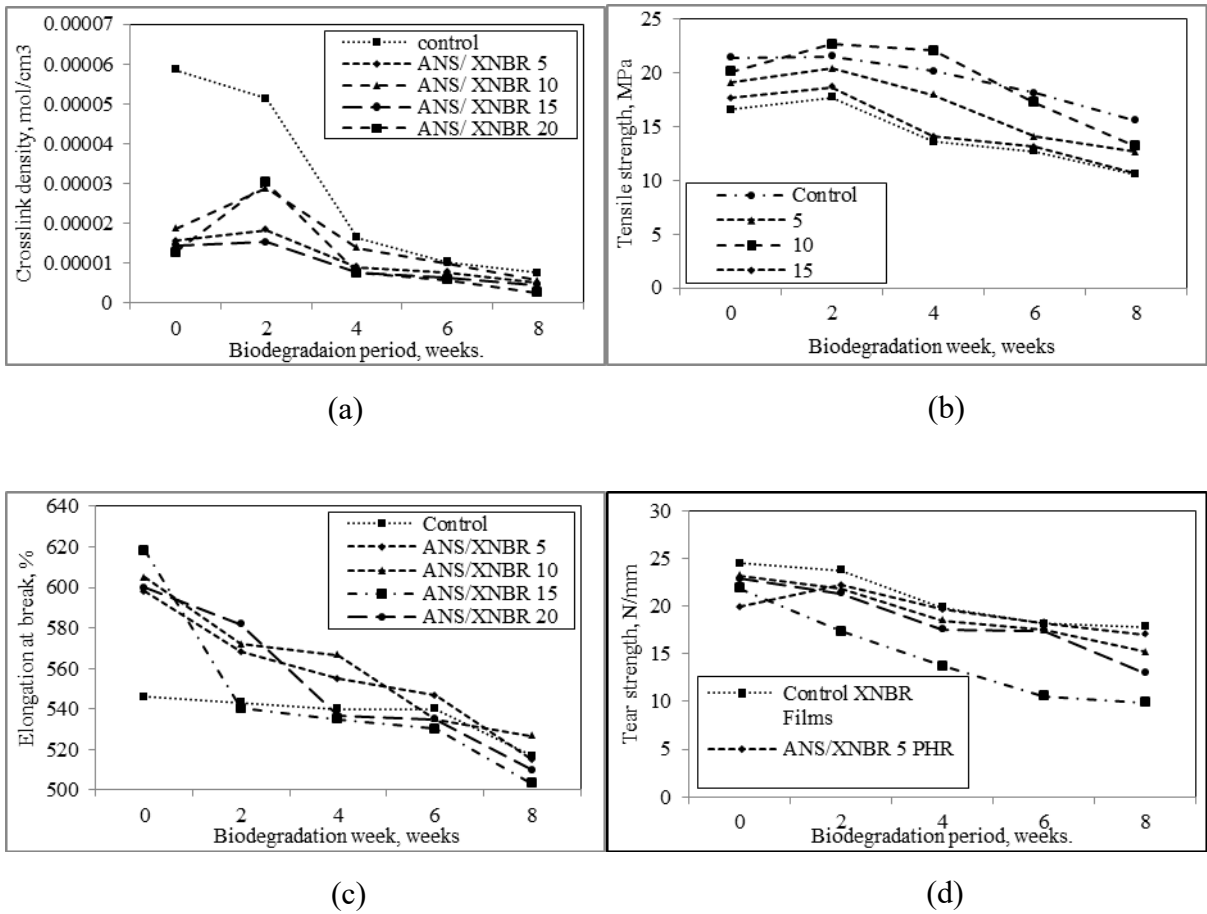


Figure 1: Mechanical properties of biodegraded ANS/XNBR latex films with respect to their weeks of biodegradation. (a) crosslink density, (b) tensile strength, (c) tear strength, and (d) elongation at break for biodegraded ANS/XNBR latex films.

The addition of ANS into XNBR latex films reduced the crosslink density of the films with ANS/XNBR 20 suffer the lowest. ANS/XNBR 10 shows the highest crosslink density compared to other ANS/XNBR latex films. At the eighth weeks of the biodegradation, the properties decreased for all films.

As indicated in Table 3 (a), for ANS/XNBR latex films, at second week of biodegradation, the films crosslink density increases up to 53% from its original value. In contrast, for control films, almost 12.3% of the crosslinks had been decreased. All films show a decreased in the crosslink density at the fourth week of biodegradation process. The highest reduction was observed for ANS/XNBR 10 and 20 with 79% and 176% reduction from the previous value recorded indicating rapid biodegradation process compared to other ANS/XNBR films.

For control XNBR latex film, at zero week, the high crosslink density was contributed by the formation of both ionic and sulfur covalent bonding [2]. As the biodegradation process proceeds, the property decreased significantly. The reduction in crosslink density is believed to be due to the solvation of ionic cluster during the biodegradation process [2, 13, 14]. The solvation effect occurred due to the presence of nitrogen element in the compost soil, which was able to solvate the interaction between zinc and oxide ions in the ionic crosslinking system.

Meanwhile, the lower crosslink density in ANS/XNBR latex films is due to the occupation of ANS in between rubber macromolecules and hindering the formation of ionic or a sulfur covalent bond. As the biodegradation process progress, the reduction in ANS volume reduced due to microorganism consumption. At second week of the degradation process, due to less hindrance in between adjacent rubber macromolecules in the films, the curing process might occur and further increased the films crosslink density for ANS/XNBR latex films.

For control XNBR latex film, during biodegradation period, it is believed that physical degradation might take place dominantly compared to microorganism induced degradation. This is evidenced by the trends shown in Figure 1 (a) that the reduction in crosslink density is proportional to the period of biodegradation. For the ANS/XNBR latex films, the fluctuation in crosslinks density experienced are due to the fluctuation of ANS volume in the films which open the possibility for further crosslinking to occur during the process. This is supported by the fact that the curative agents used in all films are similar as indicated in Table 2.

3.1.2. Tensile strength.

From Table 3 (b), in general, the addition of ANS into XNBR latex compound decreased the percentage of tensile retention for ANS/XNBR latex films. It is also indicated that for the second weeks of biodegraded samples, the tensile strength increased with the increased of the crosslink density of the films (Figure 1 (a)). The reduction in tensile strength for the ANS/XNBR latex films was postulated to be due to at least two factors which are; (1) reduction of polymer molecular weight of ANS and XNBR macromolecules, and (2) formation of void/free volume on/in the films.

For the reduction of polymer molecular weight, the process could occur in both ANS and XNBR latex macromolecules. For ANS, the reduction was due to a dextrination process of polysaccharide chain. Such reduction occurred due to the exposure of the films to a certain

temperature during drying process or due to the enzymatic reaction which induced hydrolysis process in the polysaccharide chain when the sample were buried in the soil [15]. For the dextrination of the polysaccharide chain due to environmental degradation, these phenomena were mainly due to the oxidation process. Similar pathways were postulated to occur in biodegraded samples.

For chain hydrolysis, due to hydrophilicity of ANS and XNBR latex, it could absorb the moisture from the soil to be resided interstitially within the films [16, 17, 18]. These processes could induce an interaction between polysaccharide chains of ANS with water molecules and hence, the hydrolysis of the polysaccharide chain occurred through breakage of the 4C_1 glucosidic linkages. The phenomenon was best described by Yakubu et al. [19] where reduction in starch enriches sample shown a decreasing trend in its tensile strength as the water uptake increases.

For a chain hydrolysis which were induced by enzymatic reaction, as the water uptakes by the sample increased, the ability of the microorganism to grow and utilize the polysaccharide as their sole source of nutrients. The ability of ANS to be degraded by the microorganism (biodegrade) was well studied by Navarchian et al. and Saroja et al. [20, 21]. Meanwhile, for XNBR latex, the degradation was mainly due to the physical process where the failure of the films was due to the reduction of crosslink density in the films. This was confirmed by the reduction trends in control films despite there was no addition of ANS.

For the reduction of tensile strength due to the increase of free volume/voids in biodegraded samples, the factor was the manifestation of aforementioned mechanisms. These free volume usually formed in a starch rich region and will be occupied by microorganism colony due to high nutrient in the region. As the biodegradation process proceeded, the increased in the size and number of free volume resulting in the film unable to absorb any forces exerted and breaks at lower tensile strength.

3.1.3. Elongation at break

From Figure 1 (c), Addition of ANS into XNBR latex compound increased the films elongation at break. However, the elongation at break (EB) for all film decreased with prolonged biodegradation weeks. For control films, even though the EB showed a decreasing trends alongside ANS/XNBR latex films, based on the calculated percentage of EB retention

shown in Table 3 (c), the films with ANS loading has degraded more compared to control XNBR latex films.

For control films, the rigidity of the films are the results of a dual crosslinking system. These high density of crosslink network restricts the rubber molecules to deform during applied stress. Thus, even though the film is able to withstand high tensile stress, the films become more rigid. For ANS/XNBR latex films, even though the crosslink is lesser than control films, the ability of the glucopyranosyl ring of starch to deform from a chair to a boat like structure contributes towards the ability of the films to elongate [22].

Table 3 (c) indicates that, as the ANS loading increases, the films undergo a higher reduction in its percent of EB retention. The EB of ANS depends on the flexibility of the ANS segmental chain. Thus, a reduction in its molecular chain has reduced the ability of the polysaccharide molecules to deform with applied stress [23]. Thus, it concludes that the addition of ANS contributes to the ability of the films to elongate upon application of stress.

3.1.4. Tear strength.

As shown in Figure 1(d), the tear strength for both control and ANS/XNBR latex films decreased with prolonged weeks of biodegradation. The decreasing property becomes more prominent for ANS/XNBR 20, indicated by the low tear strength retention showed in Table 3(d).

For control films, the higher tearing retention at the eighth week of biodegradation experiment signify low degradation rates of tearing strength. This is due to the absence of any hindrance to the formation of ionic or sulfidic linkages during film formation. During the biodegradation process, even though chain fragmentation of XNBR macromolecules occurred, the ability of the films to reinforce before breakage was inevitable by the mechanism of ionic cluster reformation [2].

By comparing with ANS/XNBR latex films, the retention decreases with respect to the weeks of biodegradation. The tear strength of the ANS/XNBR latex films were partly depends on the reinforcing factor of ANS in the films. As the ANS being consumed during biodegradation process, the ability of the films to resist breaking forces was reduced. The phenomenon could be observed in Table 3, where, as the ANS loading increased, the tear strength reduced with ANS/XNBR 20 showed the lowest retention.

3.2. Mass loss analysis.

From Figure 2, as the biodegradation process progress, the percentage of mass loss for ANS/XNBR increased compared to control XNBR latex films. For control XNBR latex films, the increment was not significant at the second week of biodegradation test. As the process continues, the increment becomes significant at fourth, sixth and eighth weeks. The trends were almost similar with ANS/XNBR 10. However, the trends become distinct at fourth to eighth weeks. For 5 and 15 phr, the percentage of mass loss was increased constantly with biodegradation duration. The films achieved higher mass loss for 20 phr ANS loading ANS/XNBR films. At these loadings, the percentage of mass loss shown a higher increased only after second weeks of biodegradation process.

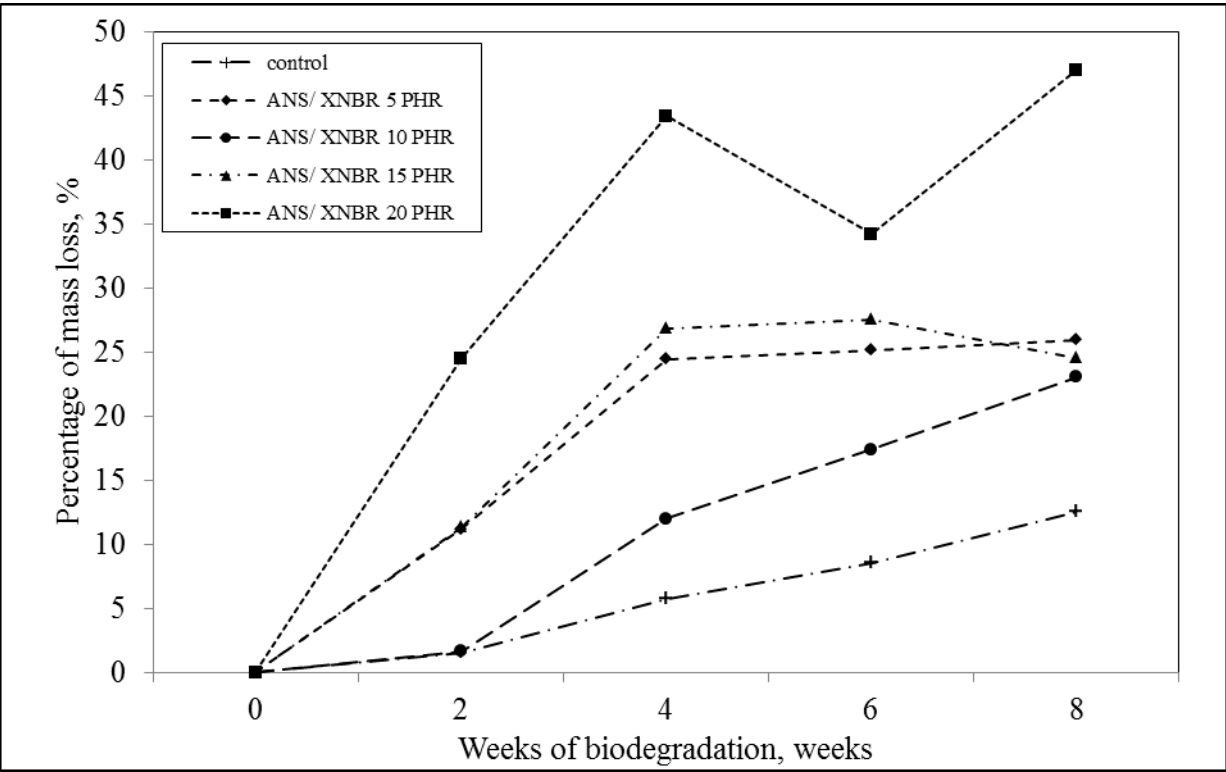
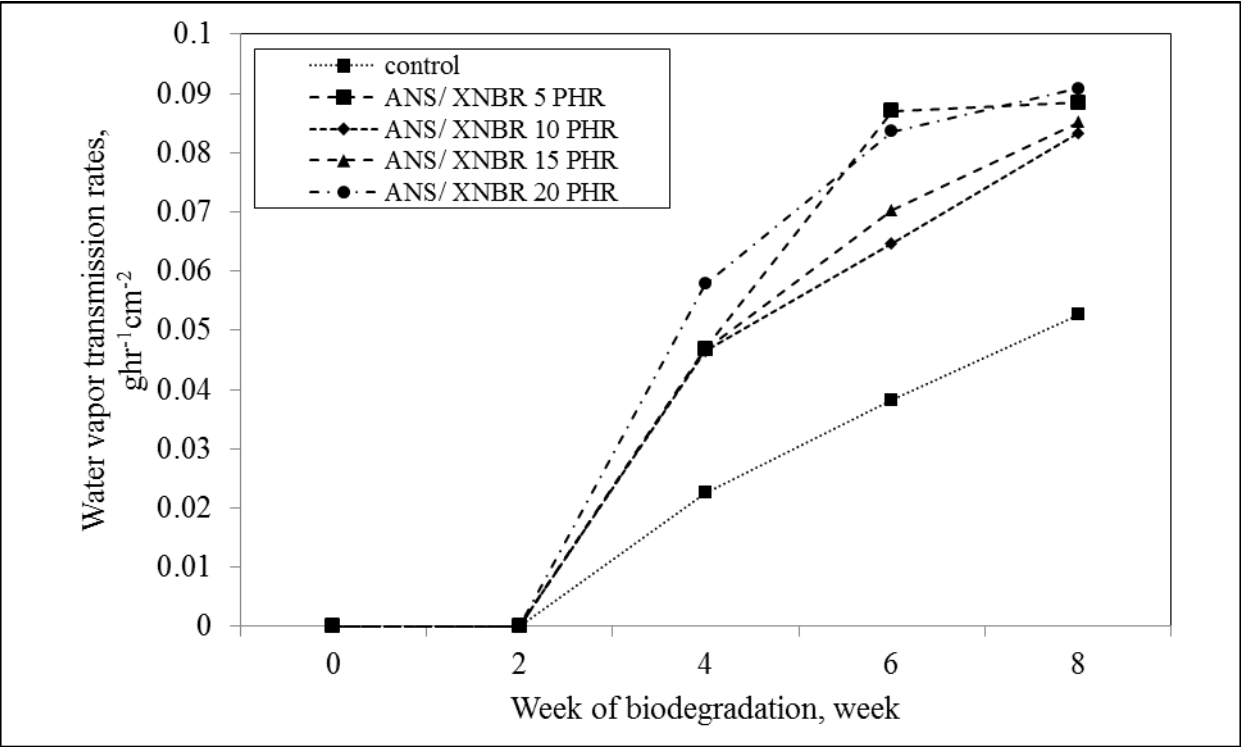


Figure 2: Percentage of mass loss for control and ANS/XNBR latex films with different biodegradation duration.

The presence of ANS in XNBR latex films increased the possibility of the films to biodegrade. Even though at higher filler loading generally did not improved the physical properties of the films. The contribution towards films degradation were more prominent due to the existence of high nutrient in the films as filler loading increased.

349 **3.3. Water vapor transmission (WVT) analysis.**

350 In general, the degradation of ANS/XNBR latex films, mechanical properties are related to
351 the loss of film mass which occur through consumption of microorganism. Despite the direct
352 measurement of the film mass retention, the effect also possible to be quantified by
353 determining the water vapor transmission via water vapor transmission rate measurement. In
354 Figure 3, the addition of ANS into XNBR latex compound increased the rates of water vapor
355 transmission through XNBR latex films which increased as the biodegradation weeks
356 progressed. The increased by an average of 1.7 times higher was recorded for ANS/XNBR
357 latex films compared to control XNBR latex films. The highest average increments for all
358 ANS/XNBR latex films WVT was recorded at fourth week, which was 2.19 times higher
359 compared to a control films.



361 Figure 3: Water vapor transmission (WVT) rates for control and ANS/XNBR latex films with
362 different biodegradation duration.

363 The formation of voids in ANS/XNBR latex films was vivid as shown in Figure 5. The voids
364 were observed as the manifestation of the microorganism consumption on the latex films. At
365 the end of the biodegradation duration, 20 phr ANS loading shown the highest WVT rates
366 compared to the loading of the ANS/XNBR films. Despite higher nutrients consumed by
367 microorganisms that leaves an empty void in the matrix of the ANS/XNBR films, the

physical of the films itself, which existing void due to irregularities in surface morphology in control weeks, increased the feasibility of the original voids to propagate further during microorganism consumption.

From Figure 3, at the beginning of biodegradation process, the WVT rates were less significant. The trends were tremendously increased at week 2 to week 4 and increasing with slower rates at the sixth week to eighth week. These trends show that the biodegradation process was optimum at second week to sixth week based on the increased of the rates obtained. The rates became slower at sixth to eighth week 8.

3.4. Morphological analysis.

From Figure 4, the appearance of yellowish spot which representing the dextrinated region of the polysaccharide chain in ANS/XNBR latex films becomes significant as the ANS loadings increases and biodegradation weeks progress. For control films, less yellowish spot was detected even in the last week of biodegradation durations. These were contributed from the absence of the polysaccharide region in the films. The degradation path for control films was depending on the degradation of XNBR latex macromolecules and the present of the crosslink in the films. These factors will delay the effect of biodegradation on the films and hence lowering the ability of the films to degrade during soil burial experiments.

For ANS/XNBR, the yellowish region was observed in the first week of the biodegradation experiment. The region continues to grow and become more significant at higher filler loading. These phenomena, which representing the dextrination of starch, indicated that the morphological properties of degraded ANS/XNBR latex films were influenced by the ANS presence in the XNBR films. Further analysis on the surface of the films as presented in SEM images (Figure 5), determine the presence of an irregular circumferences of the void with a lot of internal small pits. Some of the microbial colony remains was still can be observed even after sanitization and coating.








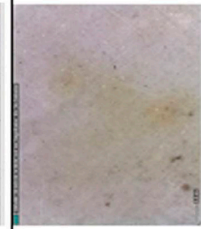
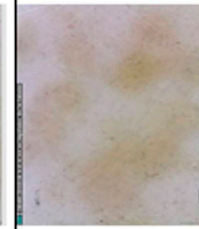



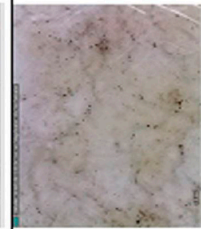
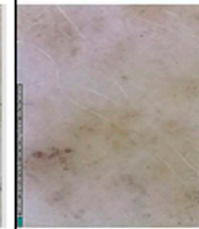






Week/PHR	Control	2 nd	4 th	6 th	8 th
5					
10					
15					
20					

Figure 4: The optical analysis of the appearance of control and ANS/XNBR latex films with respect to their filler loading and biodegradation weeks.

In order to observe the microorganism colony infections, one sample of ANS/XNBR 10 was selected and observed thoroughly. The films were assessed by optical microscope after the eighth week of soil burial to make an early screening for identification of a specific region to

be focused. SEM analysis was made to rectify the remaining of microorganisms existence in the focused area.

From Figure 5 (d), the presence of microorganisms hyphae and mycelia were observed. From the observation of microorganism colony residue shows that the microorganisms hyphae has the ability to penetrate into the films matrix to absorb the nutrients and support the growth of the microorganism colony.

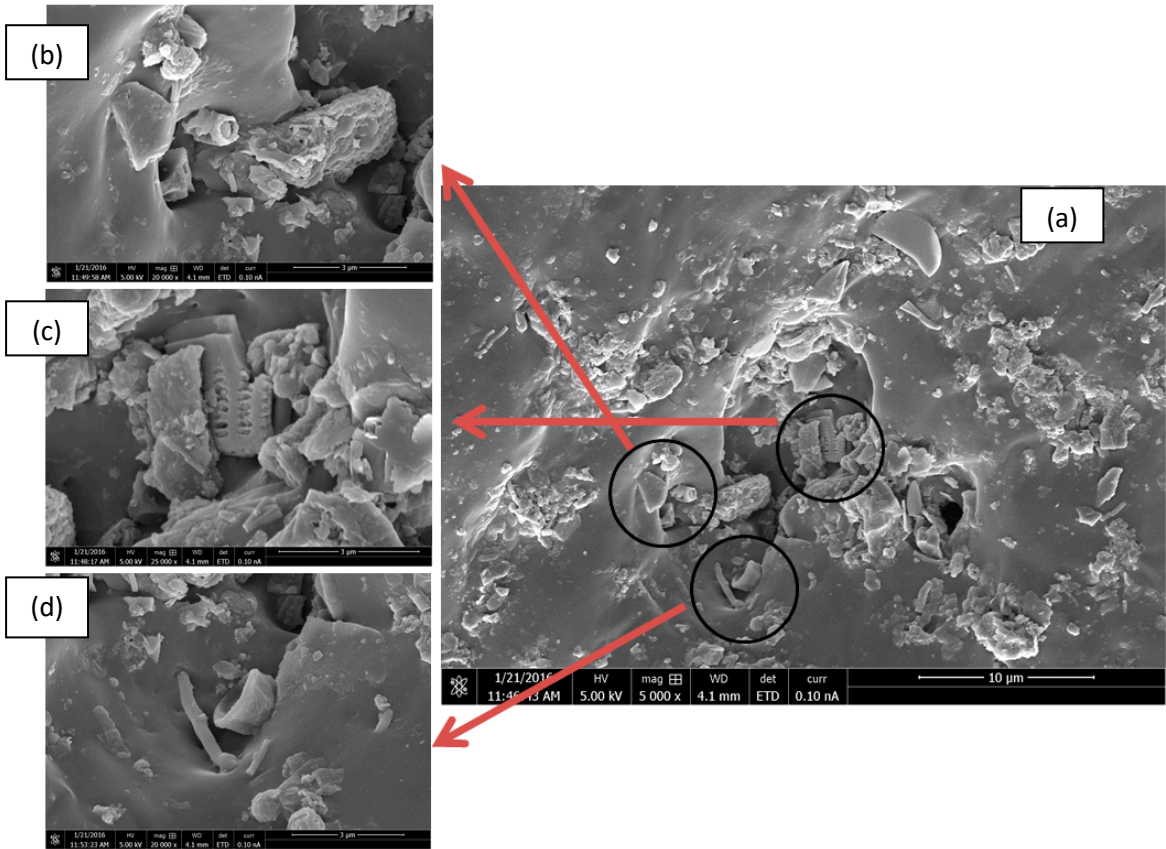
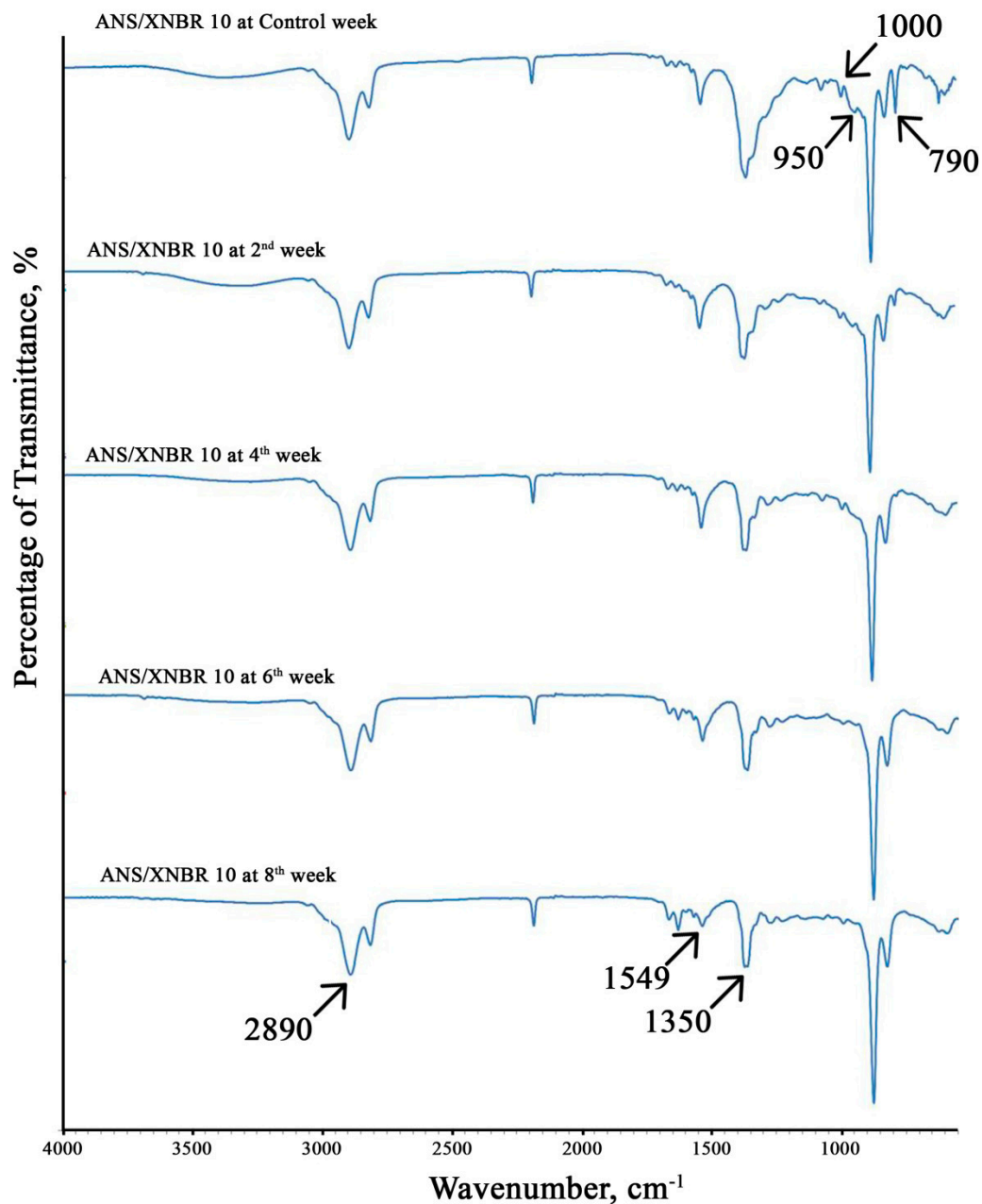


Figure 5: The morphology of biodegraded ANS/XNBR 10 latex films. (a) Selected area of biodegraded ANS/XNBR latex films, (b – c) the remains of microorganism colony and, (d) a part of the hyphae and mycelia structure of the microorganism embedded in the ANS/XNBR latex films matrix (at magnification of 5000 x for (a), and 20 000 x for (b-d)).

3.5. Fourier Transform infrared (FTIR) analysis

Figure 6 shows the FTIR spectra of the ANS/XNBR 10 films with respect to its biodegradation weeks. The most significant changes in the spectra of the films appeared in the region of 790-3000 cm^{-1} . To be specific, 6 distinct zones were monitored. For the peaks that correspond to the ANS conformational changes, the peaks are 950 cm^{-1} , 1000 cm^{-1} , and 2890 cm^{-1} which attributed to starch 1,4-glycosidic linkages, the C-O-C bond of

418 glucopyranose ring and C-H bond of starch aliphatic chain respectively [24-27]. For XNBR
 419 conformational changes, peaks at 790 cm^{-1} , 1350 cm^{-1} , and 1549 cm^{-1} were observed. These
 420 peaks correspond to the unsaturated C=C bond of butadiene in XNBR macromolecules,
 421 stretching of $\text{C}\equiv\text{N}$ and bending of N-H in a cyano functional group of acrylonitrile
 422 respectively [26].



423

424 Figure 6: FTIR spectra for ANS/XNBR 10 PHR with respect to biodegradation duration.

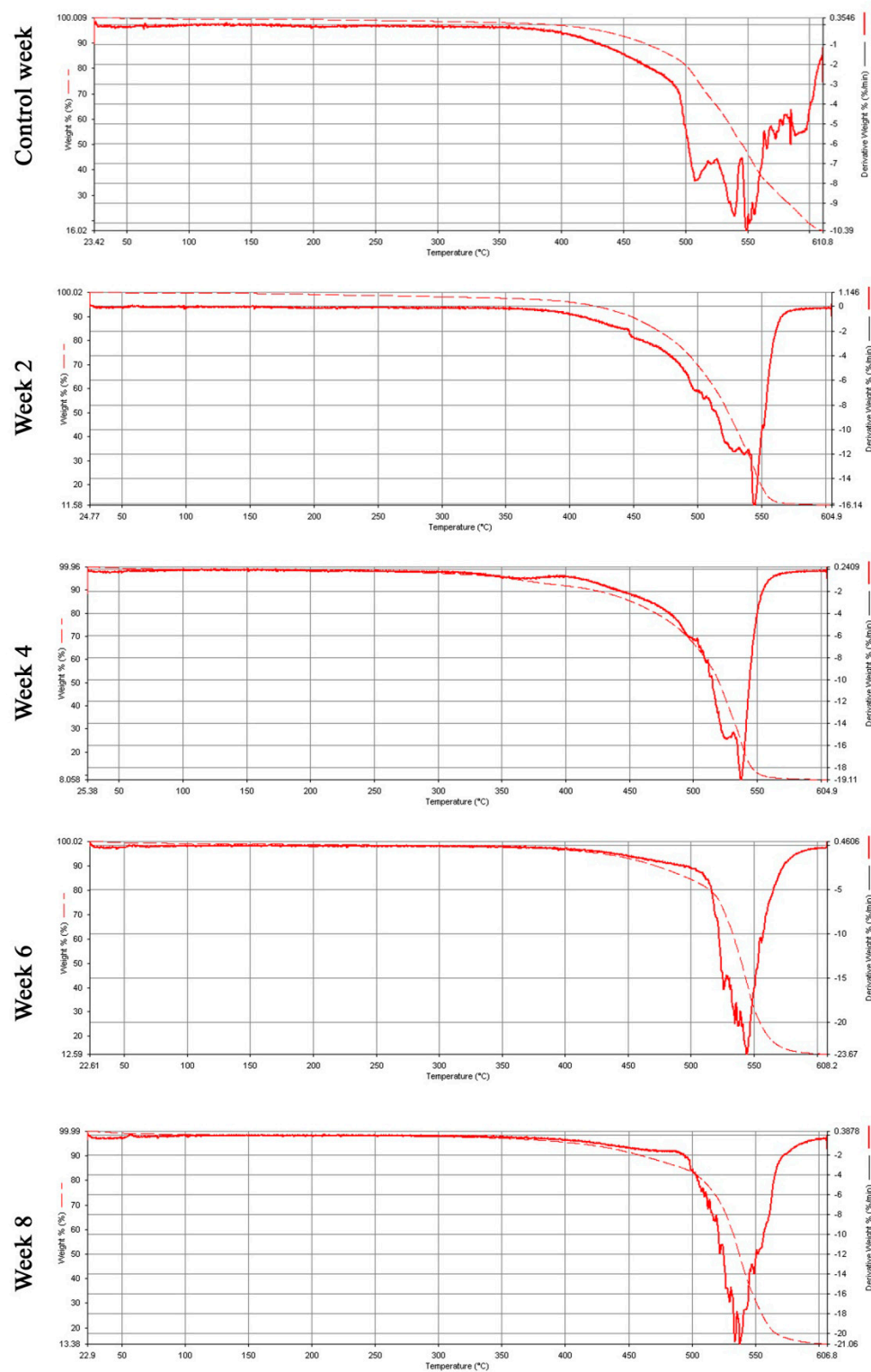
425 As the biodegradation test was done under aerobic environment, the aerobe microorganism
 426 secreted an enzyme which able to depolymerized complex polymer molecules into a smaller

oligomers, dimers, and monomers [28]. The depolymerisation of ANS can be detected by the reduction of C-O-C band with respect to biodegradation weeks. However, insignificant changes were detected for the glycosidic linkages band at peak 950 cm^{-1} suggesting that the hydrolysis of glucopyranose ring are more dominant compared to the 1,4-glycosidic linkages of polysaccharide. The reduction in C-H bond also indicates that the starch aliphatic chain were fragmented and turn into carbon and energy source for the microorganism.

For XNBR macromolecules, the process of degradation takes place concurrently with the degradation of ANS macromolecules. The hydrolysis process happens in the unsaturated C=C bond of butadiene unit. The scheme, as proposed by Rose and Steinbutchel [29] involved the formation of many potential metabolites. The oxidative cleavage of the unsaturated bond can be identified by observing the reduction of peak intensity at wavenumber 790 cm^{-1} . The depletion of interaction between the ANS and XNBR macromolecules can be detected as the stretching of C≡N and N-H functional group lessen as characterized in peak 1350 cm^{-1} and 1549 cm^{-1} .

3.6. Thermo-gravimetric analysis – Differential thermal analysis (TGA-DTG).

Figure 7 shows the TGA-DTG thermograph for control XNBR latex films at control week until the last week of biodegradation duration. At control weeks, the thermograph shows lots of maximum peaks which indicating that there are lots of materials degraded during the tests. However, the maximum peaks occurred at $550\text{ }^{\circ}\text{C}$ and the samples are kept degrading even though at maximum pre-set temperature ($600\text{ }^{\circ}\text{C}$). The thermal properties of control XNBR latex films also shown the films undergo at least three times decomposition process where the maximum decomposition was recorded at $550\text{ }^{\circ}\text{C}$. These observations indicate that the enthalpy changes (endothermic reaction) during thermal decomposition of control XNBR latex films at zero weeks were higher and the films are thermally stable compared to biodegraded control XNBR latex films.



452

453 Figure 7: TGA-DTG thermograph for control XNBR latex films with different
454 biodegradation duration.

455 As the biodegradation experiment progress, the major peaks become diminished indicating
456 the integrity of the film to withstand high temperature in the thermal degradation process also

decreased. The area under the DTG peaks has also become narrower suggesting that the endothermic reaction of the films was reduced. These were due to less thermal energy are required by the sample to decomposed as biodegradation weeks progress.

During the biodegradation process, for control XNBR latex films, a reduction in its crosslinking either ionic or sulfidic will reduce the molecular entanglement in the matrix. The reduction will contribute to the flexibility of the XNBR macromolecules and could deform easily due to the absence of any restriction. Thus, as the thermal energy supply increases, the molecules breaking energy could be achieved, which contributes the easy macromolecules to break. These indicate that the materials will show a rapid transition in its physical properties at high temperature.

For ANS/XNBR latex films, as shown in Figure 8, similar trends were recorded. However, at zero week, four physical transitions were recorded which translated into four major peaks on the thermograph. The area under the DTG curve also was larger compared to biodegraded samples. The two early peaks which registered at $\pm 510 - 540^{\circ}\text{C}$ could be attributed to the degradation of ANS in the films whilst the latter peaks ($\pm 540 - 550^{\circ}\text{C}$) could be attributed to the degradation of XNBR part in the films. It is also concluded that the thermal resistance by the ANS and XNBR part are simultaneously pronounced. These were due to the differences in ANS content in the sample even though the sampling was taken from ANS/XNBR 10 latex films. However, at the last week of biodegradation process, the peaks converged into single peaks and the properties were shifted more towards the XNBR latex degrading temperature. These signified the reduction of ANS content in ANS/XNBR latex films due to microbial consumption.

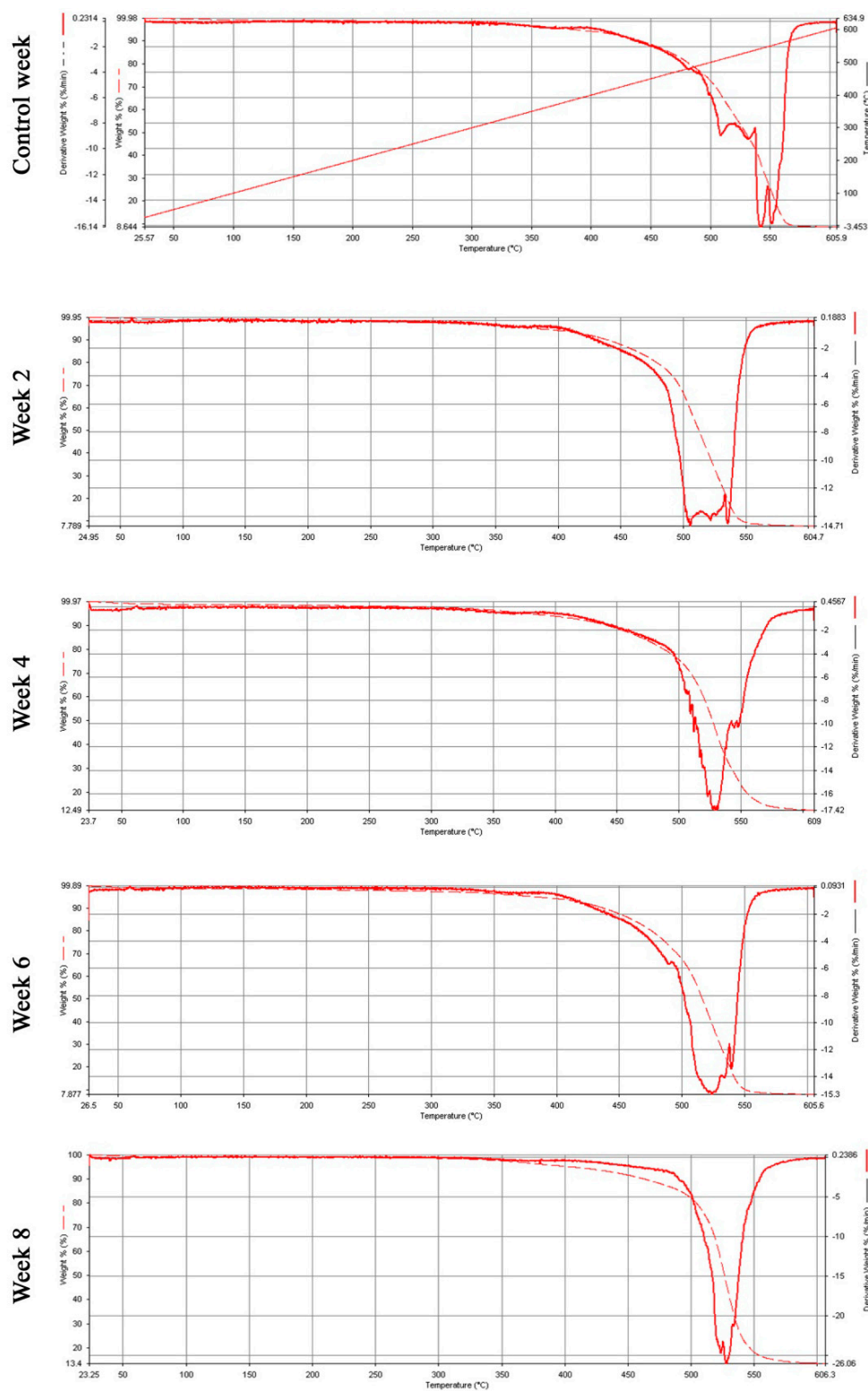


Figure 8: TGA-DTG thermograph for control ANS/XNBR 10 latex films with a different biodegradation duration.

4. Conclusion

Addition of ANS into XNBR latex compound reduces the mechanical properties of the composite ANS/XNBR latex films. As the loading increases, further reduction was recorded. This is due to the reduction of crosslink density between rubber macromolecules which was hindered by the formation and increased of the ANS rich region. As the biodegradation process proceeds, the microbial activity in the ANS rich region, which was evidenced in optical and SEM micrograph, further reduces the mechanical property of the latex films. This is due to the scission of the starch aliphatic chain during the biodegradation process that reduce the interaction between ANS and XNBR molecules. The event was evidenced in the FTIR spectral analysis, which indicates that the reductions in starch aliphatic chains at peak 1607 cm^{-1} and the stretching of N-H bond at peak 3302 cm^{-1} of the spectrograph. The biodegradation process also leads to increase in the formation of microvoids in ANS/XNBR latex films which was depicted from SEM micrographs and the increased of the WVT rates recorded. This process also was recorded by the TGA thermograph which indicates that as the biodegradation process progressed, the material degradation temperatures reduced.

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