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Keywords: wood ash; nanosilica; compressive strength; flexural strength; artificial neural network (ANN); response surface methodology (RSM); concrete optimization; sustainable concrete; pozzolanic materials; strength prediction models



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Article

# Optimization of Mechanical Properties of Eco-Friendly Concrete Containing Wood Ash and Nano silica Using Response Surface Methodology and Artificial Neural Network

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#### **Abstract**

This study investigates the mechanical performance of concrete incorporating wood ash (WA) and nanosilica (NS) as partial cement replacements, with a focus on optimizing compressive and flexural strength. A total of 21 mortar mixes were designed and tested at various curing ages. Two modelling approaches—Response Surface Methodology (RSM) and Artificial Neural Networks (ANN)—were employed to analyse the effects and interactions of WA and NS on strength development. RSM provided insight into factor significance, while ANN captured complex nonlinear relationships with higher predictive accuracy ( $R^2 = 1.000$  for 28-day strength). The results showed that NS significantly improved strength up to an optimal dosage (~2.5 g), beyond which performance declined due to agglomeration or matrix over-refinement. Conversely, high WA content generally reduced strength due to dilution effects. Optimization revealed that blends with low WA ( $\leq$ 30 g) and moderate NS (2.0–2.5 g) achieved the best mechanical performance. ANN-based predictions outperformed RSM and multilinear regression, demonstrating its utility for mix design and performance forecasting in sustainable cementitious systems.

**Keywords:** wood ash; nanosilica; compressive strength; flexural strength; artificial neural network (ANN); response surface methodology (RSM); concrete optimization; sustainable concrete; pozzolanic materials; strength prediction models

# 1. Introduction

The construction industry faces escalating sustainability pressures, with concrete—second only to water in global consumption—responsible for roughly 8–10% of CO<sub>2</sub> emissions, largely from cement production [1–4]. Coupled with depletion of natural resources and mounting waste streams, this has accelerated the search for eco-friendly alternatives to conventional concrete constituents [5,6]. Two promising supplementary cementitious materials (SCMs) are wood ash (WA), a biomass-combustion by-product that valorizes waste within circular-economy principles, and nanosilica (NS), whose high specific surface area and reactivity can refine microstructure and boost mechanical performance [7–12]. Yet, optimizing mixes that incorporate multiple sustainable ingredients remains challenging due to nonlinear, interacting effects among constituents on fresh and hardened properties; traditional trial-and-error is slow, costly, and often misses these interactions, motivating data-driven modeling via Response Surface Methodology (RSM) and Artificial Neural Networks (ANN) [13–17].

Over the past two decades, WA has been explored as a partial cement replacement with typically weaker pozzolanic activity than fly ash but meaningful contributions through both secondary

reactions and filler effects [18,19]. Several studies report viable replacement levels on the order of 10–20% without major losses in mechanical performance when WA is properly characterized and processed [20,21]. Composition varies by fuel type and combustion conditions; higher  $SiO_2/Al_2O_3$  contents generally improve pozzolanic potential [22,23]. Beyond waste diversion, life-cycle assessments indicate carbon-footprint reductions up to ~15% at optimal dosages [24,25]. Practical challenges include variability, workability penalties, and unburnt carbon that may depress strength or entrain air [10,12].

NS improves concrete through a dual mechanism: rapid pozzolanic reaction with Ca(OH)<sub>2</sub> and nano-scale packing that densifies the matrix and refines the pore system [26,27]. Reported compressive-strength gains up to ~25% are common near 2–3% (by binder) when dispersion is well controlled [28,29]. Performance depends on particle size, surface chemistry, and dispersion method; agglomeration above optimal contents can erode benefits and reduce workability [30,31]. Reviews consistently document microstructural densification, reduced permeability, and durability gains attributable to NS-driven nucleation and pore refinement [32–34].

Combining WA and NS can yield complementary effects: NS supplies abundant nucleation sites and early-age reaction kinetics, while WA contributes longer-term pozzolanic reactions and filler action, jointly enhancing microstructure when proportioned appropriately [35–37]. However, the interaction is complex—spanning chemical, physical, and rheological domains—and requires systematic optimization to balance strength, durability, and workability.

To that end, RSM offers an efficient statistical framework to map factor effects and interactions with relatively few experiments, delivering predictive polynomials and significance analyses well suited to multi-variable mix design [38–42]. Recent sustainable-concrete studies have used RSM to optimize strength, workability, and durability with good fidelity and actionable operating windows [43–46]. ANNs, in turn, capture strongly nonlinear relationships without imposing parametric forms, often achieving higher predictive accuracy when trained on sufficiently rich datasets with appropriate architectures and regularization [47–50]. Comparative surveys report ANNs outperforming traditional regressions for strength prediction in complex binders, provided data quality and model design are adequate [51–53]; R² values >0.95 for compressive-strength prediction in mixes with multiple SCMs are frequently reported [54–57].

Despite this progress, key gaps persist: (i) limited studies that co-optimize WA and NS (and other SCMs) within an integrated design space; (ii) limited standardization of testing protocols and performance criteria for greener binders; (iii) sparse long-term durability data across environmental exposures; and (iv) few head-to-head comparisons of RSM versus ANN for sustainable-concrete optimization [61–67]. Addressing these gaps, the present study investigates eco-friendly concrete with WA and NS using both RSM and ANN to (i) quantify effects on compressive and flexural strengths at multiple curing ages, (ii) compare predictive/optimization performance of RSM and ANN in a shared dataset, (iii) identify optimal WA–NS combinations that maximize mechanical performance while advancing sustainability goals, and (iv) validate predictions and distill practical guidelines for implementation.

The contribution of this study is twofold: it delivers optimized, performance-based formulations that can reduce environmental burdens while maintaining or enhancing structural properties, and it provides a comparative modeling perspective to guide method selection (RSM vs. ANN) for complex, multi-variable sustainable systems. The outcomes support the development of performance-based specifications and can facilitate broader adoption of eco-friendly concretes in practice.

# 2. Methodology

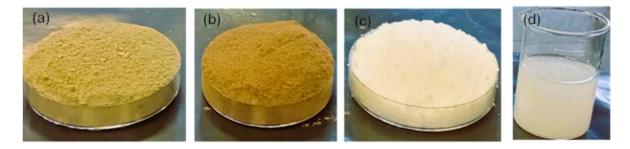
- 2.1. Materials and Methods
- 2.1.1. Chemical Properties of Materials

A previous experimental study by the authors [35] gives a full description of the materials used. Ordinary Portland cement conforming to SANS 50197-1 (CEM I 52.5 N) was used as the primary binder. Wood ash was collected from Blackwattle tree residues obtained from commercial caterers in

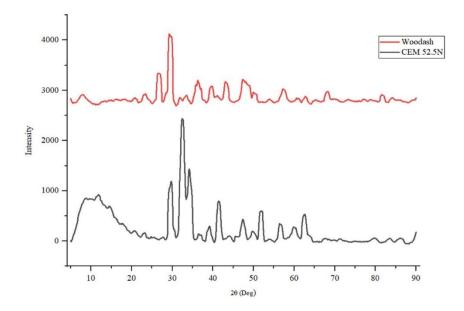
Johannesburg, oven-dried and sieved prior to use. A nanosilica solution was prepared by dissolving 3.5 g of SiO<sub>2</sub> powder in 13.201 L of distilled water as reported in the prior study this yields an approximate concentration of 0.265 mol·L<sup>-1</sup> and was used as part of the mixing water to ensure consistent dispersion during batching. Potable tap water was used for all mixes. The wood ash met the pozzolanic oxide criterion, with the combined  $SiO_2 + Al_2O_3 + Fe_2O_3$  content measured at 93.67 %, exceeding the 70 % threshold as provided in Table 1 below. X-ray diffraction patterns confirmed higher crystallinity for cement relative to wood ash, which exhibited broader humps typical of an amorphous-rich phase; peak intensity for wood ash occurred at  $2\theta < 30^\circ$ , while cement peaks were observed between 26–35°.

**Table 1.** Chemical and physical properties of wood ash (ZAWA).

Property	Value	Oxide	wt.%
Density (kg·m <sup>-3</sup> )	834	SiO <sub>2</sub>	53.57
Specific gravity	1.92	Al <sub>2</sub> O <sub>3</sub>	33.98
Mean size (µm)	0.4	Fe <sub>2</sub> O <sub>3</sub>	6.12
		MgO	6.23
		CaO	3.24
		MnO	1.66
		SO <sub>3</sub>	1.58
		Cl	0.07
		Na <sub>2</sub> O	0.00
		K <sub>2</sub> O	0.20
		TiO <sub>2</sub>	0.20
		P <sub>2</sub> O <sub>5</sub>	0.30
		SrO <sub>2</sub>	0.08
		ZrO <sub>2</sub>	0.96
		ZnO	2.66



**Figure 1.** Materials used: (a) CEM I 52.5 N; (b) wood ash; (c) nanosilica powder, (d) nanosilica solution prepared in distilled water. Adapted from the prior study [35].



**Figure 2.** XRD patterns of wood ash and CEM I 52.5 N showing lower crystallinity in wood ash relative to cement. Adapted from the prior study [35].

# 2.1.2. Mix Design and Preparation

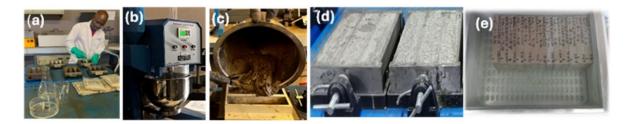
Mortar mixtures followed EN 196-1 proportions, batching  $450 \pm 2$  g cement,  $225 \pm 1$  g water, and  $1350 \pm 5$  g CEN standard sand per prism set. Wood ash replaced cement at 5, 10, 15, 20, and 25% by mass. Nanosilica was dosed at nominal 0, 0.6, 1.1, and 1.7% by binder mass and introduced as part of the mixing water to promote early dispersion. In total, twenty-one mixes were produced, with a water-to-binder ratio spanning 0.50–0.67 as determined by the fixed mass method and constant water content. Mix identities and exact batch masses are listed in Table 2.

The mixing sequence was standardized to minimize variability and ensure comparable dispersion of nanosilica. Water containing the nanosilica dose was combined with cement at time zero and mixed at low speed for 30 s. Standard sand was introduced gradually between 30 and 60 s with continuous mixing, followed by an additional 30 s at low speed to reach 90 s. A 30 s stop was used for bowl scraping, then the mix rested from 120 to 180 s, and finally was mixed at high speed from 180 to 240 s to achieve a homogeneous mortar suitable for casting.

Mix ID	PC	Sand	Water	Wood ash	NS
	(g)	(g)	(g)	(g)	(g)
CC	450.0	1350	225	0.000	0.000
WA05NS0	427.5	1350	225	16.071	0.000
WA10NS0	405.0	1350	225	31.143	0.000
WA15NS0	385.5	1350	225	48.214	0.000
WA20NS0	360.0	1350	225	64.286	0.000
WA25NS0	337.5	1350	225	80.357	0.000
WA05NS0.6	427.5	1350	225	16.071	1.350
WA10NS0.6	405.0	1350	225	31.143	1.350
WA15NS0.6	385.5	1350	225	48.214	1.350
WA20NS0.6	360.0	1350	225	64.286	1.350

Table 2. Mix proportions for wood-ash/nanosilica mortars

WA25NS0.6	337.5	1350	225	80.357	1.350
WA05NS1.1	427.5	1350	225	16.071	2.475
WA10NS1.1	405.0	1350	225	31.143	2.475
WA15NS1.1	385.5	1350	225	48.214	2.475
WA20NS1.1	360.0	1350	225	64.286	2.475
WA25NS1.1	337.5	1350	225	80.357	2.475
WA05NS1.7	427.5	1350	225	16.071	3.825
WA10NS1.7	405.0	1350	225	31.143	3.825
WA15NS1.7	385.5	1350	225	48.214	3.825
WA20NS1.7	360.0	1350	225	64.286	3.825
WA25NS1.7	337.5	1350	225	80.357	3.825

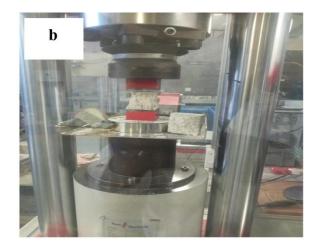


**Figure 3**. Representative preparation stages: mixing, mould filling, early-age prisms after 24 h, and water-curing. Adapted from the prior study [35].

#### 2.1.3. Casting, Curing, and Testing

Mortar prisms measuring  $40 \times 40 \times 160$  mm were cast in steel moulds. Specimens remained in the laboratory for 24 h, were then demoulded, and cured in water until the designated test ages of 3, 7, 14, 28, and 90 days. Mechanical tests followed SANS 5864. Flexural strength was determined by three-point bending on the full prism; compressive strength was measured on the two halves from the flexural test. All results represent the average of three specimens per age and mix. Testing was performed on a Toni Technik machine rated to 300 kN, with the flexural and compressive failure modes documented for quality control.





**Figure 4.** Test configurations and typical failure modes in flexure and compression on  $40 \times 40 \times 160$  mm prisms. Adapted from the prior study [35].

#### 2.2. Methods

#### 2.2.1. Response Surface Methodology (RSM)

The RSM [58] was employed to analyse the experimental results related to the flexural and compressive strength of cement mortars incorporating WA and NS. This statistical approach was used to evaluate the significance and interaction effects of the input variables—WA and NS dosage—on strength development at various curing ages. The quality of the developed model was assessed using statistical indicators such as the coefficient of determination (R²), adjusted R², and predicted R². The F-value was used to determine the relative influence of each factor, with a higher F-value indicating a more significant effect on the output response. The P-value was used to assess the statistical significance of the model and its terms; a P-value less than 0.05 was considered statistically significant, indicating that the factor or model term has a meaningful effect on strength development [59]. The RSM analysis in this study was conducted using Design Expert 12 (trial version), allowing for optimization and visualization of the influence of WA and NS contents on mortar performance.

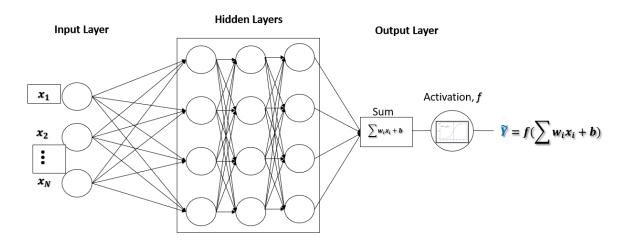
#### 2.2.2. Artificial Neural Network (ANN)

The Artificial Neural Network (ANN) approach was used to develop a predictive model for the strength performance of mortars containing wood ash and nanosilica. ANN is a computational model inspired by the biological neural networks of the human brain and is particularly effective for capturing nonlinear relationships among complex input variables[47][60,61]. In the context of this study, the ANN model was constructed using input features such as cement, sand, water, wood ash, nanosilica, and curing age, with the target output being either compressive or flexural strength. Each input parameter was weighted and combined using a set of learned coefficients (weights), followed by the application of a bias term. This process is illustrated in Figure 5, which shows a schematic representation of an artificial neuron. The mathematical formulation of a single neuron is given by Eq. (1) [62]:

$$y = f\left(\sum_{i=1}^{n} w_i x_i + b\right)$$
 1. 2. (1)

where  $x_i$  represents each input (e.g., WA, NS, water content),  $w_i$  is the corresponding weight, b is the bias, and f is the activation function applied to produce the output.

Model training and implementation were carried out using Python 3's scikit learn module [63], and hyperparameters were optimized [64] to improve prediction accuracy. The ANN model enabled robust prediction of mortar strength by learning from the experimental dataset and generalizing well to unseen mix compositions.



**Figure 5.** Schematic representation of an artificial neuron used in ANN modeling of strength in WA-NS blended mortars.

# 3. Results

# 3.1.28. Days Compressive Strength Analysis

In this section, the influence of WA and NS on the 28-day compressive strength of concrete was investigated using both RSM and ANN. The summary of the design of experiments used for RSM analysis is provided in Table 3. A total of 21 mixes were tested under a user-defined quadratic model structure with randomized run order.

**Table 3.** Design Summary of the RSM Method.

Study Type	Design Type	Design	Subtype	Runs	Blocks
		Model			
Response	User-	Quadratic	Randomized	21	No
Surface	Defined				Blocks

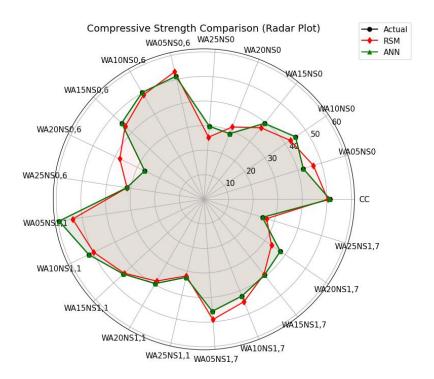
The regression model for compressive strength developed using RSM is expressed in Eq. (2):

$$f_{cs} = -0.0012A^2 - 0.0046AB - 0.2138A - 1.7224B^2 + 7.3100B + 50.3506$$
 (2)

where A is the wood ash content (g) and B is the nanosilica content (g).

Table 4. Actual and Predicted 28-Day Compressive Strength (MPa).

CC       51.2       50.35       51.2         WA05NS0       42.3       46.60       42.3         WA10NS0       45.1       42.52       45.1         WA15NS0       39.5       37.23       39.5         WA20NS0       28.7       31.61       28.7         WA25NS0       29.8       25.36       29.8         WA05NS0,6       51.3       53.23       51.3         WA10NS0,6       50.2       49.06       50.2         WA15NS0,6       45.6       43.66       45.6         WA20NS0,6       26.7       37.94       26.7         WA25NS0,6       31.7       31.59       31.7         WA05NS1,1       59.5       53.96       59.5         WA10NS1,1       51.9       49.71       51.9         WA20NS1,1       39.6       38.42       39.6         WA25NS1,1       32.6       31.99       32.6         WA05NS1,7       45.7       49.08       45.7         WA10NS1,7       42.3       44.74       42.3	Test Specimen	Actual CS (MPa)	Predicted CS (RSM)	ANN Predicted ( MPa )
WA10NS0       45.1       42.52       45.1         WA15NS0       39.5       37.23       39.5         WA20NS0       28.7       31.61       28.7         WA25NS0       29.8       25.36       29.8         WA05NS0,6       51.3       53.23       51.3         WA10NS0,6       50.2       49.06       50.2         WA15NS0,6       45.6       43.66       45.6         WA20NS0,6       26.7       37.94       26.7         WA25NS0,6       31.7       31.59       31.7         WA05NS1,1       59.5       53.96       59.5         WA10NS1,1       51.9       49.71       51.9         WA15NS1,1       44.7       44.23       44.7         WA25NS1,1       39.6       38.42       39.6         WA25NS1,1       32.6       31.99       32.6         WA05NS1,7       45.7       49.08       45.7         WA10NS1,7       42.3       44.74       42.3	CC	51.2	50.35	51.2
WA15NS0       39.5       37.23       39.5         WA20NS0       28.7       31.61       28.7         WA25NS0       29.8       25.36       29.8         WA05NS0,6       51.3       53.23       51.3         WA10NS0,6       50.2       49.06       50.2         WA15NS0,6       45.6       43.66       45.6         WA20NS0,6       26.7       37.94       26.7         WA25NS0,6       31.7       31.59       31.7         WA05NS1,1       59.5       53.96       59.5         WA10NS1,1       51.9       49.71       51.9         WA15NS1,1       44.7       44.23       44.7         WA25NS1,1       39.6       38.42       39.6         WA25NS1,1       32.6       31.99       32.6         WA05NS1,7       45.7       49.08       45.7         WA10NS1,7       42.3       44.74       42.3	WA05NS0	42.3	46.60	42.3
WA20NS0       28.7       31.61       28.7         WA25NS0       29.8       25.36       29.8         WA05NS0,6       51.3       53.23       51.3         WA10NS0,6       50.2       49.06       50.2         WA15NS0,6       45.6       43.66       45.6         WA20NS0,6       26.7       37.94       26.7         WA25NS0,6       31.7       31.59       31.7         WA05NS1,1       59.5       53.96       59.5         WA10NS1,1       51.9       49.71       51.9         WA15NS1,1       44.7       44.23       44.7         WA20NS1,1       39.6       38.42       39.6         WA25NS1,1       32.6       31.99       32.6         WA05NS1,7       45.7       49.08       45.7         WA10NS1,7       42.3       44.74       42.3	WA10NS0	45.1	42.52	45.1
WA25NS0       29.8       25.36       29.8         WA05NS0,6       51.3       53.23       51.3         WA10NS0,6       50.2       49.06       50.2         WA15NS0,6       45.6       43.66       45.6         WA20NS0,6       26.7       37.94       26.7         WA25NS0,6       31.7       31.59       31.7         WA05NS1,1       59.5       53.96       59.5         WA10NS1,1       51.9       49.71       51.9         WA15NS1,1       44.7       44.23       44.7         WA20NS1,1       39.6       38.42       39.6         WA25NS1,1       32.6       31.99       32.6         WA05NS1,7       45.7       49.08       45.7         WA10NS1,7       42.3       44.74       42.3	WA15NS0	39.5	37.23	39.5
WA05NS0,6       51.3       53.23       51.3         WA10NS0,6       50.2       49.06       50.2         WA15NS0,6       45.6       43.66       45.6         WA20NS0,6       26.7       37.94       26.7         WA25NS0,6       31.7       31.59       31.7         WA05NS1,1       59.5       53.96       59.5         WA10NS1,1       51.9       49.71       51.9         WA15NS1,1       44.7       44.23       44.7         WA20NS1,1       39.6       38.42       39.6         WA25NS1,1       32.6       31.99       32.6         WA05NS1,7       45.7       49.08       45.7         WA10NS1,7       42.3       44.74       42.3	WA20NS0	28.7	31.61	28.7
WA10NS0,6       50.2       49.06       50.2         WA15NS0,6       45.6       43.66       45.6         WA20NS0,6       26.7       37.94       26.7         WA25NS0,6       31.7       31.59       31.7         WA05NS1,1       59.5       53.96       59.5         WA10NS1,1       51.9       49.71       51.9         WA15NS1,1       44.7       44.23       44.7         WA20NS1,1       39.6       38.42       39.6         WA25NS1,1       32.6       31.99       32.6         WA05NS1,7       45.7       49.08       45.7         WA10NS1,7       42.3       44.74       42.3	WA25NS0	29.8	25.36	29.8
WA15NS0,6 45.6 43.66 45.6 WA20NS0,6 26.7 37.94 26.7 WA25NS0,6 31.7 31.59 31.7 WA05NS1,1 59.5 53.96 59.5 WA10NS1,1 51.9 49.71 51.9 WA15NS1,1 44.7 44.23 44.7 WA20NS1,1 39.6 38.42 39.6 WA25NS1,1 32.6 31.99 32.6 WA05NS1,7 45.7 49.08 45.7 WA10NS1,7 42.3 44.74 42.3	WA05NS0,6	51.3	53.23	51.3
WA20NS0,6       26.7       37.94       26.7         WA25NS0,6       31.7       31.59       31.7         WA05NS1,1       59.5       53.96       59.5         WA10NS1,1       51.9       49.71       51.9         WA15NS1,1       44.7       44.23       44.7         WA20NS1,1       39.6       38.42       39.6         WA25NS1,1       32.6       31.99       32.6         WA05NS1,7       45.7       49.08       45.7         WA10NS1,7       42.3       44.74       42.3	WA10NS0,6	50.2	49.06	50.2
WA25NS0,6       31.7       31.59       31.7         WA05NS1,1       59.5       53.96       59.5         WA10NS1,1       51.9       49.71       51.9         WA15NS1,1       44.7       44.23       44.7         WA20NS1,1       39.6       38.42       39.6         WA25NS1,1       32.6       31.99       32.6         WA05NS1,7       45.7       49.08       45.7         WA10NS1,7       42.3       44.74       42.3	WA15NS0,6	45.6	43.66	45.6
WA05NS1,1       59.5       53.96       59.5         WA10NS1,1       51.9       49.71       51.9         WA15NS1,1       44.7       44.23       44.7         WA20NS1,1       39.6       38.42       39.6         WA25NS1,1       32.6       31.99       32.6         WA05NS1,7       45.7       49.08       45.7         WA10NS1,7       42.3       44.74       42.3	WA20NS0,6	26.7	37.94	26.7
WA10NS1,1 51.9 49.71 51.9  WA15NS1,1 44.7 44.23 44.7  WA20NS1,1 39.6 38.42 39.6  WA25NS1,1 32.6 31.99 32.6  WA05NS1,7 45.7 49.08 45.7  WA10NS1,7 42.3 44.74 42.3	WA25NS0,6	31.7	31.59	31.7
WA15NS1,1 44.7 44.23 44.7 WA20NS1,1 39.6 38.42 39.6 WA25NS1,1 32.6 31.99 32.6 WA05NS1,7 45.7 49.08 45.7 WA10NS1,7 42.3 44.74 42.3	WA05NS1,1	59.5	53.96	59.5
WA20NS1,1       39.6       38.42       39.6         WA25NS1,1       32.6       31.99       32.6         WA05NS1,7       45.7       49.08       45.7         WA10NS1,7       42.3       44.74       42.3	WA10NS1,1	51.9	49.71	51.9
WA25NS1,1 32.6 31.99 32.6 WA05NS1,7 45.7 49.08 45.7 WA10NS1,7 42.3 44.74 42.3	WA15NS1,1	44.7	44.23	44.7
WA05NS1,7 45.7 49.08 45.7 WA10NS1,7 42.3 44.74 42.3	WA20NS1,1	39.6	38.42	39.6
WA10NS1,7 42.3 44.74 42.3	WA25NS1,1	32.6	31.99	32.6
	WA05NS1,7	45.7	49.08	45.7
	WA10NS1,7	42.3	44.74	42.3
WA15NS1,7 39.5 39.15 39.5	WA15NS1,7	39.5	39.15	39.5
WA20NS1,7 37.6 33.25 37.6	WA20NS1,7	37.6	33.25	37.6
WA25NS1,7 24.9 26.72 24.9	WA25NS1,7	24.9	26.72	24.9



**Figure 6.** Radar plot comparing actual and predicted (RSM and ANN) compressive strength values across all mixes.

The accuracy and significance of the RSM model were evaluated through Analysis of Variance (ANOVA), summarized in Table 5. The p-values indicate that nanosilica (NS) and its squared term  $NS^2$  significantly influenced compressive strength (p=0.0061 and p=0.0081, respectively) [59]. In contrast, WA and the interaction term  $WA \times NS$  were not statistically significant [59]. The RSM model demonstrated a high goodness of fit, with  $R^2=0.8447$  and adjusted  $R^2=0.7929$ .

		1	1	1
Source	Sum of Squares (SS)	df	F-value	p-value
WA	31.1778	1.0	1.7220	0.2092
NS	183.9173	1.0	10.1582	0.0061
WA <sup>2</sup>	7.9832	1.0	0.4409	0.5167
NS <sup>2</sup>	168.7324	1.0	9.3195	0.0081
WA × NS	0.5068	1.0	0.0280	0.8694
Residual	271.5787	15.0	-	-
Total R <sup>2</sup>	0.8447	-	-	-
Adj. R <sup>2</sup>	0.7929	-	-	-
Std. Dev.	3.5962	-	-	-
Mean	40.9714	-	-	-
C V (%)	8 7772	_	_	_

Table 5. ANOVA Table for Compressive Strength (RSM Model).

Figure 7. compares the regression fits of the two models. The ANN model achieved perfect correlation with an  $R^2=1.000$ , outperforming RSM model. This confirms that the ANN model more accurately captured the nonlinear relationships between the mix parameters and compressive strength. Ray et al. [65] likewise reported that ANN outperformed ANOVA.

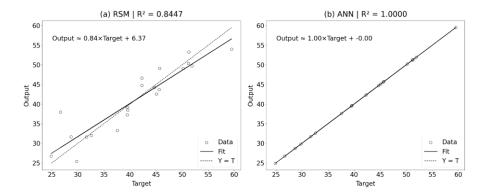


Figure 7. Predicted vs. Actual Compressive Strength: (a) RSM Model ( $R^2 = 0.8447$ ); ANN Model ( $R^2 = 1.000$ ).

The three-dimensional response surface plots shown in Figure 8 further illustrate how compressive strength varies with WA and NS. Both RSM (Figure 8a) and ANN (Figure 8b) models indicate that strength increases with NS up to a critical value ( $\sim 2$  g) beyond which it begins to decline. This trend is attributed to the beneficial pozzolanic effect of nanosilica up to an optimal dosage, beyond which particle agglomeration or excessive matrix refinement may occur [66][67]. Increasing WA, on the other hand, generally led to strength reduction, likely due to dilution of the cementitious matrix and pore structure disruption [68].

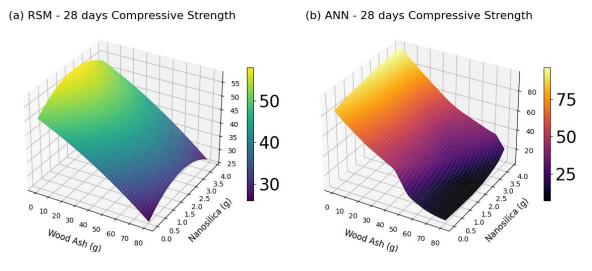


Figure 8. 3D Surface Plot of Compressive Strength: (a) RSM Model; (b) ANN Model.

Figures 9 and 10 present the optimization of compressive strength using RSM and ANN models, respectively. In the RSM model (Figure 9), the maximum predicted strength of 58.11 MPa was achieved at 0 g WA and 2.12 g NS, with a desirability of 1.00. This confirms that nanosilica significantly enhances strength, while excess wood ash reduces it [35]. The ANN model (Fig.10) predicted higher compressive strength (>60 MPa) under similar conditions. Its response surface shows greater nonlinearity and sharper gradients, highlighting its superior accuracy and sensitivity in capturing complex interactions [65]. Both models identify the same optimal region, but ANN demonstrates better predictive performance for mix design optimization.

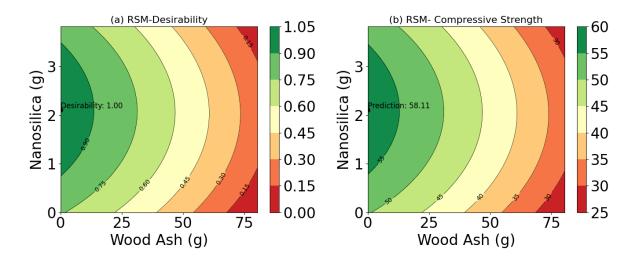


Figure 9. Optimization Plots for Compressive Strength using the RSM method: (a) Desirability, (b) Compressive Strength Surface.

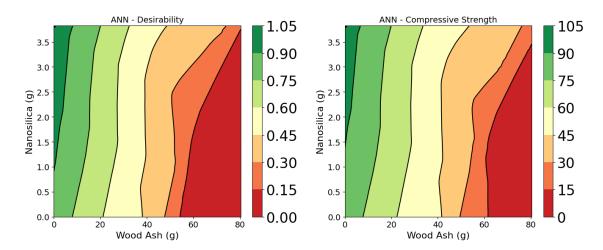


Figure 10. Optimization Plots for Compressive Strength using the RSM method: (a) Desirability, Compressive Strength Surface.

# 3.2.28. Days Flexural Strength Analysis

In this section, the effect of WA and NS on the 28-day flexural strength of concrete was investigated using both RSM and ANN. The same experimental matrix used for compressive strength (Table 3) was adopted for flexural strength analysis, under a user-defined quadratic model with randomized design.

The regression model for flexural strength using RSM is expressed in Eq. (3): 
$$f_{fs} = -0.0004A^2 - 0.0018AB - 0.0705A - 0.1183B^2 + 1.0081B \\ + 6.4034$$
 (3)

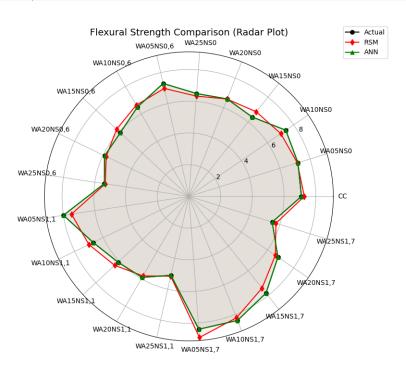
where A is the wood ash content (g) and B is the nanosilica content (g).

The experimental values and corresponding predictions for flexural strength by both RSM and ANN are presented in Table 6. The radar plot comparing actual and predicted values is shown in Figure 11, while the regression plots are provided in Figure 12.

Table 6. Actual and Predicted 28-Day Flexural Strength (MPa).

TEST SPECIMEN	ACTUAL FS (MPA)	PREDICTED FS (RSM)	ANN PREDICTED (MPA)
CC	7.10	6.40	7.10

WA05NS0	6.20	6.31	6.20
WA10NS0	5.60	5.76	5.60
WA15NS0	4.70	5.21	4.70
WA20NS0	3.20	4.30	3.20
WA25NS0	3.00	3.45	3.00
WA05NS0.6	7.40	7.14	7.40
WA10NS0.6	6.40	6.58	6.40
WA15NS0.6	5.70	6.01	5.70
WA20NS0.6	3.60	5.01	3.60
WA25NS0.6	4.00	4.11	4.00
WA05NS1.1	8.60	7.91	8.60
WA10NS1.1	7.40	7.34	7.40
WA15NS1.1	6.50	6.77	6.50
WA20NS1.1	5.10	5.76	5.10
WA25NS1.1	4.30	4.83	4.30
WA05NS1.7	6.90	7.34	6.90
WA10NS1.7	6.10	6.77	6.10
WA15NS1.7	5.10	6.20	5.10
WA20NS1.7	4.50	5.19	4.50
WA25NS1.7	3.10	4.27	3.10



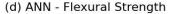
**Figure 11.** Radar plot comparing actual and predicted (RSM and ANN) flexural strength values across all mixes.

The ANOVA summary for the RSM model is presented in Table 7. Nanosilica and its square term were statistically significant (p = 0.0024 and 0.0049, respectively), while wood ash and its interaction with NS were not. The model achieved a good fit with  $R^2$  =0.8621 and adjusted  $R^2$ =0.8163, suggesting acceptable predictive capability.

Table 7. ANOVA Table for Flexural Strength (RSM Model).

Source	Sum of Squares (SS)	df	F-value	p-value
WA	6.2184	1	2.4146	0.1405
NS	27.4172	1	10.6411	0.0024
WA <sup>2</sup>	0.5801	1	0.2252	0.6410
NS <sup>2</sup>	23.8191	1	9.2410	0.0049
WA×NS	0.2186	1	0.0847	0.7743
Residual	38.6374	15	_	_
Total R <sup>2</sup>	0.8621	_	_	_
Adj. R <sup>2</sup>	0.8163	_	_	_
Std. Dev.	0.7586	_	_	_
Mean	5.6857	_		
C.V. (%)	13.3432	_	_	





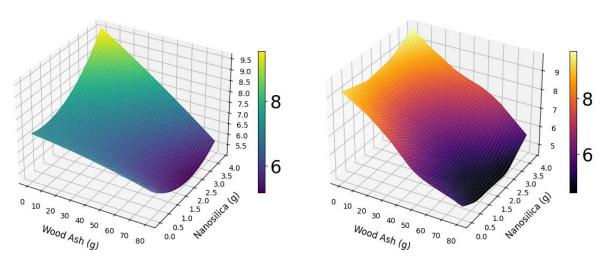


Figure 12. Predicted vs. Actual Flexural Strength: (a) RSM Model ( $R^2 = 0.8621$ ); (b) ANN Model. ( $R^2 = 1.000$ )

The 3D response surface plots in Figure 13 illustrate the effect of WA and NS on flexural strength. Both models confirm that flexural strength increases with NS content up to about 2.3 g and then declines, indicating a saturation point. Increasing WA beyond 10 g negatively affected strength, likely due to its filler role without contributing to bonding or hydration [36].

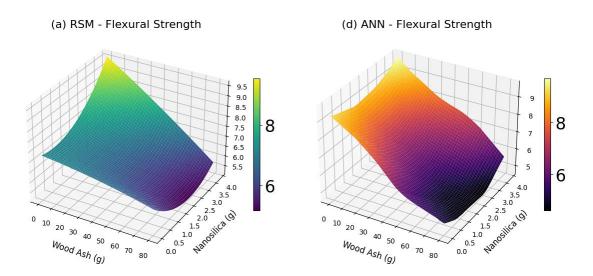
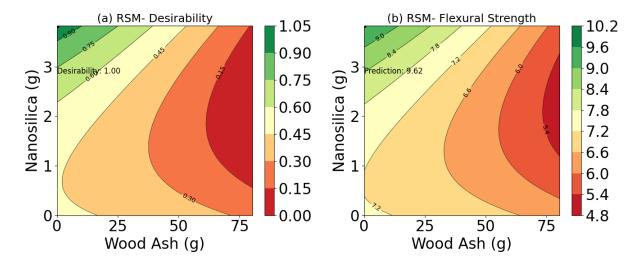
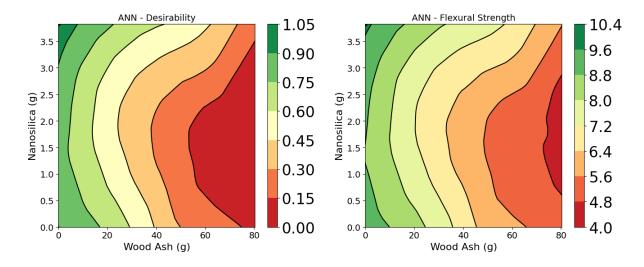


Figure 13. 3D Surface Plot of Flexural Strength: (a) RSM Model; (b) ANN Model.

Figures 14 and 15 show the desirability-based optimization plots. The RSM model (Figure 14) predicts a peak flexural strength of 9.18 MPa at 0 g WA and 2.3 g NS, with a desirability of 1.00. The ANN model (Figure 15) suggests slightly higher optimal strength, exceeding 10 MPa, within a similar input range, demonstrating a sharper optimal region. This supports the higher precision and robustness of the ANN model in capturing complex, nonlinear interactions in flexural strength behaviour [54].



**Figure 14.** Optimization plots for flexural strength using the RSM method: (a) Desirability, (b)Flexural strength surface.



**Figure 15.** Optimization plots for flexural strength using the ANN model: (a) Desirability; (b) Flexural strength surface.

#### 3.3. Compressive Strength Development with Curing Age

The development of compressive strength with curing age for the tested mortar mixtures is presented in Figs 16–18. These results are organized in two complementary ways: grouped by wood ash content (Figure 16) and grouped by nanosilica content (Figure 17). Model predictions from multilinear regression and ANN are shown in Figure 18.

#### 3.3.1. Experimental Insights

Figure 16 illustrates the effect of curing age on compressive strength across six levels of WA content (ranging from  $0.0\,\mathrm{g}$  to  $80.4\,\mathrm{g}$ ), with four NS contents  $(0.0\,\mathrm{g},\,1.4\,\mathrm{g},\,2.5\,\mathrm{g},\,\mathrm{and}\,3.8\,\mathrm{g})$  in each subplot. At  $0.0\,\mathrm{g}$  WA (Figure 16a), strength development is linear and steady across curing ages, with no variation due to NS because only one NS level was tested. At  $16.1\,\mathrm{g}$  WA (Figure 16b), the addition of NS begins to show significant early-age improvements, with NS =  $2.5\,\mathrm{g}$  and  $3.8\,\mathrm{g}$  resulting in notably higher compressive strength by 90 and 180 days.

For 31.1 g WA (Figure 16c), compressive strength continues to benefit from higher

NS content, with NS = 3.8 g yielding the highest strength (~70 MPa) at 180 days. However, as WA increases to 48.2 g and 64.3 g (Figures 16d–e), strength development begins to stagnate or decline at lower NS dosages, emphasizing the need for sufficient NS to offset the reduced reactivity and increased porosity from high ash replacement [32,37,69,70]. The 80.4 g WA mixtures (Figure 16f) show generally reduced strength, although NS = 3.8 g still provides a clear benefit. These results highlight a synergistic relationship between WA and NS, where higher NS levels can partially counterbalance the negative impact of high ash substitution [22,33,71].



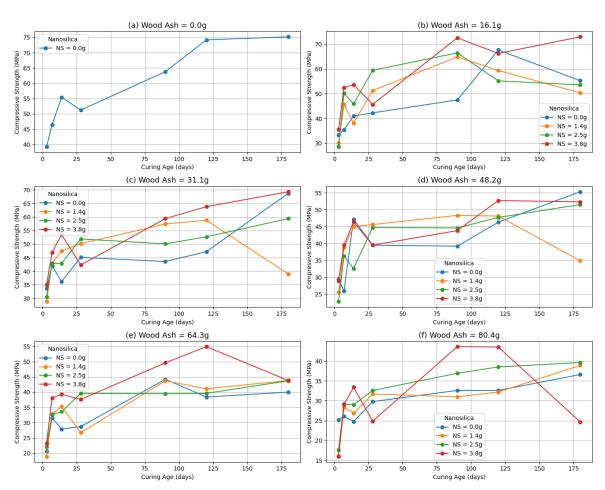
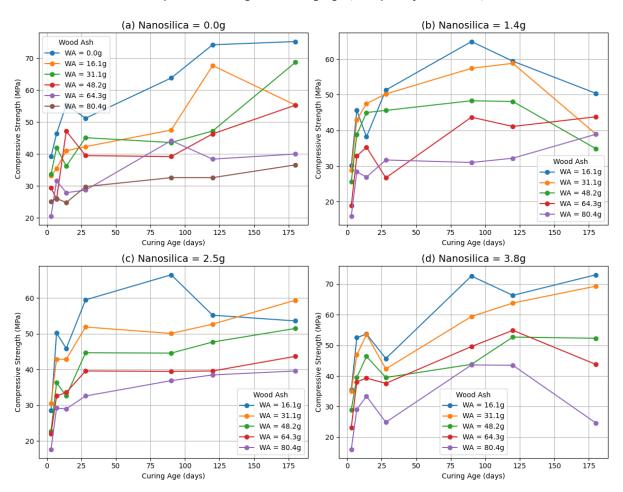


Figure 16. Compressive strength vs. curing age grouped by wood ash content: (a) WA = 0.0 g, (b) WA = 16.1 g, (c) WA = 31.1 g, (d) WA = 48.2 g, (e) WA = 64.3 g, (f) WA = 80.4 g. Each line represents a different nanosilica content.

To isolate the influence of nanosilica, Figure 17 reorganizes the dataset by NS dosage, showing four subplots for NS =  $0.0 \, \text{g}$  to  $3.8 \, \text{g}$ . Each subplot presents compressive strength evolution over time for six different WA contents. At NS =  $0.0 \, \text{g}$  (Figure 17a), strength gain is gradual but generally lower for higher WA mixtures, confirming the dilutive effect of unmodified ash [23]. With NS =  $1.4 \, \text{g}$  (Figure

17b), strength gain accelerates modestly, but inconsistencies remain at high WA levels. The NS = 2.5 g group (Figure 17c) shows significant improvement in strength consistency and overall gain, especially at 90 and 180 days. Most striking is the NS = 3.8 g set (Figure 17d), where even the high-WA mixtures achieve appreciable long-term strength. This suggests that a high NS content enhances pozzolanic reactions and improves matrix densification, thus mitigating the deleterious effects of increased ash content [67]. Overall, the data show that nanosilica not only improves early strength but sustains strength growth across a wide range of curing ages and ash replacements.

#### Compressive Strength vs Curing Age (Grouped by Nanosilica)



**Figure 17.** Compressive strength vs. curing age grouped by nanosilica content: (a) NS = 0.0 g, (b) NS = 1.4 g, (c) NS = 2.5 g, (d) NS = 3.8 g. Each line represents a different wood ash content.

# 3.3.2. Predictive Modelling and Performance Comparison

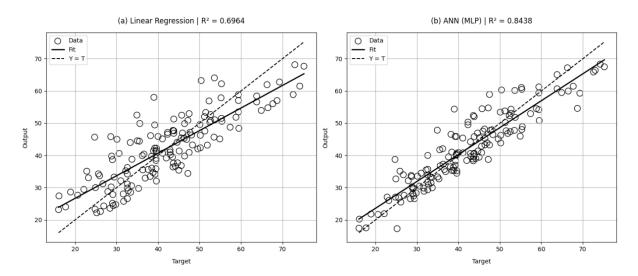
The predictive accuracy of the developed models is illustrated in Figure 18. The linear regression model (Fig.18a) shows moderate agreement with experimental data ( $R^2$  = 0.6964), with significant scatter especially at mid-strength levels. In contrast, the ANN model (Figure 18b), tuned via Optuna, achieves stronger correlation ( $R^2$  = 0.8438) and better captures the nonlinear relationship between mix proportions and strength development.

The learned linear regression model is expressed as:

$$\begin{split} f_c &= 19.90 + 0.0650 \cdot \text{ Cement } -0.0000 \cdot \text{ Sand } -0.0000 \\ & \cdot \text{ Water } -0.2485 \cdot \text{ WA } +0.7384 \cdot \text{ NS } +0.1030 \\ & \cdot \text{ Age} \end{split} \tag{4}$$

where  $f_c$  is the compressive strength (MPa), and all inputs are in grams, except curing age which is in days. The equation highlights that curing age and nanosilica content positively influence strength,

while higher wood ash content has a marginally negative effect when considered independently [28,29,34]. These results emphasize the limitations of linear models in capturing interaction effects and highlight the effectiveness of machine learning techniques for modelling complex material behaviour [51]. Both models benefit from incorporating curing age as a key predictor, reinforcing the importance of maturity in strength prediction.



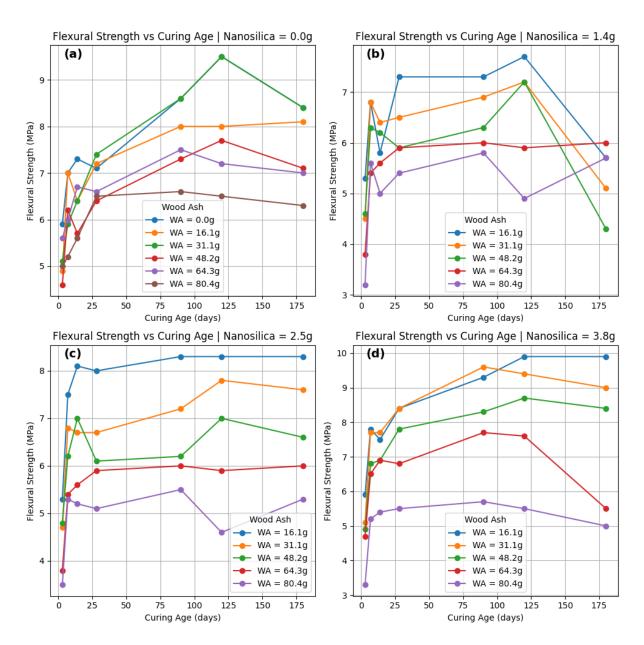
**Figure 18.** Actual vs. predicted compressive strength using: (a) Linear Regression, (b) Artificial Neural Network (ANN). Solid line = model fit; dashed line = ideal fit (Y = T).

#### 3.4. Flexural Strength Development with Curing Age

The development of flexural strength with curing age was comprehensively evaluated using both experimental analysis and predictive modelling through multilinear regression and an optimized ANN. The influence of curing age, WA, and NS on flexural performance is presented in Figure 19 - 21.

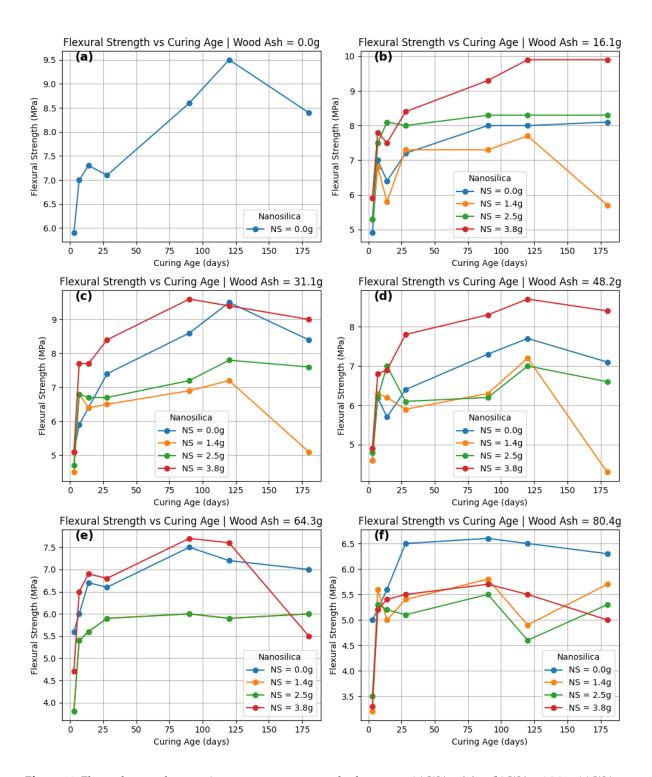
#### 3.4.1. Experimental Insights

Figure 19 illustrates the variation in flexural strength with curing age for different WA contents at fixed NS dosages. At  $0.0\,\mathrm{g}$  NS (Figure 19a), the flexural strength steadily increased with age, peaking around 120 days, especially for WA =  $31.1\,\mathrm{g}$  and  $48.2\,\mathrm{g}$ . However, strength declined at WA =  $80.4\,\mathrm{g}$ , possibly due to dilution effects [72]. As NS was introduced at  $1.4\,\mathrm{g}$  (Figure 19b) and  $2.5\,\mathrm{g}$  (Figure 19c), early-age strength improved and remained relatively stable, though higher WA levels began showing diminishing returns. At  $3.8\,\mathrm{g}$  NS (Figure 19d), strength was highest for mixes with WA between  $16.1\,\mathrm{g}$  and  $31.1\,\mathrm{g}$ , confirming an optimal synergy at moderate replacement levels.



**Figure 19.** Flexural strength vs. curing age at constant nanosilica content: (a) NS = 0.0 g, (b) NS = 1.4 g, (c) NS = 2.5 g, (d) NS = 3.8 g for varying wood ash dosages.

Figure 20 complements this by fixing WA levels and varying NS. At 0.0 g WA (Figure 20a), flexural strength peaked at 120 days with no benefit from NS. However, at 16.1 g WA (Figure 20b) and 31.1 g WA (Figure 20c), significant improvement occurred with 2.5 g–3.8 g NS. At 48.2 g WA (Figure 20d), this benefit persisted up to 120 days, while at higher WA levels (Figures 20e and 20f), flexural strength plateaued and eventually declined, indicating a threshold beyond which further WA replacement impairs mechanical gain.



**Figure 20.** Flexural strength vs. curing age at constant wood ash content: (a) WA = 0.0 g, (b) WA = 16.1 g, (c) WA = 31.1 g, (d) WA = 48.2 g, (e) WA = 64.3 g, (f) WA = 80.4 g for varying nanosilica dosages.

# 3.4.2. Predictive Modelling and Performance Comparison

Predictive models were trained to estimate flexural strength based on mix composition and curing age. The multilinear regression model produced the following equation:

Flexural Strength (MPa) = 
$$-7.0287 + 0.0321$$
·Cement +  $0.0000$ ·Sand + (5)  
 $0.0000$ ·Water +  $0.0141$ ·Wood Ash -  $0.1684$ ·Nanosilica +  $0.0086$ ·Curing Age

This model yielded an R² of 0.5445, suggesting modest predictive accuracy. In contrast, the optimized ANN model, tuned via Optuna [64], significantly outperformed the MLR, achieving an R² of 0.8408. This suggests that the nonlinear interactions among mix parameters were better captured by the ANN architecture [54,65]. Figure 21 presents the parity plots comparing predicted vs. actual values. The linear regression model (Figure 21a) shows larger scatter, especially at higher strengths, while the ANN model (Figure 21b) follows the ideal 1:1 line more closely.

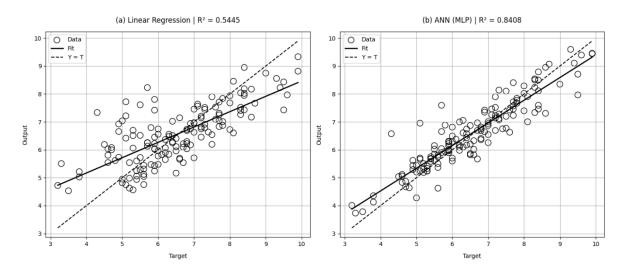


Figure 21. (a) Linear regression and (b) ANN (MLP) model predictions versus actual flexural strength values.

#### 4. Conclusions

This study investigated the optimization of the mechanical properties of concrete incorporating wood ash (WA) and nanosilica (NS) using Response Surface Methodology (RSM) and Artificial Neural Networks (ANN). Both methods were applied to model and predict compressive and flexural strengths at 28 days and across extended curing periods. The following key conclusions can be drawn:

- RSM and ANN were both effective in modelling the compressive and flexural strength of WANS blended mortars. However, ANN consistently outperformed RSM, achieving perfect correlation (R<sup>2</sup> = 1.000) for both strength types, indicating superior capability in capturing complex, nonlinear interactions among mix parameters.
- For 28-day compressive strength, RSM predicted a maximum of 58.11 MPa at 0 g WA and 2.12 g NS, while ANN predicted strengths exceeding 60 MPa under similar conditions. The analysis confirmed that nanosilica significantly enhances strength, while high wood ash content negatively impacts it due to dilution and matrix disruption effects.
- In terms of 28-day flexural strength, RSM predicted a peak of 9.18 MPa at 0 g WA and 2.3 g NS, while ANN exceeded 10 MPa, again validating the enhanced sensitivity of ANN to nonlinearities in the dataset.
- ANOVA results from RSM revealed that NS and its quadratic term were statistically significant (p < 0.01) for both strength types, while WA and interaction terms were not significant, suggesting that nanosilica primarily drives strength improvements.
- Time-dependent strength development analysis showed that:
  - Compressive and flexural strength improved consistently with curing age, especially for mixes with moderate to high NS content.
  - $\circ$  NS  $\geq$  2.5 g enhanced long-term strength, particularly in high WA mixtures, by promoting pozzolanic reactions and matrix densification.
  - o Strength deteriorated or plateaued beyond 64.3 g of WA, even with high NS, confirming the detrimental effect of excessive ash replacement.

- Multilinear regression (MLR) models performed modestly (R<sup>2</sup> = 0.6964 for compressive and 0.5445 for flexural strength), while ANN models trained with Optuna demonstrated higher accuracy (R<sup>2</sup> = 0.8438 and 0.8408, respectively), making ANN a more robust tool for predicting mechanical performance.
- Optimization analysis revealed that NS dosage in the range of 2.0–2.5 g consistently yielded the
  best mechanical properties across both strength metrics. Wood ash replacement should be kept
  below 30 g to avoid significant strength loss.

Overall, the combination of experimental validation, statistical modelling, and machine learning demonstrated that nanosilica plays a critical role in enhancing the mechanical characteristics of WA-blended concretes, while artificial neural networks offer superior performance for mix design optimization.

**Author Contributions:** Conceptualization, A.E., H.W. and A.A.R; methodology, A.E. and H.W.; validation, curation, A.E; wring-original draft preparation, A.E; writing-review and edition, A.E and H.W.; visualization, A.E; supervision, H.W. and A.A.R.; funding acquisition, A.E. All authors have read and agreed to the published version of the manuscript.

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**Data Availability Statement:** Data used in this study is part of the author's postdoctoral research Programme which can be made available upon request

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Conflicts of Interest: The authors declare no conflicts of interest.

#### **Abbreviations**

The following abbreviations are used in this manuscript:

WA Wood ash NS Nanosilica

RSM Response Surface Methodology ANN Artificial Neural Networks CS Compressive Strength

CC Control Concrete without WA and NS

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