

1 *Type of the Paper (Review)*

2 **A review on battery charging and discharging control** 3 **strategies: Application to renewable energy systems**

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14 **Abstract:** Energy storage has become a fundamental component in renewable energy systems,
15 especially those including batteries. However, during the charging and the discharging process,
16 there are some parameters that are not controlled by the user. That uncontrolled working leads to
17 aging of the batteries and a reduction of their life cycle. Therefore, it causes an early replacement.
18 Different control methods have been developed with the goal of protecting the battery and
19 extending its life expectancy, being the most used the constant current-constant voltage. However,
20 several studies show that charging time can be reduced by using Fuzzy Logic Control or Model
21 Predictive Control. Other benefits are; temperature control and an extension of life expectancy. For
22 all these reasons, FLC and MPC have proven to be more efficient than traditional charge control
23 methods.

24 **Keywords:** Energy storage; battery; control; energy management systems; FLC; MPC.

25

26 1. Introduction

27 Electrification of remote and rural isolated areas with the national grid is not always possible due to
28 the prohibitive costs. Therefore, many off-the-grid communities have been using diesel engines as
29 the main power source. To meet the energy needs, governments have opted for the installation of
30 independent renewable energy systems with battery energy storage systems (BESS) [1]. However,
31 energy storage is one of the greatest challenges for renewable energy systems, especially in
32 stand-alone solar photovoltaic system and wind farms, where the application of electrochemical
33 energy storage demonstrates high response times and round-trip efficiencies [2]. Moreover, from an
34 economical point of view, in a solar photovoltaic system, the energy storage system (ESS) represents
35 40% of the total cost [3 – 4].

36 Storage technologies are usually categorized based on time scale of applications such as
37 instantaneous (less than a few seconds), short term (less than a few minutes), mid-term (less than a
38 few hours), and long-term (days) [5]. Moreover of the BESS there are different types of energy
39 storage technologies [5 – 12]: pumped hydro energy storage (PHES), compressed air energy storage
40 (CAES), flywheel energy storage (FES), hydrogen-based Energy Storage System (HES), flow battery
41 energy storage (FBES), superconducting magnetic energy storage (SME), and supercapacitor energy
42 storage (SES). However, because of their localization flexibility, efficiency, scalability, and other
43 appealing features [13], the BESS is the preferred technology [14], (see Fig. 1).

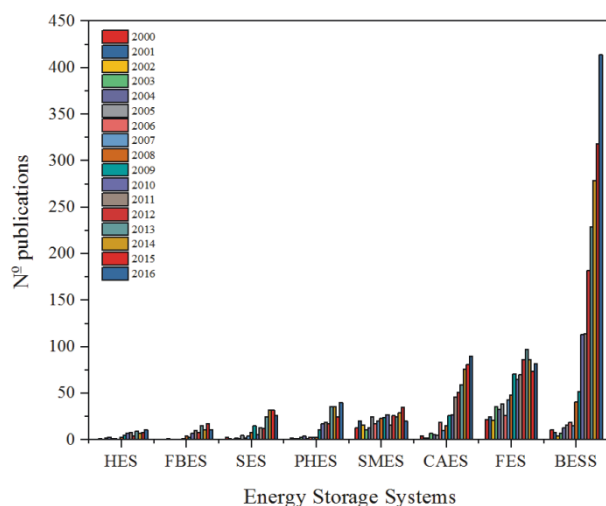


Fig. 1. Energy storage systems (ESS).

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At present, there are numerous commercial batteries used in renewable energy systems, such as: lead acid, lithium ion (Li-ion), nickel cadmium (Ni-Cd), sodium sulfur (Na-S), among other. Table 1 shows the main characteristics of this type of batteries [6, 8 – 12, 15-20].

Characteristics	Pb-Acid	Li-Ion	Ni-Cd	Na-S	PSB	VRB
Capital cost (\$/kWh)	400 [6, 12], 200-400 [8, 9, 20], 50-150 [17]	2500 [6,12], 600-2500 [8, 9, 20], 900-1300 [17]	800-1500 [6, 9, 10, 20], 1500 [11], 400-2400 [17]	300-500 [6, 9, 10, 20], 500 [11], 200-600 [17]	300-1000 [17], 150-1000 [17]	150-1000 [9, 20], 600 [17]
Efficiency (%)	70-90 [6,12], 75-80 [8], 70-92 [8], 70-80 [17], 80-90 [18]	85-90 [6,12], 85-90 [9], 75-95 [17], 85-95 [18]	60-65 [6,12], 60-70 [9], 70 [17]	80-90 [6,12], 75-85 [8], 75-90 [9], 75-89 [17], 71-90 [18]	60-65 [11], 60-75 [17]	65-85 [9,17]
Operating temperature (°C)	-5 to 40 [17]	-30 to 60 [17]	-40 to 50 [14]	325 [17]	0 to 40 [17]	0 to 40 [17]
Depth of discharge (%-DOD)	60-70 [8], 70 [17]	80 [17]	100 [17]	60-80 [7], 100 [17]	75 [17]	75 [17]
Energy density (Wh/kg)	30-50 [6, 9, 10, 12], 35-50 [17]	75-200 [6, 10, 12], 75-250 [9], 100-200 [17]	50-75 [6, 9, 10, 12], 30-80 [17]	150-240 [6, 9, 10, 12], 100-175 [17]	>400 [17]	10-75 [9], 10-30 [10], 30-50 [17]
Life cycles (cycles)	500-1200 [9], 500-1000 [10,20], 2000 [12], 500-2000 [17,18]	1000-10000 [9, 11, 20], 4500 [13], 1500-3500 [17], 1000-30000 [18]	1000-2500 [9], 2000-2500 [10, 20], 3000 [12], 3500 [17]	2000-5000 [9], 2500 [10, 17, 20], 4500 [12], 2500-5000 [18]	100-13000 [17]	13000+ [9], 12000+ [10, 20], 100-13000 [17]
Lifetime (years)	5-15 [6, 9, 10, 12, 17, 18, 20], 5-8 [8], 3-12 [19]	5-15 [6, 10, 12, 18, 20], 5-20 [9], 14-16 [17]	10-20 [6, 10, 12, 17, 20], 5-20 [9], 15-20 [19]	5-10-15 [6, 8, 10, 12, 20], 15 [9], 10-20 [17], 5-15 [18]	10-15 [10, 20], 15 [17]	10-20 [9, 17], 5-10 [10, 20]
Availability (%)	99,99 [9]	97+ [9]	99+ [9]	Up to 99,98 [9]	*****	96-99 [9]
Technological maturity level (1-lower to 5-higher)	5 [9]	4 [9]	4 [9]	4 [9]	*****	3 [9]
Response time (ms)	Fast [6, 12]	Fast [6, 12]	Fast [6, 12]	Fast [6, 12]	*****	*****
Capacity (MW)	0-40 [6, 12], 0,001-50 [9], 0,001-40 [17]	0,1 [6, 12], 0,1-50 [9], 0,001-0-40 [6, 12], 50 [17]	0-46 [9], 6,75 [17]	0,05-8 [6, 12], 0,05-34 [9], 0,4-244,8 [17]	0,005-120 [17]	0,005-1,5 [9], 2-120 [17]

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Table 1. Battery technologies in RES.

52 Regarding BESS used in photovoltaic systems, lead-acid is the most used technology [10, 16], due to
53 its low cost, maturity, high reliability, fast response and low self-discharge rate [10, 21]. However,
54 charging process is non-linear [22].

55 Due to the high economic cost generated by the replacement of a BESS, a charge control method and
56 control strategy is required to protect the battery from overcharging and over-discharging [23]. The
57 efficiency of charge control methods will depend on the amount of current used for the charging
58 process, the level of the oscillations in the charging current, the charging voltage levels, the charging
59 time, and the fluctuations in the temperature during the charging process [24]. Moreover, there are
60 battery parameters such as charging rate, the permitted maximum charging current, the internal

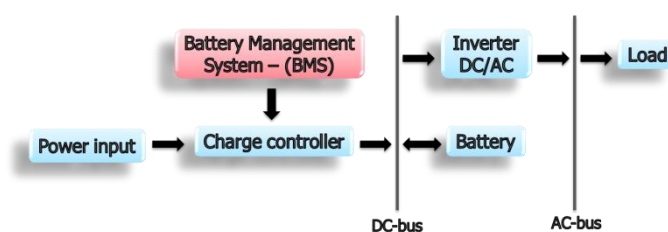
61 resistor, the port voltage, the temperature and humidity that changing during the charging and
62 discharging process and cannot be directly obtained, so it is difficult to achieve the optimal
63 operation performance by using traditional control methods.

64 This paper compiles the traditional control methods used to control the charging and discharging of
65 lead-acid batteries commonly used in renewable energy systems such as solar photovoltaic and
66 wind power. Although lithium iron phosphate (LiFePO₄) batteries are being used in renewable
67 energy systems, they will not be included in this paper.

68 Regarding battery management systems, our research focused on Fuzzy Logic Control (FLC) and
69 Model Predictive Control (MPC) due to the leading role in the battery control (Fig. 2). Where the
70 power input can be supplied by the grid, a photovoltaic system or wind power system.

71 Fuzzy Logic Control (FLC) and Model Predictive Control (MPC) have proven to have higher
72 performance than traditional charging control methods in terms of energy management, thus
73 improving charging time, charging efficiency, states of charge (SOC) and life battery expectancy. The
74 strategies used, goals, and the results reached with these controls are detailed.

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Fig. 2. Battery control scheme.

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79 The paper is structured as follows: Section 2 describes the traditional methods used to control the
80 charge and discharge of batteries, the time and the state of charge reached. Section 3 the strategies,
81 and the fields where the FLC and MPC controls have been applied. The obtained results are
82 presented and discussion in Section 4. Section 5 concludes by stating possible avenues for future
83 research while summarizing the papers principle contributions.

84

85 2. Traditional charging control methods

86 The main goal of a charge control method is to increase the SOC. Moreover, additional specifications
87 such as battery performance, charging time, protecting the battery from overcharging and
88 over-discharging, and increasing its useful life are needed too.

89 As battery charging process is non-linear [22], different methods have been developed to effectively
90 battery charging control. Control methods commonly used in battery charging are: constant current
91 (CC), constant voltage (CV), two-step charging (CC-CV), pulse charging (PC), reflex charging or
92 negative pulse charging (NPC), trickle charge or taper-current (TC) and float charge (FC) [25-27].

93 2.1. Constant current (CC): this method consists of charging the battery with a constant current.

94 This method limits the current to prevent the over current of the initial charge [28]. The

95 voltage value will depend on the charging current whereas the charging time and the SOC
96 can be easily calculated [29]. As voltage is not usually controlled, this can cause battery
97 overcharging and temperature rising, resulting in the degradation of battery life [25, 27].

98 2.2. Constant voltage (CV): it is used to charge the battery by applying a constant voltage on its
99 terminals. During the initial stage of charging the charge current is high. As the battery
100 voltage reaches the charger voltage setting, the charging current decreases [27]. This type of
101 control is used in applications that require extended charging periods to reach full charge.
102 As it requires a long charging time, this will cause temperature rises and degradation of the
103 battery life.

104
105 2.3. Constant current – Constant voltage (CC-CV): this charging method is also known as the
106 two-step method, because it combines both CC and CV. CC is applied at the initial charging
107 stage until the battery voltage reaches an over-charged stage or a pre-defined voltage. In the
108 second stage, the charging method switches to CV to maintain the battery voltage, so it
109 avoids overvoltage [25, 29].

110 Research shows that, the CC-CV charging method is the most efficient for battery charging
111 regardless of the battery type [30]. Also, it is the most used control method [31-33]. However,
112 charging speed and efficiency of the CC-CV charging strategy are very low [34]. Moreover, the
113 CC-CV is not suitable for rapid charging, because the CV charging stage extends the charging time,
114 it rises the battery temperature, and it reduces battery lifecycle [35-36].

115
116 2.4. Pulse charging (PC): this charging method consists of periodically applying a pulse current
117 to the battery. Batteries are completely discharged and recharged periodically in what is
118 called an equalizing charge [37]. This will allow the battery voltage to become more stable.
119 In this charging method, it is important to take into account the charging frequency, pulse
120 peak and pulse width, because they are related to the capacity and the charging time. This
121 method it can reduce the polarization to prevent the battery temperature rise [28], is the
122 weak point of this charging method is its complexity.

123
124 2.5. Reflex charging or negative pulse charging (NPC): this is an improvement on the PC. The
125 concept of applying a reflex charging started with the patents by W. Burkett & J. Bigbee and
126 W. Burkett & R. Jackson [29, 38] in 1971. NPC consist of performing the following charging
127 sequence: a positive charging pulse, a rest period (no charging), and a discharge pulse
128 (burp) [38]. This method can reduce the polarization to prevent the battery temperature
129 from rising. However, it also may reduce the charge efficiency [39-40].

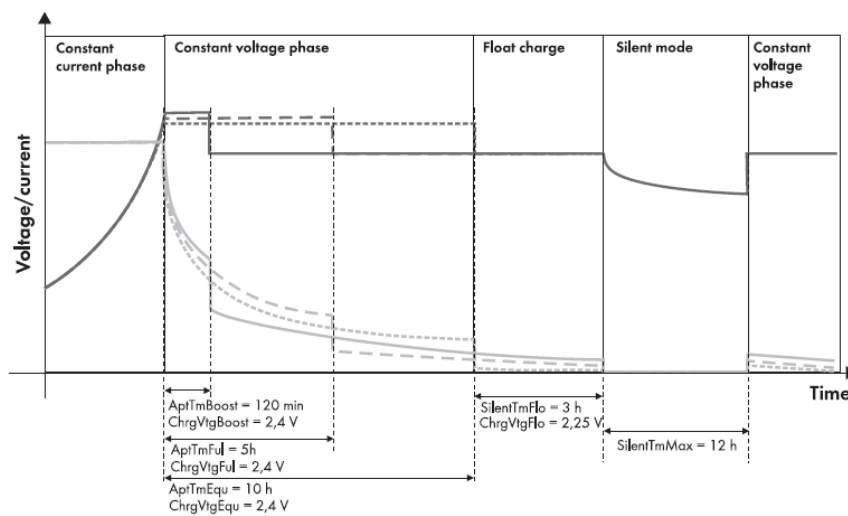
130 2.6. Trickle charge or taper-current (TC): A trickle charge is a continuous CC charge at a low
131 (about C/100) rate, which is used to maintain the battery in a fully charged condition. IT is
132 designed to compensate the self-discharge of the battery [37]. This method can charge the
133 battery up to 100% by using a very small charge current. This method is typically used for

134 SLI (Starting Lighting, Ignition SLI) battery applications but it is not suitable for batteries
 135 that are susceptible to be damaged from over-charging.

136

137 2.7. Float charge (FC): this method involves a CV charge after the charge process has been
 138 completed in which the capacity of the battery is maintained at its maximum value against
 139 self-discharge [41]. This method is used for stationary batteries mainly lead acid batteries
 140 [37].

141 These traditional charging control methods have been incorporated in commercial inverters such as
 142 Victron Energy, sunny island of SMA solar technology among others. The latter controls the charge
 143 of the battery in three phases: CC (I phase/bulk phase), CV phase (absorption phase/Vo phase), and
 144 float charge/V phase (Fig. 3).



145

146 Fig. 3. Sunny Island charging phases with sample values for an AGM battery [42].

147

148 3. Battery management systems

149 As the process of battery charging and discharging is complex, it required the design of a robust
 150 supervisory control over the classic controller presented in section 2.

151 FLC and MPC are especially suitable to battery charging management because they do not requiring
 152 precise knowledge of mathematical system models and they have high flexibility.

153

154 3.1. Fuzzy logic control (FLC)

155 In 1965, Lotfi Zadeh first proposed fuzzy theory [43]. Between the applications of fuzzy logic, fuzzy
 156 control (FC) has been one of the fields where fuzzy techniques have obtained greater amount of
 157 successful results when they work with complex nonlinear systems or even nonanalytic ones [44-45].
 158 FLC is composed by a knowledge base, which incorporates the information given by the operator of
 159 the controlled process following some linguistic control rules pattern [46].

160 In general terms, the input variables used in a FLC are battery voltage and temperature, and the
 161 output membership function generates current.

162 3.1.1. Fuzzy Logic Control of Energy Storage Systems in stand-alone applications

163

164 A FLC was developed by Bandara et al. [24] to charge a lead acid battery. The FLC charges the
165 battery at two stages. At the first stage, it uses a high current that charges the battery until 70% of its
166 full capacity. At the second stage, the battery voltage is maintained at a set value and the current is
167 left to decrease exponentially. Rahim et al. [47] showed a battery charger with a digital signal
168 processor which included FLC as a control algorithm. This approach produced a higher charging
169 current and it supported a higher input supplies. Thus, the charging time could be reduced.

170 Huang et al. [48] used a single crystal processor as the basic controller and a digital signal processor
171 to get the feedback of the voltages, temperature, and current of the batteries. This approach allowed
172 them to lower the battery temperature about four degrees. Kim et al [49] proposed a fuzzy PID
173 controller to improve the frequency control performance of microgrid islanded. The control strategy
174 was based on primary control action of the BESS and a secondary control action of the energy
175 management system. The control is composed of FLC and a conventional PI controller, connected in
176 series. The gains of conventional PI controller and fuzzy PID controller were determined by the PSO
177 algorithm. The showed simulation that with the proposed control, the performance is improved
178 compared to a conventional PI.

179 Welch et al. [50] showed that using particle swarm optimization (PSO) the optimized FLC achieves
180 performed better by 26.13% in energy usage than un-optimized FLC. The charge strategy was
181 improved about 5.22% respect to [51]. Fu-shun et al. [52] observed that using a PIC6014
182 microcontroller as control core in the design of the FLC, the battery charge time is reduced two hours
183 compared to the three stage control method. Swathika et al. [53] show that using a FLC the voltage of
184 the battery can be controlled effectively than with a conventional controller. Also, the ISE (Integral of
185 Square Error), IAE (Integral of the Absolute value of the Error) and settling time can be reduced
186 considerably in comparison to a PI control. Safari et al. [54] developed an optimized FLC based on
187 the particle swarm optimization (PSO) algorithm. In the control design took into account the weekly
188 operation and maintenance (O&M) costs and the loss of power supply probability (LPSP). The
189 results of the simulation showed that optimized FLC reduces fluctuations in batteries SOC
190 extending life battery expectancy. Moreover, can be lowered O&M costs and LPSP by 57% and 33%,
191 respectively and average SOC can be increased by 6.18%. Reducing the investment cost by up to 18%
192 in the capacity of autonomous hybrid green power system (HGPS) equipment. Improving what was
193 presented in [50]. Berrazouane et al. [55] adopts the idea of an optimized FLC but, contrary to [50]
194 and [54] use cuckoo search (CS). The CS was used to adjust the shape of the system membership
195 functions of FLC to achieve a better performance instead of using a conventional FLC or optimized
196 FLC based on PSO algorithm. The results of the simulation showed that with the proposed control
197 loss of power supply probability, excess energy, and leveled energy cost the results were improved
198 compared to optimized FLC based on PSO or a non-optimized FLC.

199

200 3.1.2. Fuzzy Logic Control of energy storage systems in grid connected applications

201 Yin et al. [22] divided the charging process into two stages. At the first stage, they implemented a
202 fuzzy control to determine the proper start charging time and to prevent overcharging or

203 insufficiently battery charging. At the second stage, they used the normal charging method.
204 However, during the simulation, the temperature was not taken into account in the inner loop of the
205 control unit.

206 Contrary to [49], Haoran et al. [56] take into account the SOC of the BESS in the control of the
207 microgrid where the FLC was used to maintain the SOC of the BESS above a certain level and to
208 mitigate the fluctuation. Thus, the FLC adjusts the active power output reference of the BESS based
209 on the SOC and the target active power for the grid-connected operation. In island mode, the FLC
210 adjusts the active power output reference of the BESS based on the SOC and the active power
211 command for frequency control. Arcos-Aviles et al. [57] divided its strategy into two stages: At the
212 first stages, it minimizes the power peaks and fluctuations in the grid power profile and it maintains
213 the lead-acid battery SOC above 70%. At the second stages, it performs an off-line optimization
214 process based on a set of evaluation quality criteria. With to simple moving average strategy the
215 proposed control reduced maxima and minimum grid power in 61% and 15% %, respectively, and
216 53% and 4%, respectively, with respect to the fuzzy based on microgrid net power trend. The
217 strategy proposed by Derrouazin et al. [58] consisted in leading to optimal use of available energy
218 resources beyond a threshold to withstand the load demand, giving priority to the highest source of
219 power, while enough available energy is routed directly to the battery through a
220 charging/discharging regulator system. This allowed them to have improved energy efficiency
221 about 7% compared with the classical FLC. Paliwal et al. [59] reveal that incorporating battery
222 charging efficiency as a battery SOC function offers a more practical approach to system planning.
223 Also, conclude that assuming a constant value of efficiency can hamper the efforts to come up
224 optimum system, because the charging efficiency obtained can be higher or lower than the constant
225 assumed value affecting charging power drawn by storage and consequently the energy availability
226 in the battery. Teo et al. [60] design a control based on Fuzzy Inference System (FIS) to determine the
227 charging/discharging rate of the ESS depending on the RES and current SOC of the ESS. Power
228 variation range (PVR), power quality (PQ) and battery dynamic range (BDR) were the quality
229 indices they took into account to evaluate the effectiveness of the proposed fuzzy controller. The
230 maximum and minimum power of the grid was reduced. Hussain et al. [61] proposed a control
231 strategy were where the controller decides the mode of BESS operation: subservient mode, resilient
232 mode or in emergency mode. In subservient mode, the BESS is fully controlled by the EMS while in
233 resilient mode minimize the operation cost of the microgrid. The goal of the emergency mode
234 operation is minimize the load shedding during the emergency period. Respect to the latter, load
235 shedding can be reduced by 92%.

236 3.2. Model predictive control (MPC)

237 Model Predictive Control (MPC) is an advanced control method which provides the sequence of
238 optimal control variables over a finite time horizon by solving an optimization problem. Therefore it
239 is widely used in many fields [62-69].

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244 3.2.1. Model Predictive Control of Energy Storage System in stand-alone applications

245 Perez et al. [70] designed a control that anticipates the future saturations of the ESS. The MPC
246 allowed the system to reduce its power production during the first hours. To obtain the optimal
247 performance of the battery Pezeshki et al. [71] focus on two goals: Energy operational cost and
248 smooth loading.

249 Based on a nonlinear model predictive control (NMPC), Dizqah et al [72], developed an energy
250 management strategy that manages the energy flow across a standalone DC microgrid. The NMPC
251 continuously solves an optimal control problem (OCP) and finds the optimum values of the pitch
252 angle and three switching duty cycles. The control had three main goals: voltage level regulation,
253 proportional power sharing, and battery management. While Morstyn [73] used a convex
254 formulation of the DC microgrid dynamic optimal power flow problem. It is, based on a static
255 voltage-current model and linear power flow approximations. Simulations were made on a real-time
256 digital simulator (RTDS) which used non-linear battery models and switching converter models. In
257 [74] this method does not assume that real and reactive power flows are decoupled; allowing line
258 losses, voltage constraints, and converter current constraints have been addressed. The simulation
259 was carried out in real time for an islanded microgrid based on the IEEE 13 bus prototypical feeder,
260 with distributed li-ion BESS and intermittent PV generation. The computational time was reduced
261 by a factor of 1000.

262 Kujundžić et al. [75] used a full-state observer to solve that problem some states of the model cannot
263 be directly measured. Also, resort to converting the model to a non-minimal state space form which
264 uses the plant input and outputs as state variables. Added additional constraints to the MPC
265 problem to keep the voltage of every battery below the upper threshold voltage level provided by
266 the manufacturer. This caused the MPC algorithm to decrease the charging current. Causing a
267 slower charging compared to a standard MPC method. The algorithm was validated on a valve
268 regulated lead acid (VRLA) battery through simulation tests and experimentally. An advantage of
269 using MPC algorithm with respect to CC-CV method was its ability to take into account the
270 constraints on the maximum temperature and the maximum voltage of individual batteries. While
271 Zeng et al [76] proposed combine an MPC and hierarchical optimization to maximize the RES
272 generation and to minimize the variations between the intraday schedule and day-ahead schedule.
273 This combination facilitated the integration between BESS and RES. The goal was to maximize
274 output using appropriate charging and discharging control strategy for ESS based on the prediction
275 of renewable power output, demand and network capability in future time horizon. The method
276 was applied as a case study to the modified IEEE-30 bus test system and northwest power grid of
277 China. Li et al. [77] presented a BESS control algorithms based on MPC to mitigate wind power
278 intermittency. The MPC algorithm considers two practical aspects: the efficiency loss of BESS and
279 the smoothness in wind power scheduling. They compare performance between the horizon-based
280 revised MPC and the instantaneous heuristic algorithm, and came to the conclusion that MPC shows
281 the best performance.

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285 3.2.2. Model Predictive Control of energy storage system in grid connected applications

286 A control system based on MPC was proposed by Khalid et al. [78] for the reliable operation of the BESS for
287 primary frequency regulation. A frequency predictor was used to optimize the performance of the controller
288 using multi-step ahead predictions. Two scenarios were presented. A first scenario where the BESS operation
289 was adjusted between 40% to 80% and a second one where the BESS was adjusted between 10% to 50%. In the
290 first case, the maximum battery SOC was reached at ~17 min, while the minimum battery SOC was reached at
291 ~70 min. In the second case, the maximum battery SOC was reached at ~80 min, while the minimum battery
292 SOC was reached at ~12 min.

293 Ferrarini et al. [79] developed a MPC to store energy that was not used by a building and to deliver it when the
294 building load requires it, instead of buying it from the grid. Two MPC controls were designed: the building
295 MPC and the battery MPC. The goal of the building MPC was to optimize the temperature control.
296 Additionally, the battery MPC had as main goal to minimize the power flow at point of common coupling
297 (PCC). The PCC power flow was successfully maintained around 50% value until the battery reaches a SOC of
298 90%. Wang et al. [80] used a MPC to optimize and distribute the PNM prosperity energy storage project in New
299 Mexico. The storage system was divided into two BESS units, a large slower moving unit for energy shifting
300 and arbitrage and a small rapid charging unit for smoothing. The first goal was to provide energy arbitrage and
301 to smooth the intermittent output from the PV array. Additionally, the second goal was to minimize the
302 excessive charge-discharge cycles of the BESS units. Petrollese et al. [81] proposed EMS based on Optimal
303 Generation Scheduling (OGS) combined with Model Predictive Control (MPC), which optimizes the short-term
304 microgrid operation. The OGS was used to compare the expected power produced by the renewable generators
305 with the expected load demand for the following days and determines the scheduling and evolution of the state
306 of charge of the different energy storage systems for the next few hours to minimize the operating cost of the
307 overall microgrid. The MPC has goal of the real-time control in order to guarantee the stability of the microgrid.
308 A stochastic approach was implemented to weather and load forecasting uncertainties. By working
309 simultaneously the OGS and MPC, the computational load is reduced as achieved in [74].

310 Matthiss et al. [82] used an MPC to maintain high levels of self-consumption, reduce the peak feed-in power for
311 improved grid compatibility and to minimize energy costs. Four battery charge algorithms were implemented:
312 charge at the earliest opportunity, linear delayed charging, peak shaving, and a model predictive control (MPC).
313 Additionally, energy pricing was used as an additional parameter to the optimization process. The results show
314 that using a MPC the use of wind energy is improved by 35% and the energy costs could be reduced about 25%.

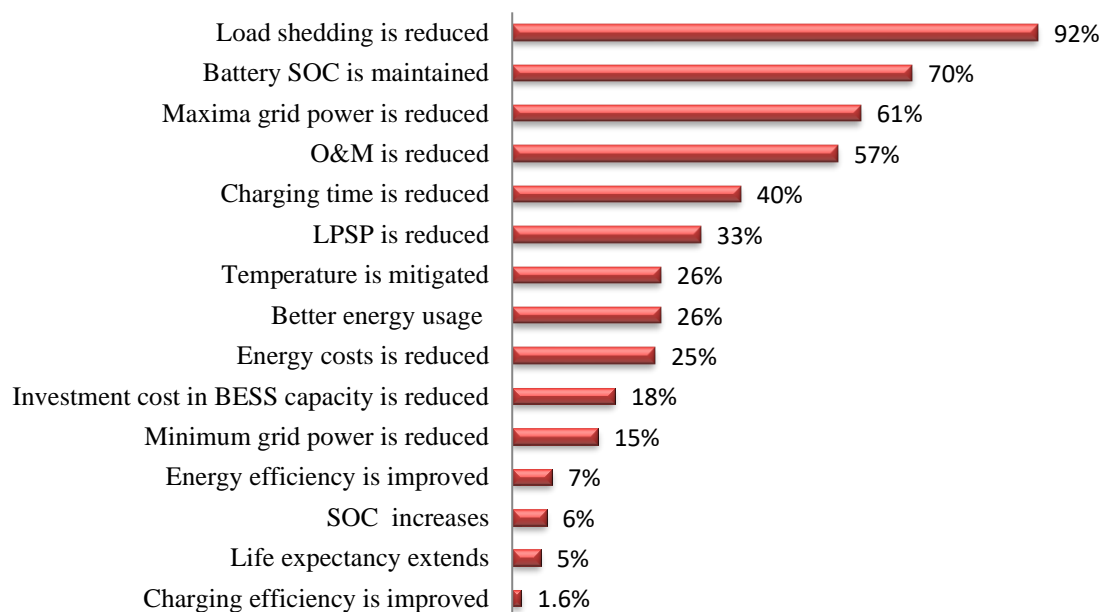
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316 4. Results and discussion

317 This research shows that in renewable energy systems with battery energy storage the most used control method
318 for controlling the charging and discharging of lead acid batteries is CC-CV. However, this control requires a
319 long time to charge the battery. This prolongation in the charging time generates battery temperature rises, so it
320 produces battery irreversible damages. Moreover, during the process of battery charging and discharging,
321 traditional controls leave some aspects uncontrolled.

322 In order to solve these events, simulations and, in some cases, experimental tests with FLC and MPC are being
323 carried out. Generally, these controls are being used in the energy management of stand-alone microgrids and
324 grid connected microgrids. These controls have been proven to be more efficient than a traditional control. Fig.

325 4 shows some results achieved using FLC or MPC in renewable energy systems with batteries energy storage.
 326 When comparing these results with a traditional control, we have found some advantages. The load shedding
 327 can be reduced up to 92%; the implementation of these controls, allows maintaining the SOC above 50%, thus
 328 avoiding deep discharges that lead to the deterioration of the battery. Through energy optimum use, the
 329 maximum and minimum power of the grid can be reduced by 61% and 15% respectively. This rational and
 330 efficient use of energy allows reducing microgrid energy costs by 25%. Also, the operation and maintenance
 331 and loss of power supply probability can be lowered around 57% and 33% respectively. Regarding to energy
 332 storage system in batteries, the charging time is reduced about 40%, which leads to a decrease in temperature
 333 about 26% and a reduction of the investment cost in energy storage capacity about 18%. So, it allowed some
 334 approaches to extend the life expectancy around 5%.



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Fig. 4. Main advantages of FLC or MPC with respect to traditional controls methods.

337

338 Despite the advantages of FLC and MPC controllers compared to traditional controls, it is required an
 339 implementation of these types of controls in real environments with large-scale energy storage systems, because
 340 many of the results have been achieved through simulation. Moreover, parameters such as dynamic selection of
 341 battery SOC limits and the influence of ambient variables such as relative humidity or SOH prediction were not
 342 studied. Finally, these controls are also being implemented to control the charging of lithium iron phosphate
 343 (LiFePO₄) batteries as shown in [83-85].

344 5. Conclusions and future work

345 Renewable energy systems have been a short-term solution in the mitigation of energy needs in isolated areas
 346 where there is no energy service grid connected. Many of these systems have battery energy storage to giving
 347 energy in those hours where natural resources such as sun or wind are not present. In in a connected microgrid,
 348 the BESS is used to minimize active power exchange at the point of common coupling of the microgrid.

349 A control and control strategy is required to optimize the energy management and to avoid overcharging and
 350 overdischarging in the energy storage system. Despite of being the constant-current constant-voltage (CC-CV)

351 the most used control method for battery charging and discharging, other method such as FLC or MPC have
352 shown better performances. The main benefits are: reduced charging time, improved charging efficiency,
353 mitigation of the temperature rises, and maintenance of the battery SOC within secure limits. Moreover, they
354 reduce of the investment cost in energy storage capacity and they extend the life expectancy.

355 Most of the papers consulted based their results on simulations and in some cases on experimental tests with
356 VRLA batteries. Therefore, much more real experiments are needed to extend the conclusion to real systems.

357 The extension to other types of batteries such as OPzS lead-acid batteries and lithium iron phosphate (LiFePO₄)
358 batteries is also a hot research topic. However, the high cost of LiFePO₄ batteries becomes a constraint for
359 large-scale implementations in RES.

360 Future work will focus on experimental application of FLC and MPC in the energy management of a
361 grid-connected system located in Departamento del Chocó – Colombia (in Spanish).

362

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370 References

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- 373 1. Khalilpour, Rajab; Vassallo, Anthony. Planning and operation scheduling of PV-battery
374 systems: A novel methodology. *Renewable and Sustainable Energy Reviews*, 2016, vol. 53, p.
375 194-208.
- 376 2. Yang, Z., Zhang, J., Kintner-Meyer, M. C., Lu, X., Choi, D., Lemmon, J. P., & Liu, J.
377 Electrochemical energy storage for green grid. *Chemical reviews*, 2011, vol. 111, no 5, p.
378 3577-3613.
- 379 3. Sayigh, Ali (ed.). *Renewable Energy in the Service of Mankind Vol I: Selected Topics from the*
380 *World Renewable Energy Congress WREC 2014*. Springer, 2015.
- 381 4. Armstrong, S.; Glavin, M. E.; Hurley, W. G. Comparison of battery charging algorithms for
382 stand-alone photovoltaic systems. In *Power Electronics Specialists Conference, 2008. PESC*
383 *2008*. IEEE. IEEE, 2008. p. 1469-1475.
- 384 5. Koochi-Kamali, S., Tyagi, V. V., Rahim, N. A., Panwar, N. L., & Mokhlis, H.. Emergence of
385 energy storage technologies as the solution for reliable operation of smart power systems: A
386 review. *Renewable and Sustainable Energy Reviews*, 2013, vol. 25, p. 135-165.
- 387 6. Kousksou, T., Bruel, P., Jamil, A., El Rhafiki, T., & Zeraouli, Y. Energy storage: Applications
388 and challenges. *Solar Energy Materials and Solar Cells*, 2014, vol. 120, p. 59-80.
- 389 7. Akinyele, Daniel; Belikov, Juri; Levron, Yoash. Battery Storage Technologies for Electrical
390 Applications: Impact in Stand-Alone Photovoltaic Systems. *Energies*, 2017, vol. 10, no 11, p.
391 1760.
- 392 8. Kaldellis, J. K.; Zafirakis, D.; Kavadias, K. Techno-economic comparison of energy storage
393 systems for island autonomous electrical networks. *Renewable and Sustainable Energy*
394 *Reviews*, 2009, vol. 13, no 2, p. 378-392.
- 395 9. Ferreira, H. L., Garde, R., Fulli, G., Kling, W., & Lopes, J. P. Characterization of electrical
396 energy storage technologies. *Energy*, 2013, vol. 53, p. 288-298.

- 397 10. Chen, H., Cong, T. N., Yang, W., Tan, C., Li, Y., & Ding, Y. Progress in electrical energy storage
398 system: A critical review. *Progress in Natural Science*, 2009, vol. 19, no 3, p. 291-312.
- 399 11. Díaz-González, F., Sumper, A., Gomis-Bellmunt, O., & Villafafila-Robles, R. A review of energy
400 storage technologies for wind power applications. *Renewable and Sustainable Energy Reviews*,
401 2012, vol. 16, no 4, p. 2154-2171.
- 402 12. Evans, Annette; Strezov, Vladimir; Evans, Tim J. Assessment of utility energy storage options
403 for increased renewable energy penetration. *Renewable and Sustainable Energy Reviews*, 2012,
404 vol. 16, no 6, p. 4141-4147.
- 405 13. Alotto, Piergiorgio; Guarnieri, Massimo; Moro, Federico. Redox flow batteries for the storage
406 of renewable energy: A review. *Renewable and Sustainable Energy Reviews*, 2014, vol. 29, p.
407 325-335.
- 408 14. Nikdel, M. Various battery models for various simulation studies and applications. *Renewable
409 and Sustainable Energy Reviews*, 2014, vol. 32, p. 477-485.
- 410 15. Hoppmann, J., Volland, J., Schmidt, T. S., & Hoffmann, V. H. The economic viability of battery
411 storage for residential solar photovoltaic systems—A review and a simulation model.
412 *Renewable and Sustainable Energy Reviews*, 2014, vol. 39, p. 1101-1118.
- 413 16. Hesse, Holger C., et al. Economic optimization of component sizing for residential battery
414 storage systems. *Energies*, 2017, vol. 10, no 7, p. 835.
- 415 17. Fathima, Hina; Palanisamy, K. Optimized sizing, selection, and economic analysis of battery
416 energy storage for grid-connected wind-PV hybrid system. *Modelling and Simulation in
417 Engineering*, 2015, vol. 2015, p. 16.
- 418 18. Battke, B., Schmidt, T. S., Grosspietsch, D., & Hoffmann, V. H. A review and probabilistic
419 model of lifecycle costs of stationary batteries in multiple applications. *Renewable and
420 Sustainable Energy Reviews*, 2013, vol. 25, p. 240-250.
- 421 19. Luo, X., Wang, J., Dooner, M., & Clarke, J. Overview of current development in electrical
422 energy storage technologies and the application potential in power system operation. *Applied
423 Energy*, 2015, vol. 137, p. 511-536.
- 424 20. Dekka, A., Ghaffari, R., Venkatesh, B., & Wu, B. A survey on energy storage technologies in
425 power systems. In *Electrical Power and Energy Conference (EPEC), 2015 IEEE*. IEEE, 2015. p.
426 105-111.
- 427 21. Hsieh, Hung-I.; Tsai, Cheng-Yuan; Hsieh, Guan-Chyun. Photovoltaic burp charge system on
428 energy-saving configuration by smart charge management. *IEEE Transactions on Power
429 Electronics*, 2014, vol. 29, no 4, p. 1777-1790.
- 430 22. Yin, Y., Luo, X., Guo, S., Zhou, Z., & Wang, J. A battery charging control strategy for renewable
431 energy generation systems. In *Proceedings of the World Congress on Engineering*. 2008. p. 2-4.
- 432 23. Dakkak, Mohamed; Hasan, Adel. A charge controller based on microcontroller in stand-alone
433 photovoltaic systems. *Energy Procedia*, 2012, vol. 19, p. 87-90.
- 434 24. Bandara, Gemdc; Ivanov, Ratcho; Gishin, Stoyan. Intelligent fuzzy controller for a lead-acid
435 battery charger. In *Systems, Man, and Cybernetics, 1999. IEEE SMC'99 Conference
436 Proceedings. 1999 IEEE International Conference on*. IEEE, 1999. p. 185-189.
- 437 25. Hua, Chih-Chiang; Lin, Meng-Yu. A study of charging control of lead-acid battery for electric
438 vehicles. In *Industrial Electronics, 2000. ISIE 2000. Proceedings of the 2000 IEEE International
439 Symposium on*. IEEE, 2000. p. 135-140.
- 440 26. Ayoub, Elie; Karami, Nabil. Review on the charging techniques of a li-ion battery. In
441 *Technological Advances in Electrical, Electronics and Computer Engineering (TAEECE), 2015
442 Third International Conference on*. IEEE, 2015. p. 50-55.
- 443 27. Rand, D. A. J., Moseley, P. T., Rand, D. A. J., Moseley, P. T., Garche, J., & Parker, C. D. Valve
444 regulated lead acid batteries, 2004. ISBN: 0-4445-0746-9.
- 445 28. Hua, A. Chih-Chiang; Syue, B. Zong-Wei. Charge and discharge characteristics of lead-acid
446 battery and LiFePO4 battery. In *Power Electronics Conference (IPEC), 2010 International*.
447 IEEE, 2010. p. 1478-1483.

- 448 29. Lee, Cheng Siong; Lin, Hsiung Cheng; Lai, Sin-You. Development of fast large lead-acid
449 battery charging system using multi-state strategy. *International Journal on Computer,*
450 *Consumer and Control (IJ3C)*, 2013, vol. 2, no 2.
- 451 30. Yan, J., Xu, G., Qian, H., Xu, Y., & Song, Z. Model predictive control-based fast charging for
452 vehicular batteries. *Energies*, 2011, vol. 4, no 8, p. 1178-1196.
- 453 31. Eldahab, Yasser E. Abu; Saad, Naggar H.; Zekry, Abdalhalim. Enhancing the design of battery
454 charging controllers for photovoltaic systems. *Renewable and Sustainable Energy Reviews*,
455 2016, vol. 58, p. 646-655.
- 456 32. Wong, Y. S.; Hurley, W. G.; Wölfle, W. H. Charge regimes for valve-regulated lead-acid
457 batteries: Performance overview inclusive of temperature compensation. *Journal of Power*
458 *Sources*, 2008, vol. 183, no 2, p. 783-791.
- 459 33. Rossinot, E., Lefrou, C., Dalard, F., & Cun, J. P. Batteries in standby applications: comparison of
460 alternate mode versus floating. *Journal of Power Sources*, 2001, vol. 101, no 1, p. 27-34.
- 461 34. Chen, Liang-Rui. Design of duty-varied voltage pulse charger for improving Li-ion
462 battery-charging response. *IEEE Transactions on Industrial Electronics*, 2009, vol. 56, no 2, p.
463 480-487.
- 464 35. Liu, C. L., Chiu, Y. S., Liu, Y. H., Ho, Y. H., & Huang, S. S. Optimization of a
465 fuzzy-logic-control-based five-stage battery charger using a fuzzy-based taguchi method.
466 *Energies*, 2013, vol. 6, no 7, p. 3528-3547.
- 467 36. Huang, Shyh-Jier; Huang, Bo-Ge; Pai, Fu-Sheng. Fast Charge Strategy Based on the
468 Characterization and Evaluation of LiFePO₄ Batteries. *IEEE Transactions on Power Electronics*,
469 2013, vol. 28, no 4, p. 1555-1562.
- 470 37. Linden, David; Reddy, Thomas B. *Handbook of Batteries*. 3rd. 2002.
- 471 38. Nasser Kutkut, Ph.D. – Power Designers, LLC - Madison, WI. Negative Pulse Charging: Myths
472 and Facts.
473 http://www.batterypoweronline.com/images/PDFs_articles_whitepaper_appros/powerdesigners.pdf.
474 [Consulted: 03-05-2017]
- 475 39. Li, Siguang; Zhang, Chengning; Xie, Shaobo. Research on fast charge method for lead-acid
476 electric vehicle batteries. *En Intelligent Systems and Applications*, 2009. ISA 2009. International
477 Workshop on. IEEE, 2009. p. 1-5.
- 478 40. James, M., Grummett, J., Rowan, M., & Newman, J. Application of pulse charging techniques
479 to submarine lead-acid batteries. *Journal of power sources*, 2006, vol. 162, no 2, p. 878-883.
- 480 41. Chuang, Y. C., Ke, Y. L., Chuang, H. S., & Chang, S. Y. Battery float charge technique using
481 parallel-loaded resonant converter for discontinuous conduction operation. *IEEE Transactions*
482 *on Industry Applications*, 2012, vol. 48, no 3, p. 1070-1078.
- 483 42. Battery Management of the SunnyIsland.
484 http://files.sma.de/dl/7910/SI_Batteriemanagement-TI-en-21.pdf. [Consulted: 22/06/2017]
- 485 43. Zadeh, Lotfi A. Fuzzy sets. *Information and control*, 1965, vol. 8, no 3, p. 338-353.
- 486 44. Hsieh, Guan-Chyun; Chen, Liang-Rui; Huang, Kuo-Shun. Fuzzy-controlled Li-ion battery
487 charge system with active state-of-charge controller. *IEEE Transactions on industrial*
488 *electronics*, 2001, vol. 48, no 3, p. 585-593.
- 489 45. Precup, Radu-Emil; Hellendoorn, Hans. A survey on industrial applications of fuzzy control.
490 *Computers in Industry*, 2011, vol. 62, no 3, p. 213-226.
- 491 46. Bago, J. C., Galán, S. G., Aguilera, J., Velasco, J. R., & Magdalena, L. Fuzzy controller
492 applications in stand-alone photovoltaic systems. *Mathware & soft computing*, 2008, vol. 9, no
493 1, p. 85-105.
- 494 47. Rahim, N. A., Mekhilef, S., Chan, E. L., & Ping, H. W. Fuzzy-controlled battery charger
495 state-of-charge controller. *International Journal of Modelling and Simulation*, 2006, vol. 26, no
496 2, p. 106-111.
- 497 48. Huang, C. H., Huang, C. C., Ou, T. C., Lu, K. H., & Hong, C. M. Intelligent fuzzy logic
498 controller for a solar charging system. In *Advanced Intelligent Mechatronics*, 2009. AIM 2009.
499 IEEE/ASME International Conference on. IEEE, 2009. p. 1412-1417.

- 500 49. Kim, J. Y., Kim, H. M., Kim, S. K., Jeon, J. H., & Choi, H. K. Designing an energy storage system
501 fuzzy PID controller for microgrid islanded operation. *Energies*, 2011, vol. 4, no 9, p. 1443-1460.
- 502 50. Welch, Richard L.; Venayagamoorthy, Ganesh Kumar. Energy dispatch fuzzy controller for a
503 grid-independent photovoltaic system. *Energy Conversion and Management*, 2010, vol. 51, no
504 5, p. 928-937.
- 505 51. Welch, Richard L.; Venayagamoorthy, Ganesh K. Comparison of two optimal control strategies
506 for a grid independent photovoltaic system. In *Industry Applications Conference, 2006. 41st*
507 *IAS Annual Meeting. Conference Record of the 2006 IEEE. IEEE, 2006. p. 1120-1127.*
- 508 52. Fu-Shun, Wang; Xue-Song, Suo. Research on Batterys charging system based on the Fuzzy
509 control. En *Proceedings of the 2nd International Conference on Computer Science and*
510 *E-lectronics Engineering. 2013.*
- 511 53. Swathika, R., Ram, R. G., Kalaichelvi, V., & Karthikeyan, R. Application of fuzzy logic for
512 charging control of lead-acid battery in stand-alone solar photovoltaic system. En *Green*
513 *Computing, Communication and Conservation of Energy (ICGCE), 2013 International*
514 *Conference on. IEEE, 2013. p. 377-381.*
- 515 54. Safari, S.; Ardehali, M. M.; Sirizi, M. J. Particle swarm optimization based fuzzy logic controller
516 for autonomous green power energy system with hydrogen storage. *Energy conversion and*
517 *management*, 2013, vol. 65, p. 41-49.
- 518 55. Berrazouane, Sofiane; Mohammedi, Kamal. Parameter optimization via cuckoo optimization
519 algorithm of fuzzy controller for energy management of a hybrid power system. *Energy*
520 *Conversion and Management*, 2014, vol. 78, p. 652-660.
- 521 56. Haoran, Z. H. A. O., Qiuwei, W. U., Chengshan, W. A. N. G., Cheng, L., & Rasmussen, C. N.
522 Fuzzy logic based coordinated control of battery energy storage system and dispatchable
523 distributed generation for microgrid. *Journal of Modern Power Systems and Clean Energy*,
524 2015, vol. 3, no 3, p. 422-428.
- 525 57. Arcos-Aviles, D., Pascual, J., Marroyo, L., Sanchis, P., & Guinjoan, F. Fuzzy logic-based energy
526 management system design for residential grid-connected microgrids. *IEEE Transactions on*
527 *Smart Grid*, 2016. doi 10.1109/TSG.2016.2555245
- 528 58. Derrouazin, A., Aillerie, M., Mekkakia-Maaza, N., & Charles, J. P. Fuzzy logic controller versus
529 classical logic controller for residential hybrid solar-wind-storage energy system. In *AIP*
530 *Conference Proceedings. AIP Publishing, 2016. Vol. 1758. No. 1p. 030055.*
- 531 59. Paliwal, Priyanka; Patidar, N. P.; Nema, R. K. Fuzzy logic based determination of battery
532 charging efficiency applied to hybrid power system. *J World Acad Eng Sci Technol*, 2012, vol.
533 71, p. 1164-1168.
- 534 60. Teo, T. T., Logenthiran, T., Woo, W. L., & Abidi, K. Fuzzy logic control of energy storage
535 system in microgrid operation. En *Innovative Smart Grid Technologies-Asia (ISGT-Asia), 2016*
536 *IEEE. IEEE, 2016. p. 65-70.*
- 537 61. Hussain, Akhtar; Bui, Van-Hai; Kim, Hak-Man. Fuzzy Logic-Based Operation of Battery
538 Energy Storage Systems (BESSs) for Enhancing the Resiliency of Hybrid Microgrids. *Energies*,
539 2017, vol. 10, no 3, p. 271.
- 540 62. Camacho, E. F., & Alba, C. B. *Model predictive control. Springer Science & Business Media.*
541 2013.
- 542 63. Qin, S. Joe; Badgwell, Thomas A. A survey of industrial model predictive control technology.
543 *Control engineering practice*, 2003, vol. 11, no 7, p. 733-764.
- 544 64. Geyer, Tobias; Papafotiou, Georgios; Morari, Manfred. Hybrid model predictive control of the
545 step-down DC-DC converter. *IEEE Transactions on Control Systems Technology*, 2008, vol. 16,
546 no 6, p. 1112-1124.
- 547 65. Cortes, P., Rodriguez, J., Antoniewicz, P., & Kazmierkowski, M. Direct power control of an
548 AFE using predictive control. *IEEE Transactions on Power Electronics*, 2008, vol. 23, no 5, p.
549 2516-2523.
- 550 66. Xie, Yanhui H. Ghaemi R. Sun J. and Freudenberg J. S. Implicit model predictive control of a
551 full bridge DC-DC converter. *IEEE Transactions on Power Electronics*, 2009, vol. 24, no 12, p.
552 2704-2713.

- 553 67. Quevedo, D. E., Aguilera, R. P., Perez, M. A., Cortés, P., & Lizana, R. Model predictive control
554 of an AFE rectifier with dynamic references. *IEEE Transactions on Power Electronics*, 2012, vol.
555 27, no 7, p. 3128-3136.
- 556 68. Townsend, Christopher D.; Summers, Terrence J.; Betz, Robert E. Multigoal heuristic model
557 predictive control technique applied to a cascaded H-bridge StatCom. *IEEE Transactions on*
558 *Power Electronics*, 2012, vol. 27, no 3, p. 1191-1200.
- 559 69. Maciejowski, J. M. *Predictive control: with constraints*. Pearson education. 2002.
- 560 70. Perez, E., Beltran, H., Aparicio, N., & Rodriguez, P. Predictive power control for PV plants with
561 energy storage. *IEEE Transactions on Sustainable Energy*, 2013, vol. 4, no 2, p. 482-490.
- 562 71. Pezeshki, Houman; Wolfs, Peter; Ledwich, Gerard. A model predictive approach for
563 community battery energy storage system optimization. En PES General Meeting| Conference
564 & Exposition, 2014 IEEE. IEEE, 2014. p. 1-5.
- 565 72. Dizqah, A. M., Maheri, A., Busawon, K., & Kamjoo, A. A multivariable optimal energy
566 management strategy for standalone dc microgrids. *IEEE transactions on power systems*, 2015,
567 vol. 30, no 5, p. 2278-2287.
- 568 73. Morstyn, Thomas; Hredzak, Branislav; Agelidis, Vassilios G. Dynamic optimal power flow for
569 DC microgrids with distributed battery energy storage systems. In *Energy Conversion*
570 *Congress and Exposition (ECCE)*, 2016 IEEE. IEEE, 2016. p. 1-6.
- 571 74. Morstyn, T., Hredzak, B., Aguilera, R. P., & Agelidis, V. G. Model Predictive Control for
572 Distributed Microgrid Battery Energy Storage Systems. *IEEE Transactions on Control Systems*
573 *Technology*, 2017.
- 574 75. Kujundžić, G., Ileš, Š., Matuško, J., & Vašak, M. Optimal charging of valve-regulated lead-acid
575 batteries based on model predictive control. *Applied Energy*, 2017, vol. 187, p. 189-202.
- 576 76. Zeng, P. P., Wu, Z., Zhang, X. P., Liang, C., & Zhang, Y. Model predictive control for energy
577 storage systems in a network with high penetration of renewable energy and limited export
578 capacity. In *Power Systems Computation Conference (PSCC)*, 2014. IEEE, 2014. p. 1-7.
- 579 77. Li, Chiao-Ting; Peng, Huei; Sun, Jing. Predictive control and sizing of energy storage to
580 mitigate wind power intermittency. *Wind Energy*, 2016, vol. 19, no 3, p. 437-451.
- 581 78. Khalid, Muhammad; Savkin, Andrey V. Model predictive control based efficient operation of
582 battery energy storage system for primary frequency control. In *Control Automation Robotics*
583 *& Vision (ICARCV)*, 2010 11th International Conference on. IEEE, 2010. p. 2248-2252.
- 584 79. Ferrarini, Luca; Mantovani, Giancarlo; Costanzo, Giuseppe Tommaso. A Distributed Model
585 Predictive Control approach for the integration of flexible loads, storage and renewables. In
586 *Industrial Electronics (ISIE)*, 2014 IEEE 23rd International Symposium on. IEEE, 2014. p.
587 1700-1705.
- 588 80. Wang, Trudie; Kamath, Haresh; Willard, Steve. Control and optimization of grid-tied
589 photovoltaic storage systems using model predictive control. *IEEE Transactions on Smart Grid*,
590 2014, vol. 5, no 2, p. 1010-1017.
- 591 81. Petrollese, M., Valverde, L., Cocco, D., Cau, G., & Guerra, J. Real-time integration of optimal
592 generation scheduling with MPC for the energy management of a renewable hydrogen-based
593 microgrid. *Applied Energy*, 2016, vol. 166, p. 96-106.
- 594 82. Matthijs, B., Müller, D., Binder, J., & Pietruschka, D. Model Predictive Control Schemes for
595 PV-Storage Systems to Increase Grid Compatibility and Optimise Energy Costs. *EU PVSEC*
596 *Proc*, 2014, p. 3581-6.
- 597 83. Kim, Jonghoon; Nikitenkov, Dmitry. Fuzzy logic-controlled online state-of-health (SOH)
598 prediction in large format LiMn2O4 cell for energy storage system (ESS) applications. In
599 *Industrial Technology (ICIT)*, 2014 IEEE International Conference on. IEEE, 2014. p. 474-479.
- 600 84. Li, Xiangjun; Yan, Heming. Fuzzy logic-based coordinated control method for multi-type
601 battery energy storage systems. *Artificial Intelligence Review*, 2016, p. 1-17.
- 602 85. Li, X., Li, N., Jia, X., & Hui, D. Fuzzy logic based smoothing control of wind/PV generation
603 output fluctuations with battery energy storage system. In *Electrical Machines and Systems*
604 *(ICEMS)*, 2011 International Conference on. IEEE, 2011. p. 1-5.