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Carbon dioxide gas sensor based on polyhexamethylene biguanide polymer deposited on silicon Nano-cylinders metasurface

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Abstract: In this paper, we have numerically investigated a metasurface based perfect absorber design established on the impedance matching phenomena. The paper comprises of two parts. In the first part, the device performance of the perfect absorber is studied which is composed of a silicon Nano-cylindrical meta-atoms periodically arranged on the thin gold layer. The device design is unique which works for both x-oriented and y-oriented polarized light, besides independent of the angle of incidence. In the second part of the paper, CO₂ gas sensing application is explored by depositing a thin layer of functional host material polyhexamethylene biguanide polymer on the metasurface. The refractive index of the host material decreases due to the absorption of the CO₂ gas. As a result, the resonance wavelength of the perfect absorber performs a prominent blueshift. With the help of the proposed sensor design based on metasurface, the CO₂ gas concentration range of 0-524 ppm is detected. The maximum sensitivity of ~17.3 pm/ppm is acquired for the gas concentration of 434 ppm. The study presented in this work explores the opportunity of utilizing metasurface perfect absorber for gas sensing applications by employing the functional host materials.

Keywords: Metasurface; Carbon dioxide gas; Sensor; functional host material; Polyhexamethylene biguanide; Perfect absorber.

1. Introduction

Metamaterials are artificial structure with permittivity and permeability unachievable in nature have gathered much attention due to their incredible electromagnetic (EM) response. This the reason, metamaterials are considered to have a bright prospective in photonics. The EM properties of materials can be modified to acquire the preferred optical properties by engineering the metamaterials. In recent years, metamaterials based EM absorbers are widely researched [1-3] which shows its potential usage in solar photovoltaic and thermophotovoltaic devices [4], spatial light modulation [5] and sensing applications [6]. Based on the range of light spectrum absorbed by the EM absorber, it is categorized into two types: Narrowband EM absorber [7] and Broadband EM absorber [8]. Typically the dimensions of the metasurfaces are far beyond the wavelength, which substitutes the need for bulk optics and is therefore capable of nanoscale light manipulation [9, 10].

Several recent works on perfect absorbers (PAs) such as metacavity model having multilayer metasurfaces [11], electromagnetically induced absorption [12], subwavelength hole arrays [13, 14] and structured metal surfaces [15] have demonstrated perfect absorption phenomena. For practical purposes, PAs that are insensitive to polarization and the incident angle of light is typically desirable

[16]. These PAs can be employed in sensing applications based on the wavelength interrogation method.

For studying global warming and other environmental-related problems triggered by anthropogenic greenhouse gas discharges, accurate measurement of carbon dioxide (CO₂) gas concentration in the atmosphere is essential. Provided that the existing level of ambient CO₂ gas concentration is swiftly reaching the 400 ppm threshold, which is far above the 350 ppm threshold to prevent inevitable climate change [17], there is a growing need for miniaturized and precise CO₂ gas sensors that can be proficiently used in large-area sensor networks to track greenhouse gas concentration patterns. In health sciences, there is also a strong interest in CO₂ gas monitoring, as it reveals an essential role in several biological activities. Non-Dispersive Infrared Spectroscopy (NDIR) is established on the recognition of the signature absorption band of CO₂ at the 4.26 μm wavelength, is currently the prevailing CO₂ sensing technology. There are two main sensor configurations which can be used to detect the toxic gases such as evanescent field gas absorption [18-20] and resonance wavelength interrogation method [21, 22]. In our previous works [23-27], we have presented distinctive designs of gas sensors based on optical waveguides working on evanescent field absorption mechanism. Here, we have proposed an attractive arrangement of a metasurface formed by a periodic array of silicon Nano-cylindrical meta-atoms (MAs) deposited on a metal layer. This configuration offers a possibility to be employed as a narrowband PA. Moreover, when the metasurface is coated with a specific thin layer of a functional host material, it can function as a gas sensor.

2. Device design and theory

Metamaterials can be described by a complex electric permittivity and magnetic permeability

$\tilde{\epsilon}(\omega) = \epsilon_1 + i\epsilon_2$ and $\tilde{\mu}(\omega) = \mu_1 + i\mu_2$, respectively. The main concern, however, was on the real

part of permittivity (ϵ_1) and permeability (μ_1) for fabricating negative refractive index materials

[28]. However, the loss components of the optical constants (ϵ_2 and μ_2) are anticipated to create a

variety of practical uses such as PAs which can be employed as a filter and sensor. By regulating the resonances in ϵ and μ independently, it is conceivable to absorb both the incident electric and magnetic field. This kind of absorber exhibits tremendous merits over its conventional predecessors due to its compact size and extraordinary features. The key perception is to reduce the reflectance by impedance matching and concurrently discarding the transmittance by magnifying the metamaterial losses. In this work, we explored two potential applications of metasurface such as narrowband PA and CO₂ gas detection by utilizing a host functional polymer layer polyhexamethylene biguanide (PHMB) deposited on top of the metasurface.

2.1. Narrowband PA design

The schematic of the proposed metasurface based narrowband PA design is presented in figure 1. It is composed of a periodic array of silicon Nano-cylindrical MAs placed on the gold (Au) layer deposited on a quartz substrate. The inset shows the zoomed image of silicon cylindrical MAs of radius R placed on the Au layer. Moreover, the general transmission, reflection and absorption spectrum is also shown. The height of the silicon cylindrical MAs and the Au is denoted as H_{Si} and H_{Au} , respectively. The H_{Au} is fixed at 100 nm throughout the paper which is bigger than the skin

depth, therefore, it is modelled as a perfect electric conductor (PEC). Thus, the EM wave does not penetrate in the near-IR range and the transmission is nearly null. The gap between the two MAs is represented as $2d$ where d is the gap between MA and the boundary.

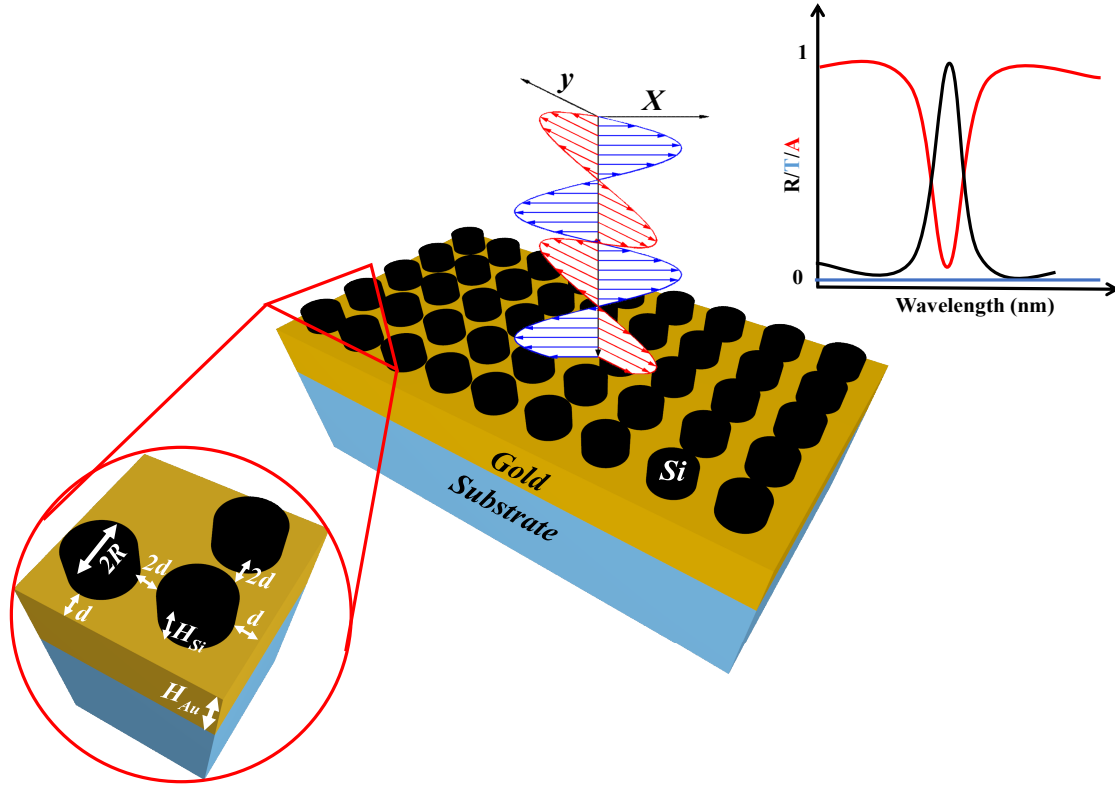


Figure 1. Schematic of a narrowband PA based on silicon nano-cylinders metasurface. Inset shows the silicon MAs periodically arranged on the gold layer (left-bottom). The transmission, reflection and absorption spectrum is also shown (right-top).

By considering a single unit cell, the additional simulation volume is avoided which leads to the reduced simulation time [29]. On four sides of the unit cell, Floquet-periodic boundary conditions are applied to mimic the unbounded 2D array. Due to the periodic boundary condition (PBC) applied on the lateral sides of the design, the distance between two MA is automatically doubled, i.e., $2d$. The refractive index ($n=1.0$) is filled in the domains above and below the absorber design which represents the air medium. The proposed absorber configuration is positioned between the source port and the output port. The source port emits the EM waves which are analyzed at the output port. Port boundary conditions are positioned on the inner boundaries of the perfect matched layers (PMLs), adjoining to the air domains which establish the transmission and reflection features in terms of S-parameters. Where S_{11} and S_{21} are the reflection and transmission coefficient that can be written as:

$$\text{Reflection: } S_{11} = \frac{(1-\Gamma^2)Z}{1-Z^2\Gamma^2}, \text{ Transmission: } S_{21} = \frac{(1-Z^2)\Gamma}{1-Z^2\Gamma^2} \quad (1)$$

$$\text{Where } Z = \exp(-jk_n n_{\text{eff}} L) = \exp(\pm \omega j \sqrt{\epsilon_{\text{eff}} \mu_{\text{eff}}} L) \quad (2)$$

L is the effective length, n_{eff} is the effective refractive index, ϵ_{eff} and μ_{eff} are the effective permittivity and permeability. Γ is the reflection coefficient which can be calculated as:

$$\Gamma = \frac{(Z_0 - 1)}{(Z_0 + 1)}, \text{ where } Z_0 \text{ is the relative impedance.} \quad (3)$$

The inner port boundaries with PMLs backing require the slit condition. For the calculation of S-parameter, the port direction is set to classify the inward direction. Since we are not interested in the higher-order diffraction modes, that is why the combination of domain-backed type slit port and PMLs are utilized in place of a diffraction order port for each diffraction order and polarization. The PMLs are employed to absorb the excited mode from the source port and any higher-order modes produced by the periodic structures. The PMLs diminishes the EM wave propagating in the direction perpendicular to the PML boundary.

2.2. Silicon Nano-cylinder metasurface coated with PHMB polymer layer for CO₂ gas detection

CO₂ is a colorless, odorless and non-flammable greenhouse gas typically generated by the combustion of carbonaceous materials or by the metabolism of animals [30]. The current CO₂ gas concentrations and its growth rates lead to global warming and unsustainable environmental challenges [31]. For that reason, high sensitivity CO₂ gas sensors have been widely researched to track patterns in the concentrations of greenhouse gases. As the concentration of the CO₂ gas in the ambient medium increases, the refractive index of functionalization layers changes. PHMB has basic amide-bearing functional groups, is a member of the guanidine polymer family [32]. It is an ideal contender for functionalization polymer layer that would be equally sensitive and selective to low concentrations of CO₂ at room temperature and atmospheric pressure. Additionally, the absorption and release of CO₂ gas of the material don't oblige water vapor to be applied, as is the case of previously reported functional materials [33]. The schematic of the gas sensor is shown in figure 2a and the inset shows the reflection spectrum in the absence and presence of CO₂ gas. Moreover, the chemical formula for CO₂ gas adsorption and release is shown in figure 2b [32]. The modification in the refractive index of PHMB layer can be expounded in terms of a redistribution of the electron density of the polymer repeating units due to the binding of the CO₂ molecules, which consequences in a variation in its polarizability.

The sensing mechanism is based on the wavelength interrogation method of the reflected light. The absorption offered by the proposed metasurface is tolerant to the angle of incidence of light (AOI) which will be demonstrated later in the paper. The broadband light is used to excite the sample at 45 degrees which absorb a certain wavelength when the impedance matching condition is fulfilled. The reflected light is collected with the help of a photodetector which is used to convert the photons into current and examined via a spectrum analyzer. When the CO₂ gas is injected in the chamber, it gets absorbed by the PHMB layer. As a result, the refractive index of the layer decreases which translates the λ_{res} to the lower wavelength. The change in the refractive index of the PHMB layer, as well as the wavelength shift, is dependent on the concentration of the gas.

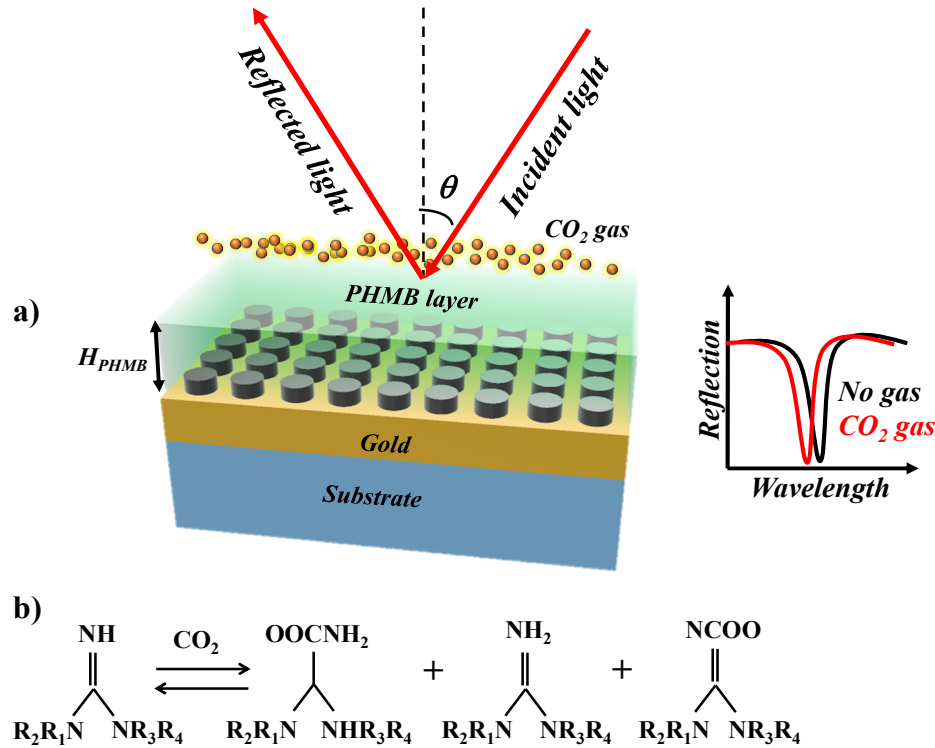


Figure 2. a) A thin layer of PHMB functional layer is deposited on the metasurface. This scheme is used to detect the CO_2 gas via wavelength interrogation method, b) Reaction between CO_2 gas and amide-bearing functional groups [32].

3. Optimization of narrowband PA design

In this section, we have optimized the performance of the PA structure by varying the geometric parameters of the device such as R , H_{Si} and d . The maximum absorption is attained when ϵ and μ should satisfy the impedance-matched condition, i.e., $\epsilon(\omega) = \mu(\omega)$, at the operational wavelength [34]. The absorption is calculated by using the following expression:

$$\text{Absorption (A)} = 1 - \text{Transmission (T)} - \text{Reflection (R)} \quad (4)$$

Where transmission ≈ 0 , due to the thick gold layer deposited on the substrate. Therefore, the absorption is directly dependent on the reflection.

3.1. Variation in R at constant remaining parameters

The resonance wavelength (λ_{res}) and absorption of the device is calculated for different values of R and maintaining other geometric parameters at a constant value such as $H_{\text{Si}}=50$ nm, $d=300$ nm and $H_{\text{Au}}=100$ nm. R is varied between 100 nm and 250 nm with a step size of 25 nm. The spectral characteristic of the device is plotted for the near-infrared region with the help of the “parametric sweep” function where the wavelength is incremented with a step size of 0.5 nm. From figure 3a, it can be seen that λ_{res} can be tuned between 821 nm to 1024 nm as R is increased from 100 nm to 250 nm. The maximum absorption of 0.905 is obtained at $R=150$ nm at $\lambda_{\text{res}}=916.5$ nm.

3.2. Variation in H_{Si} at constant remaining parameters

After optimizing the R of the MAs, the next thing is to improve the height of the MAs placed on the gold layer. For that reason, we have varied H_{Si} between 30 nm to 80 nm with a step size of 10 nm by

keeping R , d and H_{Au} fixed at 150 nm, 300 nm and 100 nm, respectively. Figure 3b presents λ_{res} and absorption plotted versus H_{Si} . It is well noting that λ_{res} shows the same trend as H_{Si} increases. So, we can tune the wavelength of the absorbing light either by manipulating R or H_{Si} . The absorption capability of the MAs increases as H_{Si} is varied from 30 nm to 50 nm. However, when H_{Si} is further increased, the absorption potential of the device decreases. This is due to the mismatch in the ϵ and μ at the operational wavelength.

3.3. Variation in d at constant remaining parameters

In section 3.1 and 3.2, the optimized values of R and H_{Si} are achieved at 150 nm and 50 nm where the absorption is 0.905. Here, we have optimized the gap between two MAs, i.e. $2d$. Figure 3c presents the absorption and λ_{res} plot versus d which is varied between 240 nm to 340 nm with a step size of 20 nm. The maximum absorption of 0.9188 is obtained at $\lambda_{res}=914$ nm where $d=260$ nm and it deteriorates as d increases. Hence, from figure 3c, it can be predicted that the gap between two MAs should be maintained at 520 nm to preserve the absorption of 0.92.

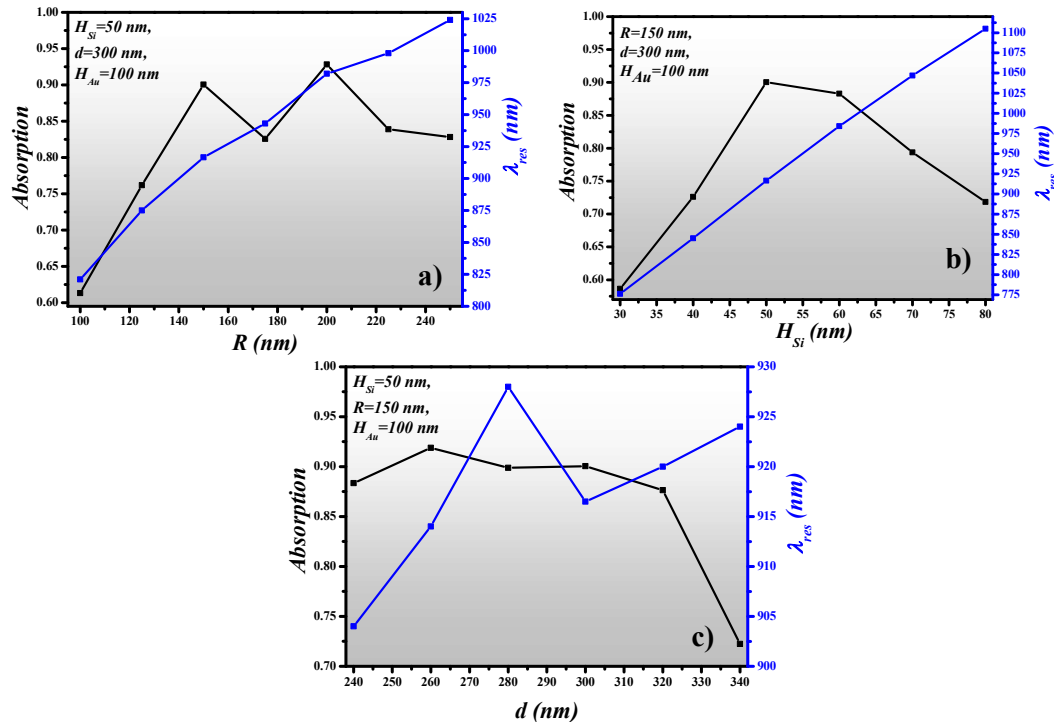


Figure 3. Spectral characteristics of the metasurface absorber, a) Radius of MA versus absorption and resonance wavelength, b) Height of MA versus absorption and resonance wavelength, c) Gap between MA versus absorption and resonance wavelength.

3.4. R/T/A plot and AOI of x-oriented and y-oriented field

The reflection, transmission and absorption spectrum is plotted for both x-oriented and y-oriented EM waves at the optimized device parameters where $R=150$ nm, $H_{Si}=50$ nm, $H_{Au}=100$ nm and $d=260$ nm as shown in figure 4a. The λ_{res} for the x-oriented field is 914 nm where absorption is 0.9188 whereas the λ_{res} for the y-oriented field is 913.5 nm where absorption is 0.9488. This specifies that the PA is polarization-insensitive and can be employed as a narrowband filter. Furthermore, the absorption potential of the device concerning the AOI of x-oriented and y-oriented field is

investigated. The absorption is retained at 0.9188 and 0.9488 for x-oriented and y-oriented polarized light for the AOI ranging between -75 degrees and +75 degrees, respectively as shown in figure 4b.

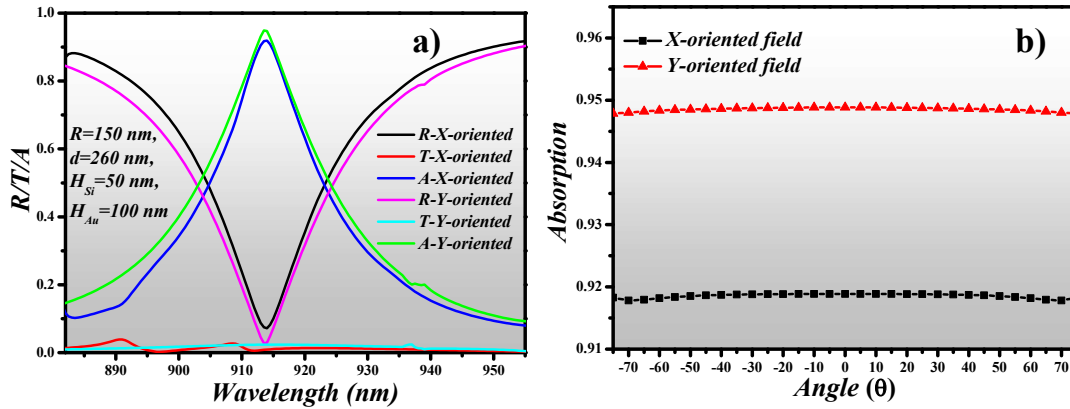


Figure 4. a) Transmission, reflection and absorption spectrum, b) AOI of X-oriented and Y-oriented field versus absorption.

Additionally, the E-field and H-field distribution at λ_{res} for x-oriented and y-oriented EM field is shown in figure 5. The 2D electric field distribution plot is taken on the surface of the MA. There is a slight difference between the λ_{res} of x-oriented and y-oriented light as can be seen in figure 5 (a, b). The cross-sectional view of the E-field distribution and H-field distribution at $\lambda_{res}=914$ nm for x-oriented light is shown in figure 5c and 5d, respectively. It is worth noting that the E-field is stronger on top and inside the MA at λ_{res} , while H-field is stronger between the MA and metal interface. The perfect matching of the E-field dipole and H-field dipole results in the eradication of the reflectance and delivers maximum absorption.

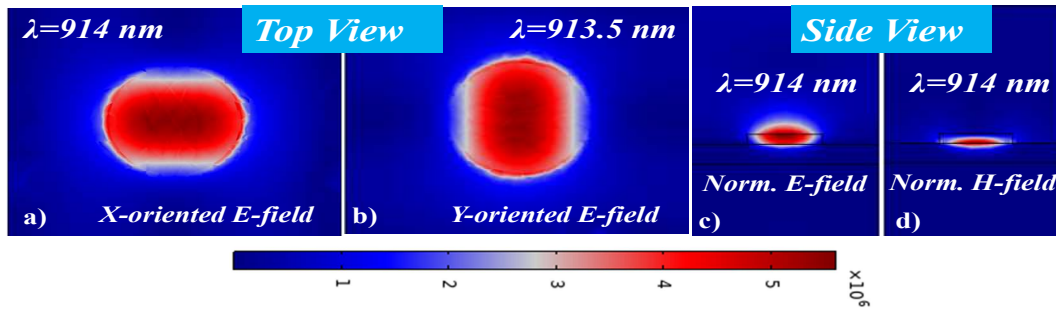


Figure 5. Electric field distribution in MA, a) X-oriented E-field distribution on the top of the MA at λ_{res} , b) Y-oriented E-field distribution on the top of the MA at λ_{res} , c) Side view of E-field distribution at λ_{res} , d) Side view of H-field distribution at λ_{res} .

4. CO₂ gas sensing based on wavelength interrogation method

The PA can be employed in the detection of CO₂ gas by depositing a thin layer of PHMB on the surface of the metasurface. In figure 6, we have investigated the dependence of absorption and λ_{res} on H_{PHMB} which is varied between 75 nm to 225 nm with a step size of 25 nm. The remaining geometric parameters of the device are as follows: $R=150$ nm, $d=260$ nm, $H_{Si}=50$ nm and $H_{Au}=100$ nm which are optimized in section 3 for best performance. From figure 6a, it can be seen that λ_{res} performs a redshift as H_{PHMB} increases while a significant enhancement in absorption is also

observed. PHMB layer forms a cladding layer on the silicon MAs which helps in the confinement of the resonant light. The maximum absorption of 0.96336 is obtained at $\lambda_{\text{res}} = 985$ nm when $H_{\text{PHMB}} = 100$ nm is deposited on the surface of the MAs. The R/T/A graph is plotted for the optimized device parameters in the wavelength range of 960 nm to 1015 nm as shown in figure 6b.

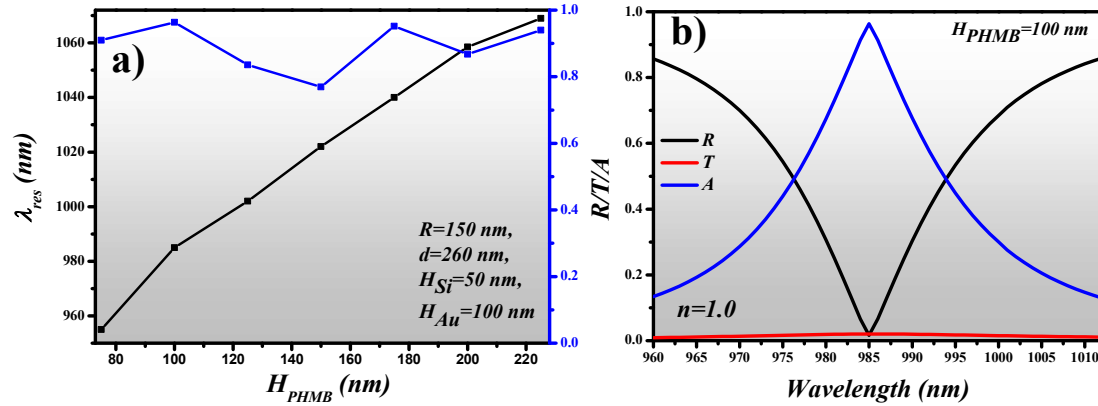


Figure 6. a) Absorption and λ_{res} dependence on H_{PHMB} , b) R/T/A plot of a PHMB coated PA. Here the PHMB is optimized at 100 nm. The geometric parameters of the design are $R=150$ nm, $d=260$ nm, $H_{\text{Si}}=50$ nm, $H_{\text{Au}}=100$ nm and $H_{\text{PHMB}}=100$ nm.

Mi et al [35] reported a silicon ring resonator CO_2 gas sensor with a PHMB functional layer deposited over the waveguide structure. By utilizing such a method, the gas concentration in the range of 0-500 ppm can be detected. The sensitivity offered by the sensor is 6×10^{-9} RIU/ppm with a detection limit of 20 ppm. In [36], a silicon dual-gas sensor realized on a wavelength-multiplexed ring resonator array for the concurrent detection of H_2 and CO_2 gases is proposed. In [37], an experimental study based on a PHMB based Fabry-Perot interferometric optical fiber sensor for the detection of CO_2 gas is conducted. The suggested sensor model offers a sensitivity of 12.2 pm/ppm for the gas range of 0-700 ppm. In [38], the authors replicated the ring resonator design proposed in [35] and carried out the numerical investigation and derived the refractive index of the PHMB layer dependence on the CO_2 gas concentration as tabulated in Table 1. From the table, it is convenient to extract the refractive index values of the PHMB layer at specific gas concentrations as well as the shift in the resonance wavelength.

Table 1: The refractive index of the PHMB layer versus gas concentration [38].

| Refractive index (n) | CO_2 gas concentration (ppm) | $\Delta\lambda_{\text{res}}$ (pm) |
|--------------------------|---------------------------------------|-----------------------------------|
| 1.54 | 215 | 0.96 |
| 1.53 | 262 | 1.15 |
| 1.52 | 328 | 1.34 |
| 1.51 | 366 | 1.53 |
| 1.50 | 366 | 1.53 |
| 1.49 | 434 | 1.72 |
| 1.48 | 524 | 1.91 |

In the absence of CO₂ gas, the refractive index of the PHMB layer is ~ 1.55 @1000 nm which is obtained by extrapolating the data using a Cauchy model fit [35]. The reflection spectrum at different CO₂ gas concentrations is plotted at 45 degrees AOI for the wavelength range of 940 nm to 1020 nm. From figure 7, it can be seen that $\lambda_{\text{res}}=985$ nm is obtained in the absence of the CO₂ gas. However, when the concentration of gas increases, λ_{res} performs a visible blueshift. In this work, the gas detection range of 0-524 ppm is investigated.

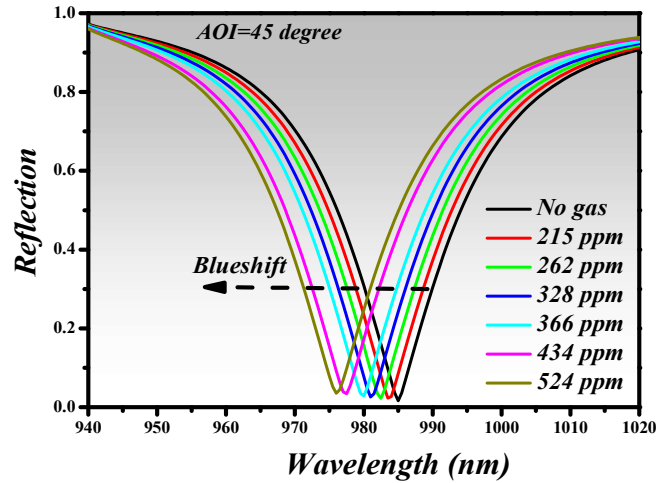


Figure 7. Reflection spectrum versus different CO₂ gas concentration in ppm.

The cross-sectional view of the E-field distribution in the silicon MA is plotted for the on-resonance and off-resonance wavelength as shown in figure 8a and 8b, respectively. At $\lambda_{\text{res}}=985$ nm, there is a perfect matching of the E-field dipole and H-field dipole which results in the suppression of the reflectance and provides a maximum absorption while at $\lambda=1020$ nm which is the off-resonance wavelength, the light is reflected from the surface resulting in an insignificant absorption.

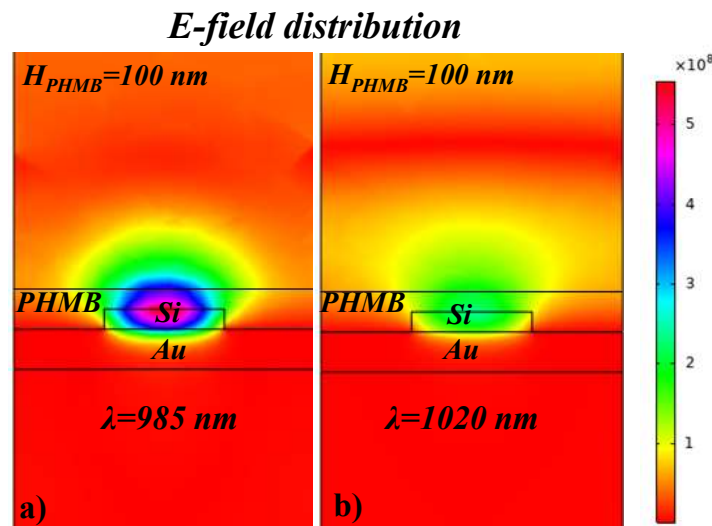


Figure 8. A cross-sectional view of the E-field distribution in the silicon MA at, a) on-resonance wavelength, b) off-resonance wavelength.

From figure 7, we have extracted the spectral characteristics and tabulated in Table 2 such as λ_{res} and $\Delta\lambda_{res}$ versus gas concentration. As in previous works [35-37], the λ_{res} is given in pm, that's why we have also converted the wavelength from nm to pm so that the spectral characteristics can be fairly related. By comparing the λ_{res} shift based on ring resonator sensor (table 1), the proposed metasurface based PA shows higher shift which can assist in higher sensitivity.

Table 2: Resonance wavelength shift versus gas concentration of the proposed sensor design.

| Refractive index (n) | CO ₂ gas concentration (ppm) | λ_{res} (pm) | $\Delta\lambda_{res}$ (pm) |
|----------------------|---|----------------------|----------------------------|
| 1.55 | 0 | 985000 | - |
| 1.54 | 215 | 983600 | 1400 |
| 1.53 | 262 | 982500 | 2500 |
| 1.52 | 328 | 981200 | 3800 |
| 1.51 | 366 | 980000 | 5000 |
| 1.49 | 434 | 977500 | 7500 |
| 1.48 | 524 | 976000 | 9000 |

For practical application in the detection of a small concentration of CO₂ gas, optical sensors with high sensitivity are desired. Sensitivity is the measure of the resonant wavelength shift concerning the gas concentration and is expressed as:

$$S = \frac{\Delta\lambda(pm)}{\Delta conc.(ppm)} \quad (5)$$

Where $\Delta\lambda$ is the change in resonance wavelength (pm) and $\Delta conc.$ is the change in gas concentration (ppm). We have plotted the λ_{res} shift versus the CO₂ gas concentration and found out that λ_{res} decreases as the gas concentration increases as shown in figure 9a. Moreover, it has a linear correlation to the CO₂ gas for the given 0-524 ppm concentration. This range is of interest for atmospheric CO₂ gas monitoring. Figure 9b presents the sensitivity of the proposed sensor design for the gas concentration of 0 ppm to 524 ppm. The maximum sensitivity of ~17.3 pm/ppm is obtained for the gas concentration higher than 400 ppm. However, for the gas concentration < 400 ppm, the concentration is still higher than the one reported in [32, 35].

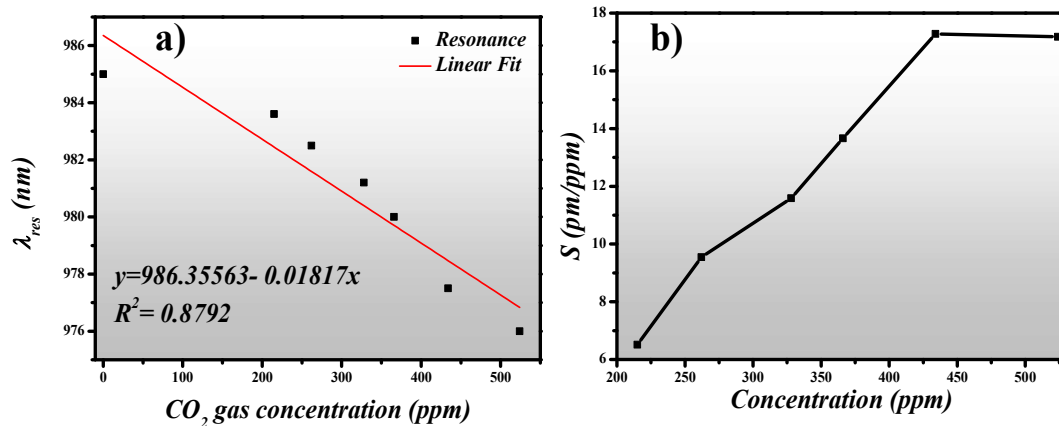


Figure 9. a) Resonance wavelength (nm) versus CO₂ gas concentration (ppm), b) Sensitivity (pm/ppm) versus gas concentration (ppm).

5. Anticipated manufacturing process

The proposed sensor device can be manufactured by the execution of the following steps as shown in figure 10. A thin chromium layer (~5 nm- 10 nm) is coated on the glass substrate followed by a thermal evaporation or electron beam (E-beam) evaporation of a gold layer. Chromium can be used to increase the gold adhesion on the substrate. Afterwards, an optimized layer thickness of silicon is deposited on the gold layer by utilizing chemical vapour deposition. E-beam lithography can be directly used to transfer the MA patterns on the electron-sensitive film known as a resist. The E-beam modifies the solubility of the resist, enabling the selective removal of the non-exposed regions of the resist by immersing it in a developer. The sample is then etched with the help of an appropriate dry etch method to form patterns of Si layers creating cylindrical MAs. In the last step, the PHMB polymer can be deposited on the metasurface by spin-coating. The thickness of the PHMB layer can be regulated by changing the spin speed in addition to the solution concentration.

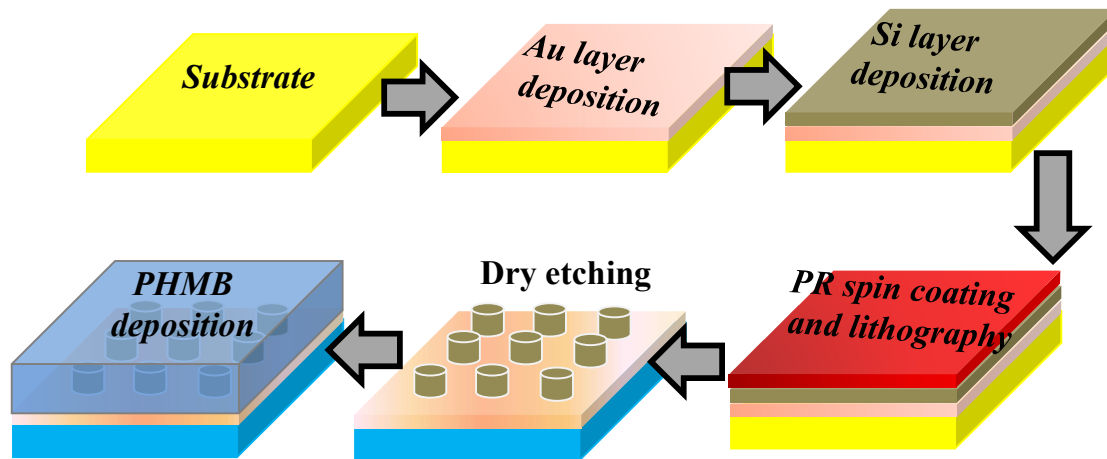


Figure 10. Proposed fabrication step of the CO₂ gas sensor.

6. Concluding remarks

In conclusion, a metasurface based perfect absorber is designed and numerically investigated via the finite element method. The metasurface is composed of silicon Nano-cylindrical meta-atoms periodically arranged on the gold layer. Due to the impedance matching of electric-field dipole and magnetic-field dipole, the maximum absorption is obtained at the resonance wavelength. The absorption > 0.9 is obtained which is independent of polarization and angle of incidence of the light. Moreover, the gas sensing characteristics of the metasurface based absorber is explored by depositing a functional host material. For the detection of CO₂ gas, polyhexamethylene biguanide (PHMB) polymer is employed which is capable of absorbing CO₂ gas. The modification in the refractive index of PHMB layer can be explained in terms of a redistribution of the electron density of the polymer repeating units due to the binding of the CO₂ molecules resulting in a variation in its polarizability. The proposed gas sensor is capable of detecting CO₂ gas within a concentration range of 0-524 ppm with a maximum sensitivity of 17.3 pm/ppm. The proposed sensor configuration can be utilized for the detection of other toxic gases by utilizing suitable functional host materials.

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Conflicts of Interest: The authors declare no conflict of interest.

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