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Article

Solar Photovoltaic Cooker or Heater with No Electronics or Battery

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Abstract: The paper offers an innovative cooking utensil design for remote, isolated, and even peri-urban communities at a low price, with high reliability and simple construction. It can alleviate energy poverty and improve food security. This utensil uses only local solar energy directly and allows comfortable indoor cooking. This paper provides the design principles of a solar cooker/frying pan or generic heater, based on a PV panel or a plurality of them, which are directly connected to a plurality of Positive Thermal Coefficient (PTC) resistors to match the power. PTCs are nowadays produced in massive quantities and are widely available at low cost. The proposed device does not require an electronic controller or a battery for its operation. The aim is for family use, although the design can be easily scaled to a larger size or power, maintaining its simplicity. Electric heating inside or attached to the cooking pot, plus the temperature self-limiting effect of PTCs, allows for thermally insulating the cooking pot from its outside using ordinary materials. Insulation enhances energy efficiency during cooking and keeps cooked food warm for a long time. Clean development would receive a significant impulse with its application. A simple mathematical model describes its functioning and states guidelines for adequate design. The results indicate a successful proof of concept and high efficiency both for water and oil as representatives of cooking.

Keywords: solar e-cooking; photovoltaics; PTC heater; sustainable development; appropriate technology; energy poverty; clean cooking

1. Introduction

According to [1] by 2030 1.9 billion people will still not have access to clean cooking technologies. This gives a scale of the problem.

Solar cooking is a relief for isolated and remote populations in favor of their energy independence and sustainable development. Aemro et al. [2] and De [3] describe solar cooking as environmentally friendly and healthy. The impact of using solar can be high as cooking usually consumes more energy than food production, processing, packaging, and distribution. Commonly, the low-income population relies on burning wood and even charcoal. This applies pressure on the vegetal cover of the territory, very frequently causing deforestation, Bailis [4], Aberilla [5] among others, even if improved cookstoves are used, Chagunda [6]. Additionally, quotidian in-home indoor combustion generates toxic fumes, Geng [7]. They can harm the human body directly or indirectly and induce several kinds of diseases, with the result in increasing high levels of premature deaths,

e.g. WHO [8], Bruce [9], WHO [10]. The use of modern energy vectors, such as LPG and kerosene, is not without problems, in addition to its excessive cost and uncertain availability to poor economies. Also, the related polluting and greenhouse gas emissions should not be ignored. Grid electricity for cooking is not always available in the herewith under-aim locations, and its cost can be too high for many low-income families [11]. Given that a significant fraction of the population affected by energy concerns is located in sunny regions, solar cooking is attractive, at least for partial fulfillment of daily needs. Many studies address this possibility, including Batchelor [12] and Lecuona-Neumann [13] among others. Halkos [14] studies the multi-dimensional aspects of energy poverty. These references indicate that solar electric cooking can fulfill some of the dimensions addressed.

Indoor cooking. Direct and indirect solar cooking is based on heating the cooking pot or a heat transfer fluid by irradiance absorption and its immediate conversion into heat, Arunachala [15]. They offer relief for the above-mentioned problem. These thermal cookers must be operated outdoors, at least partially, with low social acceptance, in addition to risks of robbery, dust, and animal aggression. To allow indoor cooking, direct cookers concentrate the solar rays into a hole in a dwelling wall, e. g. the Scheffler parabola, or other options, e.g. Balachandran [16] and Singh [17], while indirect types use a heat transfer fluid to bring heat from outdoors to the cooking utensil, which can be located indoors, e. g. Varun [18]. Varun [19] reviews the topic with particular emphasis on indoor cooking, stating that it is the need of the hour. Sizable are the solar cookers that produce steam to cook indoors using steam indirectly, typical for temples in India, Indora [20]. There is a need for practical layouts for family-size solar cookers allowing indoor cooking in a conventional kitchen. The quality of the food and the life quality of the housekeeper increases. To fulfill this need, Photo-Voltaic (PV) panels as a primary energy source, seem suitable for this, since the panels can easily be affixed to the roof. This technology is supported by the continuous decrease in PV panel prices, which have reached the order of 0.1 €/nominal watt (peak) wholesale, IEA [21], and [22] by Our World in Data. Even today, there is no technology widely used for off-grid PV cooking of the family size, although some studies address its viability, such as Dufo-López [23], Altouni [24] and Batchelor et al. [25] among others.

The heating produced by dissipating the electricity of the panels into heat can also be applied to heating air for drying vegetables, meat, or seafood, which is not the aim of this article. Moreover, the herewith proposed heaters can be added to a kind of commercial electric pressure cooker, Rose [26], modified to accept PV electricity, but still, they are not available. These devices substantially reduce the thermal energy loss of water evaporation. Simultaneously they incorporate some thermal insulation, reducing sensible heat losses, Asok Rose [27], thus also increasing energy efficiency.

Solar panels and direct drive. PV panels are sets of in-series solarized reverse-biased diodes that offer a direct electrical Current (DC) approximately proportional to solar irradiance times exposed area. However, they show a non-linear dependence on voltage. Moreover, partial shading on a conventional panel causes a considerable loss in conversion efficiency, which in standard operating conditions is 17% to 24%, for silicon-based cells. All this makes necessary an electronic controller for establishing the appropriate operating voltage and the resulting intensity. These controllers, on the one hand, try to maximize efficiency and, on the other hand, adapt voltage for electricity use e. g. [24]. Usually, the controller is embedded into the so-called inverter, as those types of equipment aim to inject Alternate Current (AC) electricity into some kind of grid, either mains or micro(smart)-grid.

When this is not the case, the Direct Current (DC) produced by the panels is usually directly consumed, sparing the inverter, e. g. Simon Prabu [28], and Atmane [29] among others. There are commercial devices that rely on charging a local battery for later use while eventually supplying a load. Using these devices makes it necessary to transport the costly, heavy, and short-lived batteries at large distances, carrying the possibility of the users abandoning them in situ when dead, with the associated pollution of the environment. These controllers/chargers are designed for standard voltage panels, such as 12 V and 24 V, for the battery's requirements. These voltages are not aimed by the standard of the nowadays massively produced panels but are in the range of 30 to 40 V for panels made with in-series 60 to 72 cells or twice in the case of the split cell type. Matching the panel intensity

and voltage with the battery charge and discharge requirements wastes substantial energy and limits the power to the additional connected load. I Zobaa [30] states that PV panel output to user electricity can be as low as 50% under normal operation. Moreover, these controller/charger devices incorporate integrated electronics and batteries that, in the event of a malfunction, in a remote or isolated location can rarely be diagnosed and replaced, making them somehow undesirable, especially for low-income economies and under the nowadays state of the art.

As a preliminary consideration, it is worth establishing if the silicon PV panels are efficient enough for family cooking. Assuming 20% as the representative efficiency from solar energy to electricity, it follows that this is lower than the representative efficiency of a thermal solar cooker, which is around 30% maximum, e. g. Onokwai [31]. This later low figure incorporates the need to reorient the thermal solar cooker to stay focused. This operation is seldom performed daily as frequently as needed and can be non-perfect. In the case of a PV-based electric cooker, sun tracking is possible but non-compulsory as there is no sun rays' concentration. The electricity can be dissipated into useful heat in direct contact with the electrified cooking pot and is always internal to the thermal insulation. The peripheral thermal insulation results in reduced losses to ambient, positioning electrical cooking in an advantageous position. This, even considering that the roof-mounted PV panel is usually in a fixed orientation towards the equator, thus losing some direct radiance, but on the other hand, it captures the diffuse component.

The paper focuses on this technology. Moreover, the low losses to ambient allow an increase in cooking temperature, suitable for frying, braising, and the like. One inrush into this technology is Watkins [32], which cast the term Insulated Solar Electric Cooking (ISEC). The peak power of a single silicon PV panel in the market is between 300 to 500 W at the present state of the art, enough for this kind of cooking. If not enough, the herewith proposed configuration allows adding panels in parallel, thus ensuring a safe voltage and multiplying the intensity. This way, the increased power can be used in a single high-power hot plate or several ones, thus allowing recipes needing in-parallel cooking of several ingredients.

This work addresses the possibility of eliminating both electronics and batteries, in an independent installation of an apriorist single PV panel and a thermally insulated cooking pot. No other publication has been found on this layout neither a model describing it. An approach is Osei [33]; there, nichrome heaters are embedded into erythritol Phase Change Material (PCM) used as thermal energy storage. The resistors are directly connected to a PV panel to form an integrated unit. When directly connecting conventional resistors to PV panels, there is a primary difficulty: as no electronics is present, it is difficult to efficiently dissipate electricity using the almost constant resistance such as nichrome wires for different irradiances. In the mentioned work this problem is overcome, a string of diodes has been tried as heaters, directly connected to a PV panel, to better match the panel intensity-voltage I-V curves so that operation near the Maximum Power Point (MPP). Some thermal problems arise with the diode semiconductors' thermal breakdown. The present paper illustrates these issues and, as a consequence, proposes using ceramic Positive Thermal Coefficient (PTC) commercial resistors as heaters, Wikipedia [34] and Yang [35].

There is an unavoidable thermal resistance from the PTC heaters up to the cooking pot. It can be avoided by using induction heating of the pot bottom, although incorporating electronics. Some studies address the topic of designing such devices using the DC electricity available from the PV panel, e. g. Sibiya [36], Anusree [37], and Dhar [38]. Even a commercial unit with an inbuilt controller and a battery has been found, Greenwax Technology [39]. This attractive option finds an additional drawback; it needs special cook pots not always available in some communities.

In the simple layout herewith analyzed that avoids a battery, there is no purpose electrical storage for off-sunshine cooking, e. g. batteries. Complementary methods can overcome this. The recently cooked meal is hot, so it has in-built thermal storage, and having it warm later on is an extra value. When cooking, the yield produces a moderately elevated temperature in the food. This forms what is called Thermal Energy Storage (TES) to replace electricity storage. It is common to use "wonder bags", Mawire [40]; this means storing the already-cooked hot meal inside a heat-insulating bag or box and even complementing this heat storage capacity with some extra material storing

sensible or latent heat, Lecuona-Neumann [41]. This will not only preserve the meal warm for later use, e. g., up to dinner time, but also prolong low-temperature “slow cooking” without any extra energy consumption. Another possibility is to incorporate a Phase Change Material (PCM) as a TES with a higher energy content, 100 to 400 kJ/kg, than a single-phase material, although at a higher cost, e. g. Opoku [42]. Such materials can be paraffin, erythritol, mannitol, xylitol, and other non-organic ones, Santhi Rekha [43]. Storing the melted PCM in a well-heat-insulated vessel can maintain its temperature above solidification. The latent heat of solidification re-heats and even can softly cook breakfast from the previous day's collected solar heat. Some of these materials are non-toxic or polluting and are mass-produced, Lecuona [44] and Agyenim [45] among others.

Not including storage in the initial layout does not preclude using the surplus electric PV production for charging appliances such as mobile phones, lanterns, radios, and the like, as needed for enhancing the quality of life in the home as their consumption is typically lower than of a solar cooker.

2. Materials and Methods

The methodology chosen models the PV solar cooker using commercial curves of PV panels to explore their direct connection to PTCs commercial heating elements, whose resistance curves have been experimentally determined. The direct connection layout is developed. The aim is to offer a simple enough model and information so that a design and later construction is possible with confidence in the performances and for diverse sizes and solar resources.

Simple cases are modeled, taking as an example a single-family single hot plate representative size. The results are explained and discussed. Finally, some conclusions are offered, such that PV-based solar cookers can be constructed quickly and reasonably priced, avoiding using electronics and batteries.

If during cooking, a power reduction is needed, there are two kinds of options, firstly mechanical, such as disorienting the panel or separating the pot from the hot plate by an insulating sheet, and secondly, electrical, such as adding or switching the PTCs elements off, away from the optimum number of them, what is built-in in the model here described.

The theory presented here uses the least possible complexity to reduce the computing requirements for a design to a minimum, allowing the use of widely available spreadsheets and, in an extreme case, a scientific calculator. It proposes a solution of appropriate technology for sustainable development and a tool for fighting energy poverty and food insecurity. For the construction, a multimeter, in addition to simple tools, is just what is needed. A sensible experimental calibration can counteract the loss of accuracy because of the low modeling mathematical order.

3. Results

Section 3.1 models a generic PV panel or set of panels, in a practical way, using only catalog data and basic properties of these devices. Section 3.2 models the PTC heaters in the same way. Section 3.3 offers the model results of matching both devices as a function of irradiance and temperatures. Section 3.4 maximizes heat production. Section 4 models two extreme cases in a time-marching way, incorporating a model of heat losses to ambient. Section 5 summarizes the results and offers a set of usable conclusions.

3.1. PV panel modeling

Detailed and highly accurate electrical modeling of PV cells is possible when numerous required physical parameters are known. Alternatively, acceptable accuracy can be reached using the basic parameters of the materials and their layout. This is possible through a multiparameter prediction or even the least square fitting to the overall characteristic curves of a whole panel such that the delivered intensity can be formulated as $I(G, T_p, V, \text{internal parameters})$, reaching a respectable accuracy. Herewith $\langle \rangle$ indicates functional dependence, G is solar irradiance, T_p is the panel temperature, and V is the output voltage. Unfortunately, such curve-fitting leads to a non-linear

procedure that is complex in its application. Semiempirical variants are available using just some parameters when all necessary ones are not given, such as in commercial panels, such as Rawat [46] and El Tayyan [47] among others. Within these approaches, one finds fitting empirical formulations based on physically reduced models. This is a practical approach that herewith is preferred for simplicity, reducing the number of parameters by using $I(G, T_P, V, \text{empirical parameters})$.

The particular model used in this paper follows Eq. (1). It discriminates two voltage ranges above and below a reference voltage $V_r(G, T_P)$:

- For voltages below this empirical reference, $V < V_r(G, T_P)$, the intensity I is assumed to be proportional to irradiance G , using the peak nominal values I_{pe} and G_{pe} for normalization. Within this range, $I(V)$ is almost constant, near the value at the short circuit. It has a low dependence with V , decreasing as Eq. [1] indicates by the effect of in-series resistance R_s , following the simple one-diode model. When operating, the panel temperature T_p is higher than ambient temperature, requiring a correction that usually is referred to as a standard $T_p = 25^\circ\text{C}$.
- Beyond the specific reference voltage V_r and the corresponding I_r , a continuous exponential decrease considers saturation down to the open circuit voltage V_{oc} when $I = 0$.

$$\left. \begin{aligned} V < V_r &\rightarrow I = I_{pe} \frac{G}{G_{pe}} \left[1 + \gamma(T_p - 25^\circ\text{C}) \right] - \frac{V}{R_s} \\ V \geq V_r &\rightarrow V = I_r - K_d \exp \left[- \left(\frac{K_e}{V - V_r} \right)^r \right] \end{aligned} \right\} \quad (1)$$

Fitting of this model to the commercial data, usually given by purchasers, has been performed in two ways, Eq. (2). (a) is a simpler one and (b) a more accurate alternative, which includes an extra fitting parameter to the expression of $V_r(G, T_p)$, leading to different parameter values.

$$\left\{ \begin{aligned} \text{(a): } V_r &= V_{r0} - \beta(T_p - 25^\circ\text{C}) \\ \text{(b): } V_r &= V_{r0} - \beta(T_p - 25^\circ\text{C}) + V_{rb} \left(\frac{G_b}{G} - 1 \right)^b ; G > 0 \end{aligned} \right. \quad (2)$$

The extra correction to V_r of the option (b) allows reproducing better $V_{oc}(G)$, especially for low values of G . These two alternatives allow for comparing two slightly different fitting options on the same panel data. Unfortunately, the herewith adopted model does not give an explicit expression for the voltage at the maximum power point (MPP) called V_{MPP} , which happens at the point that maximizes $W(V_{MPP}, G, T_p) = IV(V_{MPP}, G, T_p)$. This means $\max(IV) \rightarrow \frac{d(IV)}{dV} = 0$.

In what follows, the model is applied to an average-performance solar panel. It is representative of the average PV residential market. This one has a 1.85 m^2 aperture area, delivering a nominal peak power of $W_p = 310 \text{ W}$. Figure 1 shows the results of fitting both options in Eq. (2). Eq. (3) shows the set of empirical and manually fitted parameters. The resulting maximum peak power values obtained are (a) $W_{pe} = 306 \text{ W}$ and (b) 319 W . The most crucial zone in the $I - V$ map is the corner of the curves; as the power reaches its maximum Power Point (MPP), there as $\max(IV) \rightarrow \frac{dI}{dV} = -\frac{I}{V} < 0$ and this condition can only happen there.

Now it seems clear that a fixed resistance $R = \frac{V}{I} = \text{cnt.}$, that is the inverse of the slope of a straight line passing from (0,0) in the $V - I$ graph, can only intercept a single MPP corresponding to a single G and T_p . Figure 1 allows us to easily reason the problems associated with feeding a fixed resistance, R , with the PV panel. It would impose a fixed straight line of operation: $I = \frac{V}{R}$, coming from (0,0) to intercept the panel curve. If the value of R is chosen for the line to intercept the panel curve at the MPP for certain G and T_p , any variation on one of these parameters shifts the MPP away from the intersection.

Error! Reference source not found. shows the required value of R for operation at the MPP for different irradiance values and working temperatures. Both optional fits defined in Eq. 2 are displayed, evidencing slight differences. It shows that the MPP happens at a relatively constant $V, \forall G$ and the resistance for MPP decreases with G . It also shows the linearity of the maximum power achievable $\forall G$.

$$I_{pe} = 9 \text{ A}; G_{pe} = 1 \text{ kW m}^{-2}; \gamma = 5 \times 10^{-4} \text{ A } ^\circ\text{C}^{-1}; R_s = 200 \Omega$$

$$V_{r0} = 18 \text{ V}; \beta = 0.16 \text{ V } ^\circ\text{C}^{-1}; K_d = 800 \text{ A}; r = 1.5; K_e = 70 \text{ V}; (b): V_{rb} = 1.5 \text{ V}; b = 0.4 \quad (3)$$

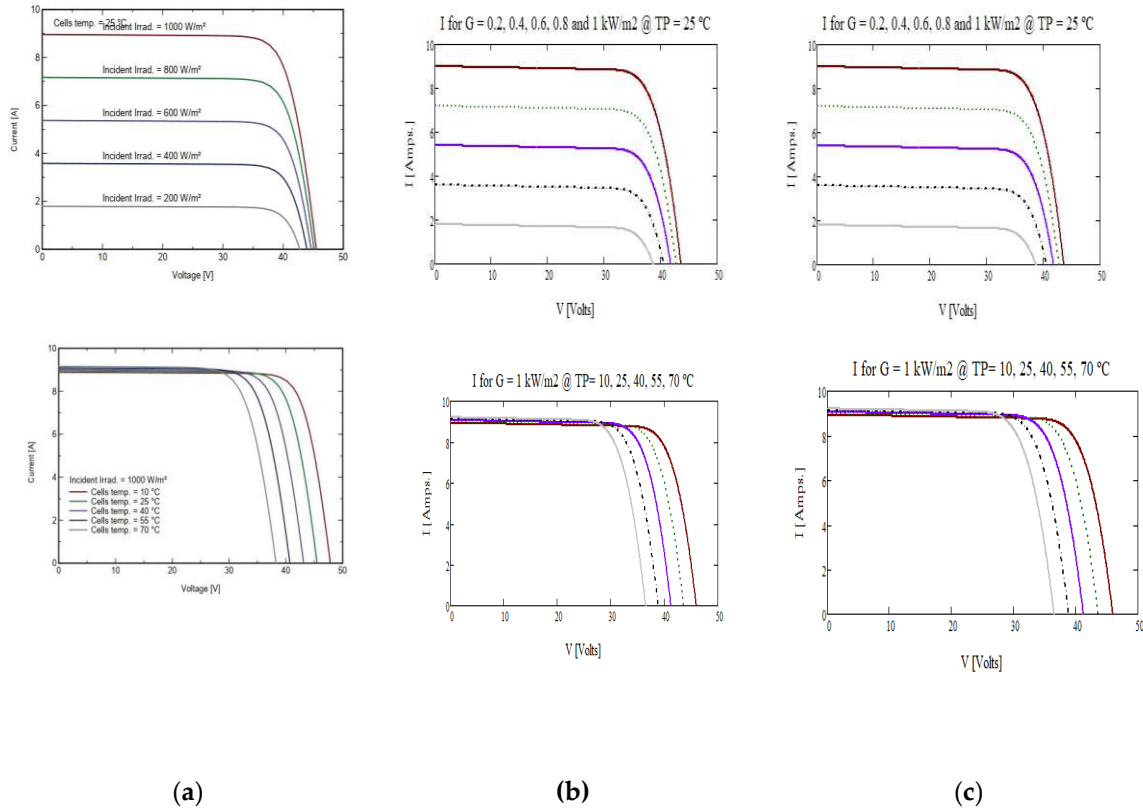


Figure 1. (a) original data for the solar panel. (b) result of the fitting, option (a). (c) result of the fitting, option (b).

If a variable linear resistance R loads the panel, working continuously on the MPP, it must increase for lower G , and it has to be sensitive to T_p . This is evident from the fact that $V_{MPP} \approx \text{cnt.}$ for fixed T_p , as **Error! Reference source not found.** shows. This figure shows the differences in power for the two optional fittings, especially on the MPP voltages, in the order of 10%.

The usual large variations in irradiance during panel operation and the associated need for a variable load resistance justify the need for a controller. It can be either the Pulse Width Modulation (PWM) type or the perturb-and-observe tracking type; more about it in Abidi [48]. Both are commercial implementations. They require a microcontroller and a battery, plus power electronics. They are oriented to properly charge and discharge the battery. The ideal way out for MPP tracking (MPPT) would be a non-linear charge that would present at every time the resistance that maximizes the panel power W_{MPP} , from now on R_{MPP} , in an automated way. **Error! Reference source not found.** represents the voltage, the R_{MPP} , and the resulting power for two values of T_p . Observing it, the trends here highlighted are evident. There, some differences can be appreciated between both fits, but overall, they are equivalent. There is an almost linear change in W_{MPP} with G .

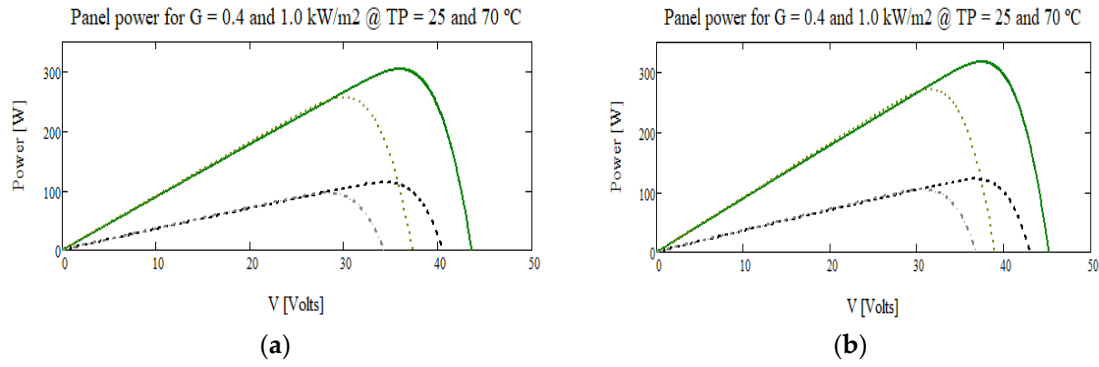


Figure 2. Power vs. voltage for two irradiances at two panel temperatures. (a) fitting option (a). (b) fitting option (b). Green upper lines for $T_p = 25$ °C and black dashed lines for $T_p = 70$ °C.

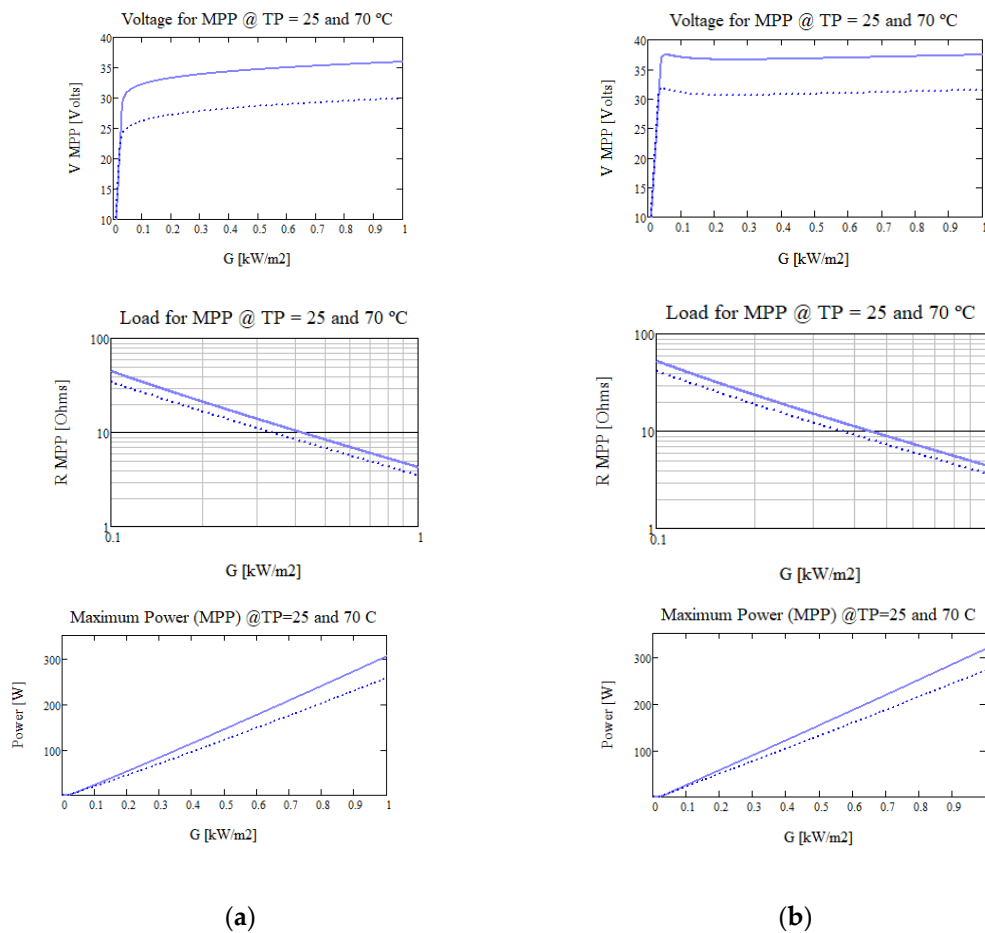


Figure 3. Results for maximizing power vs. G at two panel temperatures, continuous line for $T_p = 25$ °C and dashed line for $T_p = 70$ °C. From up to down: Voltage V_{MPP} , resistance R_{MPP} as a logarithmic plot, maximum power W_{MPP} . Left) fitting option (a). Right) fitting option (b).

Error! Reference source not found. also shows that for this panel V_{MPP} is around 25 to 32 V at the representative temperatures resulting from a cloudless day with no wind, here simplified to $T_p = 70$ °C. Incidentally, this is not too far for charging 24 V batteries. These calculations could be improved by using a time-varying T_p , but this would oblige to describe a time marching of the operating point of the panel using the NOCT (Normal Operating Cell Temperature) parameter, Alonso [49]. It would also require information on the not-always-available day temperature and wind speed, which can be quite different from day to day and for distinct locations.

As a preliminary conclusion, avoiding electronics calls for a non-linear and/or variable load. In what follows, the selected case is Positive Thermal Coefficient (PTC) variable resistors for heating.

3.2. PTC modeling

PTCs can be defined as thermally sensitive semiconductor resistors. They are polycrystalline ceramics based on barium titanate, Abidi [48], and Alonso [49]. They correspond to a class of materials named crystalline ferroelectric ceramics, which are obtained by sintering a powder typically of barium titanate at temperatures up to 1400 °C. PTC heating elements are a kind of thermistor, so they share the same principles of operation. During the fabrication of the PTC heaters herewith of interest, dopants are added to give the material specific semiconductor properties.

With the PTC temperature rising above a reference ambient $T_{at} = 25$ °C, the resistance of the PTC initially decreases exponentially with a thermal coefficient $\alpha_{low} = \frac{d\ln(R)}{dT} < 0$, behaving like an NTC. For a near ambient temperature (e.g., 50 °C), the resistance becomes relatively constant up to a second tailor-made temperature, (e.g., 100, 150, 200, 250 °C) where a phase change occurs. Above this temperature, the resistance rises steeply at a larger $\alpha_{high} = \frac{d\ln(R)}{dT} > 0$ and $> \alpha_{low}$. Figure 1 shows a realistic curve for resistance as a semi-logarithmic chart of a generic encapsulated PTC available from Asian suppliers of an active size of 60×21 mm, from now on called “full size”. It is recommended for a voltage range available in the PV panel presented above. This resistance corresponds to a non-loaded PTC, thus at very low voltage, such as the one applied by a DC multimeter. Loaded PTCs suffer self-heating, changing in a non-negligible amount the apparent resistance $R = V/I$, especially at high dissipated power. The Steinhart–Hart equation is often used to approximate this rise, Wikipedia [50]. Other models are available. Beyond the range of the large resistance rise, the resistance again decreases, out of our range of interest, and eventually, a breakdown occurs. The temperature where the resistance duplicates above the minimum is called the Curie temperature T_C . It is considered here as a limiting temperature due to the sharp reversible cutoff of power it produces, implying a safety mechanism against overheating. PTC heating elements are used widely; fuel pre-heating, compartment air warming, air hairdressers, defrosters, silicone cement melting pistols, evaporators, boilers, and electric motor protection; are just a few examples. Samples can be bought for around 1 € and one-tenth of this in quantities.

For a low applied voltage, the resulting low-temperature high resistance, and its decrease as temperature increases, together help approach the PV panel MPP at low irradiances, such as in the morning, as will be shown in what follows, Figure 3. Energizing the PTC at an initially cold state implies feeding a large resistance with the resulting low intensity. As temperature increases, the reduction in resistance helps climb the PV panel curve towards the MPP. If the MPP is surpassed towards a low PV voltage region, an excessive reduction of dissipated power would result in a reduction of temperature with the consequent backward displacement towards the MPP. From another point of view, the large resistance increase near the Curie temperature helps limit temperature as a thermostat will do. $T_C \lesssim 250$ °C is selected for the present application to avoid burning the cooking pot or its thermal insulation. The resulting hot plate temperature allows meat frying and roasting in a pot or other utensil, Sagade [51], as well as food preservation, Berk [52].

Commercial PTC heating elements sold by generic suppliers show a slender flat tablet structure. They are circular or rectangular, of some millimeters ≈ 5 mm thickness, with both sides metalized as electrodes. They usually are offered bare or electrically insulated by a temperature-resistant plastic socket. In the latter case, the set is pressed inside a flat aluminum tube, with two side leads for electrical connection, insulated from outside by the temperature-resistant material, as depicted in Figure 1. The generic commercial PTCs are specified barely by a few parameters: (i) the recommended supply voltage V_s , in our case 36 V, (ii) the minimum resistance temperature T_m , (iii) T_C , or an intermediate one. Eventually, some nominal or maximum acceptable parameters are available, such as (iv) the recommended power W_{op} although this is rarely specified, and/or (v) the maximum continuous temperature; and (vi) the maximum or breakdown voltage. Being PTCs a distributed resistor, as the electrode area increases, the usable power is proportional to it, and the resistance is

inversely proportional, ceteris paribus. The unloaded resistance vs. temperature can be measured by heating the PTC and offline immediate measuring R , Boubour [53]. Thermally insulating the PTC allows for surpassing T_c . An operating resistance can be obtained as $R_{op} = \frac{V_{op}^2}{W}$. This method does not give exactly the same result presumably because of self-heating, Musat [54].

In our case, after a measuring campaign, using type K thermocouples, batteries for heating the PTCs, and a multimeter for measuring resistance, voltage, and DC intensity, $R(T)$ has been obtained. Eq. (4) shows the data fitting expression for here proposed for the PTC resistances used for loading the PV panel. The rationale of the proposed expression is that the thermal coefficients α apply smoothly around the minimum resistance $R_m \cong R_0$ through the combining exponent n .

$$\begin{cases} T < 0.87 T_c \rightarrow R = R_0 \left[1 + \left\{ \exp \left[-\alpha_{low} \left(T - 0.19 \frac{T_c}{^\circ\text{C}} \right) \right]^n \right\} \right]^{1/n} \\ \text{otherwise} \rightarrow R = R_0 \left[1 + \left\{ \exp \left[\alpha_{high} (T - T_c) \right] \right\} \right]^{1/n} \end{cases} \quad (4)$$

Eq. (5) indicates the appropriate values found for several samples tested of generic encapsulated PTCs with active size of 35×21 mm and a recommended supply voltage of 30 V giving at R_0 a maximum power of 162 W. This size is from now on called “half size”. When applying the fitting function, the minimum resistance resulted $R_m = 7.03 \pm 1.0 \, \Omega$, $R_{25^\circ\text{C}} = 25 \pm 5.0 \, \Omega$, and the fitted $T_c = 256 \pm 6 \, ^\circ\text{C}$ with $R_{T_c} = 15 \pm 1.0 \, \Omega$, and $0.19 T_c^\circ\text{C}^{-1}$ is an empirical value. Figure 1 shows the resulting continuous function and the experimental variation found.

$$T_c = 250 \, ^\circ\text{C}; R_0 = 7 \, \Omega; n = 1.5; \begin{cases} \alpha_{low} = 0.04 \\ \alpha_{high} = 0.067 \end{cases} \quad (5)$$

Neither the applied power nor the load resistance of a single PTC element can be suitable for all the range of G and T so that a number $P \geq 1$, $S \geq 1$ of respectively in-parallel connection of P sets and of in-series strings of S elements are considered to load the PV panel. This way, the total resistance becomes $\frac{R}{Z}; Z = \frac{P}{S}$. $P = 2, S = 1 \Rightarrow Z = 2$ is anticipated as suitable in our case, but at the limit for dissipating the herewith PV panel rated power at a PTC temperature corresponding to R_0 , what does not have to occur. The following section illustrates this point.

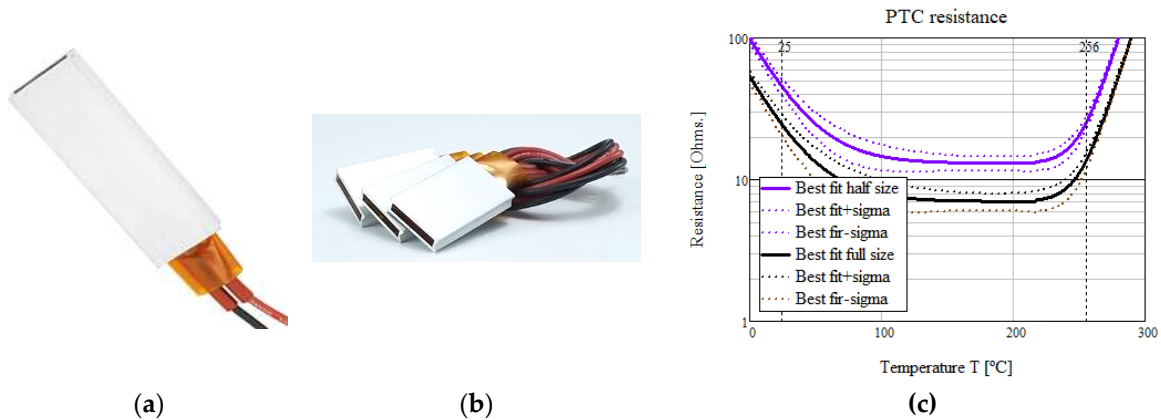


Figure 1. (a) View of a generic PTC heater selected as an example of full size; dimensions 60×21×5 mm, near to $Z = 2$ aprox. (b) half size dimensions 35×21×5 mm, $Z = 1$. (c) Single PTC resistance vs. its temperature resulted from the fit, showing the standard deviation of the performed measurements, full and half sizes.

3.3. Direct matching of the PV panel with the PTC heater

This section calculates the useful power that results when connecting both the selected PTCs and the PV panel, specifying T_p but leaving free G and T . When compared with the power at the MPP at each T_p and G condition, one can figure out how far from optimum is the operating point. Figure 2 shows the results for the (a) and (b) fits for $Z = 2$ with half size PTC heaters. Differences between both panel fits are negligible, as the knee of the curves are only marginally affected. For the two in-parallel identical half-size PTCs selected in this case, and for low G , power is close to the MPP for a

wide range of T but separates progressively for $G \gtrsim 600 \text{ W m}^{-2}$, suggesting that a lower resistance would be more suitable.

This $Z = 2$ connection also suffers from another limitation. The recommended maximum power through each single PTC of $W_{1\text{limit}} = 65 \text{ W}$ is surpassed when $@ T < 265^\circ\text{C}$ and $G \geq 150 \text{ W m}^{-2}$. The excessive power will be limited for $T \cong 265^\circ\text{C}$ but separating progressively from MPP as G increases. Even duplicating $W_{1\text{limit}}$, the $Z = 2$ connection restricts near optimum power for low G s, as Figure 5 shows.

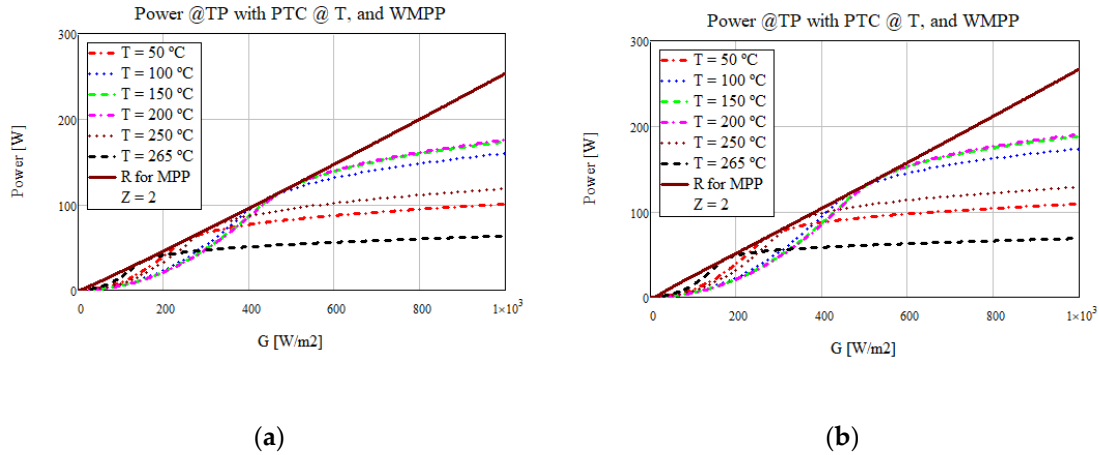


Figure 2. Steady-state power with $Z = 2$ at different PTC temperature T . Also W_{MPP} is plotted for comparison. (a) curve fit (a). (b) fit (b).

A more progressive stair of higher to lower resistances range would be to have 6 of the widely available half-size of the selected PTCs for an in-parallel layout and three switches. The possible single connections positions are:

- Position 1: Switch 1 ON and the others OFF, 1 PTC connected ($P = 1, S = 1 \Rightarrow Z = 1$), highest resistance.
- Position 2: Switch 2 ON and the others OFF, 2 in-parallel PTCs are connected ($P = 1 + 1 = 2, S = 1 \Rightarrow Z = 2$).
- Position 3: Switch 3 ON and the others OFF, 3 in-parallel PTCs are connected ($P = 3, S = 1 \Rightarrow Z = 3$).

This way, combining the three ON/OFF in-parallel switches makes six different equally stepped combinations of half-size PTCs: Position 1, 1 PTC active. Position 2, 2 PTCs active or a single full-size one. Position 1+Position 2 activating 3 PTCs, so that $Z = 1 + 2 = 3$, equivalent to Position 3 alone. Position 3 + Position 1, $Z = 4$. Position 2 + Position 3, resulting in 5 active PTCs, $Z = 5$. Position 1 + 2 + 3, all switches ON, $1 + 2 + 3 = 6$ in-parallel resistances, $Z = 6$. No in-series resistances have been contemplated in the present design as the voltage of a single PV panel is acceptable for the PTCs considered. Several in-series PV panels to multiply power could be contemplated but using a higher unsafe voltage. In parallel equal PV panels would require less load resistance, thus a high Z , not only to match them but for avoiding PTCs overload.

As a comparison with Figure 2, Figure 6 shows two cases with more resistances. Both $Z = 4$ and $Z = 6$ can be near MPP for large values of G , but they separate for low values of G , indicating that a low value of Z is necessary for low values of G for approaching MPP, indicated in Figure 5. For $Z = 4$, $W_{1\text{max}} = 65 \text{ W}$ and for $Z = 6$ $W_{1\text{max}} = 32 \text{ W}$, both happening at $G_{pe} = 1 \text{ kW m}^{-2}$ and for $T < T_C$. Both figures corroborate the suitability of the connection scheme using 3 switches indicated above. Curiously, $K = 6, T = 50^\circ\text{C}$ is near MPP @ $G_{pe} = 1 \text{ kW m}^{-2}$ but unless a cold object is in good thermal connection with the PTCs, heating will occur immediately, making this equilibrium solution not realistic. This calls for a time marching analysis.

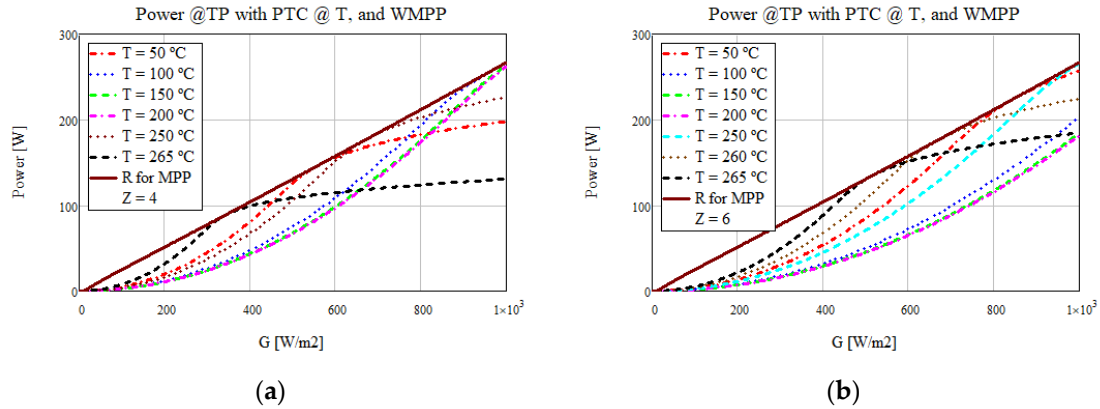


Figure 6. Steady-state power at different PTC temperature T . (a) with $Z = 4$. (b) with $Z = 6$.

The PTC temperatures can temporarily be different among them e. g., during heating, when there are some of them recently connected, thus still having a lower temperature than the others located side by side that have been operating for a longer time, thus with self-heating. In a short time, PTCs temperature homogeneity is reached owing for the low heat capacity of the PTCs.

This exercise clears the intervening non-directly-controllable factors, G and T , besides T_p . There is some way for the operator (or the controller) to select T , the PTC temperatures, by switching a number of them, and depending on the pot's temperature. Two examples are offered in Section 4 to illustrate these issues.

3.4. Practical maximization of power

As PTC resistances can only be modified by their temperature, the remaining possibility is to switch a combination to approach the MPP as much as possible, as analyzed in the previous section. This can be performed by a continuously operating perturb and observe technique. An automatic version would switch resistances through CMOS electronic elements, [53], preferably in the correct direction toward MPP, using a programmable microcontroller, and stay if there is an increase in W . This requires electronics.

A straightforward alternative technique is to offer the user both a Wattmeter (electronic), which nowadays can be purchased at a moderate cost (around 4 €), and manual switches so that the operator decides. After a learning period, the correct manual selection can be anticipated. In the specific layout selected here, the following exercises corroborates that only large resistances seem advantageous for the lower irradiances G to approach the necessarily low maximum power. An additional consideration is that low G s means low W so that approaching the MPP is of less importance than for high G s.

4. Time-marching modeling of the solar cooker

4.1. Preliminaries

For heating a non-flowing bulk thermal capacity C , the steady-state temperature has been modeled by Wang [55] in a simplified layout similar to the one in this work, obtaining a dimensionless correlation for the dimensionless overtemperature $\theta = T - T_{at}$. Here the model is refined by including the transient stage. A single lumped parameters 0D heat balance model of the entire system is used for our purpose, Eq. (6). No ohmic losses are considered between the panel and the PTCs.

$$C \frac{dT}{dt} = \frac{W}{V} - UA(T - T_{at}); \quad C = C_{PTC} + C_p + C_{pot} \quad (6)$$

UA is the heat loss conductance through a control surface A in the heat path toward the atmosphere, with an overall heat transfer coefficient from the system to ambient U . This equation

allows determining the shared system temperature T . Again, both I and V are such that $W = W(T, T_p, G)$. The stagnant (steady-state) temperature T_s is determined by $W(T_{ss}, T_p, G) = UA(T_{ss} - T_{at})$ where U would depend on T and other operating parameters, such as external wind and T_{at} .

This model is similar to the one proposed by Musat [54]. For this equation to be accurate, the Biot number Bi of the thermal mass of the system must be low enough, Incropera [56], Eq. (7). Considering an axisymmetric internal layout, the radial temperature gradient is considered negligible in front of the axial one. **Error! Reference source not found.** depicts the cylindrical layout for the prototype. It consists of the PTCs below the flat heated plate of diameter D_p and the closed pressurized pot above it of average diameter D_p and height $H_{pot} = 0.07$ m. The overall height of PTCs, plate, pot, top and bottom insulation, considering sphericity, is $H \cong D_p = 0.14$ m. Let us consider the in-series elements in the 1D geometry: from the PTC, plastic socket (s) + aluminum wall (a) Figure 1, to the flat hot plate (p), from the plate to the pot's inner bottom (pot), and from it to the liquid inside the pot (f). The external cylindrical closed surface that can be the result of a tight insulation wrapping $A_{in} = \frac{\pi}{4}(D_p + 2\delta_{in})^2 + \pi(D_p + 2\delta_{in})H$ is of similar extent than a spherical one $A_{in} = \pi(D_p + 2\delta_{in})^2$. The relation between the Biot number and the effective heat conductivity k from PTCs to water is, Eq. (7).

$$Bi = \frac{UA}{\frac{k}{H_{PTCW}}A_p}; H_{PTCW} = \underbrace{H_s}_{0.1 \text{ mm}} + \underbrace{H_a}_{1.2 \text{ mm}} + \underbrace{H_p}_{6 \text{ mm}} + \underbrace{H_{pot}}_{1.5 \text{ mm}} + \underbrace{H_f}_{\cong D_p/2} = 79 \text{ mm} \quad (7)$$

$$\delta_{in} = 20 \text{ mm}; \frac{A}{A_p} = \frac{\pi(D_p + 2\delta_{in})^2}{\frac{\pi D_p^2}{4}} = 6.6$$

This leads to Eq. (8), expressing the compound effective internal heat path length of the set H_H and the effective axial heat conductivity k :

$$\left(\frac{k_{PTCW}}{H_{PTCW}}\right)^{-1} = \left[\left(\frac{k_s}{H_s}\right)^{-1} + \left(\frac{k_a}{H_a}\right)^{-1} + K_{PCT/p}^{-1}\right] \frac{A_{PTC}}{A_p} + \left(\frac{k_p}{H_p}\right)^{-1} + K_{p/pot}^{-1} + \left(\frac{k_{pot}}{H_{pot}}\right)^{-1} + h_f^{-1} \quad (8)$$

According to Incropera [56] and Thermopedia [57], the contact thermal conductance K between flat surfaces under low joining pressure (screws for each PTC) can be estimated as $K_{PTC/p} \cong 1.4 \times 10^4 \frac{\text{W}}{\text{m}^2 \text{K}}$. For the plate/pot estimate, a realistic value can be orders of magnitude lower than the PCT/plate value because of the much less joining pressure (gravity) and the more extensive area of contact between the plate and the pot's "flat" surfaces. This is in addition to the larger thermal distortions of flatness plus the typical high roughness of pot bottoms. $K_{p/pot} \cong 1.4 \times 10^3 \frac{\text{W}}{\text{m}^2 \text{K}}$ is assumed, as a conservative value, taking into consideration that a pure conductive air layer of 0.1 mm thickness would give $K_{p/pot} = 320 \frac{\text{W}}{\text{m}^2 \text{K}}$. The result is, considering equal transfer areas $(K_{PCT/p}^{-1} + K_{p/pot}^{-1}) = 0.79 \times 10^{-3} \frac{\text{m}^2 \text{K}}{\text{W}}$. The conductivities of the materials of the plates are, for Kapton® PTC socket, $k_s = 0.20 \frac{\text{W}}{\text{mK}}$, aluminum cover $k_a = 240 \frac{\text{W}}{\text{mK}}$, brass hot plate $k_p = 150 \frac{\text{W}}{\text{mK}}$, and steel pot wall $k_{pot} = 35 \frac{\text{W}}{\text{mK}}$. One can estimate, according to [56], for the non-boiling oil or water, a heat transfer coefficient from the pot bottom to the liquid bulk $h_f = 50$ to $1.000 \frac{\text{W}}{\text{m}^2 \text{K}}$. We can adopt an average value of $h_f = 500 \frac{\text{W}}{\text{m}^2 \text{K}}$. All this results from Eq. (8) in $k_{PTCW} = 14.5 \frac{\text{W}}{\text{mK}}$. This small number suggests instead of a single temperature model, a more complex one made of two or three bulk thermal masses. Section 4.2.1 analyzes this issue.

A value for U can be estimated as an in-series of (i) atmospheric heat transfer and (ii) thermal insulation of a non-technical (discarded tissues, hay, dry leaves, ...) insulating material of an effective conductivity $k_{in} \cong 0.2 \frac{\text{W}}{\text{mK}}$, larger than usual because of the relative tight wrapping, the non-continuous covering and no external impervious cover. Taking into account a spherical external geometry, **Error! Reference source not found.**, also accepting moderate wind convection and radiation to the environment, this sums up a heat transfer coefficient $h_{outside} \cong 12 \frac{\text{W}}{\text{m}^2 \text{K}}$, according to Rahmadi [58]. The radial conductance of the sphere shell is $A_{in}U_{in} = \frac{2\pi k_{in}}{D_p^{-1} - (D_p + 2\delta_{in})^{-1}}$. Summing up,

the results is $UA = A_{in}[U_{in}^{-1} + h_{outside}^{-1}]^{-1} \cong 0.48 \frac{W}{K}$, the insulation effect in dominating this amount. This figure has been determined as realistic, although in the upper range, according to own experimental results. All this ends up in $Bi \cong 0.09$ applying Eq. (7). This value is low enough to expect a fairly homogeneous internal spatial 1D temperature, as $Bi \lesssim 0.1$ is the practical limit for accepting thermal homogeneity [56]. A precise thermal homogeneity happens after a relaxation time τ_h following the stop of heat generation, what is called the cooling process. From the 1D heat diffusion equation by conduction, for our design with $D_p \cong H$, considering that $C_{pot} \gg C_{PCT} + C_p$ such that $\frac{dT_{pot}}{dT} = 0$ during this period, Eq. (9) yields its order of magnitude.

$$\tau_h = \frac{C_{PCT} + C_p + C_w}{H_{PTCw}k_{PTCw}} \sim 9.7 \text{ min} \quad (9)$$

This τ_h , is much smaller than the free cooling time τ_{coo} with $W = 0$, Eq. (11), allowing to accept full thermal homogeneity during the cooling process as a good approximation.

The Biot number reasoning is strictly valid for no internal heat generation, and we have heat generation on the lower border. Following this consideration, to estimate the maximum internal temperature difference $\Delta T_{ss,max}$, adiabatic 1D heat flow from the PTCs is considered at half the maximum panel power owing to the power profiles in **Error! Reference source not found.** and **Error! Reference source not found.**. This leads to Eq. (10), which assumes the maximum panel power accepting equal heat losses than electric input under steady-state operation $_{ss}$. Using m, kg, K, and s as units, result is Eq. (10).

$$\Delta T_{ss,max} \sim \frac{\frac{W_{max}}{2} H_{PTCw}}{A_p k_{PTCw}} = 22 \text{ K} \quad (10)$$

If boiling water in the open air, it happens at $\cong 100^\circ\text{C}$; then, T_c seems not to happen considering the roughly estimated thermal parameters. The maximum power will be reached with the appropriate resistors, according to Figure 1, as the low resistance PTC plateau will be reached even in this case. When heating oil or heating water up to pressurized boiling, according to Figure 1, the PTCs will also reach the low resistance plateau and even can reach T_c so that heating can proceed with high power up to the limiting T_c when power will stagnate.

To obtain preliminary information on the possibilities of the cooker as a function of the solar irradiance, the numerical resolution of a time marching equation, Eq. (6), seems necessary. One must keep in mind that it deals with an average temperature. It gives quick information on the possibilities of the cooker, leaving for more complex models the discrimination between the temperatures of the different elements (e. g. a three-lumped-heat-capacities model, PTCs, hot plate, and pot commented in Section 4.2.1. Here, with a single lumped heat capacity, the rise of the temperature of the PTCs seems underestimated by an amount in the order of the result of Eq. (10).

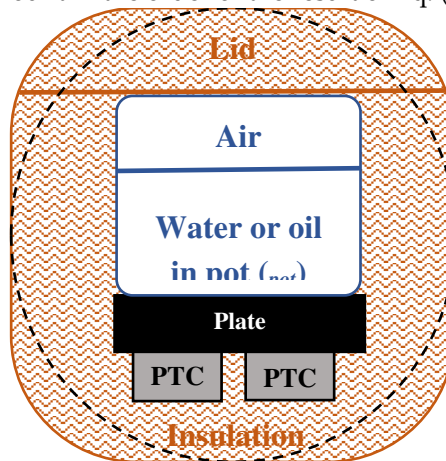


Figure 7. Layout of the PV solar cooker set, not in proportion. Indicates sphere used for UA as a dashed line.

4.2. 0D Time marching results

Two reference scenarios are relevant: heating with (i) Constant irradiance, and (ii) cloudless day irradiance pattern. For simplicity, both use the PV panel curve fit with constant T_{at} and $T_p = 70^\circ\text{C}$. Cooling with $G = 0$ follows. For both cases, Eq. (6) has been numerically integrated using an explicit Euler scheme. Data at time step i allow obtaining $T\langle i+1 \rangle$, as $\frac{dT}{dt} \cong \frac{T\langle i+1 \rangle - T\langle i \rangle}{\Delta t}$, with some loss of accuracy but facilitating the use of spreadsheets. Solar time starting at sunrise is used in the cases solved. The resistance maximizing W has been calculated and is named R_{MPP} .

The cooking medium has been represented by 1.08 l of pressurized water so that no boiling is allowed. Alternatively, glycerin weighting $m = 1.7\text{ kg}$ of average specific heat $c = 2.67 \frac{\text{kJ}}{\text{kg K}}$ equaling the heat capacity of water. This is for mimicking frying. With Eq. (6) one can check that the characteristic cooling time when $\frac{T - T_{at}}{T_{max} - T_{at}} = \exp(-1)$ can be obtained by setting $I = 0$ and constant parameters:

$$\tau_{cool} \sim \frac{\overbrace{C_{PTC} + C_p + C_{pot}}^c}{UA} = 3.0\text{ hr} \gg \tau_h \quad (11)$$

In practice, $C = \sum_i m_i c_i$ is easily determined, but not so easily UA . During a cooling experiment, measuring the temperature time marching results in a series, having T_i at each time t_i , $(UA)_i$ can be determined on the grounds of Eq. (6), resulting in Eq. (12). The resulting series can be improved by an eventual moving average smoothing to remove noise, Lecuona-Neumann [41].

$$(UA)_i = \frac{(mc)_i}{T_i - T_{at,i}} \frac{T_{i+1} - T_{i-1}}{t_{i+1} - t_{i-1}} \quad (12)$$

These values of UA_i can be used for further studies. Here, the datum already theoretically calculated has been used as it resulted coherent with own experimental values.

- **For constant maximum radiance.** The constant G_{pe} for several hours can be attempted if tracking the sun. It would be representative of starting 3 hours before noon and using the solar power up to 3 hours after noon, even without tracking. As a general case, after reaching the maximum temperature, stopping power reveals the free cooling process after $t_{end} = 6\text{ hr}$. According to Figure 7, gives slow cooking ($T > 70^\circ\text{C}$) for 5 hr after t_{end} and warm food for almost 10 hr after, ensuring warm dinner. Halving UA , e. g. duplicating the insulation thickness, approximately duplicate these times, ensuring warm food for breakfast next day.

Error! Reference source not found. shows the results for three representative cases $Z = 2, 4$ and 6 . The maximum temperature is achieved after $t \cong 2.5\text{ hr}$, being for $Z = 6$ the highest, 272°C . Reduction in power follows owing for surpassing T_c in all three Z s. For all the cases, starting at 9:00 a.m. solar time, after 7 hours, around 9+6 = 3 p.m., the temperature is high enough for cooking.

Power reductions after some hours of heating, in **Error! Reference source not found.** right, indicate that PTCs have reached the maximum temperature, beyond T_c , and there is extra power available if the cooking process required to heat food by immersion and/or evaporating water. In that case, the food would reduce the maximum temperature found for the PTCs, automatically increasing W . The individual PTC maximum recommended power of $W_{1max} = 65\text{ W}$ is surpassed for $Z = 2$ but not for $Z = 4$ and 6 . The solar efficiency, Eq. (13), for the invariable three Z s reaches $\eta_{solar} \cong 7\%$. In the case of MPPT it would raise up to $\eta_{solar,max} = 13\%$. If there is a wise selection of the available PTCs, an intermediate case would be the result.

$$\eta_{solar} = \frac{\int_0^{t_{enf}} W dt}{G_{pe} \times A_P}; \quad \eta_{solar,max} = \frac{W_{max}}{G_{pe} \times A_P} \quad (13)$$

In the same **Error! Reference source not found.**, the low PTC temperature from hours 0 to 2 hr help to deliver heat. But this is uncertain because the single bulk temperature model adopted, which

is limited. In reality, the PTCs under G_{pe} self-heats in a short characteristic time τ_{PTC} . Neglecting heat conduction and losses to ambient, as $C_{pot} \gg C_p \gg C_{PTC}$, the heating characteristic times differ, following Eq. (14), where half the power and half the temperature increase are considered.

$$\begin{aligned} \bar{W} &\stackrel{\text{def}}{=} \frac{W_{max}}{2}; \bar{\Delta T} \stackrel{\text{def}}{=} \frac{\theta_C}{2}; \tau_{PTC} \sim \frac{C_{PTC} \bar{\Delta T}}{\bar{W}} = 54 \text{ s}; \tau_{PTC+p} \sim \frac{(C_{PTC} + C_p) \bar{\Delta T}}{\bar{W}} = 4.5 \text{ min}; \\ \tau_{PTC+p+pot} &\sim \frac{(C_{PTC} + C_p + C_{pot}) \bar{\Delta T}}{\bar{W}} = 1.3 \text{ hr} \end{aligned} \quad (14)$$

As a result of these considerations, the PTCs could be in the low resistance plateau, near T_C and correspondingly near R_{MPP} after ≈ 1 minute. After about 12 minutes, both the PTC and the hot plate can be near T_C , while the pot is at almost T_{at} . Only after about 2.2 hours, the full system can be near T_C . Thus, the initial high resistance R indicated in **Error! Reference source not found.**(center) seem not to happen unless the conductivities from the PTCs to the hot plate and pot are very high, and this does not seem to be the case for the high value of τ_h , Eq. (9).

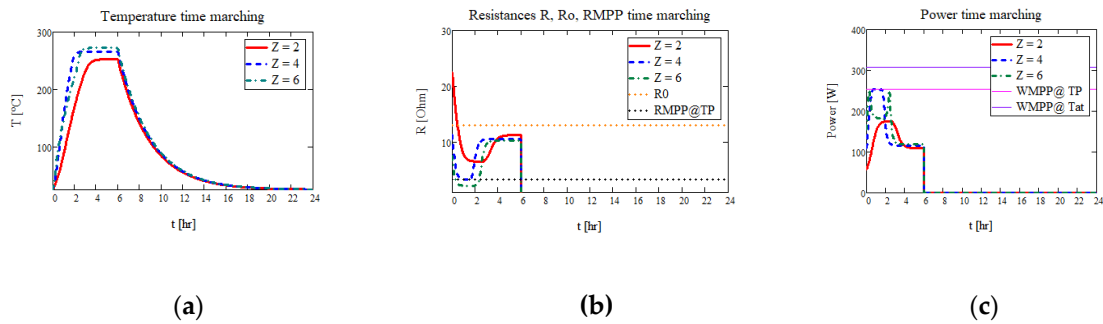


Figure 8. Time marching at G_{pe} , stopping after 6 hr, using glycerin or pressurized water for three values of Z . Left) Power. Center) Resistances. Right) Power and MPP for $T_p = 70$ °C and $T_p = T_{at}$ panel temperatures.

A higher-order modeling will be helpful for differentiate the PTC/p joint heating. Only discerning the three temperatures, PTCs, plate, and pot, this issue can be described in detail. The short time effect can be an increase of power owing to the PTC reaching the low resistance plateau or can be limiting after reaching T_C .

Error! Reference source not found. shows the extreme case when the pot contains a larger heat capacity, 10 times the one already calculated. Correspondingly, UA is estimated as 3 times larger owing to the larger size, although its influence in the case analyzed is small. The model allows us to accept that the same result would be obtained keeping all the previous data, but with $G = \frac{G_{pe}}{10} = 100 \text{ W m}^{-2}$, typical of an overcast day. Only for $Z = 6$ boiling temperature is reached after 6 hours, just when power ceases. Total resistance for both $Z = 4$ and 6 are near R_{MPP} , corroborated by the power time marching, near $W_{MPP} = W_{max}$. Both reach $\eta_{solar} \approx 10\%$, which is near the maximum, Eq. (13).

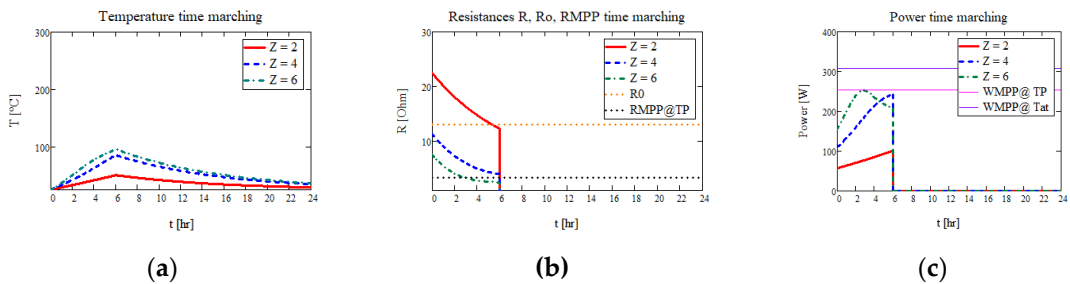


Figure 9. Time marching at G_{pe} , with same data than **Error! Reference source not found.** but 10 times heat capacity and 3 times UA .

- **A cloudless summer day.** A sinusoidal time distribution approaches reasonably well the irradiance falling on the aperture area of a PV panel even without solar tracking, aimed to the equator with a tilt near the maximum solar elevation at solar noon. At the solstice it last $t_d = 14$ hours and reaches G_{pe} , Eq. (15).

$$G(t) = \begin{cases} G_{pe} \sin\left(\pi \frac{t}{t_d}\right) & |_{t \leq t_d} \rightarrow G(t)|_{t \ll t_d} = G_{pe} \pi \frac{t}{t_d} \\ 0 & \text{for } t > t_d \end{cases} \quad (15)$$

This gives a characteristic heating time of several hours, alleviating the possibility of temperature internal differences that have been addressed in the previous paragraph.

If one imposes a fixed PTC temperature of the low resistance plateau, Figure 1, the power can approach very well $W_{max}(t)$, as **Error! Reference source not found.** indicates with $Z = 6$ with some fault near sunrise and sunset. If PTC temperature follows Eq. (6) the results are depicted in **Error! Reference source not found.**

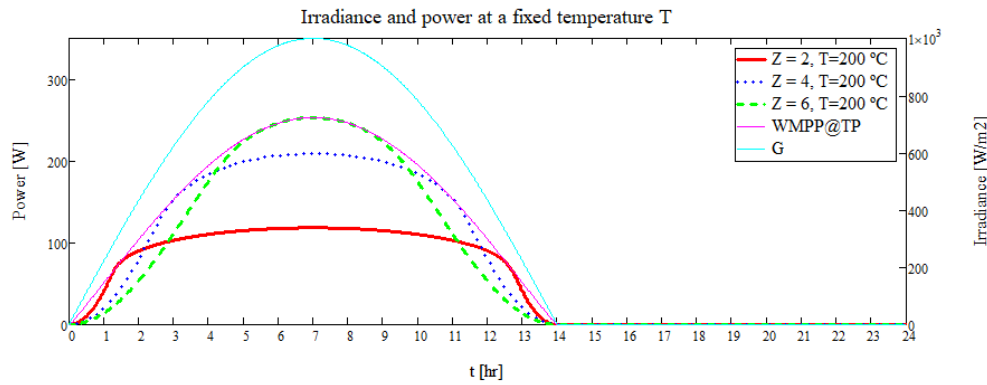


Figure 10. Time marching of power with sinusoidal irradiance G and fixed PTC temperature for three in-parallel PTCs.

One can notice that the higher resistance for $Z = 2$ fits very well R_{MPP} for the first 2 hours but fails on giving power at elevated G s after 6 hr; also, individual PTCs are overloaded. With $Z = 4$, after 5 hr, T_c is reached, limiting power. The case $Z = 6$ follows about 1 hr later and reaches a higher temperature, **Error! Reference source not found.**

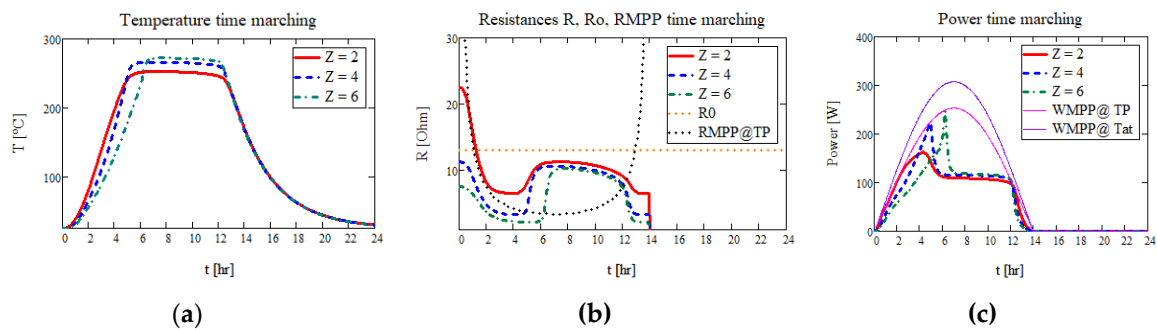


Figure 11. Time marching with sinusoidal profile irradiance, $T_p = 70$ °C. Left) Temperature Center) Resistances: arrangement of the selected PTCs, R_{MPP} and individual R_0 . Right) Power and maximum PV power for $T_p = 70$ °C and $T_p = T_{at}$.

The power time marching, **Error! Reference source not found.** Right) shows that starting with $Z = 2$, switching to $Z = 4$ at $t = 4$ hr after sunshine and switching to $Z = 6$ at $t = 6$ hr approaches $W_{max}(t) = W_{MPP}$ quite well up to power limitation after $t = 7$ h.

The maximum heat available from the panel, with R_{MPP} and no thermal losses can be the reference for the energy efficiency η_d of the solar cooker alone, thus not including the efficiency of the PV panel, Eq. (16). The results are, 0.62, 0.62 and 0.59 for respectively $Z = 2, 4$, and 6 , calculated with data from **Error! Reference source not found.** If the entire sinusoidal profile is reduced to 50%,

power limiting is not reached as $T\langle t \rangle < T_c$. The efficiencies change to $\eta_d = 0.91, 0.51$, and 0.37 , respectively, highlighting the convenience of large resistances for low G s, e. g. $Z = 2$.

$$\eta_d = \frac{\int_0^{t_d} W dt}{\int_0^{t_d} W_{MPP, T_P} dt} \Big|_{T_P} \quad (16)$$

4.2.1. Three bulk thermal masses

The results and especially, values for η_d , are a first estimation, as the resistance increase of the PTCs at ambient temperature, already approaching R_{MPP} , could not be accurate. This is a limitation of the single thermal inertia model that equals all the temperatures. Eq. (17) indicates a three thermal inertia model: PTC, hot plate, and pot with its content.

$$\begin{aligned} \text{(a): } C_{PTC} \frac{dT_{PTC}}{dt} &= IV + K_{PTC/p} A_p (T_p - T_{PTC}) - UA_{PTC} (T_{PTC} - T_{at}) \\ \text{(b): } C_p \frac{dT_p}{dt} &= K_{PTC/p} A_p (T_{PTC} - T_p) + K_{p/pot} A_p (T_{pot} - T_p) - \\ &\quad UA_p (T_p - T_{at}) \\ \text{(c): } C_{pot} \frac{dT_{pot}}{dt} &= K_{p/pot} A_p (T_p - T_{pot}) - UA_{pot} (T_{pot} - T_{at}) \\ A &= A_{PTC} + A_{pot} \end{aligned} \quad (17)$$

The PTC and hot plate lateral areas are considered negligible in front of the lateral, bottom, and top, respective areas of PTC and pot, **Error! Reference source not found.** U is common to PTC, plate, and pot.

It can be noted that, for the particular case of $T_{PTC} = T_p = T_{pot}$, the summation of (a) to (c) equations in Eq. (17) gives Eq. (6) with $C = C_{PTC} + C_p + C_{pot}$.

The previous section indicated that Eq. (6) was not appropriate for early times. Here a further insight on the early times seems illustrating. It can be considered that $C_{pot} \gg C_p \gg C_{PTC}$. Also, on the grounds of $K_{PTC/p} \gg K_{p/pot}$ one can assume for the initial times that $T_{PTC} = T_p$; $T_{pot} = T_{at}$. Accepting the definitions of Eq. (18) summation of Eq. (17)(a) and (b) results in Eq. (19), considering Eq. (15).

$$\theta \stackrel{\text{def}}{=} T_{PTC} - T_{at}; \tau_K \stackrel{\text{def}}{=} \frac{\frac{C_{PTC} p}{C_{PTC} + C_p}}{A_p K_{p/pot} + UA_{PTC+p}} \cong \frac{C_p}{A_p K_{p/pot}} \quad (18)$$

$$\frac{d\theta}{dt} + \frac{\theta}{\tau_K} = \frac{IV}{C_{PTC+p}} \stackrel{\text{def}}{=} wt \quad (19)$$

This last equation assumes a linear power increase to approach the initial stages of Eq. (15). As a result, this equation has an analytic solution given by Eq. (20) in non-dimensional terms, assuming as initial condition $t = 0 \rightarrow \theta = 0$:

$$\frac{\theta}{w\tau_K^2} = \left[\frac{t}{\tau_K} - 1 + \exp\left(-\frac{t}{\tau_K}\right) \right] \quad (20)$$

This solution indicates a temperature linear increase versus the non-dimensional time t/τ_K plus an exponential heat loss, negligible for $\frac{t}{\tau_K} \gg 1$, with τ_K the characteristic time, thus $\theta \rightarrow \theta_{K\infty}$. Eq. (21) gives the values for τ_K and w , according to Eq. (18) and assuming MPP invoking the correct PTC resistance in the initial times.

$$\begin{aligned} \tau_K &\cong \frac{C_{PTC} m_{PTC} + C_p m_p}{A_p K_{p/pot}} = 16 \text{ s} \\ w &= \frac{W_{max} \pi}{t_d C_{PTC+p}} = \frac{253 \text{ W} \times 3.1416}{14 \times 3600 \text{ s} \times 353 \text{ J K}^{-1}} = 4.5 \times 10^{-5} \text{ K s}^{-2} \end{aligned} \quad (21)$$

This makes, Eq. (22).

$$\theta_{K\infty} = w\tau_K t = \pi \frac{W_{max}}{A_p K_{p/pot}} \frac{t}{t_d} \quad (22)$$

Eq. (20) and (22) with data from Eq. (21) predict a quite slow and low temperature increase, thus removing the worry of initial times elevated temperatures, owing to the large conductance towards the pot here assumed and its very large heat capacity. If this conductance is ignored, an adiabatic evolution occurs, e. g. unloaded cooker. Then, the reduced differential equation and its solution is Eq. (23), which includes the value of w in Eq. (21). It shows a larger overtemperature versus time. This indicates the importance of the heat transport to the pot.

$$\left. \begin{array}{l} \frac{d\theta}{dt} = wt \\ t = 0 \rightarrow \theta = 0 \end{array} \right\} \rightarrow \theta = \frac{W_{max}}{C_{PTC+p}} \frac{\pi}{2} \frac{t^2}{t_d} \quad (23)$$

On the other hand, if one assumes constant maximum power W_{max} , the solution of the full differential 0D equation for the subsystem PTC+p, Eq. (6), with $T_{at} = \text{cnt.}$ and $t = 0 \rightarrow \theta = 0$, results in Eq. (24), but with only C_{PTC+p} for the initial times here considered. At these initial times, where the loaded cooker has the pot near ambient temperature, while the PCTs and hot plate are rapidly heating, their thermal losses conductance to the atmosphere is meager, $UA_{PTC+p} \ll UA$, being one half to one third an upper estimation, according to **Error! Reference source not found.** Thus, the full solution, Eq. (24), can be approached by the initial evolution, giving Eq. (25), valid for $\frac{t}{\tau} \ll 1$ although τ is uncertain because the uncertainty in UA_{PTC+p} .

$$\theta_{PTC+p,max} = \frac{W_{max}}{UA_{PTC+p}} \left[1 - \exp\left(-\frac{t}{\tau}\right) \right]; \quad \tau = \frac{C_{PTC+p}}{UA_{PTC+p}} \quad (24)$$

If one estimates $UA_{PTC+p} = \frac{UA}{3} \rightarrow \tau = 37 \text{ min}$ making the initial approach justified.

$$\theta_{PTC+p,max} \Big|_{\frac{t}{\tau} \ll 1} \cong \frac{W_{max}}{UA_{PTC+p}} \frac{t}{\tau} = \frac{W_{max}}{C_{PTC+p}} t \quad (25)$$

Comparing Eq. (25) with Eq. (23), a PTC+p subsystem heating occurs faster with constant maximum power than with the sinusoidal time profile. Eq. (25) gives the initial time marching of $\theta_{PTC+p,max}$.

These solutions fail when heat losses to atmosphere are comparable to thermal inertia in terms of power, which occurs at time τ , or when the pot heating power becomes comparable to thermal inertia power, which is estimated in Eq. (14), which one becomes sooner. To analyze this issue and the resulting PTC+p temperature discrepancy with the pot, the full three thermal masses model needs further study.

As a conclusion, only with constant power from the beginning, comparable with the maximum power quantity, the initial overtemperature of the subsystem PTC+p can separate substantially from the pot temperature.

5. Conclusions

The proposed PV solar cooker allows indoor off-grid e-cooking and avoids electronics by directly connecting the right amount of PTC heaters to a solar panel or a plurality. No controller or battery charger is needed for its functioning, which can reach high efficiencies. The innovative design offers a better energy transfer from the PV panel to the cooker than linear resistors reaching an electrical energy efficiency of up to 91% for a particular operation, even without any PTC switching. PTCs offer resistance growth at their low temperatures and a temperature-limiting effect, avoiding overheating.

Simplified models have been developed to ascertain the adequate PV panel and PTC characteristics for this duty, illustrating the basic working and the relevant parameters. The energy and temperature-time evolution have been described by a transient 0D ordinary differential equation that allows the use of ordinary calculation methods such as spreadsheets, thus allowing dimensioning a system with a small budget. The differential equation has been numerically solved using two representative forcing functions: constant peak irradiance for midday operation and

sinusoidal irradiance mimicking a full-day operation. Both cases reveal relevant characteristics. A more complex three bulk thermal masses has been analyzed to highlight some features without having to solve the whole mathematical model.

Thermally insulating the outside of the cooker is of paramount importance, which, in this case can be performed with ordinary materials.

Switching several ordinary PTCs by any means offers the possibility of a wider energy match between the panel and the PTCs. The selected generic PTC heaters offer a good enough match for both low and elevated temperatures. Insufficient PTCs' resistance when starting cold with low irradiance can be overcome by disconnecting in-parallel PTCs and/or preheating either the empty pot or loaded with a small amount of oil for pre-cooking/frying or sauteing, as many recipes ask for.

Overcoming cloudy periods, extending cooking in the afternoon, and even cooking or heating breakfast before the next day sunrise is possible by heating a load of sensible Thermal Energy Storage (TES) or solid/liquid Phase Change Material (PCM). These replace batteries in the duty of cooking, keep the food warm, and extend the usability of PV solar cookers in a low-cost and environmentally friendly way. A single PV panel from the residential rooftop market with around a 2 m² aperture surface offers enough heat for cooking for an average family inside locations with good solar resources. This allows elementary indoor solar cooking and, in addition, other electrical services for fighting energy poverty.

Some issues need further research. Along with the running experimental campaign for characterizing the PTC performances, some unexpected phenomena have been experienced. When cooling, a sudden, short-time off-circuit resistance increase can happen at moderate temperatures. Additionally, a persistent low resistance can last until a slight shock returns to normal when reaching the ambient temperature. Whether this is caused by a PTC material phase change or by a contact deficiency must be investigated. Self-heating modifies the resistances of the PTCs; its relevance needs further research. Testing solar cooker prototypes under realistic conditions will illuminate the promising performances offered by the design.

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