

Article

Aerosol depolarization ratio measurement capabilities for an elastic LIDAR: implementation and first measurements

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Abstract: A new approach to the measurement with elastic lidar of depolarization produced by atmospheric aerosols is presented. The system uses two different telescopes: one for depolarization measurements and another for total-power measurements. The system architecture and principle of operation are described. The first experimental results are also presented, corresponding to a collection of atmospheric conditions over the city of Barcelona.

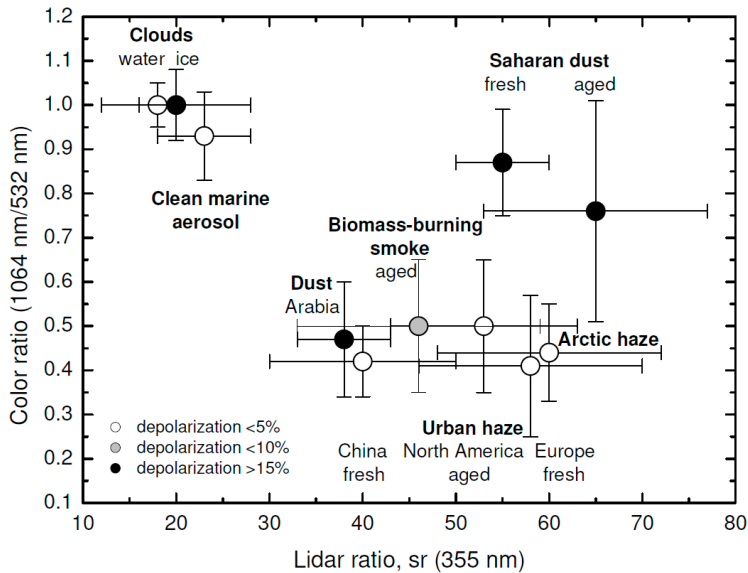
Keywords: Lidar system, depolarization channel, calibration, stability, depolarizing particles

1. Introduction

Multi-wavelength lidars provide a number of measurements that can be used to characterize the nature and origin of the aerosols present in the atmosphere. The most relevant [1] are: the lidar ratio, defined as that between the retrieved extinction and backscattering at a given wavelength; the ratio of lidar ratios at two different wavelengths and the color ratio (also known as the Ångström coefficient [2]), also computed by comparing the retrieved backscattering and extinction at different wavelengths.

Additionally, since the 1970s the use of the lidar depolarization technique has proven to be a valuable tool for atmospheric sciences, e.g. [3] or [4]. Regarding aerosol characterization, the depolarization information has been widely used for aerosol typing when combined with additional optical properties (e.g. [5–10]). In this sense, it can also be very useful in the retrieval of the planetary boundary layer (PBL) height since it allows to discriminate between the aerosol within this layer and different aerosol types coupled to the PBL height based on aerosol data [11]. Fig. 1 shows, in a very visual manner, how the depolarization data combined with the color ratio allow for discriminating among different kinds of aerosols and clouds. So depolarization information can be added to the set of parameters to be considered in aerosol classification [12,13].

Besides aerosol typing, the depolarization technique also provides relevant information for the retrieval of aerosol microphysical properties. Due to the particle shape information associated to lidar depolarization, retrievals of non-spherical particles by inversion methods can be highly improved (see e.g. [14–17]).



42

43 **Fig. 1.** Color ratio vs lidar ratio and particle depolarization ratio for different aerosol and cloud types.
44 Figure from [18] with information from [1]. Reproduced with permission from the authors.

45 Because of the importance of depolarization measurements for aerosol science, a new
46 depolarization measurement channel [19] has been developed and implemented for the
47 BarcelonaTech (UPC) 6-channel elastic/Raman lidar [20]. The main difference with other present
48 lidar systems with depolarization measurement capability (see, for instance, [21] or [22]) is the use of
49 an additional telescope (in fact, a telephoto lens) to measure the cross-polarized return signal,
50 without altering the rest of the original system.

51 Section 2 describes the system architecture; section 3 contains the basic formulation for
52 retrieving the information about depolarization profiles; section 4 details the calibration process and
53 section 5 presents some measurements corresponding to a collection of atmospheric conditions over
54 the city of Barcelona.

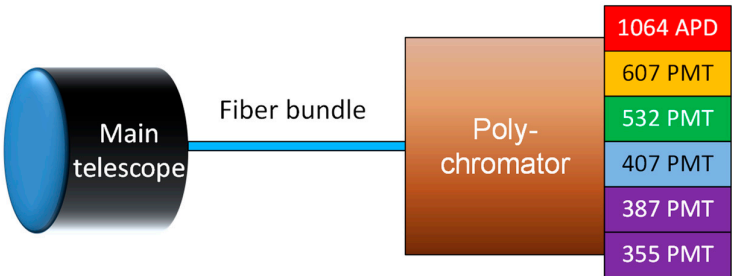
55 **2. System architecture**

56 A complete description of the UPC main lidar instrument can be found at [20]. The transmitter
57 is based on a Quantel® Brilliant® laser, equipped with second and third harmonic generators. The
58 laser produces 3.6-ns pulses at with energies 130 mJ at 1064 nm and 532 nm and 40 mJ at 355 nm.

59 The 6-channel main receiver unit is sketched in Fig. 2. A 356-mm diameter telescope
60 (CELESTRON® C14-A XLT) collects backscattered light and couples it (with the help of a field lens)
61 to a 3-mm diameter fiber bundle (manufactured by CeramOptec®, custom-made). This bundle
62 delivers the light to a poly-chromator, which splits the beam to the different channels. They include:
63 three elastic backscattering channels (1064, 532 and 355 nm) and three Raman channels (607 and 387
64 nm for nitrogen and 407 nm for water vapor).

65 The axes of the laser beams and the telescope are parallel, with an approximate distance of 30
66 cm between them. This fact causes the partial overlap between the part of the atmosphere
67 illuminated by the laser beams and that “seen” by the receivers, which affects to the amount of light
68 collected from short distances [23].

69 We have tested the polarization performance of the fiber bundle [24], finding that, for a linearly
70 polarized input, the circularity of the polarization ellipse of the light at the output is better than 93%
71 (in power terms). This fact permits to consider that the 6 channels (including the 532-nm one) are
72 basically sensitive to the total collected power, without any polarization discrimination, even though
73 the poly-chromator includes several beam-splitters that could cause diattenuation. The overall
74 calculated transmission of the fiber bundle and the poly-chromator at the 532-nm output is 6.18%
75 [20]. Further measurements (see section **Error! Reference source not found.**) suggest that the 532-nm
76 channel transmission could be lower.

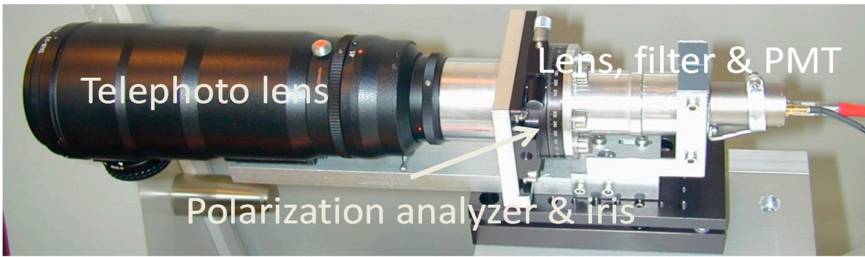


77

78 **Fig. 2.** Main receiver in UPC lidar [20].

79 The signal collected in the different channels is detected by means of an APD photo-receiver
80 (for the 1064 nm channel) and five photo-multiplier tube modules (for the remaining channels) and
81 digitized by a parallel Licel® Transient Recorder [25] with analog and photon-counting capabilities.
82 The aerosol depolarization ratio measurement requires the comparison of the signals recovered
83 by two channels in the system: one proportional to the total power and another proportional to
84 either the co-polar or cross-polar component of the signal collected [26]. These two channels operate
85 at 532 nm.

86 The depolarization auxiliary channel [19,24,27] is shown in Fig. 3.



87

88 **Fig. 3.** Auxiliary channel for depolarization measurements, where the most relevant elements are
89 labelled

90 The depolarization channel uses a separate telescope (a 70-mm aperture, 300-mm focal distance
91 TAIR-3S telephoto lens). The rest of the optical arrangement, sketched in Fig. 4, includes a 1-mm
92 field-of-view stop iris (D) in the focal plane, a polarization analyzer (P), and eye-piece lens (L4) and a
93 Barr® interference filter (IF) centered at 532 nm, with 0.5-nm spectral width. The polarization
94 analyzer is made by a linear polarizer mounted on a goniometric mount that can be seen in Fig. 3.

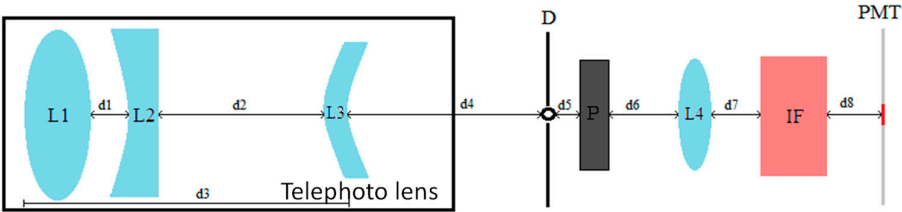


Fig. 4. Depolarization channel optical configuration

The different distances are indicated in Table 1. Some of the parameters provided in Table 1 have been experimentally determined and adjusted for an optimal performance of the depolarization channel. Every component (except for the telephoto lens) has a diameter of 2.54 mm.

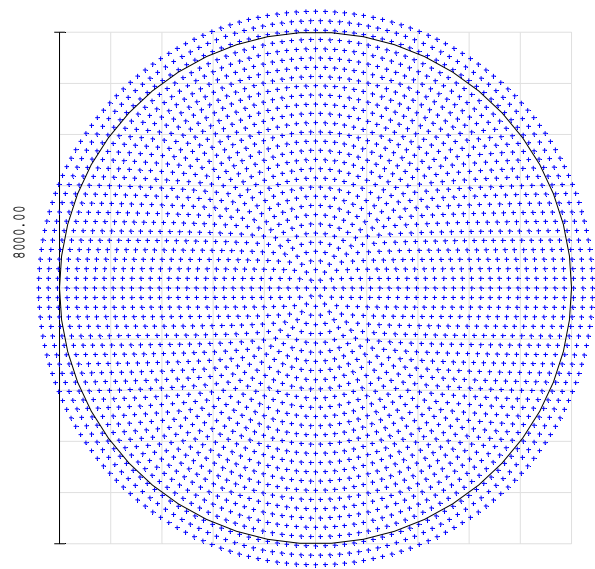
Table 1. Parameters of the different optical elements of the depolarization channel.

Parameter	Value
d4	138.9 mm (estimated)
d5	1 mm
d6	39.4 mm
d7	5 mm
d8	23 mm
Telephoto lens focal distance	300 mm
Eye-piece lens focal distance	38 mm
Interference filter	
Center wavelength	531.9 nm
Spectral width	0.5 nm
Thickness	11 mm

The collected light is detected by the active surface of a Licel® R9880U PMT module (PMT in Fig. 4) [28], which feeds the detected current to a dedicated Licel® transient recorder.

The iris is located at the focal plane of the telephoto lens and limits the field of view to a theoretical value of 3.33 mrad (reduced partially due to building compromises, as it will be pointed out later), which is essential to limit the amount of background diffuse light that reaches the PMT active surface, as it is the reduced value of the filter spectral width; the eye-piece produces an image of the telephoto lens input aperture onto the PMT detection surface, optimizing the detection process.

A ray-optics simulation of the receiver has been performed, using the software ZEMAX®. Fig. 5 plots the axial ray distribution over the plane of the active surface of the photo-multiplier tube. The plot shows the impinging points of the rays parallel to the optical axis. The PMT active surface has an 8-mm diameter. According to the optical analysis, the r.m.s. diameter of the ray distribution is 6.2 mm, while all the traced rays lay within a 8.6-mm diameter, which leads to an expected 16% overspill.

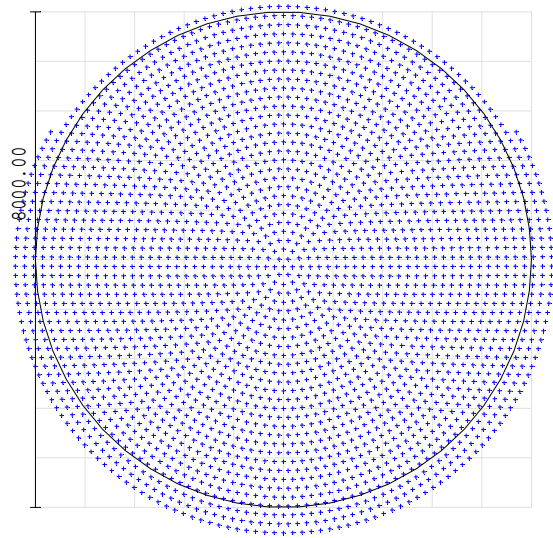


117

118 **Fig. 5.** Spot diagram of the distribution of the collected rays, parallel to the optical axis, over the
119 8-mm diameter active surface of the photo-multiplier detector tube calculated with ZEMAX®
120 software.

121

122 Fig. 6 shows the ray distribution of those entering the telephoto lens with the maximum
123 effective field of view which, according to the simulation has been reduced to 0.09 degrees (equal to
124 a maximum effective field of view of the optical system of approximately 3.14 mrad). For these rays,
125 the r.m.s. diameter is 6.15 mm and the maximum deviation from the center of the PMT active surface
126 is 4.41 mm, which would lead to a maximum overspill of 22% approximately. The overall field of
127 view (including only the rays that reach the PMT surface) is then reduced to approximately to 2.85
128 mrad.



129

130 **Fig. 6.** Spot diagram of the distribution of the collected extreme rays, entering the optical system with
131 an angle equal to half the effective field of view (0.09 deg), over the 8-mm diameter active surface of
132 the photo-multiplier detector tube calculated with ZEMAX® software.

The telephoto lens axis is approximately 40 cm from the laser beams (refer to the laser description above), which affects to the partial overlap at short distances as indicated earlier in the text. Fig. 7 shows the complete system in our laboratory. The lidar is pointed in a vertical direction; whenever it is not been used, a motorized hose covers the equipment.

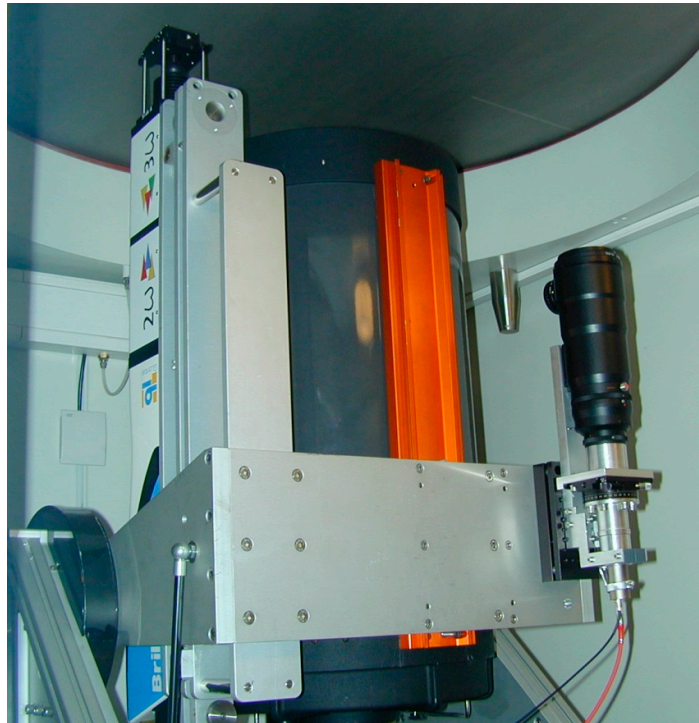


Fig. 7. Complete view of the UPC lidar system: the laser on the left (including 2nd and 3rd harmonic generators), the main telescope in the middle and the depolarization auxiliary channel on the right.

The nominal position of the polarization analyzer is 90-degrees from the transmitted beam polarization plane. In this way the channel is sensitive to the cross-polarized fraction of the light backscattered by the atmosphere.

3. Theory of operation

The lidar measures along a vertical axis, so in every expression the distance R to the lidar is equivalent to the height over the system.

The voltage signal obtained at the total-power PMT output can be written:

$$S_{Tot}(R) = V_{Tot}(R) \cdot P_{Tot}(R) \quad (1)$$

Where:

$V_{Tot}(R)$ is the total-power 532-nm channel responsivity, as a function of the distance to the lidar system R , including the effect of the partial overlap (see section **Error! Reference source not found.**).

$P_{Tot}(R)$ is the backscattered light power collected by the main telescope @532 nm.

The voltage signal obtained at the depolarization channel PMT output can be calculated:

$$S_{Dep}(90^\circ, R) = V_{Dep}(R) \cdot P_{\perp}(R) \quad (2)$$

Where:

157 $V_{Dep}(R)$ is the depolarization channel responsivity, as a function of the distance to the lidar
 158 system R , including the effect of the partial overlap.

159 $P_{\perp}(R)$ is the cross-polar fraction power of the depolarized backscattered light, function of R .
 160 We will define the depolarization channel system function as:

$$161 \quad V^*(R) = \frac{V_{Dep}(R)}{V_{Tot}(R)} \quad (3)$$

162 While it is extremely difficult to determine $V_{Dep}(R)$ and $V_{Tot}(R)$, it is possible to determine
 163 $V^*(R)$ by means of a calibration process that compares the output signals of the total-power
 164 channel and the cross-polar channel, when the polarization analyzer of the latter is set successively +
 165 and - 45 degrees from its nominal position [21]:

$$166 \quad V^*(R) = 2 \sqrt{\frac{S_{Dep}(90^\circ - 45^\circ, R)}{S_{Tot}(R)} \times \frac{S_{Dep}(90^\circ + 45^\circ, R)}{S_{Tot}(R)}} \quad (4)$$

167 The factor 2 takes into account that, at the calibration positions, the auxiliary channel is
 168 detecting half of the total backscattered power.

169 The volume depolarization is usually defined [21]:

$$170 \quad \delta^V(R) = \frac{P_{\perp}(R)}{P_{\parallel}(R)} \quad (5)$$

171 Accepting that $P_{Tot}(R) = P_{\parallel}(R) + P_{\perp}(R)$, and operating with the previous results, we can
 172 calculate the volume depolarization [24] as:

$$173 \quad \delta^V(R) = \frac{\delta^*(90^\circ, R)}{V^*(R) - \delta^*(90^\circ, R)} \quad (6)$$

174 Where:

$$175 \quad \delta^*(90^\circ, R) = \frac{S_{Dep}(90^\circ, R)}{S_{TOT}(R)} \quad (7)$$

176 Finally, the particle depolarization ratio can be computed by combining the volume ratio with
 177 the molecular and aerosol backscattering profiles [21]:

$$178 \quad \delta^p(R) = \frac{[1 + \delta^m] \cdot \delta^V(R) \cdot \rho(R) - [1 + \delta^V(R)] \cdot \delta^m}{[1 + \delta^m] \cdot \rho(R) - [1 + \delta^V(R)]} \quad (8)$$

179 Where:

$$180 \quad \rho(R) = \frac{\beta^m(R) + \beta^p(R)}{\beta^m(R)} \quad (9)$$

181 With $\beta^m(R)$ and $\beta^p(R)$, molecular and aerosol backscattering profiles retrieved by means
 182 of a Klett –Fernald ([29], [30]) or Raman ([31], [32]) inversion performed over the signal of the
 183 total-power channel.

184 Finally, the molecular volume depolarization ratio

$$185 \quad \delta^m = \frac{\beta_{\perp}^m}{\beta_{\parallel}^m} \quad (10)$$

186 was computed by Behrendt and Nakamura [33] and has an approximately constant value of
 187 3.8×10^{-3} for a receiver with a spectral width of 0.5 nm.

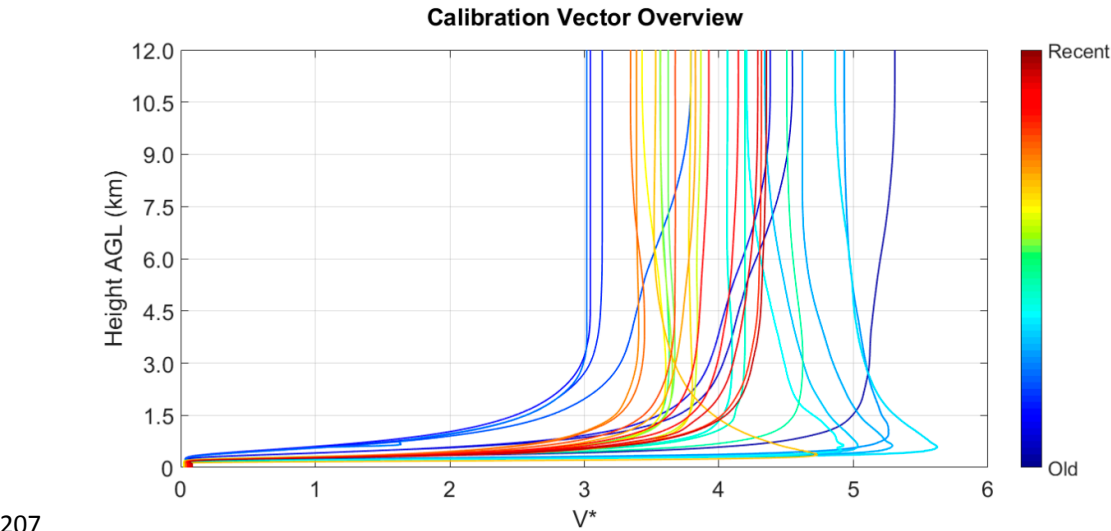
188 The error analysis of the different magnitudes obtained in the data analysis is detailed in the
189 appendix.
190

191 **4. Calibration process**

192 The determination of the depolarization channel system function is made by means of a
193 calibration procedure that compares the outputs of the depolarization and the total power channels
194 [21,35,36]; during the calibration the polarization analyzer of the depolarization channel is set first at
195 +45 degrees, and second at -45 degrees from the nominal (cross-polar) position. Each one of the
196 calibrations runs for 15 minutes, which amounts 18000 laser pulses.

197 The outputs of the two channels are divided and then a geometrical average is computed (as
198 indicated in equation (4)) between the system profiles obtained at the two positions; after that a
199 zero-phase low-pass spatial filter is applied to the average, to reduce noise effects; finally, the values
200 obtained for heights over ~10km are discarded, also due to noise effects, considering the value
201 obtained at 10 km for greater height values.

202 A number of calibrations have been performed since the implementation of the depolarization
203 channel, and the historic is presented in Fig. 8. The color sequence shows the time evolution of the
204 estimated system functions. As the colder colors point out, the early functions were affected by
205 misalignments between the laser and the receiver. The most recent calibrations are stabilized to a
206 medium-height value around 4.



208 **Fig. 8.** Historic of the calibrations of the depolarization channel system function obtained from March 2016 to
209 June 2017. The colder colors refer to early calibrations while the warmer ones to the recent ones.

210 Fig. 9 shows the temporal evolution of the far range value of V^* for the different calibrations
211 presented in Fig. 8 with the values obtained between realignment procedures grouped. The first
212 group of calibrations shows a deviation of more than 30%. After this period, an improvement in the
213 anchorage of the receiving optics was implemented and the deviation was reduced to less than 10%,
214 which was maintained after following realignment procedures. Anyway this diagram points out
215 that different phenomena (thermal changes, mechanical relaxation, state of the atmosphere) affect
216 V^* in a way that cannot be ignored.

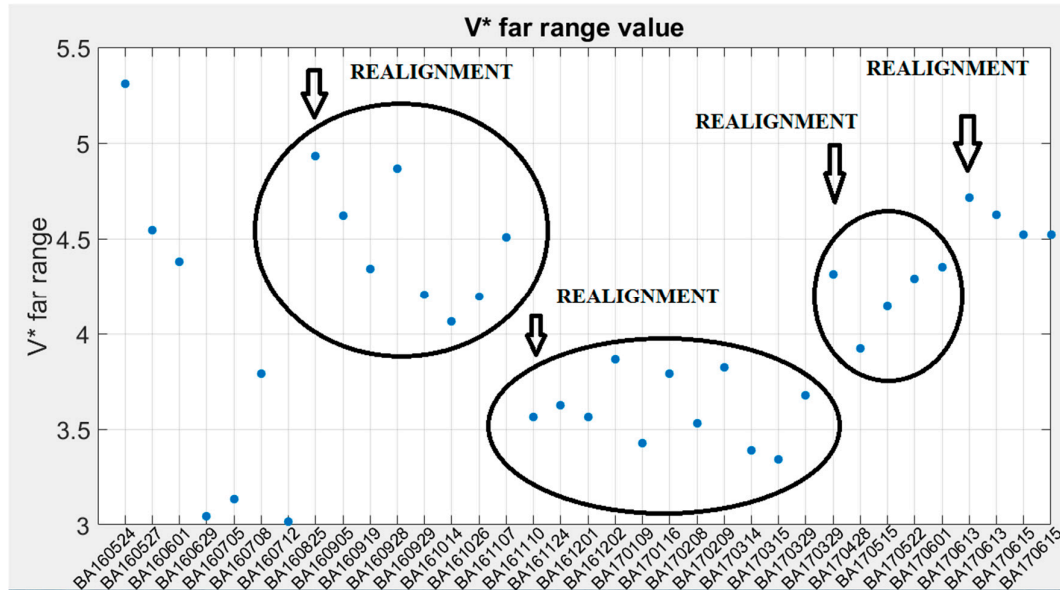


Fig. 9. Stability of the value of the depolarization channel system function for far range; the values comprised between realignment actions are marked by closed curves.

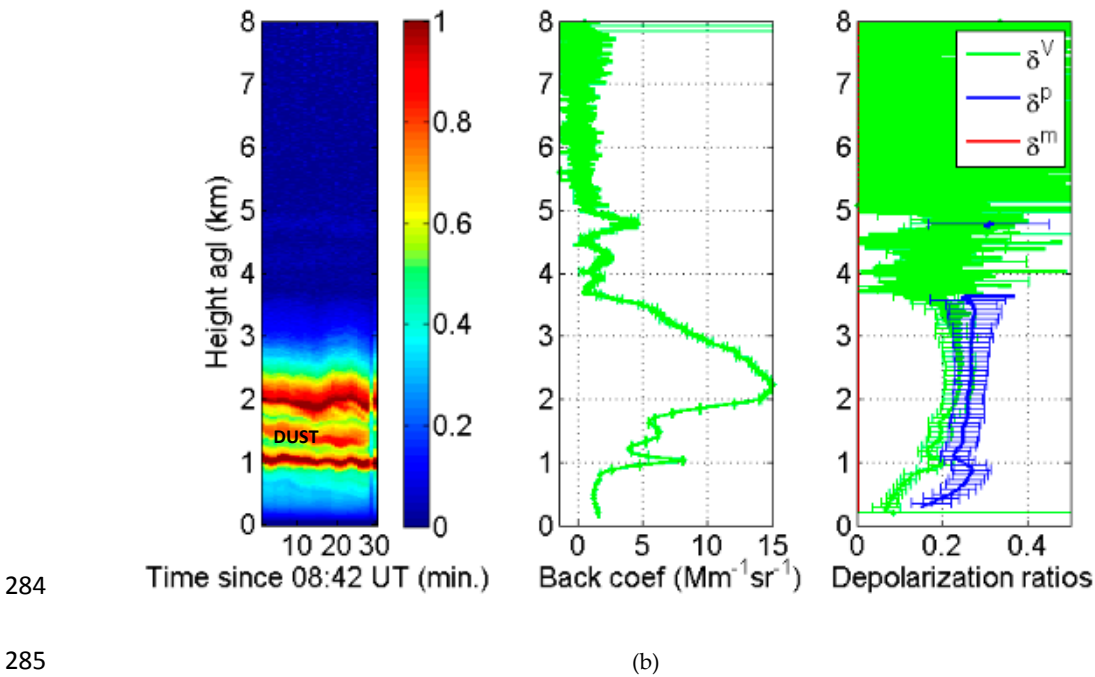
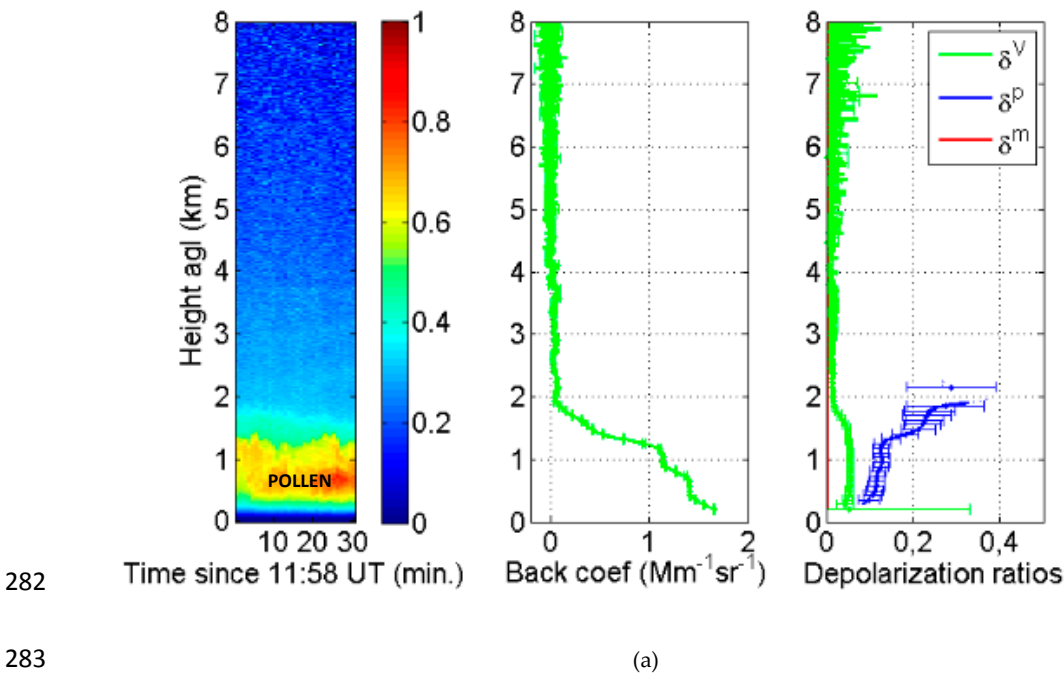
The system function includes the effect of the different overlap functions of the two channels; it also draws attention on the fact that, even though the ratio of the main telescope and the telephoto lens collecting surfaces is approximately 25, the depolarization channel optics has a higher transmission and a more responsive PMT receiver. This result also suggests that the transmission of the 532-nm total-power channel must be lower than that indicated in section **Error! Reference source not found.** These uncertainties make the periodic calibrations unavoidable.

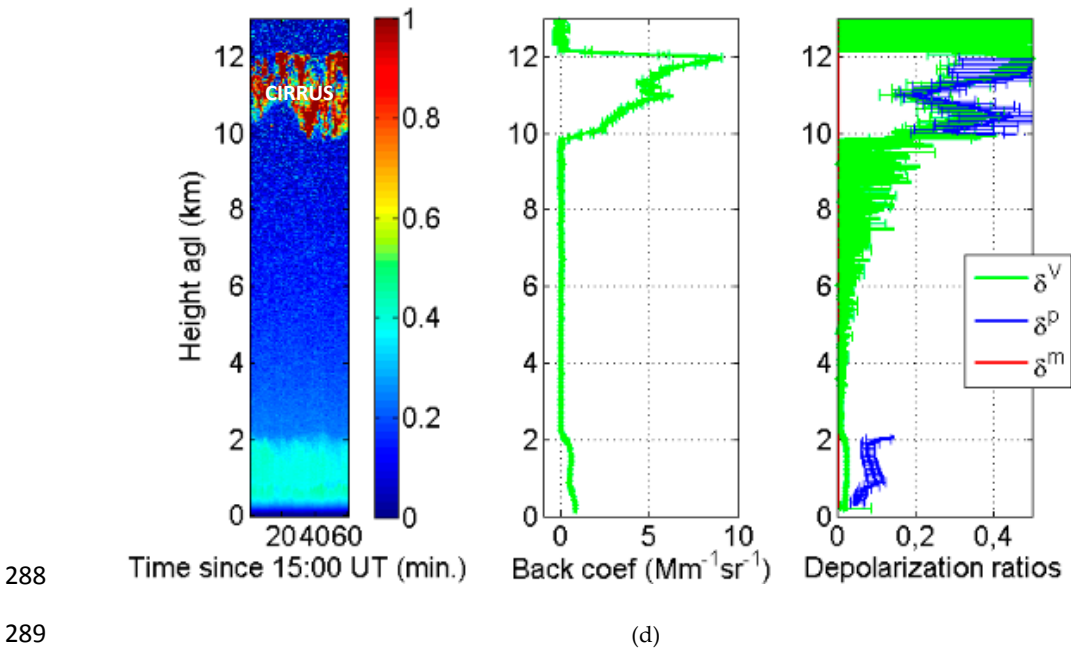
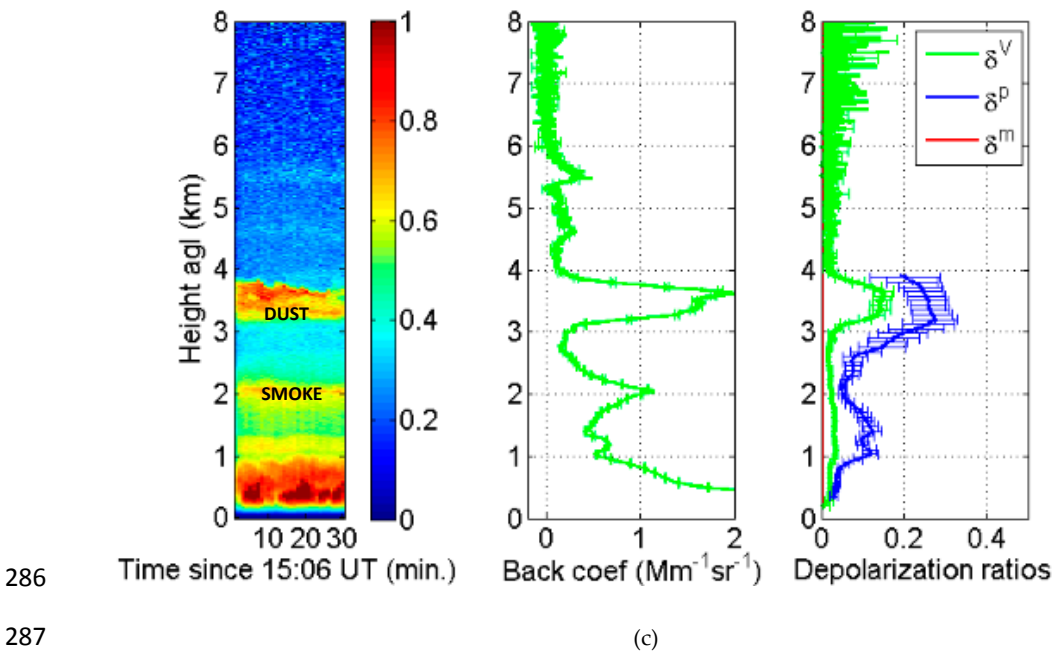
5. Depolarization ratio measurements

Some depolarization measurements are presented next for different aerosol loads. The volume depolarization ratio is retrieved from both total and perpendicular signals with Eq. (6) and a calibration depolarization channel system function, V^* . In all cases the depolarization channel system function is taken from the closest (in time) calibration performed prior to the measurement considered. The particle depolarization ratio is then retrieved with Eq. (8) from the volume depolarization ratio and the particle backscatter coefficient, β^p . All cases presented are daytime measurements, so that no Raman inversion is possible and thus β^p is retrieved with the Klett – Fernald ([29], [30]) method and a constant lidar ratio of 50 sr, except in the cirrus cloud case. In this case, as there is a molecular region below and above the cloud, the iterative backward-forward method [36] was applied to invert the cloud backscatter and extinction coefficients without the need to assume a lidar ratio. All profiles of the molecule backscatter coefficient, β^m , are calculated with the closest (in time) radiosoundings either at 12 or 00 UT. The error bars are calculated following the equations detailed in the appendix. For the sake of clarity, the points of the profiles of the particle depolarization ratio for which the error bar is larger than 50 % are not represented.

Fig. 10 shows the retrieval of volume and particle depolarization for different aerosol loads: pollen, mineral dust, fire smoke and a case of local urban aerosol, as well as a cirrus cloud case. In the case of pollen (Fig. 10a) the atmospheric boundary layer (ABL) extends up to ~1.5 km. In this layer δ^v is rather constant ~0.055 while δ^p varies slightly between 0.10 and 0.13. These values are in agreement with depolarization ratios measured during another pollen event in Barcelona by [37] who found mean values of δ^v (δ^p) of 0.06-0.10 (0.11-0.18) averaged over the period 9 – 17 UT.

For the day considered here, 14th March, 2017, [38] counted a total pollen near-surface concentration in Barcelona of 1746 grains per cubic meter, being 90 % of them *Platanus*, which is in the lower range of values 1082-2830 found in [37]. The second case (Fig. 10b) gives typical values of depolarization for mineral dust. It is taken from an outstanding desert dust intrusion over Iberia with aerosol optical depths as large as 2 [39]. Above 1 km δ^V is in the range 0.17-0.24 and δ^P in the range 0.23-0.28. The small differences between δ^V and δ^P are due to the high values of the particle backscatter coefficient ($\sim 15 \text{ Mm}^{-1}\text{sr}^{-1}$) in the dust layer. According to [40] the values of δ^P found in our work are in the upper range of desert dust mixtures (0.14-0.28) and below the values of pure desert dust (0.30-0.35). The example shown in Fig. 10c illustrates the transport of Canadian fires over the Iberian Peninsula on 24th May, 2016, at 15 UT. The smoke layers were first detected on the evening of 22nd May (see Barcelona Micro Pulse Lidar quicklooks at <https://mplnet.gsfc.nasa.gov/data?v=V3&s=Barcelona&t=20160522>) and lasted until the evening of 24th May. In Fig. 9b one sees the fire smoke layer at $\sim 2 \text{ km}$ and a dust layer above 3 km . To illustrate a case of fire smoke, we looked into our short database but unfortunately we could not find a situation clearly identified as fire smoke and with no other aerosol type. In the fire smoke plume δ^P varies in the range 0.05-0.10. Here again our findings are in agreement with the literature, in particular with [40] which collects values of δ^P for pure biomass burning measured in several places around the globe in the range 0.02-0.08, being values of fresh smoke slightly lower than for aged smoke. Our values fall into the interval representative of aged smoke. We extend now the illustration of particle depolarization ratios retrieved with the UPC new depolarization channel to ice particles in cirrus clouds. Fig. 10d shows a case of cirrus clouds extending between 10 and 12.2 km with a rather clean troposphere below. The application of the iterative backward-forward method [36] gives a mean cirrus lidar ratio of 19 sr and a cirrus optical depth of 0.19. The cirrus cloud is quite heterogeneous in time and vertical range during the 60 min. of the measurements, which results in a large variability of the particle depolarization ratio which varies between 0.20 and 0.52, being the mean value 0.39 ± 0.11 . This high value of δ^P is in agreement with former studies such as [41] who found values in the range 0.30-0.45 for cirrus clouds at ~ 9.5 -11.5 km height observed in north-central Oklahoma. Finally to give an idea of the particle depolarization ratio in background conditions in Barcelona, i.e. when the aerosol is from local urban origin and probably mixed with marine particles, a case without long-range transport is selected (Fig. 10e). The ABL is developed up to 1.25 km. δ^P is nearly constant and its mean value is 0.066 ± 0.005 . If we compare this value to the collection of depolarization ratios of [40] measured around the globe for anthropogenic pollution (0.06-0.10) and marine aerosols in different relative humidity conditions (0.01-0.10) we find a good agreement. However, at this point, from the depolarization ratio alone it does not seem possible to distinguish the fractions of anthropogenic pollution and of marine particles.





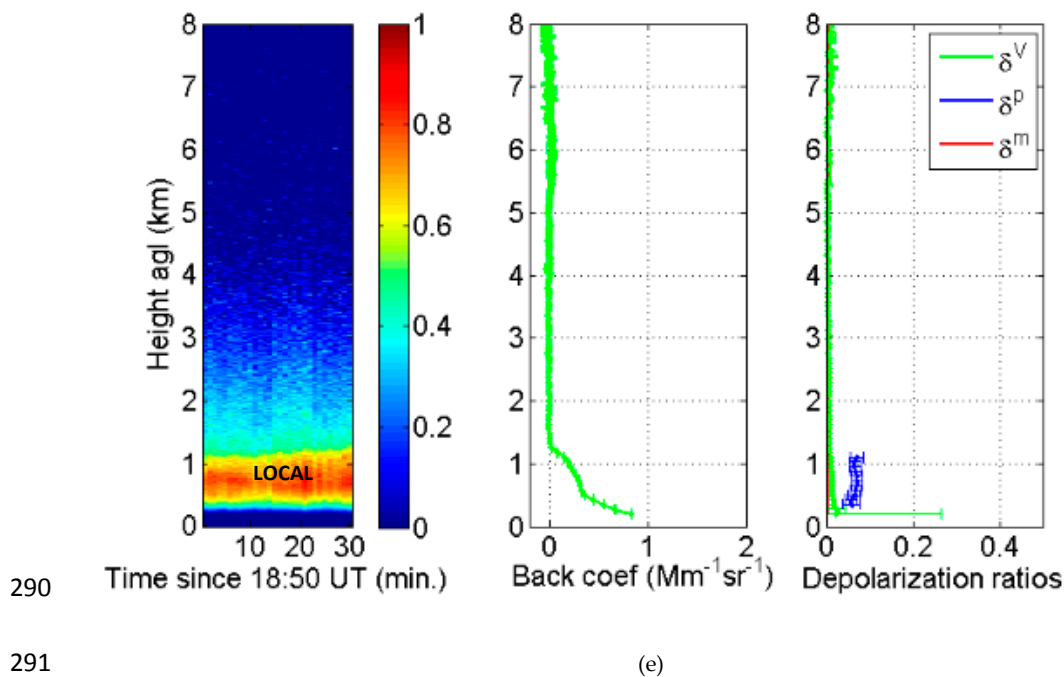


Fig. 10. Some examples of volume and particle depolarization ratio retrievals showing (left) time-height plots of range-square corrected signals in arbitrary units, (center) particle backscatter coefficient at 532 nm, (right) volume and particle depolarization ratios at 532 nm for (a) pollen, (b) dust, (c) dust and fire smoke, (d) cirrus cloud, (e) local urban. The points of the particle depolarization ratio profiles for which the associated error is larger than 50 % are not represented.

6. Conclusions

A new depolarization sensing subsystem has been implemented to a 6-channel elastic/Raman lidar. The architecture is based on a dedicated sub-telescope (a telephoto lens). The theory of operation has been presented, including the calibration procedure. Measurements performed during two Saharan dust intrusion events are used to test the new channel. Particle depolarization ratios varying between 10 and 40 % are found in the dust layers. Comparisons of the volume depolarization with an MPL system show a good agreement between both systems and demonstrate the reliability of the new depolarization channel of the UPC multi-wavelength lidar.

Acknowledgements

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Appendix: error estimation

The error analysis presented in this section is based in the well-known technique of the error propagation. If we have a function y that depends on n uncorrelated variables x_i :

$$y = f(x_1, x_2, \dots, x_n) \quad (11)$$

Which are known with a standard deviation Δx_i

The most reliable value of y can be computed as:

$$\bar{y} = f(\bar{x}_1, \bar{x}_2, \dots, \bar{x}_n) \quad (12)$$

With a standard deviation that can be computed as [43,44]:

$$\Delta y = \sqrt{\sum_{i=1}^n \left(\left. \frac{\partial f}{\partial x_i} \right|_{\bar{x}_i} \right)^2 (\Delta x_i)^2} \quad (13)$$

Where $\left. \frac{\partial f}{\partial x_i} \right|_{\bar{x}_i}$ is the partial derivative of function f with respect to variable x_i , evaluated in the average value \bar{x}_i .

According to this method, the following standard deviations can be obtained for the observable $\delta^*(90^\circ, R)$, defined in equation (7):

$$\Delta \delta^*(90^\circ, R) = \sqrt{\left(\frac{1}{S_{TOT}(R)} \right)^2 (\Delta S_{Dep}(90^\circ, R))^2 + \left(\frac{S_{Dep}(90^\circ, R)}{S_{TOT}(R)^2} \right)^2 (\Delta S_{TOT}(R))^2} \quad (14)$$

Where

$\overline{S_{TOT}(R)}$ is the average value of the signal detected by the total power channel, as a function of range,

$\overline{S_{Dep}(90^\circ, R)}$ is the average value of the signal detected by the depolarization channel (with the polarizer oriented 90° from the transmitted beam polarization,

$\Delta S_{TOT}(R)$ is the standard deviation of the signal detected by the total power channel.

$\Delta S_{Dep}(90^\circ, R)$ is the standard deviation of the signal detected by the depolarization channel.

According to the calibration method, the uncertainty associated to the estimation of the depolarization channel system function is reduced by the signal smoothing that is performed.

According to the different calibrations presented in Fig. 8, an absolute error around $|\Delta V^*(R)| = 1$ will be considered in the computation of the error of the volume depolarization ratio, defined in equation (6):

$$\Delta \delta^V(R) = \sqrt{\left(\frac{V^*(R)}{V^*(R) - \delta^*(90^\circ, R)} \right)^2 (\Delta \delta^*(90^\circ, R))^2 + \left(\frac{\delta^*(90^\circ, R)}{V^*(R) - \delta^*(90^\circ, R)} \right)^2 (V^*(R))^2} \quad (15)$$

The computation of the error of the backscatter ratio, defined in equation (9), considers only the random variations of the retrieved particle backscatter ([30–33]):

$$\Delta \rho(R) = \sqrt{\left(\frac{1}{\beta^m(R)} \right)^2 (\Delta \beta^p(R))^2} \quad (16)$$

Finally, for the computation of the error of the particle depolarization ratio, defined in equation (8), we will simplify the expression by defining:

$$\begin{aligned} Num(R) &= [1 + \delta^m] \cdot \delta^v(R) \cdot \rho(R) - [1 + \delta^v(R)] \cdot \delta^m \\ Den(R) &= [1 + \delta^m] \cdot \rho(R) - [1 + \delta^v(R)] \end{aligned} \quad (17)$$

And then writing:

$$\begin{aligned} \Delta \delta^p(R)^2 &= \left(\frac{[1 + \delta^m] \cdot \rho(R) - \delta^m}{(Den(R))^2} \cdot Den(R) + Num(R) \right)^2 \cdot (\Delta \delta^v(R))^2 + \\ &+ \left(\frac{(1 + \delta^m) \cdot \delta^v(R) \cdot Den(R) - (1 + \delta^m) \cdot Num(R)}{(Den(R))^2} \right)^2 \cdot (\Delta \rho(R))^2 \end{aligned} \quad (18)$$

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