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[N. L. Lethole](#) * and [E. H. Onah](#)

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Article

Exploration of Structural, Thermodynamic, Magnetic and Mechanical Properties of Martensite Fe₃Pt Alloys: A Density Functional Theory Study

N. L. Lethole* and E. H. Onah

Department of Computational Sciences, University of Fort Hare, Private Bag X1314, Alice, 5700, RSA

* Correspondence: nlethole@ufh.ac.za

Abstract

The current study explored the martensite structures of Fe₃Pt alloys, specifically *Cmmm*-Fe₃Pt, *P63/mmc*-Fe₃Pt, *P4/mmm*-Fe₃Pt, and *R $\bar{3}m$* -Fe₃Pt, aiming to provide a comprehensive understanding of the mechanisms that govern their physical and chemical properties. We have focused on their structural, thermodynamical, magnetic, electronic, and mechanical characteristics, utilizing the Density Functional Theory (DFT) technique. Our study revealed that in addition to the previously reported austenitic cubic *Pm $\bar{3}m$* -Fe₃Pt and martensite tetragonal *I4/mmm*-Fe₃Pt with L1₂ structure, there exist additional Fe₃Pt phases that exhibit excellent structural, thermodynamic, magnetic and mechanical properties. The calculated enthalpies of formation were found to be negative and less than -0.39 eV in all the structures considered, indicating thermodynamic stability and formation under experimental synthetic conditions. Moreover, the computed magnetic moments are in the range 2.94 to 3.04 μ_B , which is relatively comparable to 3.24 μ_B of the widely reported *Pm $\bar{3}m$* -Fe₃Pt alloy. The analysis of the electronic structure also revealed strong magnetism due to the presence of asymmetry in the spin up and down states of the density of states (DOS) plots. To determine the mechanical response of Fe₃Pt structures under loading conditions, we computed the independent elastic constants, macroscopic properties and stress-strain relationship under hydrostatic stress. All four phases, but the hypothetical *P63/mmc*-Fe₃Pt showed excellent mechanical stability at ambient conditions and exceptional hardness and resistance to compression in the elastic region $0\% \leq \text{strain} \leq 10\%$. This evidence is provided by satisfying the Born necessary stability conditions, large bulk modulus and a strong linear relationship fit (R^2) of greater than 0.94.

Keywords: martensite Fe₃Pt; thermodynamic stability; magnetic moments; mechanical stability; spin asymmetry

1. Introduction

The exploration of bimetallic Fe-Pt alloys has long garnered significant attention due to their intriguing properties and promising applications in various fields such as ultra-high density data storage, spintronics, catalysis, and nanotechnology [1, 2, 3, 4]. As indicated by their binary stability phase diagram [5], there have been three well-known and widely reported structures of Fe-Pt alloys which are chemically ordered. These include the tetragonal L1₀ *P4/mmm*-FePt phase which exhibits ferromagnetic ordering, and the face-centered cubic (FCC) phases FePt₃ and Fe₃Pt, both crystallizing in the *Pm $\bar{3}m$* space group with L1₂-type crystal symmetry. The latter two phases support both antiferromagnetic and ferromagnetic magnetic ordering [6]. These alloys have been previously investigated both experimentally and computationally and have been found to exhibit excellent thermodynamic, vibrational and mechanical stability. Moreover, they possess desirable magnetic properties due to large magnetic moments, large uniaxial magnetocrystalline anisotropy (MCA) energies originating from spin-orbit interactions and asymmetry of spin up and down in the electronic density of states [7, 8, 9]. Variations in crystallization and chemical composition

significantly influence their magnetic behavior, electronic structure, and lattice dynamics. For instance, although both Fe and Pt contribute to the magnetic moments, Fe contributes approximately eight times more than Pt, thereby making the magnetic behavior predominantly dependent on the Fe content [10]. The $P4/mmm$ -FePt phase crystallizes at temperatures below 1570 K in equiatomic Fe:Pt concentration, while the FCC structures crystallize around 25 % and 75 % Fe contents at temperatures below 1120 K and 1620 K, respectively [11]. The tetragonal $L1_0$ FePt shows one of the highest MCA energy ranging from $6 \times 10^6 \text{ J/m}^3$ to $9 \times 10^6 \text{ J/m}^3$ along the magnetically easy c axis [001], making it a promising candidate to overcome superparamagnetic limit, which is the loss data due to thermally activated fluctuations of magnetization [12, 13]. It consists of alternating stacked atomic layers of Fe and Pt atoms along [100] direction similar to the AuCu structure, leading to a tetragonal distortion along the c -axis. As per the previous communication, the cubic Fe_3Pt and FePt_3 alloys exhibit the highest MCA energies of $1.1 \times 10^6 \text{ J/m}^3$ (0.375 meV) and $1.5 \times 10^5 \text{ J/m}^3$ (0.055 meV) along the [100] easy axis [12]. In the Fe-rich Fe_3Pt alloy, Fe atoms occupy the corner lattice positions, while Pt atoms are located at face-centered positions. Conversely, in the Pt-rich FePt_3 alloy, Pt atoms occupy the corner positions, and Fe atoms are situated at the face-centered positions.

In addition, the $L1_2$ face-centered cubic (austenitic) Fe_3Pt alloy is reported to exhibit strong magnetoelastic coupling and undergoes a thermoelastic martensitic transformation from the ordered $L1_2$ phase into low-temperature martensitic structures, which inherently depend on the degree of order of the $L1_2$ structure [14, 15]. One such martensite structure is the body-centered tetragonal (BCT) Fe_3Pt phase, which crystallizes in the $I4/mmm$ space group [16, 17]. The equilibrium cell parameters of the $I4/mmm$ bulk structure as produced by X-ray diffraction are $a = 5.73 \text{ \AA}$ and $c = 6.34 \text{ \AA}$ [18]. It was found that the spin up Fe d states in the density of states (DOS) in this martensite structure are situated below the Fermi level, while the spin down states overlaps above the Fermi, indicating a pronounced spin asymmetry. Consequently, this spin polarization results in relatively large magnetic moments of $2.61 \mu_B$ and $2.82 \mu_B$ for Fe1 and Fe2 atoms, respectively. Moreover, Pt atoms were also found to exhibit a finite magnetic moment of $0.45 \mu_B$, suggesting a degree of spin polarization induced by hybridization with neighboring Fe atoms [16]. Our previous communication further reported magnetic moments of $2.744 \mu_B$ for Fe and $0.45 \mu_B$ Pt along with the MCA energy of 1.364 meV along the [001] easy axis [12], which are higher than those of the austenitic Fe_3Pt .

The structural models of other Fe_3Pt martensite phases have long been proposed, however, their properties remain unstudied [19]. According to the Materials Explorer within the Materials Project database [20, 21], three additional martensitic phases of Fe_3Pt are predicted to exist whose structural, thermodynamic, magnetic and mechanical properties are not yet fully explored. These correspond to the $P4/mmm$, $Cmmm$, and $R3m$ space groups as shown in Figure 1. The $Cmmm$ - Fe_3Pt phase crystallizes at approximately 55 K in an orthorhombic lattice characterized by primitive lattice parameters ($a = 3.732 \text{ \AA}$, $b = 3.714 \text{ \AA}$, $c = 3.750 \text{ \AA}$) as determined by XRD. The structure comprises two crystallographically distinct Fe sites. This orthorhombic structure is an intermediate phase, appearing between face-centered tetragonal (FCT1) ($c/a < 1$) and FCT2 ($c/a > 1$) [15]. The system considered in this current work is a conventional c -centered (centering doubles the number of lattice points along one direction) orthorhombic Fe_3Pt which is equivalent, but twice the volume and number of atoms (eight) as the primitive (four atoms) reported in literature. In the first site, Fe atoms adopt a two-coordinate geometry, bonded to two Fe and two Pt atoms, whereas the second Fe site exhibits eightfold coordination with neighboring Fe atoms. The Pt atoms display a four-coordinate geometry, each bonded to four Fe atoms, completing the orthorhombic network. The $P4/mmm$ - Fe_3Pt phase exhibits a USi_2 -type structure and crystallizes in a body centered tetragonal (BCT) lattice. This phase forms through a thermoelastic transformation. During the formation, the tetragonality ratio c/a shifts from 1 to 0.79 at the transformation temperature, signifying a discontinuous lattice distortion characteristic of a first-order martensitic transformation [15, 17]. The structure contains two inequivalent Fe sites. Each Fe atom is coordinated by eight Fe and four Pt atoms, forming distorted FeFe_8Pt_4 cuboctahedra. These polyhedra interconnect through corner-, edge-, and face-sharing with neighboring FeFe_8Pt_4 and PtFe_{12} units, forming a highly integrated three-dimensional framework.

The Pt atoms are twelvefold coordinated by Fe atoms, generating PtFe_{12} cuboctahedra that are similarly interconnected through shared corners, edges, and faces with surrounding FeFe_8Pt_4 polyhedra. The $R\bar{3}m$ - Fe_3Pt phase crystallizes in a rhombohedral centered hexagonal or trigonal lattice. Each Fe atom is surrounded by nine Fe and three Pt atoms, forming distorted FeFe_9Pt_3 cuboctahedra that share corners, edges, and faces with adjacent FeFe_9Pt_3 and PtFe_6Pt_6 polyhedra. The Pt atoms are coordinated by six Fe and six Pt atoms, creating PtFe_6Pt_6 cuboctahedra that link through corner-, edge-, and face-sharing, producing a robust trigonal framework. Lastly, the $P63/mmc$ - Mn_3Ir structure served as a prototype for Fe_3Pt , since Fe and Mn as well as Pt and Ir are chemically analogous neighboring transition metals with comparable atomic radii and electronic configurations. Such substitution preserves the symmetry and coordination environment, enabling reliable DFT modeling of synthetical Fe–Pt system within the same crystallographic framework. This is beta Cu_3Ti and Mn_3Ga type structure which crystallizes in the hexagonal lattice with eight atoms in a primitive cell [22, 23]. Fe is bonded to four equivalent Pt atoms to form a mixture of distorted corner, edge, and face-sharing FePt_4 cuboctahedra. Pt is bonded to twelve equivalent Fe atoms to form a mixture of corner and face-sharing PtFe_{12} cuboctahedra.

The magnetic, thermodynamic and mechanical properties of these four martensite phases are yet to be systematically explored either experimentally or theoretically, which limits a comprehensive understanding of the structure–property relationships and the potential functional applicability in advanced magnetic and electronic technologies. Experimental exploration of these alloys may be challenging due to the complexities associated with detecting such phases arising from dynamical effects on diffraction reflections [16]. However, the development of density functional theory (DFT)-based first-principles methods enables theoretical exploration and optimization of L_{12} bimetallic alloys by accurately calculating the interatomic forces acting on the nuclei [24, 25, 26]. The current study focuses on the structural, thermodynamic, magnetic, electronic and mechanical properties of the four martensite Fe_3Pt bimetallic alloys at 0K to assess their stability and deduce their suitability as magnetic materials. We have employed the density functional theory (DFT) quantum mechanical method embedded in the CASTEP code to perform first-principles quantum mechanical calculations on Fe_3Pt alloys. Our computational findings revealed that three martensite Fe_3Pt alloys exhibit excellent thermodynamic and mechanical stability and magnetic moments comparable to those of the extensively studied Fe–Pt alloys.

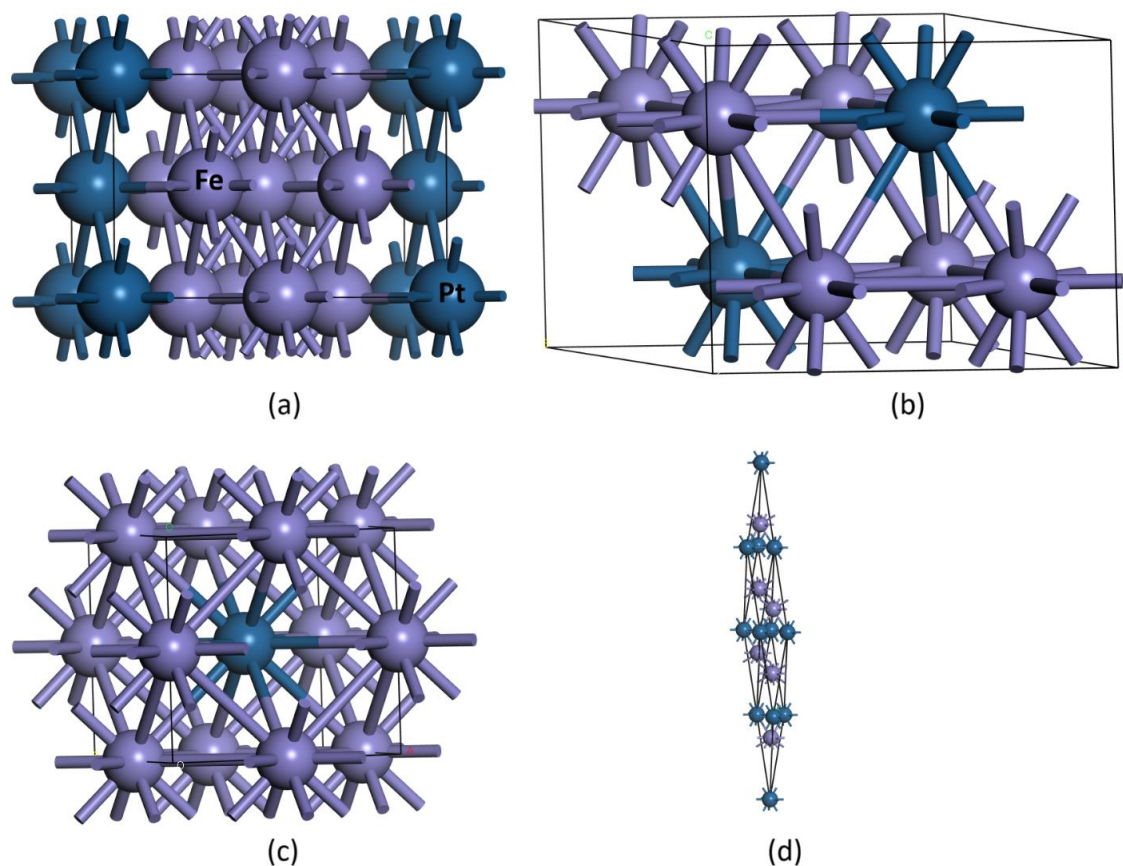


Figure 1. Schematic representation of atomic arrangements in (a) $Cmmm$ (b) $P63/mmc$ (c) $P4/mmm$ and (d) $R3m$ Fe_3Pt alloys.

2. Computational Approach

The present study utilized the Cambridge Serial Total Energy Package (CASTEP) [27] which employs the plane-wave density functional theory (DFT) plane-wave pseudopotential method to perform first-principles calculations on Fe_3Pt alloys. The Generalized Gradient Approximation (GGA) and Perdew-Burke-Ernzerhof (PBE) exchange-correlation functional were preferred since they account for inhomogeneities in the electron distribution [28, 29]. To determine the minimum optimal plane-wave cut-off energies that converge the total energy, single-point energy calculations were performed for all the systems at several increasing cut-off values without relaxing the atomic positions and cell parameters. This was done until the total energy between successive steps was below 1 meV. The cut-off energies 400 eV, 300 eV, 400 eV and 300 eV were respectively found sufficiently to converge the total energies of $Cmmm$, $P63/mmc$, $P4/mmm$ and $R\bar{3}m$ systems. Moreover, the customized Monkhorst-Pack [30] k-points grid size of $9 \times 7 \times 4$, $4 \times 4 \times 6$, $5 \times 5 \times 6$ and $8 \times 8 \times 1$ for self-consistent field (SCF) calculations were applied for Brillouin zone sampling. Before subsequent calculations of electronic structure and elastic properties, full geometry optimization was performed to obtain the arrangement of atoms and cell parameters corresponding to the minimum total energy and zero net forces on atoms, i.e. the ground-state structures. Both cell volume and shape were allowed to change until the final energy between two iterations was less than 5.7 meV. To allow separation of majority and minority spin projections, the spin density was treated by the collinear spin polarization using formal spin as initial. The low-memory Brayden-Fletcher-Goldfarb-Shanno (LBFGS) algorithm [31] that scales linearly in memory and performs better for large systems was preferred for cell optimization over the normal BFGS [32] that scales as a square of the system size for cell. Furthermore, the LBFGS algorithm employs a general sparse preconditioner that enhances the efficiency of geometry optimization, achieving up to a twofold speed increase for small systems

and up to tenfold for large systems [33]. Subsequent computation of density of states and elastic constants were done using the equilibrium structures. Calculation of the elastic properties was performed using the Elastic Constants task with a maximum strain amplitude of 0.003, which is adequately low for the material to stay in the linear elasticity. The calculation of electronic band structure and density of states was done with and band energy tolerance of 10^{-5} eV.

3. Results and Discussion

3.1. Structural Properties

The equilibrium cell parameters, densities and enthalpies of formation of the four martensite Fe₃Pt structure as shown in Table 1 were obtained by performing full geometry optimization. The experimental volume for the orthorhombic *Cmmm*-Fe₃Pt and lattice parameters of the previously reported austenitic *Pm3̄m* -Fe₃Pt are given in parenthesis to validate DFT calculations against existing experimental data. The calculated lattice parameters of *Pm3̄m* -Fe₃Pt are more than 99 % in agreement with experimental data [34] and previous calculations [8], while the optimized volume of *Cmmm*-Fe₃Pt in 96 % in agreement with the XRD results [15]. These agreements indicate that the employed approach correctly predicts the ground state properties of Fe₃Pt alloys. The conventional hexagonal *P63/mmc*-Fe₃Pt structure shows the largest unit cell volume and smallest density corresponding to weaker interatomic interactions. The enthalpies of formation (ΔH_f) were computed according to equation 1,

$$\Delta H_f = E_{Fe_3Pt} - \sum_i n_i E_i^{element} \tag{1}$$

where E_{Fe_3Pt} is the total ground state energy of Fe₃Pt formula unit and $E_i^{element}$ the elemental energies of Fe and Pt atoms. Negative enthalpies of formation indicate the release of energy when forming a compound (exothermic reaction) and thus thermodynamic stability of the compounds in relation to its constituent elements, i.e. $E_{compound} < E_{elements}$. Our DFT calculations predict that all the four martensite Fe₃Pt alloys are thermodynamically stable due to negative enthalpies of formation. Expectedly, the enthalpy of formation values of austenitic *Pm3̄m* and martensite *Cmmm*, *P63/mmc*, *P4/mmm* and *R3̄m* are similar since they have the same stoichiometry and elemental reference state.

Table 1. Calculated equilibrium cell parameters, densities and enthalpies of formation and density of Fe₃Pt alloys.

Parameter	<i>Pm3̄m</i>	<i>Cmmm</i>	<i>P63/mmc</i>	<i>P4/mmm</i>	<i>R3̄m</i>
a (Å)	3.756 (3.73) [34]	4.089	5.262	3.827	8.550
b (Å)	-	4.092			
c (Å)		6.197	4.685	3.593	
V (Å ³)	53.000	103.694	112.34	52.620	54.330
ΔH_f (eV/atom)	-0.391	-0.391	-0.391	-0.391	-0.391
ρ (g/cm ³)	11.361	11.614	10.720	11.440	11.082

3.2. Magnetic Properties

Table 2 presents the calculated spin polarized magnetic moments and charge distribution characteristics of the four considered Fe₃Pt crystal structures derived from Mulliken atomic population analysis. The magnetic moments are calculated as the difference between spin up and spin down ($\uparrow - \downarrow$) charge densities. Moreover, the average of Fe1 and Fe2 were taken when quantifying the total spin moment per formula unit. The calculated total moments for *Cmmm*, *P63/mmc*, *P4/mmm* and *R3̄m* are 3.01 μ_B , 3.04 μ_B , 2.94 μ_B and 2.97 μ_B , respectively. These values are comparable with those reported for other Fe-Pt alloys and bimetallic systems of similar composition [10, 35, 36]. For all space groups, the Fe atoms exhibit substantial local magnetic

moments compared to Pt, indicative of strong ferromagnetic ordering within the Fe sublattice and large spin–orbit effects from Pt. Moreover, in all the structures, the spin up (↑) for both Fe1 and Fe2 are more densely than the spin down (↓) revealing pronounced spin asymmetry in the electronic density of states and confirming strong magnetic polarization within the system.

Our DFT calculations reveal that the orthorhombic *Cmmm* space group possesses the largest Fe1 magnetic moment (2.98 μ_B), followed by the hexagonal *P63/mmm* (2.92 μ_B), while the trigonal *R $\bar{3}m$* and tetragonal *P4/mmm* display relatively decreased moment values of 2.87 μ_B and 2.83 μ_B , respectively. This may be attributed to the increase of restrictions on independent lattice parameters and angles, i.e. symmetry from orthorhombic to tetragonal, which slightly decreases the exchange splitting, consistent with increased Fe–Pt orbital hybridization. The smaller variation in Fe2 moments indicates comparable local environments across the structures, except for the *P6₃/mmc* phase, where Fe occupies only one unique crystallographic site due to higher symmetry. The Pt atoms exhibit relatively small induced magnetic moments, ranging from 0.12 μ_B to 0.30 μ_B , arising from Fe–Pt hybridisation and spin polarization of Pt 5d orbitals. *Cmmm*-Fe₃Pt shows the largest Pt moment (0.30 μ_B), whereas the *P63/mmm* phase displays the smallest (0.12 μ_B).

Table 2. Calculated magnetic moments, Hirshfield spins and charges Fe₃Pt alloys.

Magnetic Moments (μ_B)				
	<i>Cmmm</i>	<i>P63/mmc</i>	<i>P4mmm</i>	<i>R$\bar{3}m$</i>
<i>Fe</i> ₁ ↑	5.35	5.33	5.29	5.34
<i>Fe</i> ₁ ↓	2.38	2.41	2.47	2.46
<i>Fe</i>₁ ↑ – <i>Fe</i>₁ ↓ (μ_B)	2.98	2.92	2.83	2.87
<i>Fe</i> ₂ ↑	5.18	-	5.26	5.29
<i>Fe</i> ₂ ↓	2.74	-	2.50	2.64
<i>Fe</i>₂ ↑ – <i>Fe</i>₂ ↓ (μ_B)	2.43	-	2.75	2.65
<i>Pt</i> ↑	16.46	16.45	16.43	16.34
<i>Pt</i> ↓	16.16	16.34	16.29	16.13
<i>Pt</i> ↑ – <i>Pt</i> ↓ (μ_B)	0.30	0.12	0.15	0.21
Total ($\mu_B/f.u.$)	3.01	3.04	2.94	2.97
Hirshfeld Analysis (μ_B)				
<i>Fe</i> ₁	2.83	2.81	2.72	2.82
<i>Fe</i> ₂	2.45	-	2.68	2.61
<i>Pt</i>	0.57	0.45	0.44	0.35
Charge (e)				
<i>Fe</i> ₁	0.27	0.26	0.24	0.20
<i>Fe</i> ₂	0.08	-	0.24	0.07
<i>Pt</i>	-0.62	-0.79	-0.72	-0.46

The Hirshfeld partitioning of electron density into atomic contributions further confirms the dominance of Fe atoms in the overall magnetic behavior. The Fe1 moments range from 2.72 μ_B to 2.83 μ_B , while Fe2 moments vary between 2.45 μ_B to 2.68 μ_B . In contrast, Pt contributes only 0.35–0.57 μ_B , consistent with the induced magnetization mechanism. The *Cmmm* structure again exhibits the highest overall Fe magnetization, while the *P4/mmm* phase shows a marginally reduced value, reflecting differences in local coordination and exchange interactions.

Hirshfeld charge analysis indicates notable charge redistribution between Fe and Pt atoms. Fe atoms possess positive charges (+0.07 to +0.27 e), signifying electron donation, while Pt atoms carry negative charges (–0.46 to –0.79 e), confirming their role as electron acceptors. The *P63/mmm* phase shows the highest charge transfer (–0.79 e), suggesting stronger Fe–Pt bonding and more effective hybridization.

3.3. Electronic Structure

Figure 2 presents the electronic total and orbital-projected spin polarized density of states (DOS) for the martensitic Fe₃Pt, with the Fermi level set as the origin of the energy scale. As anticipated, all the investigated Fe₃Pt alloys display metallic behavior, as indicated by the finite density of states at the Fermi level arising from the overlap of valence and conduction bands, most prominently in the spin-down states. In all total DOS plots, the spin-up states are predominantly located below the Fermi level, whereas the spin-down states extend into the conduction band above the Fermi level, reflecting a pronounced spin asymmetry which indicates spin polarization and gives rise to substantial magnetic moments and strong ferromagnetic character consistent with previous experimental findings on Fe₃Pt thin films [37]. Notably, the *P63/mmc* phase exhibits a further strong asymmetry (enhanced spin polarization) in the valence states between -4 eV and -2 eV, consistent with its highest calculated magnetic moment. There exist shallow pseudo-gaps near the Fermi level, indicating enhanced Fe-Pt hybridization and electronic stability for all phases.

The orbital-projected DOS shows a dominant contribution from Fe 3d states in the total plots, with minor contribution from the Pt 5d states hybridizing with Fe d-bands. Moreover, there exist strong spin asymmetry in Fe states and weaker in Pt. This strong exchange splitting reflects localized Fe moments stabilized by the low structural symmetry. Furthermore, the strong spin polarization arises from the Fe 3d orbitals, while Pt-5d orbitals show small but non-zero induced moments, contributing slightly to the total magnetization.

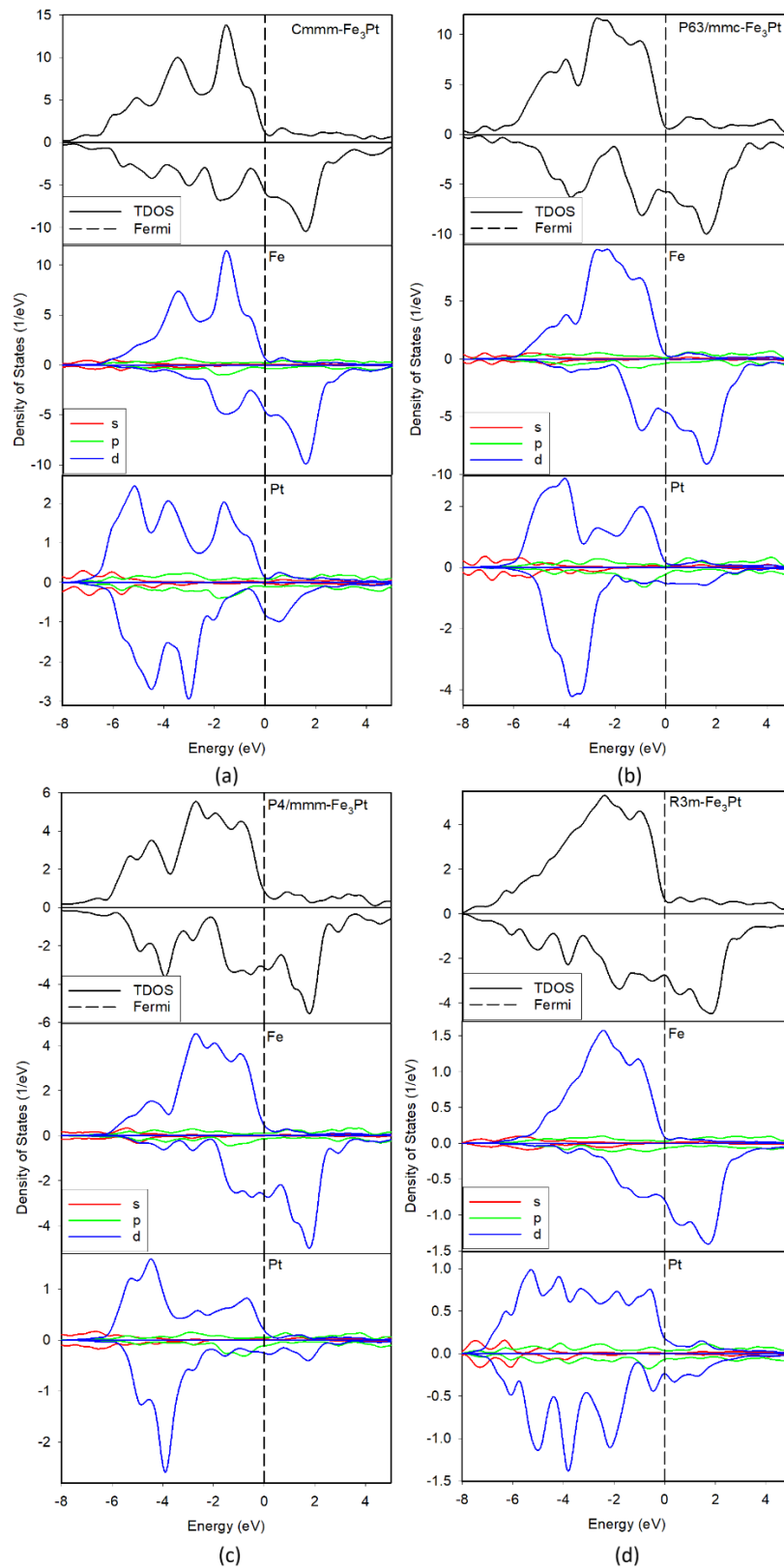


Figure 2. Total and partial density of states for $Cmmm$, $P63/mmc$, $P4/mmm$ and $R\bar{3}m$ Fe_3Pt alloys. The Fermi level is taken as the origin of the energy axis ($E_F = 0\text{eV}$).

The electronic properties of these systems were further analyzed using the band structure along high symmetry direction in the Brillouin zone as presented in Figure 3. All four structures exhibit metallic characteristics, as evidenced by the continuous overlap of energy bands at the Fermi level and the finite DOS at E_F and transitioning of electron wave highest to lowest energy levels through

the Brillouin zone [38]. Moreover, there exists a clear spin splitting: red and blue bands diverge near the Fermi level. Interestingly, the $R\bar{3}m$ phase shows almost similar spin up (red) and spin down (blue) bands, indicating nearly degenerate spins.

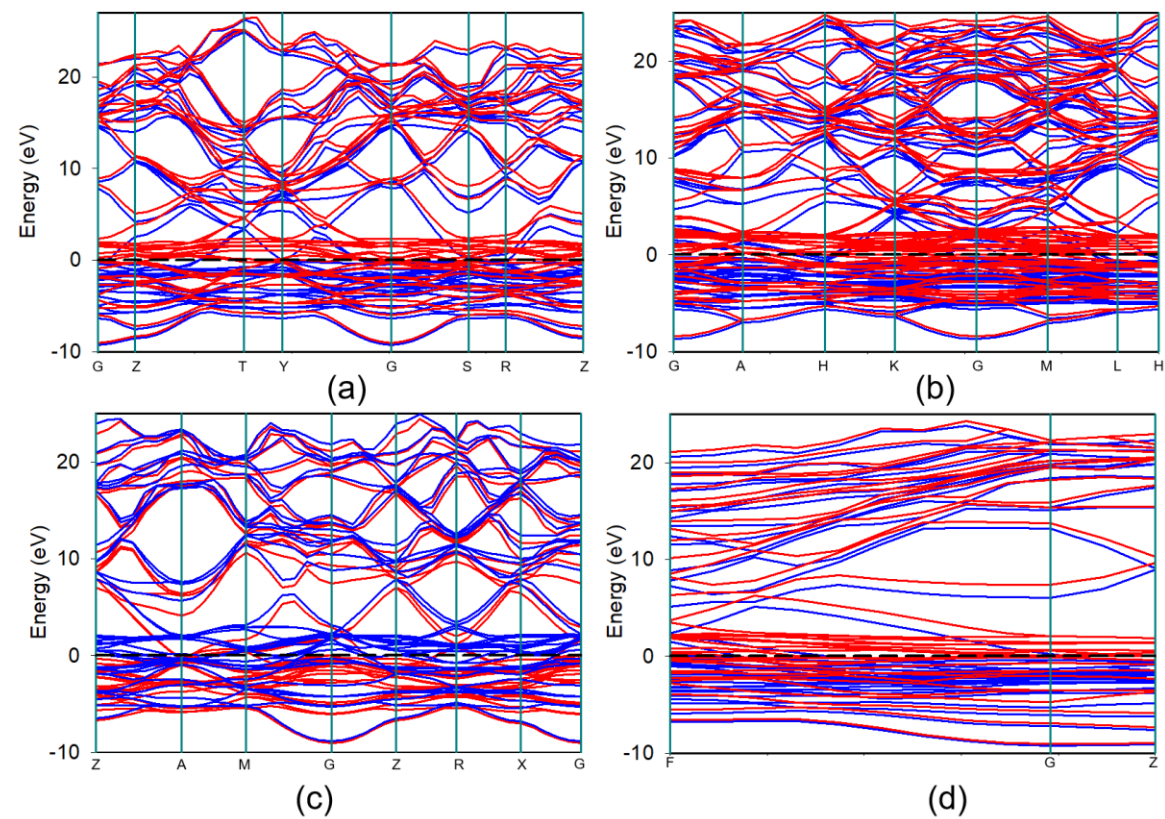


Figure 3. Electronic band structure plots of $Cmmm$, $P63/mmc$, $P4/mmm$ and $R\bar{3}m$ of Fe_3Pt along high symmetry line in the Brillouin zone. The Fermi level is taken as the zero line ($E_F = 0eV$).

3.4. Mechanical Properties

Table 3 shows the calculated independent elastic constants (C_{ij}) and derived macroscopic properties of the orthorhombic, hexagonal, tetragonal and trigonal Fe_3Pt alloys at 0 K. CASTEP uses the generalized Hooke’s law shown in equation 2) to fit the linear relationship between stress and strain components in the elastic regime to compute the independent elastic constants.

$$\sigma_i = \sum_j C_{ij} \varepsilon_j$$

(2)

where σ_i and ε_j are the Voigt notation components of the stress and strain tensor, respectively. Calculation and elastic constants and macroscopic mechanical properties are crucial in understanding the intrinsic mechanical stability, bonding nature and deformation behavior of solid-state materials. For any solid-state crystal lattice to be considered mechanically stable, certain stability conditions as postulated by Born must be satisfied [39].

Table 3. Calculated independent elastic constants and macroscopic properties of Fe_3Pt alloys.

Structure	C_{11}	C_{22}	C_{33}	C_{44}	C_{55}	C_{66}	C_{12}	C_{13}	C_{14}
$Cmmm$	300.43	298.95	224.53	120.12	119.83	36.27	92.71	161.85	
$P63/mmc$	249.31		22.23	-302.21			92.47	41.74	
$P4/mmm$	198.88		166.50	46.35		12.11	141.24	190.46	
$R\bar{3}m$	239.92		152.93	48.48			125.14	88.28	5.36
Macroscopic Properties (GPa)									
	B		G	E	σ	B/G		A	

<i>Cmmm</i>	183.77	70.85	188.34	0.33	2.59	1.97
<i>P63/mmc</i>	57.87	-25.51	74.88	0.76	-2.27	-14.01
<i>P4/mmm</i>	179.09	38.75	108.44	0.40	4.62	-2.79
<i>R3m</i>	131.99	52.15	138.23	0.33	2.53	0.24

Hexagonal crystals possess five independent elastic constants, while the tetragonal contain six due to the added $C_{66} = (C_{11} - C_{12})/2$. Since the Laue classes of the hexagonal and tetragonal crystal lattice have similar elastic matrix, their Born necessary stability conditions are also similar and are given as [40]:

$$C_{11} > |C_{12}|; 2C_{13}^2 < C_{33}(C_{11} + C_{12}); C_{44} > 0; C_{66} > 0$$

(3)

The condition $C_{66} > 0$ is redundant for hexagonal crystal lattices. The trigonal or rhombohedral lattice has 6 independent elastic constants and like the hexagonal one $C_{66} = (C_{11} - C_{12})/2$ dependent. The following four conditions are sufficient for stability:

$$C_{11} > |C_{12}|; C_{44} > 0; C_{13}^2 < \frac{1}{2}C_{33}(C_{11} + C_{12}); C_{14}^2 < \frac{1}{2}C_{44}(C_{11} - C_{12}) = C_{44}C_{66}$$

(4)

The orthorhombic crystal lattice with lower symmetry contains larger number (nine) independent elastic constants and the born stability conditions are:

$$C_{11} > 0; C_{11}C_{22} > C_{12}^2; C_{11}C_{22}C_{33} + 2C_{12}C_{13}C_{23} - C_{11}C_{23}^2 - C_{22}C_{13}^2 - C_{33}C_{12}^2 > 0;$$
$$C_{44} > 0; C_{55} > 0; C_{66} > 0$$

(5)

The independent elastic constants of the orthorhombic *Cmmm*, tetragonal *P4/mmm* and trigonal *R3m* structures are positive and obey all the necessary Born stability conditions, which indicates mechanical stability. In contrast, the *P63/mmc* phase exhibits anomalous elastic constants, due to a negative C_{44} value which violates the Born stability criteria. Such behavior signifies mechanical instability, suggesting that this hypothetical hexagonal structure cannot exist under ambient conditions and would spontaneously transform into a lower-symmetry, more stable phase with space group *mmm* [11, 41]. The elastic stiffness coefficients C_{11} , C_{22} , and C_{33} for the *Cmmm*-Fe₃Pt are relatively high, above 224.53 GPa, which signifies a strong resistance to axial deformation along all crystallographic directions. Furthermore, the off-diagonal $C_{12} = 92.71$ GPa and $C_{13} = 161.85$ GPa are also large, indicating considerable interplanar coupling, while the comparatively smaller shear constant ($C_{66} = 36.270$ GPa) reveals moderate shear anisotropy. The *P4/mmm*-Fe₃Pt structure shows moderately high values of C_{11} and C_{33} , indicating fair axial stiffness. However, its small C_{66} value (12.11 GPa) reflects weak shear resistance, implying significant anisotropy in its mechanical response. The *R3m*-Fe₃Pt phase displays intermediate stiffness with $C_{11} = 239.92$ GPa and $C_{33} = 152.93$ GPa, while the relatively small off-diagonal C_{14} value (5.36 GPa) indicates limited shear coupling.

The corresponding macroscopic mechanical properties representing a polycrystalline aggregate using Voigt–Reuss–Hill (VRH) averaging schemes were computed from the independent elastic constants to determined deformation characteristics [42]. Table 4 summarizes the expressions and descriptions of the calculated macroscopic properties.

Table 4. Mathematical expressions and descriptions of the macroscopic mechanical properties of the polycrystalline material. .

Property	Expression	Description
Bulk modulus (B)	$B_V = \frac{1}{9}(C_{11} + C_{22} + C_{33}) + \frac{2}{9}(C_{12} + C_{13} + C_{23})$	Resistance to uniform volume compression
	$B_R = [S_{11} + S_{22} + S_{33} + 2(S_{12} + S_{13} + S_{23})]^{-1}$	
	$B = \frac{B_V + B_R}{2}$	
Shear modulus (G)	$B_V = \frac{1}{15}(C_{11} + C_{22} + C_{33} - C_{12} - C_{13} - C_{23}) + \frac{1}{5}(C_{44} + C_{55} + C_{66})$	Resistance to shape change
	$B_R = 15[4(S_{11} + S_{22} + S_{33} - S_{12} - S_{13} - S_{23}) + 3(S_{44} + S_{55} + S_{66})]^{-1}$	
	$G = \frac{G_V + G_R}{2}$	

Young's modulus (E)	$E = \frac{9BG}{3B + G}$	Stiffness
Poisson's ratio (σ)	$\sigma = \frac{3B - 2G}{6B + 2G}$	Ductility and brittleness
Pugh Ratio	$\frac{B}{G}$	Ductility
Anisotropy factor (A)	$A = \frac{2C_{44}}{C_{11} - C_{12}}$	Elastic anisotropy

S_{ij} represents the compliance tensor, the inverse of C_{ij} .

The $Cmmm$ Pphase shows large bulk modulus $B = 183.77$ GPa and shear modulus $G = 70.85$ GPa further confirming its robustness and greater resistance to compression, while the relatively high Young's modulus $E = 188.34$ GPa indicates good stiffness and metallic bonding characteristics. Moreover, the Pugh ($B/G = 2.59$) ratio greater than the critical value 1.5 of ductility and brittleness and Poisson's ratio ($\sigma = 0.33$) classifies this phase as ductile, while the positive anisotropy factor ($A = 1.97$) that diverge from unity suggests moderate elastic anisotropy.

The calculated Poisson's ratio ranges from 0.33 to 0.40, except for $P63/mmc$ are within the error limit (0.32 ± 0.09) and similar to $\sigma = 1/3$ recorded in most alloys [11, 43]. Consistent with the negative C_{44} , the hexagonal $P63/mmc$, shows a negative shear modulus and Pugh ration. Its Poisson ration is 0.76 which is beyond the metallic limit (~ 0.5), indicating that this phase exhibits extreme lateral expansion when compressed (or contraction when stretched), very high ductility, low shear resistance, and strong anisotropic bonding or magnetostrictive behavior. This phase likely reflects magnetoelastic softening, not purely mechanical elasticity. The bulk modulus (179.09 GPa) of the $P4/mmm$ phase is relatively larger than the shear (38.75 GPa), leading and larger Pugh ratio, confirming a ductile but less rigid nature relative to the orthorhombic phase. The moderate Poisson's ratio (0.40) also supports a metallic and ductile bonding character. Similar behavior is observed for the $R\bar{3}m$.

To further analyze the mechanical properties of the martensite Fe_3Pt alloys, we plotted stress vs strain profiles which represent the elastic response of crystal systems under applied strain, from which elastic constants and mechanical stability are evaluated. Figure 4 illustrates the calculated stress vs strain relationships for the $Cmmm$, $P63/mmc$, $P4/mmm$, and $R\bar{3}m$ phases of Fe_3Pt . The $Cmmm$, $P4/mmm$ and $R\bar{3}m$ structures exhibit smooth and well-defined linear elastic regions, $0\% \leq \text{Strain} \leq 10\%$ (red line) with strong correlations between the fitted and computed data ($R^2 = 0.980, 0.939$ and 0.970 , respectively). This excellent agreement confirms excellent elastic behavior, numerical accuracy, mechanical stability with the elastic regime and validates the reliability of the derived elastic constants. Conversely, the hypothetical $P63/mmc$ - Fe_3Pt phase displays a noticeable deviation from linearity even at small strains, reflected by a relatively low $R^2 = 0.860$. The irregular stress response suggests internal atomic relaxations or numerical instabilities during deformation, which consistent with the observed negative C_{44} elastic constant and shear modulus values. This behavior indicates that although predicted to be thermodynamically stable, the hypothetical $P63/mmc$ - Fe_3Pt phase is mechanically unstable and prone to soft-mode distortions under elastic perturbation. Therefore, the combination of stress vs strain analysis and correlation fitting provides a robust means of assessing the elastic consistency and mechanical resilience of crystal systems.

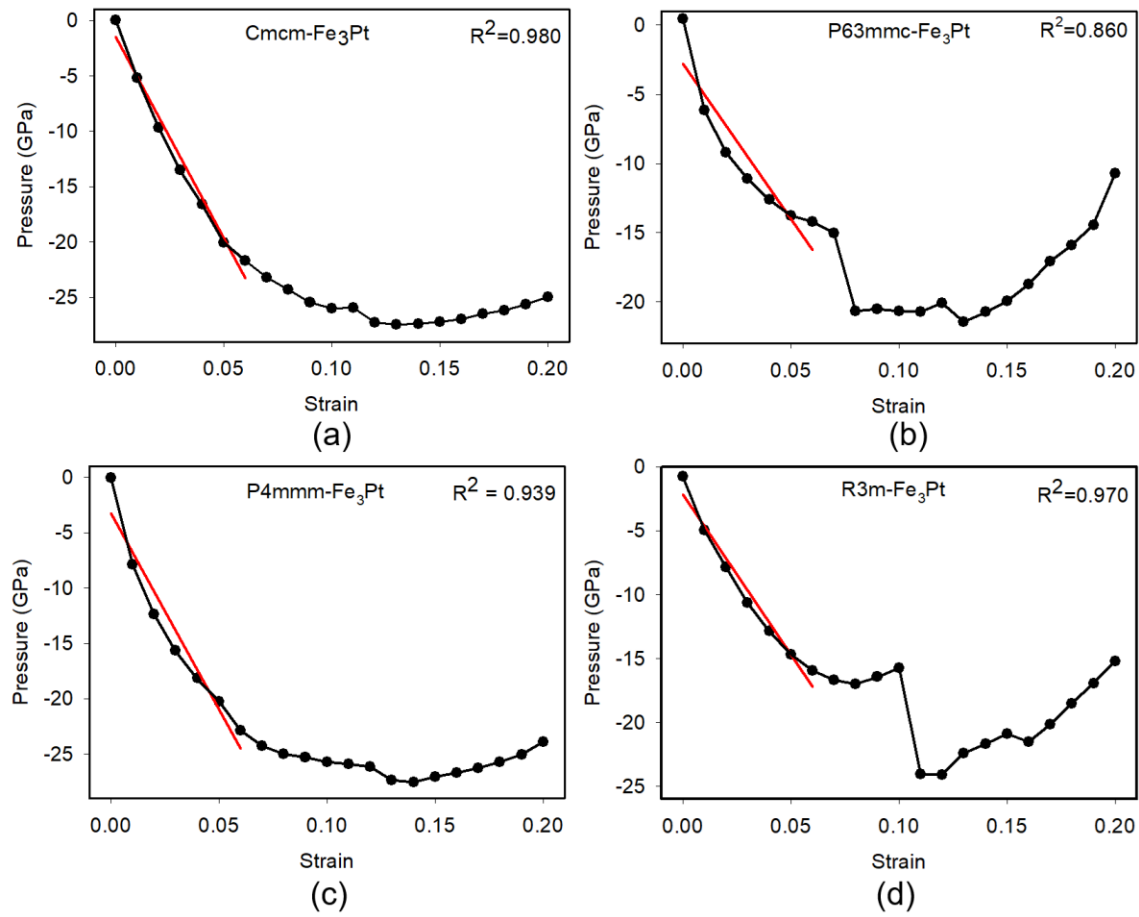


Figure 4. Stress vs strain curve with linear fit in the elastic region for Fe_3Pt alloys.

4. Conclusions

Density functional theory calculation on the martensite $Cmmm$, $P63/mmc$, $P4/mmm$ and $R\bar{3}m$ Fe_3Pt alloys were successfully carried out to determine the structural, thermodynamic, magnetic, electronic and mechanical properties. The negative enthalpies of formation showed that all the structures are thermodynamically stable. The substantial magnetic moments ranging from $2.94 \mu_B$ to $3.04 \mu_B$ and strong asymmetry of the spin up and down in the density of states plots, suggest strong magnetism and ferromagnetism behavior of the Fe_3Pt alloys. Calculations of independent and macroscopic elastic constant predicted mechanical stability on the $Cmmm$, $P4/mmm$ and $R\bar{3}m$ phases. However, the hypothetical $P63/mmc$ phase possesses negative C_{44} and shear modulus values, suggesting that it cannot exist under ambient conditions and would transform into a lower-symmetry and more stable phase. The observations collectively demonstrate that in addition to the $I4/mmm$ - Fe_3Pt alloy, there exist other martensite $Cmmm$, $P4/mmm$ and $R\bar{3}m$ phases which are thermodynamically and mechanically stable, highly magnetic, strongly ferromagnetic, ductile, and stiff, consistent with their martensitic character.

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