1 Article.

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Operational monitoring and balance the 3 mass in biodegradation of oil for two scenarios: Experimental Plant of 4 Active Sludge and Aerobic Digestor 5

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17 Abstract: Fats and oils are the most common contaminants in wastewater and are usually discarded 18 through physical processes. This paper studies its elimination through an environmentally friendly 19 biological treatment, yielding good results on both laboratory scale and in the field. In this study a 20 comparative evaluation of the biodegradation of fats and oils in two scenarios were developed in 21 an activated sludge plant at laboratory scale, and a wastewater treatment plant. The full-scale values 22 for some key parameters are compared, such as the oil concentration in the influent and effluent, 23 mass loading and removal efficiency and biodegradation systems. Activated sludge plant at 24 laboratory scale working on a mass load range from 0.2 to 0.8 (kg COD / day / kg MLSS) initially 25 reaches levels of 75% biodegradation thereafter influent concentration is increased and thereby the 26 mass load is increased in a range of working system under high load and biodegradation rates 27 ranging from 71 to 64% are achieved. The actual system consists of a treatment plant wastewater 28 with an aerobic digester for sludge treatment. Fats and oils are retained in a previous degreaser to 29 biological treatment and subsequently sent to the aerobic sludge digester, constituting of thus on a 30 single substrate, resembling an activated sludge plant with extended aeration mode, and levels of 31 biodegradation in the range of 69 to 92%. From this work, we can say that the choice of biological 32 treatment for fats and oils is feasible and adequate. Furthermore, the biomass presents great 33 adaptability to the oil substrate, favored in this case for being the only source of carbon, therefore 34 fats and oils should be removed using biological treatment, instead of the flotation procedure or at 35 most using it as an intermediate process.

- 36
 - Keywords: Biodegradation; fats and oils; activated sludge.
- 37

38 1. Introduction

39 The following work will study the elimination and behavior of fats and oils using a biological 40 treatment with active sludge in two structurally and different magnitude scenarios: on a laboratory 41 scale and a real scale.. We make a comparative analysis between the field scale, where fats and oils 42 are eliminated in the sludge digester, very similar to an extended aeration regime, and on the

- 43 laboratory-scale experience, where sunflower oil is the only source of carbon. In both cases, a 44 triacylglyceride is eliminated through the biological route which is a better environmentally
- 45 alternative to the commonly recurrent option of flotation.
- 46

Table 1. Conditions of design and systems operation

Parameter	Real situation sludge digester [1].	Laboratory scale aeration tank active sludge			
Single substrate	Fats and oils	Sunflowers oil			
Mass loading	0.08-0.42	0.15-1.0			
Structure	SBR	Conventional-continuous			
Concentration range of affluent Fats and Oil	1000-2500	333-460			
SSLM	8.8-14	302-4.8			
% Fats and oils biodegradation	69-95	64-71			
Volume (m ³)	5128	0.01			
Affluent flow (m ³ /day)	1000	0.024			
Generally, residual water treatment plants eliminate fats and oils by flotation. In this case the					

48 biological pathway to eliminate fats and oils is an environmentally appropriate option with excellent

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49 field results.

50 Fats and oils are a very important component in domestic and industrial wastewater. The 51 amount of lipids in municipal wastewater is in the order of 30% to $40\\%$ of the organic matter 52 measured as chemical oxygen demand [2]. The displacement of oils and fats has been based on its 53 lower density with respect to water, between 920-964 g / l, which allows its flotation [3]. That is the 54 reason why the Residual Water Treatment Plants eliminates fats and oils through flotation. Until now 55 the fats and oils have always been separated from the influent that contain them, through physical 56 processes, in order to prevent them from reaching the stage of biological treatment. Flotation is used 57 in the separation of immiscible or solid fluids and the use of flotation is an increasing methodology 58 in wastewater treatment. Flotation may be done by air at atmospheric pressure, by air dissolved 59 under pressure or by induced air. The difference lies in the way of introducing air into the sewage 60 [4].

61 Therefore, biological treatment must be considered for water mixed with oils and fats contents 62 in order to reduce the fatty residues that will potentially be disposed. Such methodology has 63 considerable advantages from an environmental point of view. Fats and oils are classified as slowly 64 biodegradable substances. Cells initially store these substances in their cytoplasm and then they use 65 hydrolytic enzymes to convert fats and oils into an assimilable and biodegradable substrate [5].

The biological pathway to treat wastewater mixed with fats and oils, on a real scale and on a laboratory scale is compared. At the laboratory-scale experiment, the removal of sunflower oil in wastewater is studied through an active sludge treatment system. The assay experimented with sunflower oil which is of easy access and a standardized product in Chile and for that reason is commonly used for domestic consumption. The chemical composition of sunflower oil is shown in table 2.

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Table 2. Fatty acids of the sunflower oil and analysis specific stereo [6]. Results are given in %

moles.

Fats	Position	16:0	18	18:1 (9)	18:2 (9.12)	18:3 (9.12.15)
Sunflower oil	1	10.6	3.3	16.6	69.5	
	2	1.3	1.1	21.5	76	
	3	9.7	9.2	27.6	53.5	

The wastewater treatment plant utilized in this work is located in Los Angeles city, Chile. This treatment plant treats the oils and fats in an aerobic digester along with the sludge obtained from the

⁷⁶ biological treatment, then the fats and oils are retained by a degreaser and sent to the aerobic digester.

The biodegradation of organic matter in an active sludge system is enhanced by the cultivation and development of a dispersed bacterial biomass in form of flocs. Those are called active sludge dispersed in an aerated and agitated pond which is continuously fed by sewage with organic matter or sludge. The stirring of the tank aims to homogenize the mixture constituted by the bacterial biomass and the residual water avoiding sediments and zones of short distance circuit. Aeration is carried out to supply oxygen to the purifying bacteria, since its metabolism requires to carry out biological degradation of organic matter or sludge [7].

84 Parameters Design and operation of an active sludge treatment system: 85 - Mass loading (ML): It is called the aeration tank mass loading (ML) in relationship between the daily 86 feed mass of biodegradable organic matter entering the aeration tank and the degrading biomass 87 contained therein [8].

88

The behaviors of lipids elimination in biological treatment systems have been exhaustively
evaluated. The literature shows that lipids eliminated by biological treatment, also inhibit microbial
growth, and are the cause of foaming, filamentous bacteria and floc flocculation [9].

In an active sludge biological treatment system, the efficient contact of the microorganisms present in the aqueous phase and oil is fundamental. It requires a considerable interfacial area, this can be extended by delivering energy to the system, either by mechanical agitation or by electric fields. The increase of the interfacial surface between the aqueous phase and the oily or greasy phase is often implemented by mechanical agitation [10].

97 There are two important factors that determine an extension of the level of emulsivity in the full-98 mix stirred aeration tank and the corresponding dispersion level. The influencing factors are the 99 bubble size distribution and the dispersed phase fraction. The average bubble size is between 150 μm 100 and 250 μm [11], this is achieved with a suitable impeller and fine bubble diffusers.

101A suitable enzymatic concentration and optimum interfacial area, must be obtained between the102aqueous phase and the oily phase, in order to solve the mass transfer and the hydrolysis step. [12].103For the estimation of biodegradability the oil entering the aeration tank in the laboratory104experience and the fats and oils entering to the aerobic digester of the treatment plant are considered105as the basis of the calculation, both cases corresponding to a treatment process Active sludge. In this106work, a comparative analysis is performed on the levels of biodegradation of oils and greases107achieved both in the treatment plant on a real scale and on a laboratory scale.

108The estimation of the biodegradable material is obtained from a mass balance and in addition a109monitoring of the operational parameters is carried out, which provide information on the behavior110of the respective systems, when fed with an influent possessing sunflower oil or fats and Oils.

111 2. Materials and Methods

There are two clearly differentiated systems and therefore the applied methodology is conditioned by each empirical situation studied. It is pertinent to point out that the similarity between these two plants is the substitution of the flotation by biological treatment to remove fats and oils. Furthermore the similarity will be given at the process level by the aeration tank of the active sludge plant at laboratory scale and by the digester + aeration tank, in the real scale plant. Those are the facilities of both plants in which the charge of fats and oils is eliminated by biodegradation.

118 In both cases, a balance of matter is made to estimate the fraction of fats and oils biodegraded, 119 then the corresponding plants studied are described and the development of the respective balance 120 of matter is exposed.

121 2.1 *Test y parameter performed*

- 122
- 123 2.2.1
- Total Suspended Solids (TSS), TSS was determined by sample filtration of a known volume
 through Whatman 4.7 cm GF/C glass fiber filters and drying at 103-105°C. The difference in

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- weight of the filter before and after filtration is used to estimate the TSS, 209C method [13].[15].
- 128 2.1.2 Fats and oils

For determination of fats and oils, groups of substances with similar characteristics are
 qualitatively measured on basis of their common solubility in a suitable solvent. Gravimetric / Soxhlet
 Test Method (Method 213E, Standard MethodS 14 TH).

132 2.1.3 Chemical Oxygen Demand (COD)

COD has been determined using a variation of the potassium dichromate method [14]. [16]. This method uses a much smaller amount of sample and reagents. The sample is chemically oxidized through the action of potassium dichromate at a temperature of 150 °C for two hours. Silver sulfate is used as the catalyst and mercury sulfate to avoid potential chloride interference. Measurements are done by spectrophotometry at 600 nm.

- 139 2.1.4 Monitoring Parameter
- 140

138

ML= kg BOD applied /day] /[kg of total suspended solids in aeration tank] (1)

$$ML = Q \cdot BOD / (V \cdot MLTSS)$$
⁽²⁾

- Alternatively $ML = Q \cdot COD / (V \cdot MLTSS)$ (3)
- 141 Where:
- 142
- 143 BOD : Biochemical Oxygen Demand
- 144 COD: Chemical Oxygen Demand
- 145 MLTSS : Mixed liquor total suspended solids
- 146 Q: Influent Flow rate
- 147 V: Volume of aeration tank
- 148
- 149 2.2 Laboratory scale plant
- 150 2.2.1 Description of equipment

151 The equipment used was BIOCONTROL, model MARK 2. The laboratory scale active sludge 152 plant estimates the biodegradability of sunflower oil in wastewater. Experimental work is required 153 to obtain information about parameters describing the dynamics of the active sludge process. The 154 process will depend on the content of fats and oils present in the incoming wastewater.

155 2.2.1.1 Unit control of the equipment

156 It consists of a main switch, an air cylinder complete with a flow meter, a system flow control 157 rate, as well as a feed pump for the waste water to be purified, complemented by a rate control 158 system. A timer for intermittent operations, ON-OFF switch and a pump that recycle sedimentation 159 tank sludge to the aerator tank.

160 2.2.1.2 Aeration tank of the equipment

161 Transparent Plexiglas® cylinder of 38 cm height and 20 cm diameter, it has outputs at various 162 heights that are associated with different volumes: 7, 8, 9 and 10 liters. There are two inputs, on one

heights that are associated with different volumes: 7, 8, 9 and 10 liters. There are two inputs, on one hand: the recirculation sludge that are fed by the top and the influent to the lower level has in its

hand: the recirculation sludge that are fed by the top and the influent to the lower level has in its upper part an outlet for the mixing liquor that goes to the secondary settler. In addition, there are two

165 ceramic diffusers that are placed in the bottom, in a way that disperses the air in very small bubbles166 [15]. [13].

167 2.2.1.3 Sedimentation tank of the equipment

168 It consists of a transparent cylinder made of Plexiglas® such that the basal part has the shape of 169 a cone in order to facilitate the sedimentation and thickening of the sludge. Receives the mixed liquor 170 from the aeration tank by overflow, when it reaches the clarifier it gives rise to a downward flow, 171 such that the sludge decants and is separated and recirculated by the bottom through a pump, the

- 172 clarified water also uses the mechanism of Overflow to be evacuated to the accumulation tank.
- 173
- 174

Figure 1. Diagram of the experimental equipment.

- 175 Description:
 176 A: Feed pump.
 177 B: Recirculation pump.
- 178 **C:** Feed tank.
- 179 **D:** Aeration tank.
- 180 E: Sedimentation tank.
- **F:** effluent collection tank.
- 182 **G:** Block of oxygenation.
- 183 **H:** Airflow meter.
- 184



Description

- A: Feed pump
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- H: Air flow meter

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186 2.2.2 Experimental methodology

187 2.2.2.1 Food preparation

188 The treatment system was fed with synthetic wastewater prepared in the laboratory according 189 to the COD (Chemical Oxygen Demand) concentrations of urban residual water. The concentrations 190 were in the range of medium to strong [16]. [14], with a C: N: P = 100: 5: 1 ratio. Food was prepared

daily and the nitrogen and phosphorus were increased in accordance with the organic intake fromthe sunflower oil.

193 2.2.2.2 Determination of the relationship between COD and FAT

194 Determination of the relationship between fat and oils and COD, for sunflower oil and pork fat, 195 is performed by linking the fat and oil concentration and the resulting COD using the test described

- in the methodology.
- 197 2.2.2.3 Operation modes

198 The synthetic wastewater was prepared daily and deposited in a 50 liter storage tank, where a 199 stirrer was installed to disperse the oil or grease. Through a peristaltic pump, operated from the 200 control unit, it drives the feed to the aeration tank. The oxygen supply and the recirculation flow rate 201 are controlled from the control unit. The effluent from the process is collected in a tank of 30 liters of 202 volume, from which the samples are removed for the analyzes that are made to this one.

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205 2.3 Real scale plant

The real-scale plant of the Aerobic Digestor, consists of an active sludge sewage plant of conventional type or medium load, 0.6 (kg BOD / day) / kg MLTSS, which includes an aerobic sludge digester and where the fats and oils retained in the degreaser, are also sent and biodegraded. The plant has 3 similar modules with an aeration tank of 5108 m³, a settler of 2400 m³ and an aerobic

210 digester of 5108 m³, which has an average cell residence time of 25 days.

The full-scale plant consists of a Wastewater Treatment Plant that includes an aerobic digester (figure2).



Figure 2. Served water treatment plant (WWTP).

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215	W	here:
216	1, 2, 3	: Clarifier
217	4, 5, 7	: Reactor
218	6	: Aerobic digestor
219		

- 220 **3. Results**
- 221 3.1 Characterizacion of fats and COD

It shows the relationship of fats and oils and chemical demand for oxygen, for sunflower oil and pork fat both highly consumed in Chile. From these relationships it is possible to estimate the COD loading associated with the presence of oils in wastewater.

The empirical values obtained for the correlation (COD / fats and oils) of vegetal and animal origin are consistent with the literature [17].



227 228

Figure 3. Relationships of COD vs Pork Fat.





Figure 4. Relationships COD vs Sunflower Oil.





In this experiment, the water and oil are mixed in the feed tank by means of a mechanical type of agitation, part of the aggregate oil is accumulated in the oil tank, so the fraction of the oil that does

235 not enter the aeration tank is determined.

The influent contains sunflower oil and the concentration thereof is gradually increased; on the other hand the initial concentration of the biomass present in the aerobic reactor is of the order 4000

238 mg / 1 of Total Suspended Solids.



239



Figure 5. Process diagram of active river plant process.

241 Where:

242 F0, C0 : Flow and concentration of oil entering the mixing tank

243 F1, C1 : Flow and concentration of feed oil to the aeration tank.

244 F2, C2 : Flow and concentration of fats and oils leaving the aeration tank.

245 F3, C3 : Flow and concentration of fats and oil of the purified effluent.

- 246 F4, C4 : Flow and concentration of grease and oil in the recirculation flow rate.
- 247 M1 : Mass of oil that is contained in the mixing liquor of the aeration tank.
- 248 M2 : Mass oil that floats on top of the sedimentation tank and mass of oils that is at the

249 bottom of the sedimentation tank by adhesion to the biomass.

- 250 3.3 Balance of matter: determination of biodegradability:
- From the balance of matter, the mass of biodegraded sunflower oil is obtained which is part of
 the affluent that is fed to the treatment system, it is assumed that initially the system has no oil.
 For aeration tank:

$$\Delta M_{1} / \Delta t = F_{1} \cdot C_{1} - F_{2} \cdot C_{2} - r_{A} \cdot V + F_{4} \cdot C_{4}$$
(4)

254 For Secondary sedimentation tank:

$$\Delta M_{2} / \Delta t = F_{2} \cdot C_{2} - F_{3} \cdot C_{3} - F_{4} \cdot C_{4} - F_{6} \cdot C_{6}$$
(5)

- It is pertinent to point out that, $F_6 = 0$
- 256 M_1 : It corresponds to the oils and fats that are in the aerator tank.
- 257 M_2 : Corresponds to the oils and fats that are in the sedimentation pond.

nit of time, is the oil definitely biodegraded by the microorganisms, suc
$r_{A} \cdot V = F_{1} \cdot C_{1} - F_{3} \cdot C_{3} - \Delta M_{1} / \Delta t - \Delta M_{2} / \Delta t$
An important part of the oil floats and therefore does not biodegrade edimentation pond in which it accumulates. For reasons of technical feasibility, the balance of matter must be i nce it is possible to measure the accumulation of fats and oils caused neasuring the level of biodegradation of oil containing the influent. When performing the integral material balance for a certain period
$M_1 + M_2 = F_1 \cdot C_1 \cdot \Delta_t - F_3 \cdot C_3 \cdot \Delta_t - r_A \cdot V \cdot \Delta_t$
Where Δ_t : Time lapse
Each day is characterize by a subscript as the examples below:
For day 1:
$M_{11} + M_{21} = F_{11} \cdot C_{11} \cdot \Delta_t - F_{31} \cdot C_{31} \cdot \Delta_t - r_A \cdot V$
For day 2:
$M_{12} + M_{22} = F_{12} \cdot C_{12} \cdot \Delta_t - F_{32} \cdot C_{32} \cdot \Delta_t - r_A \cdot V$
For day n:
$M_{1n} + M_{2n} = F_{1n} \cdot C_{1n} \cdot \Delta_t - F_{3n} \cdot C_{3n} \cdot \Delta_t - r_A \cdot V$
Then the mass balance for a given number of days of operation:
$\sum (M_{1i} + M_{2i}) = F_{1i} \cdot \Delta_t \cdot \sum (C_{1i}) - F_{3i} \cdot \Delta_t \cdot \sum (C_{3i}) \cdot \sum (C_{3i}$
Then the biodegradability is:
$B = r_A \cdot V \cdot \Delta_t / F_{1i} \cdot \Delta_t \cdot \sum (C_{1i})$
$B = \{F_{1i} \cdot \Delta_t \cdot \sum_{l} (C_{1i}) - F_{3i} \cdot \Delta_t \cdot \sum_{l} (C_{3i}) - \sum_{l} (M_{1i} + M_{2i})\}$

259 : Disappearance rate of vegetable oil. r_A

260 The balance for the system as a whole is:

$$\Delta M_1 / \Delta t + \Delta M_2 / \Delta t = F_1 \cdot C_1 - F_3 \cdot C_3 - r_A \cdot V \tag{6}$$

261 From this expression we have to $r_A \cdot V$ Corresponds to the vegetable oil that disappears per 262 ch that: u

$$r_A \cdot V = F_1 \cdot C_1 - F_3 \cdot C_3 - \Delta M_1 / \Delta t - \Delta M_2 / \Delta t$$
(7)

- 263 and passes to the secondary 264 se
- 265 ntegral for a period of time, 266 d by flotation, which allows si 267 m
- 268 of time you have to:

$$M_1 + M_2 = F_1 \cdot C_1 \cdot \Delta_t - F_3 \cdot C_3 \cdot \Delta_t - r_A \cdot V \cdot \Delta_t$$
(8)

269 Where Δ_t : Time lapse	
Each day is characterize by a subscript as the examples below:	
271	
272 For day 1:	

$$M_{11} + M_{21} = F_{11} \cdot C_{11} \cdot \Delta_t - F_{31} \cdot C_{31} \cdot \Delta_t - r_A \cdot V \cdot \Delta_t$$
(9)

273

$$M_{12} + M_{22} = F_{12} \cdot C_{12} \cdot \Delta_t - F_{32} \cdot C_{32} \cdot \Delta_t - r_A \cdot V \cdot \Delta_t$$
(10)

274

$$M_{1n} + M_{2n} = F_{1n} \cdot C_{1n} \cdot \Delta_t - F_{3n} \cdot C_{3n} \cdot \Delta_t - r_A \cdot V \cdot \Delta_t$$
(11)

275

$$\sum (M_{1i} + M_{2i}) = F_{1i} \cdot \Delta_t \cdot \sum (C_{1i}) - F_{3i} \cdot \Delta_t \cdot \sum (C_{3i}) - r_A \cdot V \cdot \Delta_t$$
(12)

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277

$$B = r_A \cdot V \cdot \Delta_t / F_{li} \cdot \Delta_t \cdot \sum (C_{li})$$
⁽¹³⁾

$$B = \{F_{1i} \cdot \Delta_t \cdot \sum(C_{1i}) - F_{3i} \cdot \Delta_t \cdot \sum(C_{3i}) - \sum(M_{1i} + M_{2i})\} / F_{1i} \cdot \Delta_t \cdot \sum(C_{1i})$$
(14)

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efficiency.						
Days of operation Includes balance	Mass of oil fed (g)	Dough Of retained oil (g)	Dough Of oil in the effluent (g)	Dough Of biodeg. (G)	Dough Of sedimentation oil (g)	Biodegradation Efficiency (%)
1 to 8	79	12,3	5,4	54,8	6,5	75
9 to 16	120	28	8	65	19	71
17 to 23	157	70	10	56	21	64

Table 3. Balance of matter in active sludge with influent oily agitation and biodegradation

284 3.4 Mass balance at Wastewater Treatment Plant (WWTP)

285 Mass balance was done on the real-scale treatment plant, which has a different structure in 286 comparison to the laboratory-scale plant. In general, the entry of fats and oils corresponds to the load

287

that transport the affluent; and the outputs of this contaminant correspond to the fats and oils that go 288 out for the effluent of the active sludge plant and in the sludge line, the difference between the input

289 and the output mass corresponds to the mass of biodegraded fats and oils (figure 6).



290

291

Figure 6. Flow diagram of aerobic digester.

- 292 The flow diagram of the Wastewater Treatment Plant Los Angeles, (Figure 6).
- 293 Mass balance at wastewater treatment plant (WWTP-LA):
- 294 Mass of Biodegradable Oil = Mass of entry - Mass exiting by effluent - Mass coming out by sludge

$$M_{GYA} = Q_{af} \cdot C_{af} - Q_L \cdot C_L - Q_{ef} \cdot C_{ef}$$
(15)

295	V	Where:
296	Q_{af}	: Flow of the affluent, l/day.
297	C_{af}	: Concentration of fats and oils of the tributary, mg/l.
298	Q_{L}	: Flow rate from the Digester to the Sludge Dehydrator, l/day.
299	C_{L}	: Concentration of Fats and Oils of the Digester, mg/l.
300	$Q_{\rm ef}$: Outflow from Effluent, l/day.
301	Cef	: Concentration of Effluent Fats and Oils, I/day.

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303 Figure 7. General flow diagram of the Los Angeles WWTP.

Table 4. Mass of fats and oils.

Period	Affluent	Effluent	Mud	Biodegradable mass	% Biodegradation
	(kg)	(kg)	(kg)	(kg)	
1	46.604	2.072	264	44.268	95
2	19.005	1.456	676	16.872	89
3	25.572	3.164	85	22.323	87
4	10.083	1.045	110	8.927	89
5	16.562	4.725	439	11.398	69
6	11.031	1.446	118	9.467	86
7	9.269	987	0	8.282	89
Total	138.126	14.895	1.693	121.538	

305 *3.5 Operation parameters*

302

304

306 3.5.1 Efficiency of elimination of fats and oils by biological means

307 In the lab-scale plant, there are three periods of 8 days each in which the oil concentration of the 308 influent is practically constant. Initially the oil concentration is 333 mg / l, then it increases to 309 approximately 460 mg / l and for the last days of operation, an oil concentration in the influent next 310 to 500 mg / l is reached. The sunflower oil is eliminated by biodegradation and by flotation, it must 311 be emphasized that it is the only carbon source. Figure 8 shows the oil leaving the effluent; on the 312 other hand we have the curve that represents the oil of the effluent and to which is accumulated in 313 the sedimentation, that is to say the non-biodegradable oil. We can observe that the effluent and 314 accumulated oil increases with the concentration of the influent.





315



Figure 8. Efficiency of biodegradation and elimination as a function of the bulk load.

317 Given the configuration of the process of treatment of waste water in real scale, necessarily the 318 fats and oils are retained in the degreaser and sent to the sludge digester. It constitutes an important 319 structural variant with respect to the traditional solutions and the remaining fraction. What remains 320 part of the wastewater is treated by biological treatment of active sludge in a conventional mode.

321 Therefore, the residue of fats and oils not eliminated becomes part of the contaminants of the 322 effluent and the rest becomes part of the sludge leaving the filter.

The mass of fats and oils that leaves the effluent is greater than the mass that leaves in the sludge (figure 9).



325

326

Figure 9. Efficiency of biodegradation and elimination as a function of the bulk load

Figure 9 shows the mass of fats and oils in the influent and effluent of the biological treatment plant and in the sludge leaving the digester, which shows optimistic results regarding the elimination of fats and oils at a global level. The fats and oils are retained in the degreaser and is subsequently subjected to biodegradation in the aerobic digester.

The biodegradation efficiency of fats and oils in the digester and the plant at pilot scale allows adequate acclimatization by the biomass. The only source of carbon and energy are fats and oils, so there is no situation of competitiveness with other substrates.

334 3.5.2 Mass loading, biodegradation and oil and fat removal

At the laboratory scale, a considerable fraction of the sunflower oil accumulates in the secondary
 settler; the magnitude of this accumulation of oil mass is correlated with the oil concentration in the
 influent.

The values of eliminated vegetable oil in the effluent report that the sum of the phenomena of biodegradation and oil flotation reaches a high global elimination of vegetable oil. In addition, the biodegradation of oil does not depend on the mass loading (Figure 10).

341 Considering the values of the mass load, at an initial stage the conventional regime is conducted,
342 later a regime of high rate are used (Figure 10). The value of the mass load does not affect the quality
343 of the effluent, which is coherent with the theory and the experience of wastewater treatment.

The percentage of removal of vegetable oil is over 90% which is mainly due to the biodegradation of vegetable oil. About 70% and 20% corresponds to flotation, considering the balance of matter shown in Table 4. This is comparable with experience in the active sludge system, which achieved COD removals of 80%, for waste water from the olive oil refining industry [18].

For aerobic biological treatments we have experiences in plants on a real scale. An evaluation of municipal water treatment plants was carried out in USA; it was mainly found that the concentration of fats and oils in the influent had an average value lower than 80 mg / l and a BOD of Mom g / L. The effluent had a concentration of fats and oils lower than 10 mg / l and BOD less than 40 mg / effluent level. Furthermore the elimination of fats and oils does not present a seasonal variation [19]. Our results are consistent with those of the literature.

The amount of accumulated oil increases with the oil concentration in the influent and affects the quality of the effluent, which is corroborated by the results of the material balance, which establish a biodegradability of 75% for a concentration of 340 mg / l, from 71% to 460 mg / l and from 64% to 500 mg / l.

Aerobic experiments with granular sludge in a sequential batch reactor for the treatment of dairy effluents, rich in fats and oils, reached COD elimination levels of 90%, after separation of the biomass from the blend liquor [20].

Another experiment was performed to characterize the transformation of lipids into active sludge under aerobic conditions; the results showed that the total lipid content in the effluent would not be reduced to values below 300 mg / l from an initial 2000 mg / L [21].

In the same active sludge experimental plant of this work, 400 mg / l of saccharose were added to similar concentrations of fats and oils in the influent, the oil and fats concentration range was 100 to 850 mg/L, biodegradation was in the range of 60% to 51% [22], what show the competitive effect of other substrate, fact to consider.

Anaerobic biodegradation experiments reach a level of oil removal ranging from 81% to 97%(23), which is relatively similar to this system when considering flotation.





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Figure 10. Efficiency of biodegradation and elimination as a function of bulk load.

372 Considering the empirical antecedents of the biological treatment of waste water, fats and oils 373 are physically eliminated generating a considerable amount of waste that must be disposed in a 374 landfill, with a high economic and environmental cost. For the case studied there is a degreaser, 375 which eliminates 80% or more of the incoming fats and oils, obtaining concentrations in the effluent 376 of the treatment plant of 10 mg / l. This is a conventional treatment with loading ranges High mass 377 and therefore a considerable availability and variety of substrate, which compete with fats and oils 378 advantageously as they possess simpler mechanisms of biodegradation. Both systems show high 379 levels of biodegradation since they work with a single substrate, fats and oils, which favors the 380 acclimatization of the biomass [24].

381 It should be noted that in the specific case of the Los Angeles treatment plant there is an aerobic 382 sludge digester which also removes fats and oils, therefore the volume of fats and oils physically 383 retained in the degreaser is finally treated biologically.

384 Figure 11 shows grease and oil removal efficiencies by biodegradation in the sludge digester and 385 the overall efficiency resulting from both processes. The elimination efficiency in the sludge digester 386 is well above that in the active sludge process, this difference is mainly explained by the high 387 concentration of biomass in the sludge digester. Higher than the one of the aeration tank from the 388 process of active sludge of the plant in a pilot scale. The results lead to a greater amount of active 389 biomass, generating an extended aeration system. Therefore the quantity of substrate is poor in 390 relation to the biomass, which stimulates the use of fats and oils as a substrate for the construction of 391 cellular tissue and energy source by the biomass.

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Figure 11. Efficiency of biodegradation and elimination as a function of the bulk load in WWTP.

Both systems have biomass, fats and oils, and both are the support for activity of the enzyme
lipase. Biodegradation is measured using the lipase activity; the enzyme is extracted from the active
sludge, after environmentally safe verification [25].

397 The digestion of sludge, fats and oils in the aerobic digester is close to a biological treatment of 398 activated sludge in extended aeration for fats and oils, the only substrate present. Therefore this 399 methodology, for the elimination of fats and oils, is an innovative experience and is considerably 400 similar to the laboratory experience with which it is compared.

401 Real experience shows a result that is consistent with the one performed at the laboratory and 402 does not generate fats and oils as final residue, which eliminates the problem of its final disposition.

403 4. Conclusions

- Sunflower oil is biodegradable and reaches a range of biodegradation between 64% and 75%, for
 a wide range of concentration of this type of substrates in the influent in Laboratory scale active
 sludge plant. The fats and oils are biodegraded between 69% a 92% in the aerobic real digester.
- 407 The oil removed in the wastewater treatment process is by means of flotation and
 408 biodegradation mechanisms, and when added together the elimination becomes above 85% on
 409 the Laboratory scale active sludge plant.
- Elimination and the efficiency of biodegradation are between 69% to 92% with previous
 separation of fats and oils by flotation in aerobic real digester.
- The higher biodegradation efficiency (75%) for the experimental plant sludge active, and the
 biodegradation efficiency of the aerobic digester, 92%, corresponds to the lowest mass loading
 condition in both cases.
- The biomass presents great adaptability to the oil substrate, favored in this case for the lack of
 competitiveness being fats and oil the only source of carbon.
- Fats and oils should be removed by biological treatment, replacing the flotation and at most using it as an intermediate process
- 420 **Conflicts of Interest:** The authors declare no conflict of interest.

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