

## Set-up method on properties of $\text{Ba}_x\text{Sr}_{1-x}\text{TiO}_3$ thin films deposited by RF-magnetron co-sputtering by projecting temperature and stoichiometric effect

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### Abstract

Thin films (100–400 nm) of  $\text{Ba}_x\text{Sr}_{1-x}\text{TiO}_3$  ( $0 \leq x \leq 1$ ) deposited in RF-magnetron co-sputtering equipment are presented in this research work. The change of deposition rate, gap energy, and resistivity as a function of temperature- applied power change in the growth parameters was studied through the ISO colour-code lines constructed with MATLAB:

By analysing the trend information and take into account the influence of the calculated "x" parameter with the Boltzmann profile fitting is proposed a method to allow a controlled set up of the RF-magnetron co-sputtering system and predict the  $E_g$  and resistivity values in the  $\text{Ba}_x\text{Sr}_{1-x}\text{TiO}_3$  solid solution with  $0 \leq x \leq 1$  for amorphous and crystalline phases. Also, a versatile tool to optimise the deposition process and material properties.

**keywords:**  $\text{Ba}_x\text{Sr}_{1-x}\text{TiO}_3$  films; boltzmann modelling; optical band gap; deposition rate; stoichiometric content

## 1. Introduction

The solid solution  $\text{Ba}_x\text{Sr}_{1-x}\text{TiO}_3$  (BST), is a ceramic material with perovskite structure, whose technological applications are extensive in the elaboration of optical devices, resistive memories, solar cells, sensors, etc. [1,2,3]. The deposition rate (DR) and the stoichiometric parameter "x" are influenced by geometric deposition system, the gas pressure and the power applied to each of the magnetrons. From the geometry, the DR follows an exponential growth profile, and the parameter "x" follows a sigmoid profile when the target distance decreases while keeping the gas pressure and the temperature of the reservoir constant. The effects of the stoichiometry defined by the value of the parameters x and 1-x. In the BST chemical formula have been investigated in some physical properties such as resistive switching [5,6], resistivity (RST) in crystalline and amorphous phases [7,8,9], the thickness [10], the gap energy ( $E_g$ ) [11,12,13]. The  $E_g$  as a function of temperature and its effect on the improvement of crystallinity [14,15] and the amorphous to crystalline phase change [16,17,18].

Based on the literature review, the combined effect of the parameter "x" with values of  $0 \leq x \leq 1$  in applied power and temperature ranges to predict DR values,  $E_g$  and RST, has not been investigated; only DR and RST as a function of the power applied, for different deposition pressures in thin films of molybdenum by means of RF-sputtering [19].

In this manuscript the Boltzmann profile fits (BP) of the experimental data of parameter "x" were calculated using: a) %atomic measured by BST/Nicromel EDS at 495 °C ( $\text{BP}_{\text{EDS}}$ ) [6], b) method of normalization and transformation of the positions of the BST/Quartz diffraction peaks at 549 °C ( $\text{BP}_{\text{DRX}}$ ) [10].

Total applied power on targets of  $\text{BaTiO}_3$  and  $\text{SrTiO}_3$  for every discrete experimental point is applied power ratio  $P_{\text{Ba}}/P_{\text{Sr}}$  (APR). The "y" axis on ISO colour-code lines (ISO lines: ISO-DR, ISO- $E_g$ , ISO-RST) represent the next APR: 0/120 W, 15/105 W, 30/90 W, 45/75 W, 60/60 W, 75/45 W, 90 / 30 W, 105/15 W and 120/0 W, however, for simplicity only the applied power values on  $\text{BaTiO}_3$  target are shown.

## 2. Experimental details

BST films were prepared by RF-magnetron co-sputtering in a system equipped with two magnetrons working simultaneously by different power totalling a total of 120 watts:  $\text{BaTiO}_3$  (99.95%, SCI Engineered Materials Inc) and  $\text{SrTiO}_3$  (99.9%, SCI Engineered Materials Inc.). Targets were 2" diameter and 0.125" thick. Before solid film deposition, the sputtering chamber was evacuated to a base pressure around  $1.2 \times 10^{-3}$  Pa; then, an Ar flushing was done filling the chamber to a pressure of 3.9 Pa during 10 minutes. For the film substantial deposition, an  $\text{Ar}^+/\text{O}_2$  gas mixture was introduced into the chamber with an  $\text{Ar}/\text{O}_2=90/10$  ratio at an initial pressure of 6.6 Pa to ignite the plasma and perform a target pre-sputtering during 15 minutes. After that, the working pressure was set at 3.9 Pa

to carry out the deposition. Quartz substrates  $1 \times 1.5 \text{ cm}^2$  were successively rinsed with trichloroethylene, acetone, and ethanol before depositing. A stainless-steel substrate holder was fixed at a distance of 8 cm from the magnetron in off-axis configuration. The substrate holder was rotated at 100 rpm for ensuring film uniformity, and the substrate temperature was set at room temperature (as-deposited),  $375^\circ\text{C}$ ,  $435^\circ\text{C}$ ,  $495^\circ\text{C}$  and  $549^\circ\text{C}$ . The total RF-magnetron applied power was 120 W, distributed between the two magnetrons as shown in Table 1, to produce  $\text{Ba}_x\text{Sr}_{1-x}\text{TiO}_3$  films with different stoichiometric *compositions*. The sputter time for all of the samples was 68 minutes. Chemical composition was obtained by energy dispersive X-ray spectroscopy (EDS) employing a Jeol JSM-5300 electron microscope equipped with a Kevex Delta 1 spectrometer. The optical transmission spectra of the films were obtained in a Perkin-Elmer, Lambda 40 Spectrophotometer in the range of 250 to 800 nm. Film thicknesses were calculated from the transmittance spectra using the SCOUT software. The X-ray diffractograms were acquired in a Phillips X'Pert diffractometer using  $\text{CuK}\alpha=1.54060 \text{ \AA}$ .

Temperatures As-deposited, $375^\circ\text{C}$ , $435^\circ\text{C}$ , $495^\circ\text{C}$ , $549^\circ\text{C}$	RF-Magnetron applied power (W)		Total applied power
Sample	BaTiO <sub>3</sub>	SrTiO <sub>3</sub>	
B0S120	0	120	120
B15S105	15	105	120
B30S90	30	90	120
B45S75	45	75	120
B60S60	60	60	120
B75S45	75	55	120
B90S30	90	30	120
B105S15	105	15	120
B120S0	120	0	120

**Table 1.** RF- applied power to BaTiO<sub>3</sub> and SrTiO<sub>3</sub> targets and deposition temperatures for each sample.

### 3. Results and discussion

Figure 1 shows the experimental discrete points values of the parameter "x" and "1-x", and the solid lines represent the setting of the BP for each storage temperature. The difference among all of the BP can be explained because of BST/Quartz deposition, there are areas rich in Ba (Ba-rich) and rich in Sr (Sr-rich) due to the substrate effect and plasma geometry into RF-sputtering deposition system,

causing a differentiated distribution in the substrate; see figure 4 in [20]. For example, in  $\text{Ba}_{0.4}\text{Sr}_{0.6}\text{TiO}_3$  ( $\text{Ba}/\text{Sr} = 2/3$ ) and  $\text{Ba}_{0.5}\text{Sr}_{0.5}\text{TiO}_3$  ( $\text{Ba}/\text{Sr} = 1$ ) thin films deposited by direct current arc discharge plasma process in the Sr-rich zone, the original Ba/Sr ratio decreases to approximately 1/3 and 2/3 respectively [21].

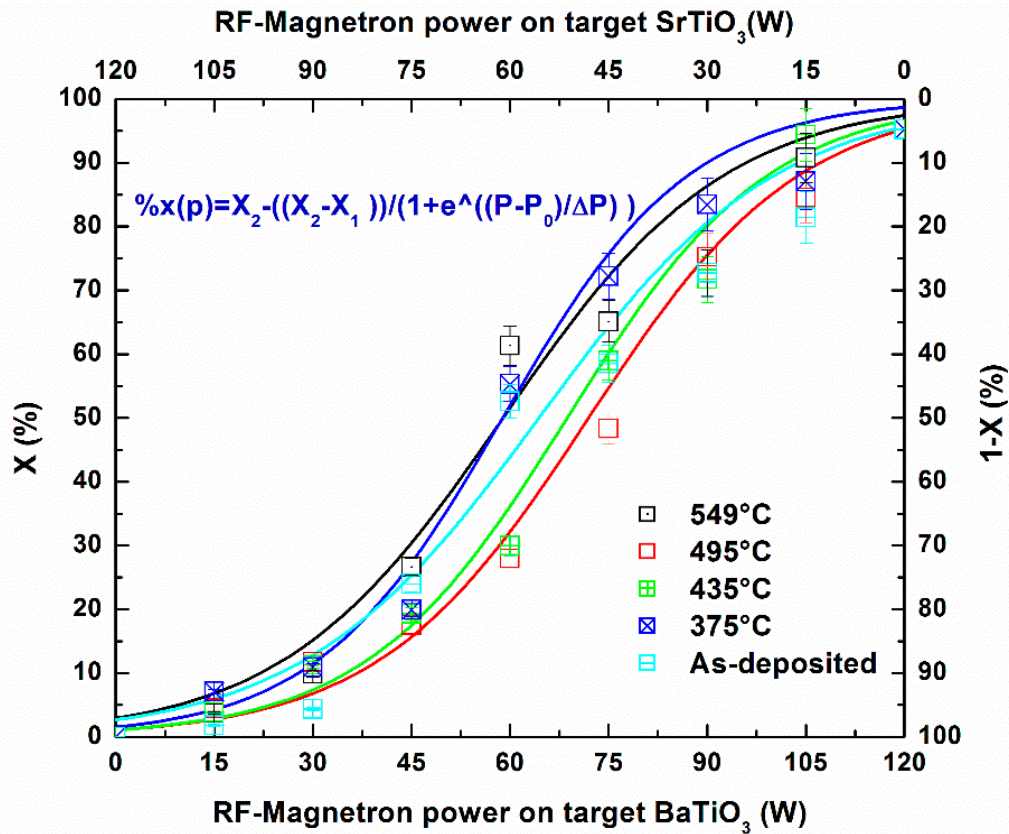


Figure 1. Boltzmann profile of the parameter "x" obtained by EDS and power dependent on the different in-situ deposition temperatures.



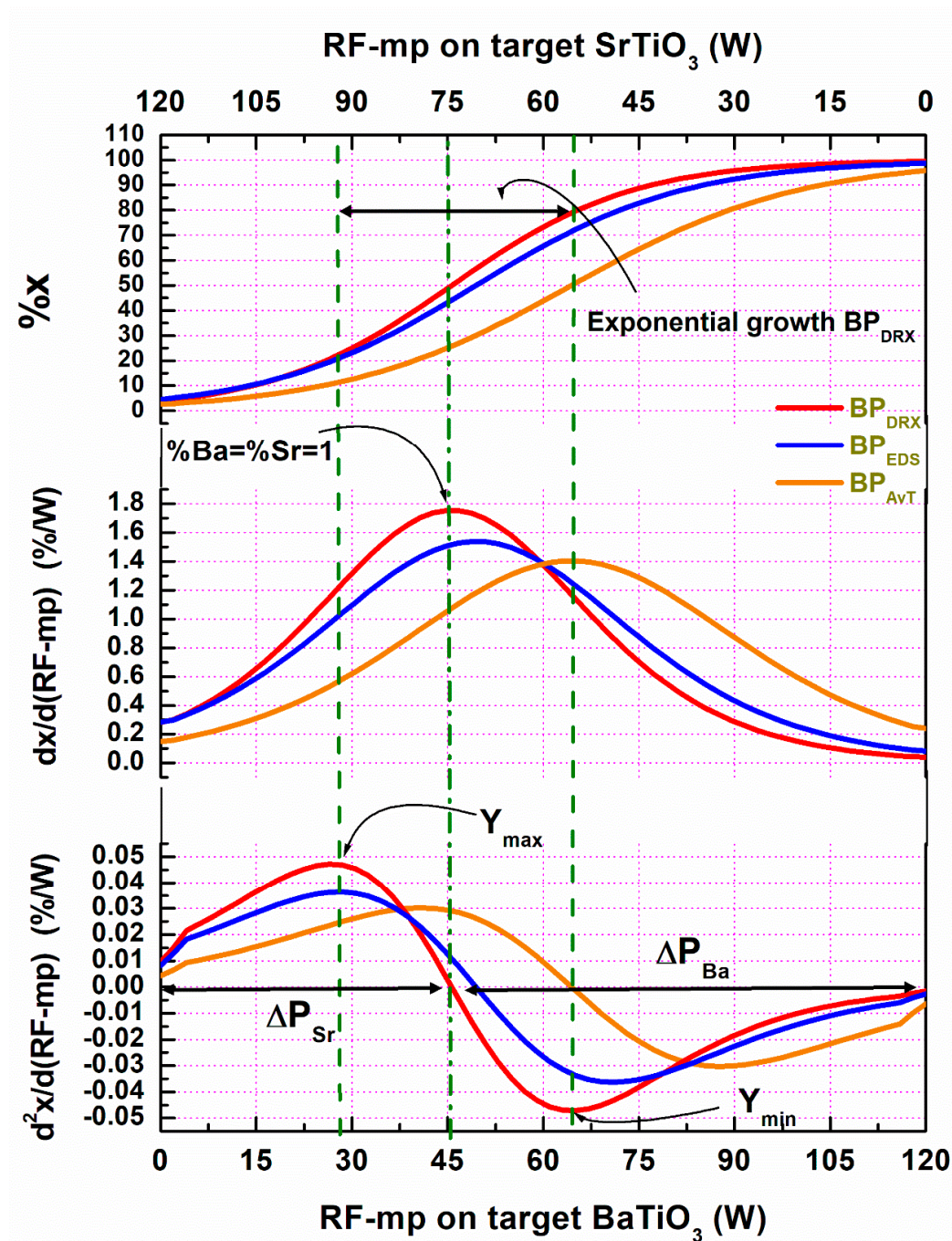


Figure 2. (a)  $\text{BP}_{\text{DRX}}$ ,  $\text{BP}_{\text{EDS}}$ ,  $\text{BP}_{\text{AvT}}$ , (b) first derivative 2a., (c) second derivative fig. 2a.

Figure 2 (a) shows fit:  $\text{BP}_{\text{DRX}}$ ,  $\text{BP}_{\text{EDS}}$  and  $\text{BP}_{\text{AvT}}$  this last one obtained from the experimental values, averaging the fit of parameter "x" from temperatures: as-deposited, 375, 435, 495 and 549 °C. Comparing  $\text{BP}_{\text{EDS}}$  and  $\text{BP}_{\text{AvT}}$ , the effect of the substrate on the Ba/Sr ratio is evident. The

characterization method to calculate the parameter "x" and the storage temperature between  $BP_{DRX}$  and  $BP_{EDS}$  are different. The area under the curve  $BP_{DRX} \approx 3/2$ .

Therefore, it is defined that the applied power intervals with higher content of Sr and Ba in ISO lines are: 0-45 W and 45-120 W, respectively

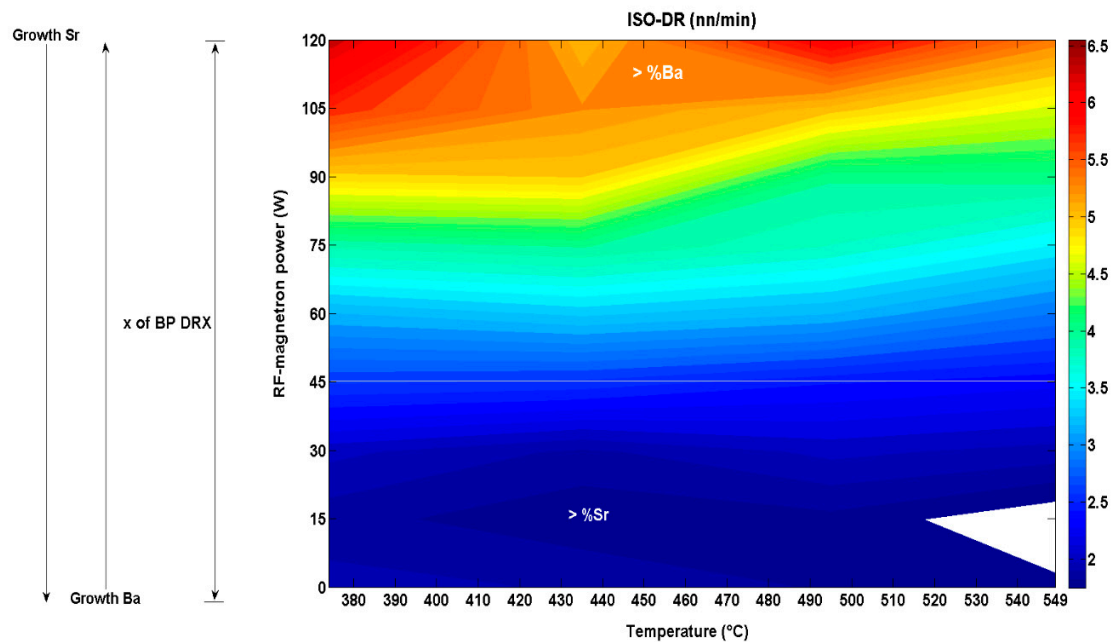
However, the fit values are very close; assuming that thickness between substrate and the film has no decisive influence on the Ba/Sr ratio [13], and that  $BP_{DRX}$  is more accurate (for the  $R^2$  fit value and for measuring the substitution of Ba into BST in a more significant volume than the  $BP_{EDS}$ ). The  $BP_{DRX}$  is used to obtain x parameter vs APR and calculates the associated value of DR,  $E_g$  and RST into ISO colour-code lines corresponding to Figures 3a, 4a and 6a respectively. The maximum and minimum values of DR,  $E_g$ , and RST are obtained from the intersection of APR, and temperature ranges (375-435 °C), (435-495 °C) and (495-549 °C) and this are shown in Table 2.

Figure 2b the maximum peak of  $BP_{DRX}$  derivative, the applied power equilibrium ratio to obtain Ba/Sr = 50%/50% is reaching with  $PAR \approx 45/75$  or  $5/3$ .

Highest content zone >%Sr <sup>2+</sup> (APR=0-45 W) >%Ba <sup>2+</sup> (APR=45-120 W)		Temperature ranges (°C)					
		375-435		435-495		495-549	
		Max	min	Max	Min	Max	min
Deposition rate (nm/min)	(Sr)	2.53	1.84	2.63	1.84	2.43	1.74
	(Ba)	6.45	2.82	6.25	2.63	5.57	2.43
$E_g$ (eV)	(Sr)	4.52	3.94	4.51	3.82	3.91	3.80
	(Ba)	4.52	3.89	4.49	3.82	4.39	3.79
RST $\rho$ ( $\Omega \cdot \text{cm}$ )	(Sr)	0.03	0.03	0.84	0.03	1	0.09
	(Ba)	0.57	0.03	0.84	0.03	0.84	0.06

**Table 2. Analysis of RD,  $E_g$  and RST maximum and minimum values, replicated with ISO-colour coded lines in APR and temperature intersection**

Figure 2c (second derivative of  $BP_{DRX}$ ) represents the stoichiometric difference related to  $\Delta(\text{Sr-Ba})/\Delta(P_2-P_1)$  gradient. The positive gradient corresponds to the zone with Sr excess ( $\Delta P_{Sr} \approx 45-0 \approx 45$ ) and the negative gradient to the zone with Ba excess ( $\Delta P_{Ba} \approx 120-45 \approx 75$ ). The area under the curve ( $\Delta P_{Sr}$ ,  $y_{\max}$ ), defines the magnitude of Sr excess that reaches a maximum peak and decreases until  $\Delta(\text{Sr-Ba}) = 0$ . Similarly, the negative gradient with an area under the curve ( $\Delta P_{Ba}$ ,  $y_{\min}$ ) is interpreted. The BP second derivative helps to understand the joint operation of the two magnetrons and deposit stages where Ba has a higher sputtering yield than that of Sr due to its higher ionic radius.



**Figure 3a. ISO-DR lines with APR of 0-120 (W) and temperature range 375-549 °C.**

Figure 3a represents DR projection values (dimensioned in the right column) by ISO colour-coded lines for APR and temperature ranges indicating that DR decrease when the temperature range and Sr content increase, particularly notorious when APR=45-120 W and temperature 435-549 °C zones. The highest DR values APR=105-120 W and <375 °C ranges. The temperature range of 375-460 °C shows an instability region by the transition from amorphous to the crystalline phase. The maximum and minimum values confirm this trend, see Table 2.

When the deposition temperature increases the DR profile decreases, this behaviour can be explained by ideal gases law ( $PV = nRT$ ), where "n" is ionised argon atoms number, when deposition temperature increase the working pressure too, to keep it constant, the system decreases the reactive gas flow [20].

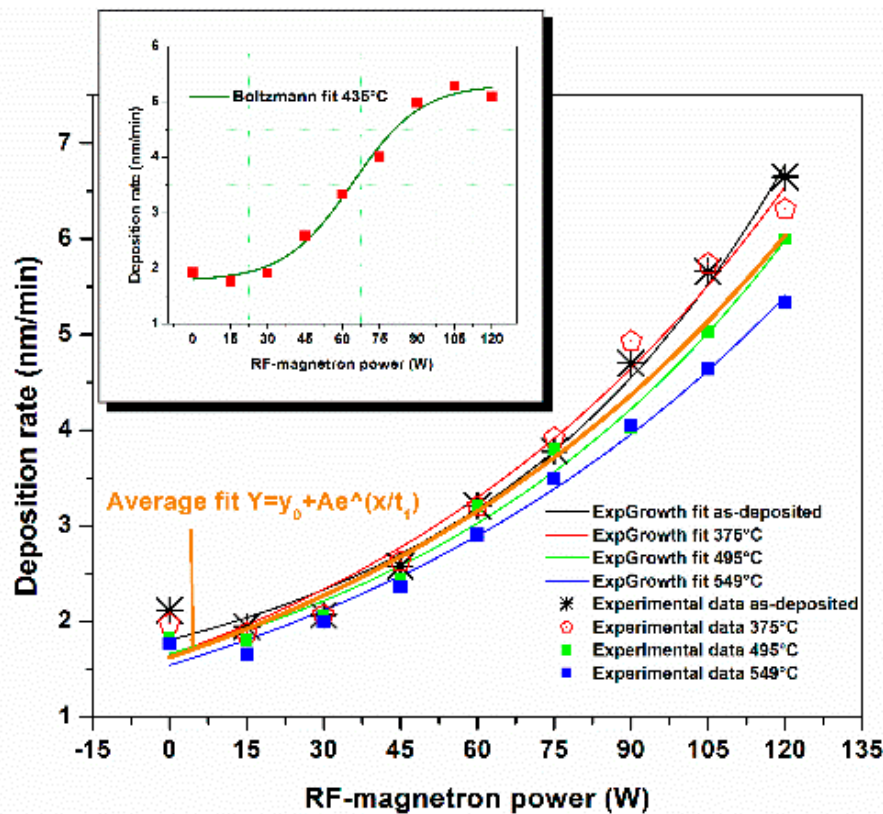


Figure 3b. DR for each temperature and fit with EG for as-deposited temperatures, 375 ° C, 495 ° C, 549 ° C, and average fit, the inset shows the ratio of deposit and the fit with the BP for the temperature of 435 °C.

Figure 3b shows DR for each temperature and fit with  $E_g$  for temperatures: as-deposited, 375, 495, 549 °C, whose equation is defined as:

$$Y = DR_0 + Ae^{P/t_1}$$

Where:  $DR_0$  is the deposition rate,  $A$  and  $t_1$  are constants and  $P$  are applied power.

In the average DR fit (discrete experimental data) the deposition ratio  $Ba/Sr \approx 3/1$  corresponding to maximum and minimum points respectively.

The inset in figure 3b shows DR vs BP fit for 435°C. This behaviour can be explained due to target erosion rate (TER) may vary when the reactive gas supply is kept constant [20]. As will be seen, this temperature is critical in the transition from the amorphous to the crystalline phase.



Figure 4a represents  $E_g$  values projection (dimensioned in the right column) using ISO colour-coded lines for APR and temperature ranges. The maximum and minimum values obtained from ISO lines for  $E_g$  indicate a downward trend when temperature and Ba content increase (see Table 2), however, there is a transition zone with the highest  $E_g$  values in the power range 45-60 W and temperature 375-495 °C, because of these zones are transitions between the amorphous and crystalline phases, as shown in figure 4b and confirmed by XDR, in addition, the value of  $E_g$  can be affected by stoichiometric ratio Sr-rich and/or Ba-rich of the area where the transmission spectrum is taken.

The trend when "x" increases is according to [11,12,13, 22]. Comparing  $E_g$  between 375-495 °C and 45-75 W ranges, when the temperature increases the  $E_g$  too, this behaviour can be attributed to Ba content and the amorphous phase.

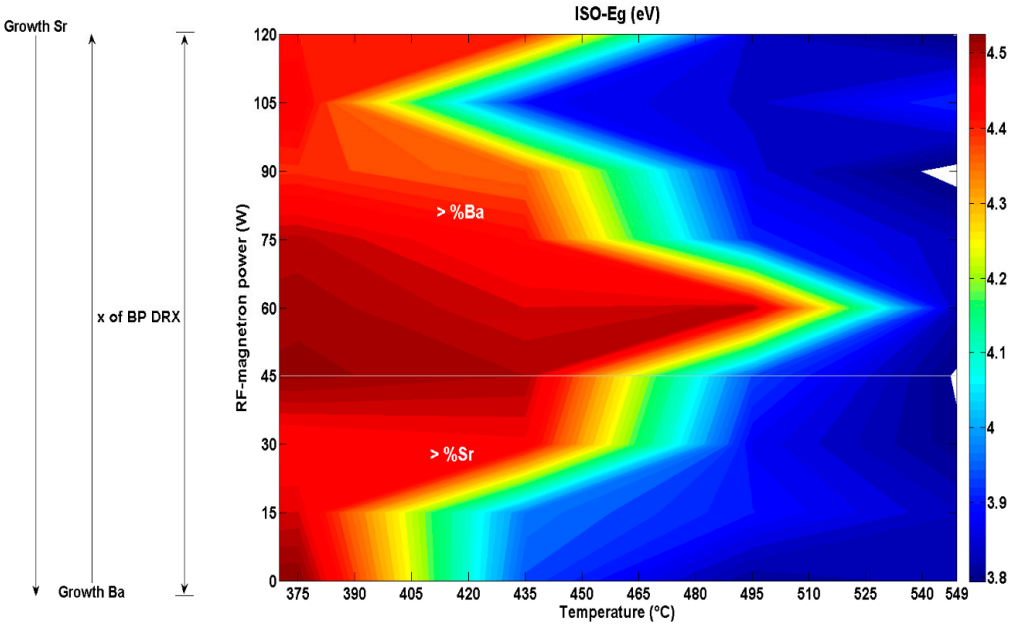


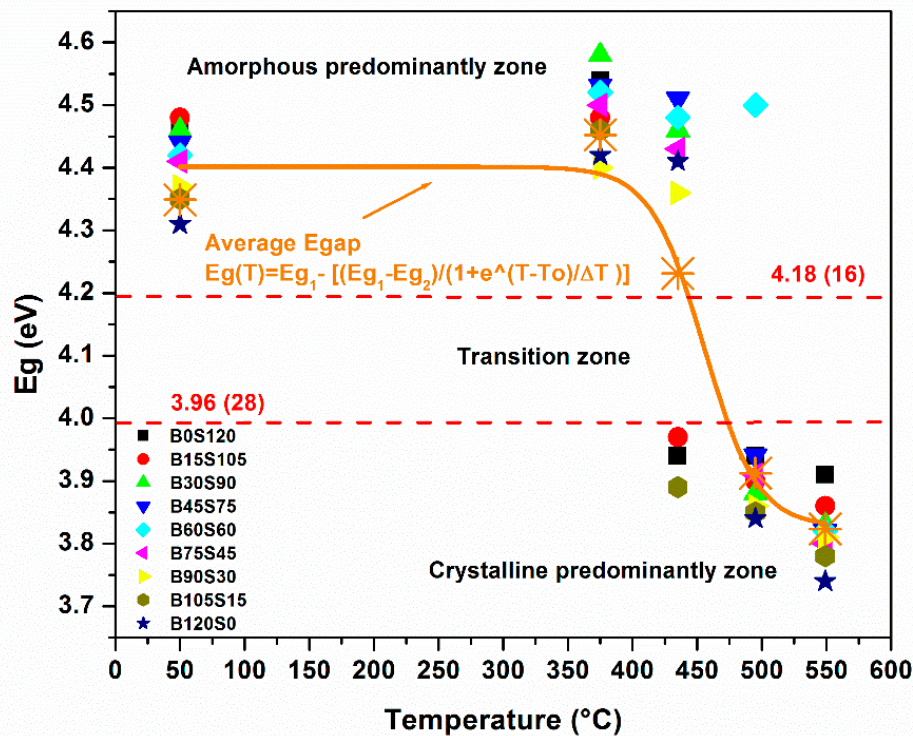
Figure 4a. ISO- $E_g$  lines with APR of 0-120 (W) and temperature range of 370-549 °C.

Table 3 shows the applied power-temperature relationships related to the parameter "x" where the ISO- $E_g$  lines (obtained into figure 4a values) replicate the  $E_g$  values and the "x" parameter of the bibliographic references [R] for amorphous and crystalline phases.

Amorphous phase		T (°C)	APR (W)	[R]	Crystalline phase		T (°C)	APR (W)	[R]
%x	E <sub>g</sub> (eV)				%x	E <sub>g</sub> (eV)			
80	4.18	495	65/55	[16]	80	3.8	>535	65/55	[16]
70	4.27	495	55/65	[25]	75	3.88-3.83	>535	60/60	[15]
70	4.58	<375	55/65	[17]	70	3.94	>535	55/65	[17]
65	4.39	475	52/68	[27]	50	3.96	495	45/75	[28]
50	4.2	465	45/75	[18]	60	3.81	549	50/70	[11]
50	4.75	<375	45/75	[14]	100	3.75	>549	120/0	[11]
					0	3.88	495	0/120	[11]

**Table 3 Analysis to replicate E<sub>g</sub> and parameter "x" values as a function of APR and temperature rate**

Figure 4b shows E<sub>g</sub> values for all samples (B0S120 to B120S0) and temperatures: as-deposited (50°C as reference), 375, 435, 495, and 549°C. The broken red lines represent the lowest and highest E<sub>g</sub> values of the BST referenced in the literature and define the transition zone between the amorphous and crystalline phases. The solid line is the BP fit of the E<sub>g</sub> average at each temperature. From the experimental data, E<sub>g</sub> decreases when the temperature increases according to [14,15,17]. The results of XDR confirm that some samples of the temperatures 375, 435, 495, 549 °C have different crystallinity degrees and suggest the presence of both crystalline and amorphous phases, in addition to improvement in crystallinity with the increase of the temperature. The difference in amorphous and crystalline E<sub>g</sub> values suggests that there may be band bending in the amorphous phase and decreasing with increasing temperature or crystallinity. The reduction in the E<sub>g</sub> with increasing crystallinity indicates that the separation between the levels of the oxygen and titanium ions are influenced by a long-range order and crystal size. The role of electron-phonon interaction may be determinant in the optical properties of BST [17].



**Figure 4b.  $E_g$  values, B0S120-B120S0 samples as a function of temperature, as-deposited samples have been plotted at 50 °C as the reference temperature.**

Another possible reason for larger values of  $E_g$  in the amorphous phase is the existence of the density of states as explained by Davis and Mott [18]. The  $E_g$  values of this research work and the bibliography of Table 3 were found above some reported [22,23,24].

The authors explain these differences due to: a) the change in crystal structure [11], b) phase change [15], c) the increase in interatomic space due to excess volume and absence of long-range order in the lattice, in addition to the Burstein-Moss effect due to oxygen vacancies [14] d) the change in size of the microstructure [16], e) the presence of amorphous material and the effect of quantum size [25,26,28].

For the temperature of 549 °C, the XDR spectrum (not shown here) defines a polycrystalline film with cubic, tetragonal and orthorhombic phases. [13]. These results suggest that the crystalline structure through a transition state to achieve stability and that  $E_g$  values can decrease with higher deposit temperatures.

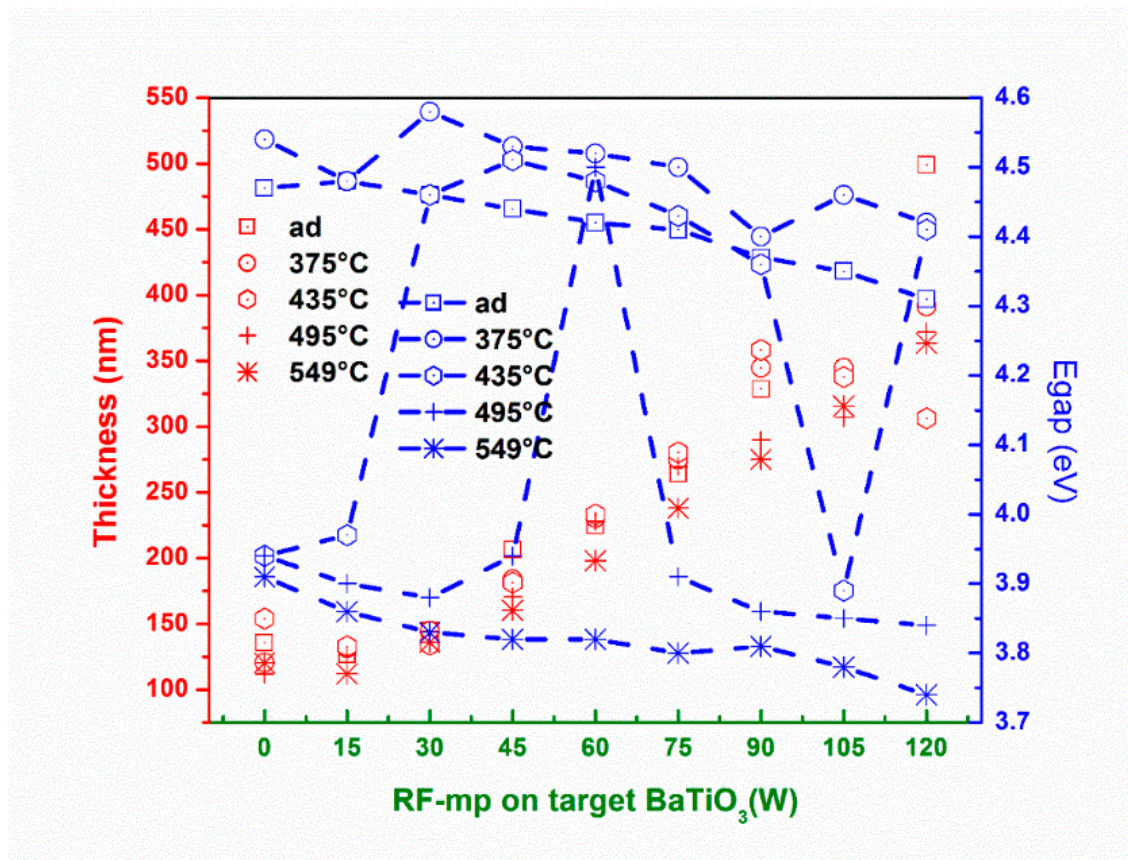
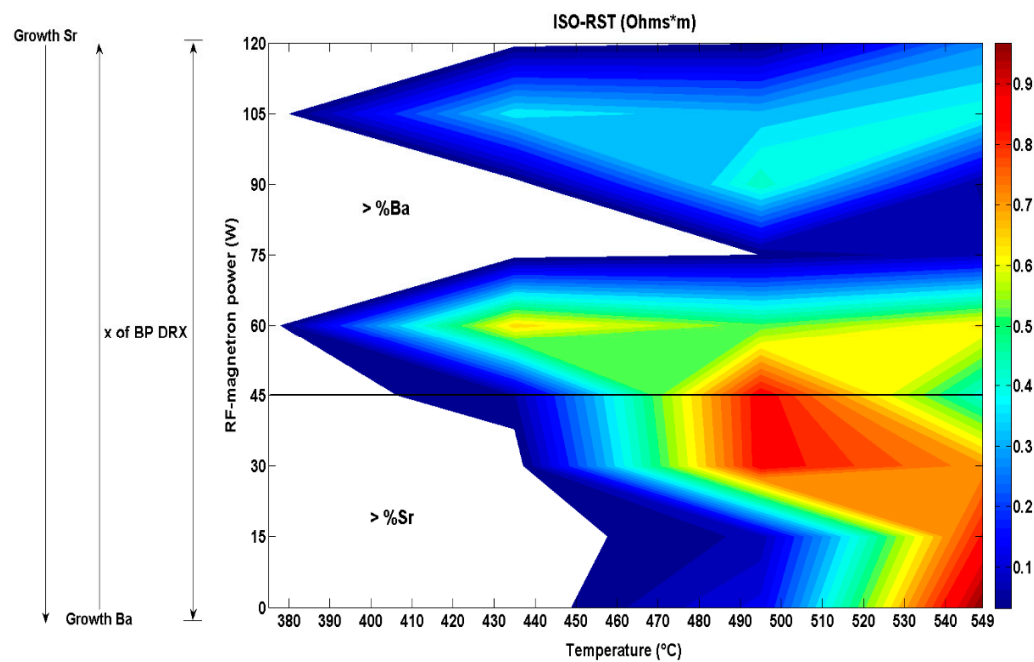


Figure 5. Thickness and  $E_g$  as a function of RF-mp.

In figure 5 comparing the  $E_g$  values (samples B0S120-B120S0, except B60S60) from the temperatures 495°C and 549°C, and taking into account the trends of the ISO lines DR, we can observe that the effect of film thickness has a slight effect on the  $E_g$  [12].

Figure 6a represents RST values projection (dimensioned in the right column) using ISO colour-code lines for APR and temperature ranges, the maximum and minimum values of RST are obtained (see table 2), which show a tendency to higher values of RST when the temperature and Sr content increase [14], particularly in the applied power zone 0-45 W and temperature 495-549 °C. White applied power and temperature ranges would indicate conductivity and the necessity of more samples to achieve complete the ISO-RST lines. Other authors report only lower resistivity with Sr increase [15,20].





**Figure 6a. ISO-RST lines with APR of 0-120 (W) and temperature range 375-549 °C.**

Figure 6b shows RST values for all of the samples (B0S120 to B120S0) and, temperatures. The drawn profile of the S-shaped average RST, similar to BP, has been reported for compositions of “x” from 10 to 70 percent and temperatures from -150 to 150 °C [7]. The down-values of RST for all compositions by the effect of the temperature from as-deposited up to 375 °C coincides with the change from amorphous to a crystalline phase, and it is evident that at 375 °C there is a much more marked transition into phases.



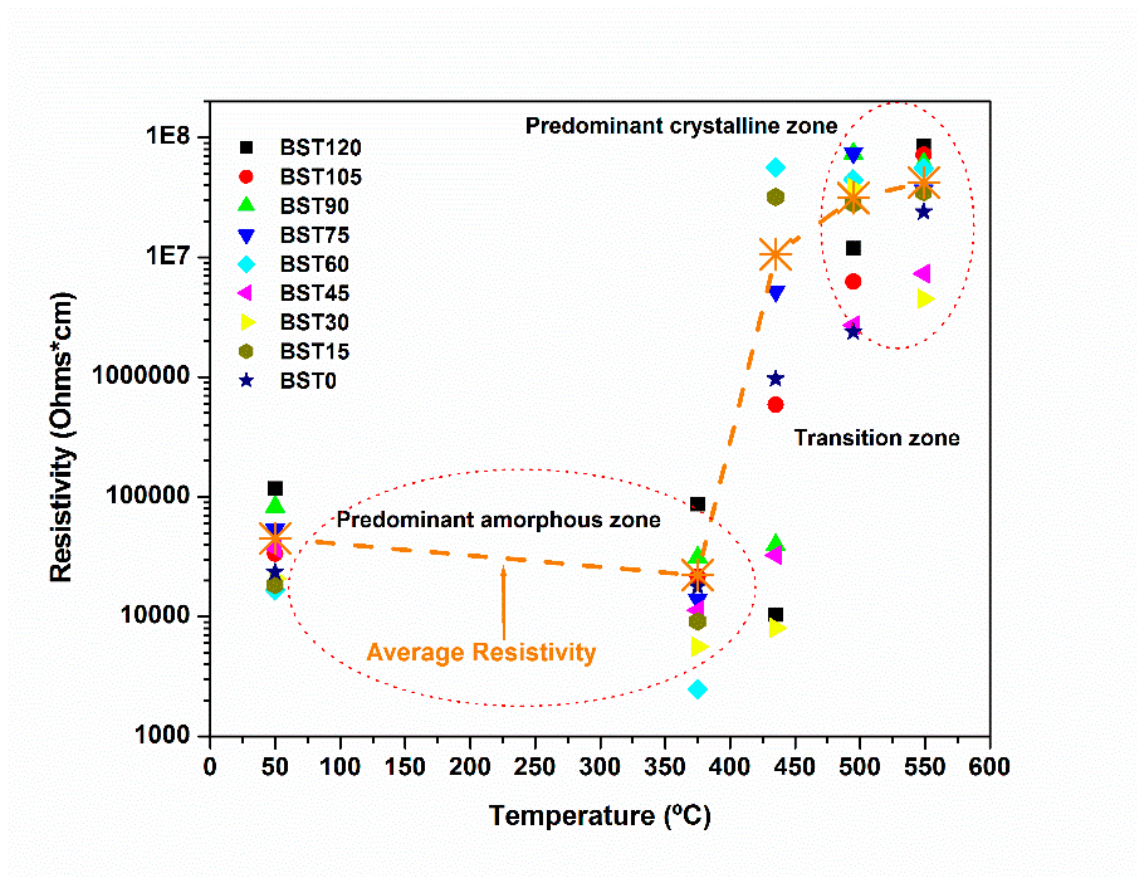


Figure 6b. RST values, samples of B0S120-B120S0 as a function of temperature, as-deposited samples have been plotted at 50 °C as the reference temperature.

#### 4. Conclusions

The DR,  $E_g$  and RST analysis of the combined effect of applied power control parameters, in situ temperature and stoichiometric content, for thin films deposited by RF-co-sputtering allows a correct interpretation of the system and can make much more accurate the experimentation and control of material properties. This methodology can be applied when control parameters such as the work pressure and the Ar/O<sub>2</sub> ratio are variable. BP is present in the system as follows: "x" vs P for amorphous and crystalline phases,  $E_g$  vs T (°C) transition between amorphous and crystalline phase,  $E_g$  vs "x" for crystalline phase. The "S" shape of RST vs T (°C) can be analyzed in limits containing the BP for the transition from amorphous to the crystalline phase.

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