

Review

Not peer-reviewed version

Properties, Advantages and Prospects of Use in Industry Cobalt-Free Composites Based on Tungsten Carbide

<u>Sherzod Kurbanbekov</u>*, <u>Yernat Kozhakhmetov</u>, <u>Mazhyn Skakov</u>, <u>Bekbolat Seitov</u>, Madina Aidarova, Yerkezhan Tabiyeva

Posted Date: 28 November 2024

doi: 10.20944/preprints202411.2212.v1

Keywords: cobalt-free solid composites; tungsten carbide; nickel; iron; SPS



Preprints.org is a free multidisciplinary platform providing preprint service that is dedicated to making early versions of research outputs permanently available and citable. Preprints posted at Preprints.org appear in Web of Science, Crossref, Google Scholar, Scilit, Europe PMC.

Copyright: This open access article is published under a Creative Commons CC BY 4.0 license, which permit the free download, distribution, and reuse, provided that the author and preprint are cited in any reuse.

Disclaimer/Publisher's Note: The statements, opinions, and data contained in all publications are solely those of the individual author(s) and contributor(s) and not of MDPI and/or the editor(s). MDPI and/or the editor(s) disclaim responsibility for any injury to people or property resulting from any ideas, methods, instructions, or products referred to in the content.

Article

Properties, Advantages and Prospects of Use in Industry Cobalt-Free Composites Based on Tungsten Carbide

Sherzod Kurbanbekov ^{1,2,*}, Yernat Kozhakhmetov ¹, Mazhyn Skakov ³, Bekbolat Seitov ², Madina Aidarova ¹ and Yerkezhan Tabiyeva ¹

- ¹ D. Serikbayev East Kazakhstan Technical University, 070004, UstKamenogorsk, Kazakhstan
- ² International Kazakh-Turkish University named H.A.Yassawi, 161200, Turkestan, Kazakhstan
- National Nuclear Center of the Republic of Kazakhstan, 180010, Kurchatov, Kazakhstan
- * Correspondence: sherzod.kurbanbekov@ayu.edu.kz; Tel.:+7 702 400 34 88

Abstract: This paper reviews recent advances in the synthesis of cobalt-free high-strength tungsten carbide (WC) composites as sustainable alternatives to conventional WC-Co composites. Due to the high cost of cobalt, limited supply and environmental concerns, researchers are exploring nickel, iron, ceramic binders and nanocomposites to obtain similar or superior mechanical properties. Various synthesis methods such as powder metallurgy, encapsulation, 3D printing and spark plasma sintering (SPS) are discussed, with SPS standing out for its effectiveness in densifying and preventing WC grain growth. The results show that cobalt-free composites exhibit high strength, wear and corrosion resistance, and harsh environment stability, making them viable competitors for WC-Co materials. The use of nickel and iron with SPS is shown to enable the development of environmentally friendly, cost-effective materials. It is emphasized that microstructural control and phase management during sintering are critical to improve material properties. The application potential of these composites covers mechanical engineering, metallurgy, oil and gas, and aerospace, emphasizing their broad industrial relevance.

Keywords: cobalt-free solid composites; tungsten carbide; nickel; iron; SPS

1. Introduction

As is known, solid composites are complex materials consisting of two or more elements that combine to achieve unique physical and mechanical properties. In this category, tungsten carbide (WC) takes center stage, acting as the main phase responsible for the high hardness and wear resistance of the composite. However, it is important to utilize suitable metallic elements as bonding phases to provide the required strength and fracture resistance.

Cobalt, often acting as a bonding phase, plays a crucial role in the mechanical performance of the composite. Its ability to form strong bonds with tungsten carbide particles increases the shear strength, which is especially important under intense mechanical loading conditions [1,2]. Due to this, WC-Co based composites have a wide range of applications in various industries including metalworking, mining and cutting tools.

Currently, WC is widely used in mechanical engineering, mining and machine tool industries. Due to their high wear resistance, chemical resistance (corrosion resistance), melting point and hardness, ceramics and tungsten carbide-based solid composites are used as wear-resistant materials [3,4].

At the same time, pure tungsten carbide has low fracture resistance and bending strength, therefore, to reduce the sintering temperature and increase physical and mechanical properties, plastic fusible metals (cobalt, nickel, iron, etc.) are introduced into the composition of ceramics [5,6].

However, in spite of a number of advantages, problems associated with the use of Co - price instability, toxicity and deterioration of some properties have recently appeared in the use of WC-Co composite, which requires the fabrication of WC parts without binder [7]. On the other hand, WC, or WC based composites, have not been commercialized and produced on an industrial scale so far, but have been used only to a limited extent for specialized applications such as high wear mechanical

seals and high temperature electrical contacts [8]. As follows from the analysis of the available literature, there are two problems in WC development: complete sealing of the sintered body and achievement of high impact toughness. A number of papers [9] provide a comprehensive summary of the current knowledge on sintering behavior, microstructure and mechanical properties of WC. They propose, to varying degrees, strategies for improving compaction, strengthening methods and reference materials for material practitioners who wish to improve WC characteristics with greater reliability, marketing them for further widespread use and preparing the material in an environmentally friendly way and inexpensive production. It is shown in [10] that the production of high density and high performance WC is economically and technically feasible. The practically important properties of WC can be tuned by a judicious choice of chemical composition combined with careful consideration of the influence of production methods and processing parameters.

Along with this, WC-Co composites are known to be the strongest known sintered carbide composites, although they do not always fulfil the requirements for serviceability. Thus, in the total mass of amortized tools, wear and breakage of carbide elements account for 80%. Therefore, it is believed that one of the promising directions of improving the properties of solid composites is the development of technologies for obtaining, providing increased wear resistance while maintaining the necessary toughness. It is the totality of such properties of materials that provides durability of any tool made of them, perceiving high-intensity loads during cutting, stamping, rock drilling, etc. [11,12].

The most commonly used cemented carbides in practice consist of ceramic grains of tungsten carbide embedded in a metal matrix of cobalt. These WC-Co composites have an excellent combination of mechanical, physical and chemical properties, making them suitable for a wide range of applications requiring high values of hardness, mechanical strength and heat resistance [13,14].

Currently, there are many WC-Co based composites, differing in cobalt content, carbide particle size, the presence of various hardening and inhibiting additives, etc. Such composites always contain two obligatory components in their composition: WC tungsten carbide, which acts as a "solid phase", and cobalt Co, which is used as a binder [15]. The combination of the excellent mechanical properties of tungsten carbide with the ductility and high fracture toughness of cobalt provides high hardness, strength and wear resistance of WC-Co composites. Due to this, they are widely used as tool materials in metalworking and mining industries [16]. Moreover, many researchers believe that the most promising way to improve the performance characteristics of WC-Co-based solid composites is to create fine-grained microstructures or even nanostructures in them. This requires the use of fine and nanocrystalline powders of both tungsten carbide and cobalt, as well as special sintering procedures [17].

Cemented WC is commonly used for wear-resistant applications such as cutting tools and abrasives because of its extremely high hardness [18]. This hardness causes WC post-processing to become labor intensive and expensive. The bonding phase in the fabricated samples is an iron-based composite that has a lower melting point than cobalt, a common bonding agent in cemented WC. In this paper [19], cube-shaped WC samples with a low iron-based composite binder were printed; the effect of different processing conditions on the resulting density and microstructure of the material was investigated. Theoretical densities of up to 95% were achieved using this method. Artefacts indicative of the manufacturing process are present in the samples and the problems associated with removing the processing history from the final microstructure are discussed.

Current research shows the possibility of improving the properties of WC composites by introducing new materials and technologies to increase density and mechanical strength while reducing environmental and economic risks. The development of composites with reduced cobalt content or its complete exclusion is a promising direction and an alternative solution, contributing to the expansion of WC composites application in industry and reducing their negative impact on the environment and human health.

2. Problems of Cobalt Utilization in Traditional Composites: Resource, Environmental and Economic Aspects

A detailed analysis of the studies performed shows that the use of cobalt in traditional composites faces a number of science-based challenges. Firstly, cobalt is a rare element, which creates resource constraints as its reserves are concentrated in a limited number of countries, resulting in

unstable supply chains. Second, the mining and processing of cobalt involves environmental risks, including pollution, as cobalt has toxic properties. Third, the high cost of mining and refining cobalt makes its use in composites uneconomical, especially with the increasing demand for this metal in modern technologies such as batteries and electronics [20–24].

This is because the raw materials used in production, i.e. WC and Co, are considered strategic by the European Union due to its supply risk [25,26]. In addition, the law on the regulation of the registration, evaluation, authorization and restriction of chemicals of the European Union (EU-REACH programmer) and other studies classify cobalt and metal dust as potentially hazardous substances for living organisms, which further substantiates the need for solid materials alternatives to conventional WC-Co composites [27–29].

Thus, the need to find alternatives to conventional WC-Co composites is due to the high strategic importance of cobalt as a raw material whose reserves are mainly controlled by the People's Republic of China [30]. In conditions of limited access to this metal, the risks of disruptions in its supply are increasing, which is especially relevant for the countries of the European Union, where cobalt is a key element not only for the production of WC based tooling materials, but also for the manufacture of batteries for electric vehicles. With the development of the electric vehicle market, cobalt consumption is growing rapidly, increasing its scarcity and price volatility. These factors emphasize the importance of developing alternative materials, such as nickel and iron-based composites, which can not only replace cobalt in WC composites, but also ensure supply stability and reduce dependence on limited and expensive raw material sources [31–34]. It should be noted that of the three elements, iron (Fe), nickel (Ni), cobalt (Co) has traditionally been the most favored choice due to its outstanding properties such as high wettability and excellent adhesion to tungsten carbide. These characteristics make cobalt an important component in traditional WC-Co composites, where it not only contributes to the formation of a homogeneous microstructure but also provides strength, fracture resistance and excellent mechanical properties [35].

However, there is thus some motivation for scientists and engineers to search for alternative metallic binders to cobalt that can provide comparable or even better mechanical performance at lower cost and with less environmental impact. Therefore, the study of cobalt-free tungsten carbide-based composites without cobalt is becoming an important area in materials science, opening new horizons for the development of sustainable and cost-effective materials for industry.

Based on the above considerations, there is an urgent need to find substitutes for the traditional cobalt binder phase in WC based metal-ceramic hard coatings. This has prompted researchers to look for alternatives to cobalt and iron, nickel and some of their compounds are suggested as substitutes.

3. Alternative Bonding Materials for Tungsten Carbide-Based Composites

Cobalt-free WC composites are promising materials with significant advantages over traditional WC-Co composites. Eliminating cobalt from the composition reduces health and environmental impacts, making such composites more sustainable and safer for humans. In addition, lower manufacturing costs due to the absence of cobalt make cobalt-free composites cost-effective. They exhibit high mechanical properties including strength, wear resistance and corrosion resistance, which enhances their application in industries such as mechanical engineering, metallurgy and oil and gas [36]. Due to the technological flexibility provided by various synthesis methods, including powder metallurgy and 3D printing, cobalt-free composites can be adapted to specific operating conditions, including high temperatures and aggressive environments, which emphasises their relevance to modern manufacturing technologies.

Along with this, cobalt-free WC based solid composites are promising materials for applications with high mechanical loads, temperatures and wear resistance [37].

Growing concerns about the use of cobalt as a binder in WC based hard composites have led to the investigation of iron alloys as alternatives. Studies show that replacing cobalt with Fe alloys under strict control of carbon content significantly improves mechanical properties. In addition to improving hardness and fracture toughness, the transverse tensile strength of WC-Fe composites

show significant potential for further improvement through microstructure optimisation, such as reducing porosity during sintering [38–41].

Studies also show that cobalt-free solid composites containing nickel (Ni) and iron (Fe) as binders exhibit high levels of strength, wear resistance and hardness. For example, the work of Qu et al. [42] shows that Ni-Fe-based composites can achieve compressive strengths of up to 3.5 GPa, while improving wear resistance by a factor of 1.5 compared to their cobalt counterparts. Furthermore, the results of a study by Wang et al. [43] emphasize that nickel and iron have good adhesion properties to tungsten carbide, providing a strong bond between WC particles, which is crucial for improving the mechanical properties of composites.

One of the key advantages of cobalt-free composites is their resistance to corrosive environments, making them attractive for corrosive applications. Studies confirm that nickel provides high corrosion resistance in chemically aggressive environments such as acids and alkalis [44]. Iron, in turn, improves mechanical properties and contributes to the hardness of the material. The work of Xu et al. [45] showed that the combination of nickel and iron can produce property-balanced composites with good strength and wear resistance, which is a significant advance over traditional cobalt composites.

Current research also shows the high potential of cobalt-free composites for applications in various industries including engineering, oil and gas, metallurgy and aerospace. For example, research [46] demonstrates that the application of SPS technology can achieve high composite densities with minimal grain growth, which is crucial for maintaining the wear resistance of the material. In addition, [47] emphasizes that Ni-Fe based composites are not only able to compete with their cobalt-based counterparts, but also open new horizons for the creation of safer and more cost-effective materials.

Apparently, the development and study of cobalt-free composites based on tungsten carbide with nickel and iron is an actual direction of scientific research that can significantly influence the future of materials science and industrial application of solid composites.

Nickel is known to have sufficient mechanical strength, good corrosion resistance and relatively low cost. Therefore, it may be one of the most promising solutions to replace cobalt in WC composites. When nickel is added, WC-Ni composites can retain high hardness and wear resistance, although these values may be lower compared with WC-Co. The use of nickel not only reduces the material cost but also the environmental load. Indeed, as follows from the results of [48–51], the replacement or displacement of Co by Ni improved the corrosion resistance as well as the wear resistance of WC based hard composites in aggressive environments. Fe and Ni as alternative binders in WC-(Fe-Ni) composites provide significant advantages. Ni is more suitable for applications requiring corrosion and oxidation resistance, mainly in tribological applications [52,53]. In [54,55], studies were carried out on the preparation of WC-(Fe-Ni) based solid composites using iron and nickel, as substitutes in whole or in part. They showed that WC-(Fe-Ni) composite can have better mechanical and microstructural properties compared to WC-Co composites. In addition, WC-Ni-Fe components are mutually inert, without chemical interaction during sintering, which can preserve the shape and high strength of the composite [56]. However, a significant amount of Fe can reduce the optimal range of free carbon ("carbon window") and thus favor the formation of η -phase.

Aluminum is less commonly used in WC composites and is added to reduce the overall density of the material and to improve oxidation resistance at high temperatures [57]. Aluminum can contribute to hardness, but excessive amounts can reduce the ductility of composites [58]. However, when combined with other elements such as molybdenum or copper, aluminum can help to improve the overall balance of properties. Silicon is added to WC composites to improve thermal stability and wear resistance [59]. It also helps to improve corrosion resistance by reducing the tendency to oxidise at high temperatures. However, at high concentrations, silicon can increase the brittleness of composites, which limits its application.

In [60], the interfacial bonding properties of WC/Co and WC/ CoNiFe were investigated based on the aforementioned physical and mechanical properties. WC/Co and WC/ CoNiFe materials were synthesized using conventional powder metallurgy and the modelling results were verified by

microstructure analysis, electron function gradient method and mechanical property evaluation. The main findings of the study are as follows:

- The binding energies at the WC/Co and WC/CoNiFe interfaces were calculated according to the first principle, and the binding energy of Co with WC is slightly higher than that of CoNiFe with WC. This suggests that replacing Fe and Ni with part of Co weakens the bonding properties at the WC/Co interface, but the effect is negligible.
- The atomic bond strength at the WC/Co and WC/CoNiFe interfaces is mainly determined by the contribution of the d-electron orbitals of the atoms. According to the difference of charge density and density of states, the atomic bond strength is W-Fe>W-Co>W-Ni. Fe atoms play a major role in the strength of WC/CoNiFe interface.
- The porosity of WC/CoNiFe carbide is 0.78%, which is much lower than that of WC/Co material. The WC/Co material has non-uniform pore distribution. The highest average hardness and lowest average hardness of WC/Co carbide are 1320 HV and 1182 HV samples with non-uniform hardness distribution. The hardness of WC/ CoNiFe carbide is relatively more uniform, with the highest value of 1192 HV.

The densification mechanism at the first heating stage is related to the plastic flow process, the intensity of which is limited by the diffusive creep rate of cobalt. Increasing the concentration of free carbon in the composition of the initial WC-10Co mixture does not affect the intensity of the densification process and, consequently, the activation energy of EIPS in the region of "average" heating temperatures. The activation energy of isothermal and non-isothermal sintering in the region of "medium" temperatures is close to the activation energy of grain boundary diffusion in cobalt. In the region of "high" temperatures, the activation energy of non-isothermal sintering monotonically decreases with increasing concentration of free carbon in WC-10Co carbide. It was shown by X-ray phase analysis that the reason for the decrease in the activation energy of EIPS may be a change in the concentration of tungsten and carbon atoms in cobalt [61].

In addition to the above studies conducted to completely replace Co with alternative bonding components, a study was also conducted to partially replace Co with Ni and Fe [62].

The effect of composition on carbide formation in the WC-M (M = Fe/Ni/Cr) system was studied with three compositions containing 10 wt.% metallic binder [63]. Replacing half of the Fe binder with Ni stabilized the formation of austenite Fe (γ). Adding Cr to the binder led to Cr₂C carbide formation, while reducing Cr content resulted in M₆C carbide instead. To eliminate M₆C, 3.6 wt.% excess carbon was added. These results were analyzed based on phase formation, binder composition, and carbon content. In this paper [64], a method for obtaining WC-5TiC-10Co carbide with a density equal to 100% of the theoretical value, hardness 1484 HV and bending strength 1924 MPa is presented. The high quality of the product is provided by the original research method based on mechanochemical synthesis of WC and TiC powders using available precursors. and implementation of high-speed SPS-compacting of the obtained powder with achievement of high packing degree with minimum grain growth at temperature 1200 °C and processing time not more than 13 min. Experimental data on the compaction dynamics, phase composition, morphology and mechanical properties of WC-TiC-10 Co using SPS in the temperature range from 1000 to 1200 °C are presented. Pan et al. [65] confirmed the formation of η - phase in composites of WC-30% wt. Fe, WC-50% wt. Fe and WC-70% wt. Fe.

The use of cobalt-free WC based composites, in which cobalt is replaced by nickel and iron, represents an important technological step in the development of sustainable and cost-effective materials [66]. These composites retain key mechanical properties such as high hardness and wear resistance, while exhibiting improved corrosion and crack resistance due to the uniform distribution of nickel and iron in the WC matrix. Not only are cobalt-free composites less expensive due to the substitution of scarce and expensive cobalt, but they are also more environmentally friendly, reducing environmental impact. In addition, the stability of their supply reduces dependence on strategically limited resources, making such materials more attractive for use in a variety of high-tech industries, including mechanical engineering, aerospace and energy.

4. Technologies for Synthesis of WC Composites

Synthesis technologies for WC composites include various methods aimed at optimising the mechanical properties and performance of the materials. The most common technologies are powder metallurgy, SPS, hot isostatic pressing (HIP), and 3D printing.

To date, there are many technologies for the synthesis of cobalt-free solid WC composites. For example, in [67] on the partial substitution of Co by Ni and Fe, WC/Co and WC/CoNiFe materials were prepared using conventional powder metallurgy. WC, Co, Ni and Fe powders (with a mass ratio of 6:2:1:1:1) and WC and Co powders (with a mass ratio of 6:4) were mixed using a Retch GmbH planetary ball mill for 1 h at a rotational speed of 200 rpm, and then the mixed powders were pressed into cylindrical billets with a diameter of 3 mm and a height of 12 mm using a WDW-300 universal testing machine at an instantaneous pressure of 1000 MPa. Kelvin probe force microscopy (KPFM) results showed that the interface bond strength of conventional WC/Co carbide is consistent with the results of first-principles calculations and slightly higher than that of WC/CoNiFe carbide, but the addition of Ni and Fe atoms does not weaken the interface strength significantly.

The following encapsulation technology is a technique in which WC particles are coated with a layer of binder material [68]. This process favors a more uniform distribution of the binder on the surface of the carbide particles, which improves the quality and homogeneity of the composite [69]. In addition, encapsulation provides better wetting and fluidity of the material during the sintering process, which helps to reduce porosity and increase mechanical strength [70]. This method is particularly effective for the creation of composites with fine-grained structure, which have increased hardness and wear resistance [71]. However, encapsulation requires careful selection of binder and shell materials to prevent structure failure at high temperatures [72]. The encapsulation process can lead to non-uniform coating of carbide particles, which deteriorates the mechanical properties of the composite and its wear resistance Additive manufacturing technologies such as 3D printing open new horizons in the synthesis of cobalt-free composites [73]. The layer-by-layer deposition of powder materials and their sintering allows the fabrication of products with precise geometries while reducing material and manufacturing costs [74]. However, the disadvantage is that 3D printing is slow and less productive for large-scale industrial production, which limits its application.

There is also a method of OPS - oscillatory pressure sintering. This method can improve compaction and reduce the grain size of the material and was applied in [75]. This work showed that the OPS-sintered composite exhibited solid-phase sintering at low temperatures (<1240 °C) and liquid-phase sintering at higher temperatures (>1240 °C). In both temperature ranges, the OPS-sintered samples have higher densities.

WC based sintered carbides are widely used as hard materials, but their conventional processing requires long production cycle and high cost due to the need for mould design. In this study, the effect of additive manufacturing parameters by laser powder bed fusion (LPBF) on the formability of sintered WC carbides with different amounts of Ti as binder (WC_xTi, x = 10, 15 and 20 wt%) was examined. The results showed that WC-20Ti has the best formability and the highest density. The optimum printing parameters for this alloy are laser power of 175 W and scanning speed of 600 mm·s⁻¹. The printed WC-20Ti accessories and gears achieved a hardness of 1476±50 HV1, a compressive strength of 1.75 GPa, and good corrosion resistance (0.1986 mm·a⁻¹). These properties are attributed to the high density, homogeneous microstructure with an average grain size of 5.02 μ m and the formation of solid phases (WC, W₂C and TiC) during printing [76].

WC-Co hard metal samples were fabricated using WC-Co nanopowder with selective laser melting (SLM) and fused deposition modeling (FDM). Carbon loss during SLM led to lower relative density and hardness, while FDM produced more stable WC phase cemented carbide with higher density due to optimized filament packing. Sintered FDM samples achieved a relative density of 96.3%, hardness of HRA 89.06, and a carbon content of 5.47-5.52 wt.% [77].

WC-Co composite was produced by material extrusion 3D printing, overcoming casting challenges due to high melting points. A 54 vol% solid content paste was optimized for dispersant, solvent, and binder composition, achieving homogeneity through a binder coating. Sintering at $1400\,^{\circ}$ C in vacuum yielded a relative density of 99%, with hardness and fracture toughness measured at $16.5\,^{\circ}$ GPa and $16.5\,^{\circ}$ MPa·m¹/², comparable to powder metallurgy WC-Co. This method improves

Liquid ink-printing followed by sintering was used to fabricate WC-Co microlattices and cutting tools, with WC-xCo (x = 0.5-20 wt.%) microstructures examined at varying Co ratios and sintering temperatures. Microlattices with 0.5-5 wt.% Co showed residual porosity due to incomplete densification, while fully dense struts were achieved with 10 wt.% Co at 1450 °C. WC-10Co lattices, modeled by finite-element methods, demonstrated elastic support through a 0/90° cross-ply structure, while Cu infiltration at 1300 °C formed WC-Cu composites with high thermal conductivity (140±7 W/(m·K)). The WC-Cu structure exhibited ductile compression behavior, contrasting with brittle WC-Co lattices. A 3D-printed WC-Cu tool exhibited lower temperatures under laser heating than a uniform WC-Co tool due to its enhanced internal architecture [79].

3D gel-printing (3DGP) is an innovative method for creating 3D components by layering and gelatin metal slurry. Using WC-20Co slurries with 47-56 vol.% solid loading, components were formed by 3DGP and sintered in a vacuum furnace. The slurries' fluidity and shear-thinning behavior supported the 3DGP process, with nozzle diameter and filling rate affecting surface quality and dimensional accuracy. Optimal samples showed good shape retention, uniform microstructure, density of 13.55 g/cm³, hardness of HRA 87.7, and transverse rupture strength of 2612.8 MPa, making 3DGP effective for near-net shaping of complex WC-20Co parts [80–82].

In [83] this technique, a slurry of powder and organic monomers is fed into a screw extruder with compressed air pressure, where an initiator and catalyst are added, mixed, and extruded layer by layer onto the build platform which is shown in Figure 1. The organic monomer quickly polymerizes, fixing the solid powder in place, forming a green body.

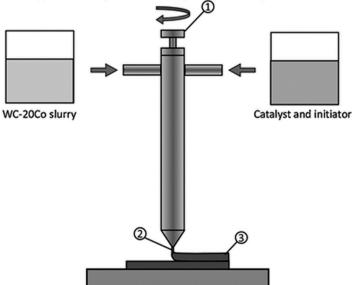


Figure 1. Schematic diagram of 3DGP, (1) screw extruder, (2) nozzle, and (3) green body [83].

Binder Jet Additive Manufacturing (BJAM) is an additive technology in which metal powders are bonded with a liquid binder and then sintered to form high-strength parts. In the BJAM process, the powder is distributed on a substrate and bound with liquid binders to produce a 'green' part, which then goes through a binder removal and sintering step to form a metal part. The sintering temperature for WC-Co is typically above 1400 °C. The fabricated parts are often highly porous and may be impregnated with a metal such as cobalt to improve properties, making it difficult to accurately control the Co content of the sample [84,85].

In work [86] WC-Co alloy was obtained by 3D printing by material extrusion. A paste with a high solid content was prepared and the paste composition was optimised for rheological characteristics depending on the dispersant, solvent and binder content which is shown in Figure 2.

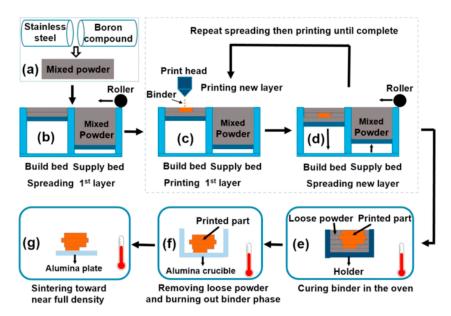


Figure 2. Schematic diagram of BJAM process [86].

Kim et al. [87] investigated WC based cermet's with Ni as a bonding phase. They were able to fabricate WC-Ni based cermet's with a density of 98% using high frequency induction heating by sintering (HFIHS). The sample had a WC grain size of 300 nm after sintering. The measured hardness values were significantly higher than for the traditionally sintered WC-Co and WC-Ni systems without any noticeable decrease in fracture toughness.

Fused Filament Fabrication (FFF) is an additive manufacturing technology similar to 3DGP but uses powder to prepare filament instead of powder slurry as the printing material. The filament preparation involves mixing the powder with a main binder and a backbone, followed by extrusion using a high-pressure capillary rheometer. During printing, the filament is deposited on a printing platform to form a green part. After printing, a deboning process, including solvent deboning followed by thermal deboning, is performed before sintering the part [88].

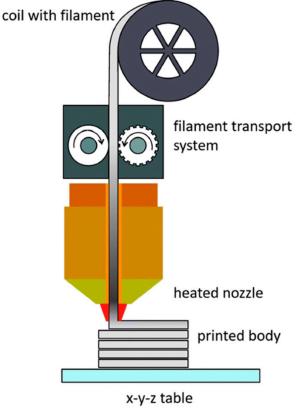


Figure 3. Schematic diagram of FFF [88].

In [88] this basic principle allows the production of complex parts without a moulding tool, except for a die with a simple geometry, usually circular. Depending on the type of extruder used, additive manufacturing by material extrusion can be classified into different types, which will be described in the next section and are shown schematically in Figure 3.

Selective Electron Beam Melting (SEBM) is limited to conductive materials because it requires electrical conductivity. The main difference is in the heat sources: SEBM uses a steerable electron beam with a higher scanning speed, requiring a vacuum, while Selective Laser Melting (SLM) uses a laser and argon shielding. The electron beam penetrates deeper into the material than a laser, and the temperature is higher in SEBM. SEBM also requires fewer support structures because the sintered powder supports the product, giving SEBM more geometric freedom compared to SLM [89].

Table 1. Additive manufacturing techniques used for printing WC-Co hard metals [89].

| AM Process | Abbreviation | Other names | Advantages | Disadvantages |
|-----------------|--------------|---------------|----------------|----------------|
| Selective Laser | SLM | Laser Powder | High | High residual |
| Melting | | Bed Fusion | dimensional | stress |
| | | (L-PBF) | accuracy | Uneven |
| | | | High geometric | microstructure |
| | | | freedom | Carbon loss |
| | | | Less steps | and |
| | | | High hardness | evaporation of |
| | | | | Co |
| Selective | SEBM | Electron Beam | High | High residual |
| Electron Beam | | Powder Bed | dimensional | stress |
| Melting | | Fusion | accuracy | Uneven |
| | | (E-PBF) | High geometric | microstructure |
| | | | freedom | Expensive |
| | | | Less steps | equipment |
| | | | High hardness | Needs vacuum |
| | | | High scan | |
| | | | speed | |
| Binder Jet | BJAM | Binder Jet 3D | Uniform | Complicated |
| Additive | | Printing | microstructure | processes |
| Manufacturing | | (BJ3DP) | High | Large |
| | | | toughness | shrinkage |
| | | | Low cost | Low hardness, |
| | | | Low residual | moderate |
| | | | stress | strength |
| 3D gel- | 3DGP | N/A | Low residual | Complicated |
| printing | | | stress | processes |
| | | | Uniform | Large |
| | | | microstructure | shrinkage |
| | | | Low powder | |
| | | | requirements | |
| | | | No raw | |
| | | | material loss | |

FFF N/A **Fused** Low residual Complicated Filament stress processes Fabrication Uniform Large microstructure shrinkage Low powder Needs filament fabrication requirements No raw equipment material loss Rough surface

In summary [89], the five additive manufacturing (AM) processes discussed can be divided into two categories: selective melting processes and shaping-deboning-sintering (SDS) processes. SLM and SEBM, use a heat source to melt powder and form parts, offering a simple, one-step molding process but often requiring post-processing to address stress and defects. The SDS processes, including BJAM, 3DGP, and FFF, involve forming a green part using organic binders, followed by sintering. These processes are more complex than selective melting, as they require a powder spreading step, which necessitates good powder flowability in SLM, SEBM, and BJAM. However, 3DGP and FFF use powders in slurry or filament form, eliminating the need for powder flowability. SEBM's application is limited due to its high equipment cost, while SLM faces issues with uneven microstructure, carbon loss, and Co evaporation.

A novel tungsten steel was prepared using selective laser melting (SLM) and hot isotropic pressing (HIPing). Initially, a powder mixture of maraging steel and WC was used in SLM to produce a net-shaped composite with γ (Fe, Ni) (austenite) and WC phases. After HIPing, the microstructure evolved into an α -Fe matrix (ferrite and martensite) with Fe(Ni)-W-C η phase precipitates in submicro and nano scales, located at grain boundaries and within grains. The process formed a stable graded multi-scaled structure at WC-matrix interfaces. HIPing improved mechanical properties, increasing ultimate tensile strength from 980 MPa to 1470 MPa and yield strength from 561 MPa to 1025 MPa, with elongation slightly reduced from 7% to 6% [90].

Cemented WC-Co is widely used in cutting, machining, and mining tools due to WC's hardness and Co's toughness. However, Co is a critical material with carcinogenic concerns, prompting research into alternative binders like nanostructured FeNiZr. Consolidation of WC-FeNiZr powders using Field Assisted Sintering and Hot Isostatic Pressing produced dense samples with superior hardness (16 GPa) and toughness (13 MPa·m¹/²). Electron Backscatter Diffraction and Transmission Electron Microscopy reveal the structure-property relationships, demonstrating FeNiZr's potential as a non-toxic Co substitute [91].

In work [92] the microstructural development and mechanical properties of tungsten heavy alloys (WHAs) with FeNiCoCrMn high-entropy alloy (HEA) and conventional FeNi binders were compared. Both WHAs were fabricated via hot isostatic pressing at 1450 °C in argon. Scanning electron microscopy showed uniform, refined microstructures for both binders, with HEA forming a skeletal network around tungsten grains. HEA binder increased micro Vickers hardness by 42% and enhanced the hardness of the WHA. However, WHA with HEA exhibited faster strain hardening and premature failure, resulting in lower ultimate strength and reduced ductility compared to the Fe-Ni binder.

This study examined the effects of NbC on densification, grain growth, and properties of WC-10AISI304 hard metals sintered via pseudo hot isostatic pressing at 1300 °C under vacuum and 20 MPa pressure. Adding 2 wt.% graphite reduced η-phase formation, while varying NbC content (1-5 wt.%) influenced microstructure and properties. NbC addition refined WC grains and reduced ηphase formation, with 2 wt.% NbC achieving the best results: the highest hardness (1820 kg/mm²) and moderate fracture toughness (7.7 MPa·m¹/²). Excess NbC (5 wt.%) led to coarse (Nb, W)C grains and decreased hardness [93].

High-density WC-FeNi cermet composites were fabricated via liquid-phase spark plasma sintering (SPS/FAST) using micron-sized powders of WC, Fe, Ni, and C. The in-situ formation of an FeNi alloy binder was enabled by a eutectic reaction, with carbon stabilizing the binder phase. The composite achieved 99% theoretical density with a microstructure of rounded WC grains averaging

10.5 µm in size. It exhibited a maximum hardness of 16.1 GPa, offering a fast and cost-effective method for producing hard metals [94].

Taking into account the above, it should be noted that the technologies of synthesis of WC based composites continue to develop, aimed at improving their mechanical and operational properties. Techniques such as powder metallurgy, encapsulation, SPS and hot isostatic pressing produce composites with high hardness, density and wear resistance. Alternative approaches, such as partial replacement of cobalt with nickel and iron, as well as the introduction of additive technologies and sintering, open new perspectives in the production of environmentally friendly and cost-effective materials. However, despite the successes achieved, further research and development is needed to scale up these technologies and their application in industry.

5. SPS Synthesis for WC Sintering

The SPS method is a transformative technology for manufacturing and advanced material research. Fifth-generation SPS systems provide enhanced functionality, reproducibility, and cost efficiency, enabling the production of larger, high-quality components for applications in electronics, automotive, cutting tools, fine ceramics, clean energy, and biomaterials. For instance, nano WC powder is densified with a nano-grain structure for optical uses [95,96].

Invented in Japan, SPS has become a global innovation, with over 600 units in Japan and 1100-1300 worldwide as of 2020, facilitating advanced material fabrication across industries in Europe, the USA, and Asia.

In optics, an SPSed aspheric glass lens mold is made from binder-less pure WC (HV2600) without additives. Starting with powders below 200 nm, the material is sintered into a nanostructured fine grain, achieving a mirror surface roughness of R_a 2-6 nm after post-processing. This mold, consisting of an upper punch, lower punch, and sleeve die, demonstrates SPS's advantages: additive-free sintering, finer grains, and 30-60% better oxidation resistance than conventional methods after a 10-hour test at 973 K which shown in Figure 4.

Oxidation resistance test on Binder-less WC sintered materials

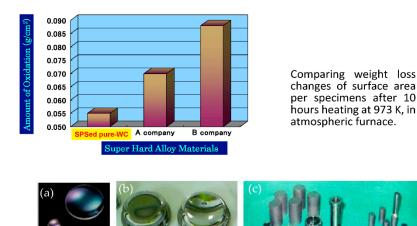


Figure 4. Examples of pure WC Aspheric glass lens mold materials s: (a) Formed small and large Aspheric glass lens; (b) Large-size aspheric glass lens molding die; (c) various SPSed compacts for glass lens die material and finished parts; (d) Finished glass lens sleeve die and punches for mobile phone applications; and (e) Finished glass lens sleeve die and punches for digital camera applications [97].

A practical application of SPSed mass production is in the cutting tools and wear-resistant materials industry. Factories run 2-3 shifts daily, producing 15-20 plates per batch. Co-bonded WC

dicing blades (100-150 mm diameter, 0.35-0.4 mm thickness) achieve flatness within $\pm 20~\mu m$ with minimal residual stresses, as shown in Figure 5. SPS processing at 1473-1523 K results in WC/Co plates with 99-100% density and Young's moduli of 500-580 GPa, eliminating the need for grinding and significantly reducing costs. Additionally, SPS facilitates the production of Cu-based dicing blades under 0.3 mm width. Its efficiency in near-net and net-shape forming has led to widespread adoption by several companies for large-scale production.



Figure 5. WC/Co sintered very thin plate with a diamond dicing blade [97].

WC/Co and WC/Ni cemented carbides are widely used as high wear-resistant materials in press-stamping dies and cutting tools. While conventional sintering requires extended processing times, new automated SPS systems enable rapid fabrication of these materials, significantly reducing production time which shown in Table 2. SPS technology's rapid sintering capabilities enhance efficiency and maintain high material quality. Typical mechanical properties of SPSed WC/Co alloys and binder-less nano-grain WC products demonstrate superior performance, highlighting the advancements in this technology.

| | <i>J</i> 1 | 1 1 | | • | , | . , |
|-------------------------|----------------------|--------------------------------|------------------------------|-----------------|--|---|
| Product Code Name | Co Content wt% | WC pdr. Grain Size µm | Density g/cm ³ | Hardness mHv | Transverse Rupture Strength MPa | Fracture Toughness K ₁ C |
| TC-05 | <2 | < 0.5 | 15.2 | 2350 | 2300 | 6.2 |
| TC-10 | <4 | < 0.5 | 15.0 | 2150 | 2640 | 6.5 |
| TC-20 | <6 | < 0.5 | 14.8 | 2050 | 2940 | 7.3 |
| M78 | 0 | < 0.2 | 15.4 | 2600 | 1500 | 5.1 |
| WC100 | 0 | < 0.08 | 15.6 | 2700 | 1470 | 5.6 |
| NC100 | 0 | < 0.5 | 15.4 | 2570 | 1180 | 5.4 |

Table 2. Typical mechanical properties of Fine WC/Co hard alloys sintered by SPS [97].

This paper highlights the history, fundamentals, and industrial applications of SPS, particularly in ceramics, nanocrystalline materials, FGMs, and wear-resistant hard materials. The rapid global adoption of SPS has driven a surge in research and patents over the last decade. SPS's unique energy concentration in conductive areas enables high-density, dynamic sintering, paving the way for expanded applications and cost-effective production. With its versatility and efficiency, SPS has significant potential as a key manufacturing tool across industries, including automotive, electronics, mold and die, clean energy, and aerospace, supporting both high-value-added and mass production.

The SPS method's key advantage is its ability to control nano-microstructures during sintering. Over the past 10-15 years, research has highlighted its effectiveness for nanophase ceramics and composites. Notably, SPS enables the solid-phase sintering of pure nano-WC powder to 99-100% density, which has been successfully commercialized for glass lens molds in the optical industry [97].

As a review of the available literature shows SPS is a promising synthesis method for creating WC based hard composites. SPS promotes uniform phase distribution in the material, which enhances its crack and wear resistance. Due to the fast heating rate and reduced holding time at high temperatures, this method minimizes the formation of defects such as porosity and unwanted phases.

Therefore, the use of SPS for the synthesis of WC composites ensures high strength, microhardness, and structural stability, making this method particularly effective for producing high-performance and durable hard materials for various industrial applications.

SPS [98,99] has been particularly developed in the last decades. The SPS method, as electro-discharge sintering [100], is a promising technology for the consolidation of powder materials. This method, also known as Field Assisted Sintering Technology (FAST), Plasma Assisted Sintering (PAS), Electro consolidation, High Energy High Rate Processing (HEHR), Electric Discharge Compaction (EDC) [101] is a new sintering technique used to produce nanostructured, composite and gradient materials. SPS method was applied in [102,103] to obtain Ti-Al-Nb based metalohydrides. SPS - technology consists of passing an electric current directly through the mound and the work piece to be pressed, rather than through an external heater. This results in a "spark plasma effect" and provides very sharp heating and consequently short cycle times. This fact makes it possible to suppress grain growth and obtain an equilibrium state. This opens up the possibility of creating new materials with previously inaccessible compositions and properties, materials with submicron or nanoscale grains, and composite materials with unique or unusual compositions [104,105].

By now it is generally accepted by most researchers that the technology is essentially hot pressing, but has original modern design features that distinguish this technology from classical hot pressing. Such features of SPS technology include: high precision control of the high-speed heating process, controlled hydraulic pressure application system, and a high level of automation of modern SPS systems, which are equipped with an efficient feedback system, pyrometers for temperature control, in-built dilatometers for online shrinkage control and powder shrinkage rate [107].

Modern systems for SPS allow to change all important process parameters (heating rate, temperature and sintering heating process. This makes the SPS method an extremely effective way to control the microstructure parameters of ceramics and tungsten carbide-based hard composites [108].

In this work, a SPS machine (SPSS DR.SINTER Fuji Electronics model 5015) was used. In the NSFSPS configuration, unlike traditional SPS, two graphite foils are inserted in a 0.4 mm gap, and the inner die surface is coated with an insulating boron nitride layer to concentrate the current on the sample, as shown in Figure 6. Powders with different electrical conductivities were used to test the method: Ni, Al_2O_3 , and 3Y- ZrO_2 [109,110].

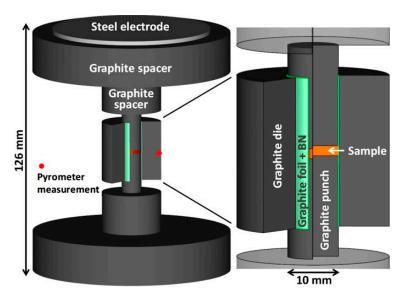


Figure 6. Structure of SPS synthesis [109].

WC without binder phase was successfully sintered and investigated by SPS method with the rapid development of SPS technology [111]. Compared with the LPS method, the hardness of WC sintered using SPS was significantly increased and the sintering time was also greatly reduced, but the impact toughness was seriously reduced. Zhao et al. [112] reported that sintered WC with a relative density of 99.5% and a Vickers hardness of 2414 kg·mm-² was obtained by sintering at 1500 °C

without soaking time, but the grain size increased from nanosize to microsize. In addition, the presence of brittle subcarbide W_2C phase was found in the sintered products, which reduced the fracture toughness and WC hardness (since the W_2C phase had a Vickers hardness of 17.1 kg·m⁻² and a fracture toughness of 3.6 MPa·m^{1/2}). By adding free carbon to the starting material, the influence of W_2C phase can be reduced and a pure sintered WC sample can be obtained.

But it should be considered that the addition of carbon creates two effects that act opposite to each other with respect to mechanical properties. The addition of carbon reduces or eliminates the brittle W_2C phase and this improves the fracture toughness, but carbon promotes abnormal grain growth and this secondarily reduces the fracture toughness of WC [113].

Nominally stoichiometric WC powders with grain size in the range of 40-70 nm can be compacted to near theoretical density (99.1%) with a grain size of 305 nm when heated at high speed to $1750\,^{\circ}$ C without soaking time. However, the sintered material contained W_2 C, and the effect of carbon addition on the presence of this phase was investigated using these powders and powders with a grain size of 12 nm. The effect of carbon on anomalous grain growth (AGG) as a function of temperature and carbon addition was investigated. The effect of heating rate to sintering temperature and holding time at this temperature was also investigated [114].

The effect of SPS sintering process on the density, microstructure, mechanical properties and fracture morphology of sintered gold was studied for WC-6Co-1.5Al ball powder. The results show that with process parameters: base value of pulse current 360 A, peak value 3000 A, frequency 50 Hz, duty cycle 50%, direct current 1500 A, total sintering time 6 min and sintering pressure 30 MPa, density, hardness and flexural strength 14.2 g/cm³ 94HRA and 1 can be obtained after sintering with pulse current for 1 min followed by sintering with direct current for 5 min. 660 MPa is an ultrafine-grained bulk material of cemented WC-6Co-1.5Al carbide with a density of 660 MPa; With further increase or decrease of the pulse current sintering time, the density, hardness and bending strength of the sintered product decrease [115].

The IPS of plasma-chemical nanopowders of WC-(0.3; 0.6; 1) wt. % Co has peculiarities. The IPS process of solid composites with ultra-low cobalt content can be consistently represented as a change of the following stages: rearrangement of particles at lower temperatures (stage I) \rightarrow sintering of WC-Co particles due to creep of Co γ phase of cobalt, the intensity of which is determined by the diffusion rate along the grain boundary (stage II) \rightarrow sintering due to diffusion creep, which rate is limited by volume diffusion in cobalt (stage III-1) \rightarrow sintering of tungsten carbide particles along WC/WC grain boundaries under conditions of intensive grain growth (stage III-2). Samples with high density (96.4-98.4%) and high mechanical properties (for WC-0.3% Co carbide: HV \sim 20.5 GPa, K_1 C = 7.1 MPa m^{1/2}) were obtained [116].

In [117], the possibilities and prospects of the chemical-metallurgical method and self-propagating high-temperature synthesis for obtaining submicron and nanoscale carbide powders, which form the basis of modern high-performance materials and products, are discussed. SEM images of these powders are presented in Figure 7. Specific examples of the use of submicron and nanoscale powders for obtaining tungsten-based heavy metal composites (TVS grade) and tungsten carbide-based solid composites (WC grade and its variants) for various purposes are also presented.

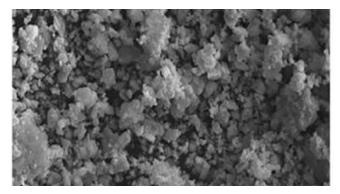


Figure 7. SEM image of WC-Co powder [117].

In [118], WC-Fe-Ni- Nb and conventional WC-Co were prepared by SPS method. The prepared powders were placed in a cylindrical graphite matrix. Then sintering was carried out using an SPS

15

setup. (Dr Sinter SPS 211 LX). The sintering temperatures used for WC-Fe-Ni-Nb consolidation were 1100 °C, 1200 °C and 1300 °C. The SPS displacement curves obtained from the equipment provide information on how the sintering process promoted consolidation in each temperature range. From this information, the shrinkage rates of the sintered specimens were calculated. Densities are determined using Archimedes' law using water as the immersion medium by measuring dry and immersed masses. Relative densities are presented as a percentage of the ratio of the density calculated using Archimedes' method to the theoretical density estimated using the mixing rule.

More readily available elements with similar effects are Ni, Cr, Cu, Mo, Al, Si, Fe. SPS is a synthesis and processing technology that allows sintering and bonding of agglomerate at low temperatures and in short time intervals by discharge between energetic particle surfaces and/or secondary discharge by Joule heating. By applying continuous on-off switching of high-power pulsed direct current at low voltage with a spark arrester, it effectively affects the high-temperature spark plasma generated in the initial stage of short-term switching on and the electromagnetic field by pulsed direct current [119,120].

Along with this, this sintering process is characterized by energy efficiency and high densification performance, and is also characterized by low energy consumption (1/5 to 1/3 compared to conventional sintering methods) such as pressure less sintering (PLS), hot pressing (HP) and hot isostatic pressing (HIP). Externally, the system resembles a standard hot pressing apparatus, but without the external heating element. However, the SPS method shows excellent results: structural adaptation, minimal grain growth, increased electrification and a pronounced preferential orientation effect.

The SPS method is sometimes referred to as pressure pulse sintering, electric current sintering (ECAS), pulsed electric current sintering (PECS) or magnetic field sintering technology (FAST). ECAS covers a wide range of processing methods using electric current. SPS is part of this group, but currently the most popular technical term worldwide is SPS or SPS process, so in this paper we generally use the term "SPS". It is well known that SPS is an advanced processing technology for the production of homogeneous, high-density, nanostructured sintered compact materials with functional properties (FGMs), fine ceramics, composite materials, novel wear-resistant materials, thermoelectric semiconductors and biomaterials [121].

The SPS process is a dynamic non-equilibrium treatment whose phenomenon varies from early stage, middle stage to late stage sintering mechanism, together with the characteristics of the reacting material. Despite years of research work by many materials researchers concerning the SPS mechanism, the SPS effect, in other words, the effect of pulsed strong current on spark plasma generation, the special properties of consolidated materials remain unclear [122–124].

This synthesis method was used in this work to sinter WC-6.4Fe-3.6Ni composite. SPS sintering was carried out on an SPS 211 LX (Dr. Sinter LAB) at temperatures of 1100, 1200 and 1300 °C under pressure of 35 MPa and vacuum of 10-5 bar, with a heating rate of 65°C/min to synthesize solid WC-6.4Fe-3.6Ni composites. The control WC-Co composite was prepared at 1200 °C. The sintered samples were held at maximum temperature for 5 min and cooled to room temperature for 40 min in a sintering chamber. The samples were sintered in a graphite mould, resulting in a cylindrical geometry with approximate dimensions of 6 mm (diameter) and 5 mm (height). Heating was performed with a constant pulsed current of 20.0 ms duration. The maximum achieved current was 366 A and the voltage was 7.6 V.

SPS was used in [125] to synthesize the WC-8Ni-8Fe composite, focusing on obtaining a high-quality, dense material using low-cost precursors. Tungsten (VI) oxide, magnesium, carbon, nickel, and iron were used as starting materials. Figure 8 shows the SEM image of the materials mentioned above. The sintering process was carried out at temperatures of 1000-1200 °C under a pressure of 57.3 MPa, with heating rates of 50° C/min and 87.5°C/min. The optimum sintering temperature of 1200 °C resulted in a uniform distribution of the Ni-Fe phase and improved mechanical properties: hardness of 1303 HV, fracture toughness of 12.4 MPa, and flexural strength of 1365 MPa. The composite showed a decrease in porosity from 13% to 0%, reaching full density. This method is suitable for industrial applications due to its cost-effective materials and high productivity.

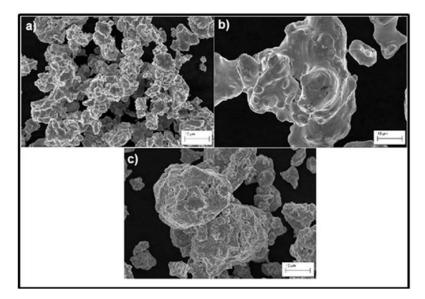


Figure 8. SEM images of ground powders of (a) iron, (b) nickel and (c) Fe-Ni [125].

And WC-Co powder mixtures were sintered at $1200\,^{\circ}$ C, which was considered a satisfactory temperature as shown in previous works [126] related to SPS WC-10% wt. Co. Both composites were processed under the following parameters: heating rate of 65 °C/min, pressure of 40 MPa, dwell time of 5 min and vacuum atmosphere of 102 Pa.

SPS shows significant advantages for the synthesis of cobalt-free composites in which cobalt is replaced by nickel and iron. First of all, SPS allows effective control of the material microstructure, ensuring a uniform distribution of nickel and iron in the WC matrix. This improves phase adhesion and enhances mechanical properties such as strength and wear resistance [127]. Due to the low temperatures and short sintering cycles, SPS minimizes the risk of porosity and grain growth, which is particularly important for maintaining high hardness and durability of cobalt-free composites. The use of SPS also enhances corrosion resistance due to the uniform distribution of iron and nickel, which makes such composites more resistant in corrosive environments compared to conventional WC-Co composites [128]. As a result, SPS makes it possible to create high-performance cobalt-free composites with optimized properties suitable for applications in various high-tech industries such as aerospace, energy and mechanical engineering.

6. Conclusion

Thus it should be noted that the studies highlight the importance of developing cobalt-free WC based solid composites as a promising direction in materials science and industrial applications. Conventional WC-Co composites, despite their excellent mechanical properties, face the problems of high cost, cobalt scarcity and environmental risks. Replacing cobalt with more affordable and environmentally friendly materials such as nickel and iron provides an effective solution that not only maintains but also improves key composite performance including strength, wear resistance and corrosion resistance. Synthesis techniques such as powder metallurgy, encapsulation, 3D printing and especially SPS have demonstrated high efficiency in creating composites with optimized microstructure and minimal grain growth. These technologies produce composites with high density, excellent mechanical properties and resistance to aggressive environments, making them attractive for use in engineering, metallurgy, mining and aerospace applications. Cobalt-free WC based composites using nickel and iron as binders not only match the performance of WC-Co materials, but also outperform them in a number of parameters, making them a key element in the future development of environmentally friendly and cost-effective solutions for industrial needs.

Author Contributions: Conceptualization, Sh.K., Y.K., and M.S.; investigation, Y.T., M.A.; writing—original draft preparation, Sh.K., Y.K., B.S., and M.S.; writing—review and editing, Sh.K., Y.K., M.S.; and B.S.; visualization, Sh.K.; project administration, Y.K.; funding acquisition, Y.T., M.A. All authors have read and agreed to the published version of the manuscript.

17

Institutional Review Board Statement: Not applicable.

Informed Consent Statement: Not applicable.

Data Availability Statement: Data are contained within the article.

Acknowledgments: This research is funded by the Committee of Science of the Ministry of Science and Higher Education of the Republic of Kazakhstan (grant No. BR24992925) "Development of Technology and Materials for Innovative Development of Manufacturing Industry of the Republic of Kazakhstan").

Conflicts of Interest: The authors declare no conflict of interest.

References

- 1. Viswanadham, R. *Science of Hard Materials*; Springer: Berlin, 2012; p 1012.
- 2. Shatov, A. V.; Ponomarev, S. S.; Firstov, S. A. Hardness and deformation of hardmetals at room temperature. *Comprehensive Hard Materials*; Elsevier, 2014, pp 647-699. https://doi.org/10.1016/B978-0-08-096527-7.00009-X.
- 3. Shatov, A. V.; Ponomarev, S. S.; Firstov, S. A. Fracture and strength of hardmetals at room temperature. *Comprehensive Hard Materials*; Elsevier: Oxford, 2014, pp 301-341. https://doi.org/10.1016/B978-0-08-096527-7.00010-6.
- 4. Multanov, A. S. Especially coarse-grained WC-Co composites for the equipment of rock-crushing tools for mining machines. *Phys. Mesomech.* **2002**, *5* (4), 113-116. https://doi.org/10.24411/1683-805X-2002-00019.
- 5. Sun, J.; Zhao, J.; Gong, F.; Ni, X.; Li, Z. Development and Application of WC based Composites Bonded with Alternative Binder Phase. *Crit. Rev. Solid State Mater. Sci.* **2018**, 1-28. https://doi.org/10.1080/10408436.2018.1483320.
- 6. Mukhopadhyay, A.; Basu, B. Recent developments on WC based bulk composites. *J. Mater. Sci.* **2011**, *46*, 571-589. https://doi.org/10.1007/s10853-010-5046-7.
- Fang, Z. Z.; Koopman, M. C.; Wang, H. Cemented Tungsten Carbide Hardmetal-An Introduction. Comprehensive Hard Materials; Elsevier, 2014, pp 123-137. https://doi.org/10.1016/B978-0-08-096527-7.00004-0.
- 8. Trofimenko, N. N.; Efimochkin, I. Y.; Dvoretskov, R. M.; Batienkov, R. V. Production of Fine-Grained Hard Alloys in the WC-Co System (Review). Trudy VIAM 2020, 1 (85), 92-100
- 9. Sun, J.; Zhao, J.; Huang, Z.; et al. A Review on Binderless Tungsten Carbide: Development and Application. *Nano-Micro Lett.* **2020**, *12*, 13. https://doi.org/10.1007/s40820-019-0346-1.
- 10. Oskolkova, T. N. Wear-Resistant Coating on Hard Composite. *Appl. Mech. Mater.* **2015**, 788, 281-285. https://doi.org/10.4028/www.scientific.net/AMM.788.281.
- 11. Oskolkova, T. N. Tungsten carbide is a hard composite with a wear-resistant coating. *Proc. Samara Sci. Cent. Russ. Acad. Sci.* **2013**, *15* (4-2), 473-475.
- 12. Oskolkova, T. N. Improving the wear resistance of tungsten-carbide hard composites. *Steel Transl.* **2015**, *45*, 318-321. https://doi.org/10.3103/S0967091215050137.
- 13. Ezquerra, B. L.; Rodriguez, N.; Sánchez, J. M. Comparison of the damage induced by thermal shock in hardmetals and cermets. *Int. J. Refract. Met. Hard Mater.* **2016**, *61*, 147-150. https://doi.org/10.1016/j.ijrmhm.2016.09.008.
- 14. Ezquerra, B. L.; Lozada, L.; van den Berg, H.; Wolf, M.; Sánchez, J. M. Comparison of the thermal shock resistance of WC based cemented carbides with Co and Co-Ni-Cr based binders. *Int. J. Refract. Met. Hard Mater.* 2017, 72, 89-96. https://doi.org/10.1016/j.ijrmhm.2017.12.021.
- 15. Kurlov, A. S.; Gusev, A. I. Vacuum annealing of nanocrystalline WC powders. *Inorg. Mater.* **2012**, *48*, 680-690. https://doi.org/10.1134/S0020168512060088.
- 16. Kurlov, A.; Gusev, A. I. Peculiarities of vacuum annealing of nanocrystalline WC powders. *Int. J. Refract. Met. Hard Mater.* **2012**, 32, 51-60. https://doi.org/10.1016/J.IJRMHM.2012.01.009.
- 17. Kurlov, A. S.; Rempel, A. A. Effect of cobalt powder morphology on the properties of WC-Co hard composites. *Inorg. Mater.* **2013**, 49, 889-893. https://doi.org/10.1134/S0020168513080086.
- 18. Zhang, X.; Guo, Z.; Chen, C.; Yang, W. Int. J. Refract. Met. Hard Mater. 2017, 70, 215. https://doi.org/10.1016/j.ijrmhm.2017.10.005.
- 19. Ku, N.; Pittari, J. J.; Kilczewski, S.; et al. Additive Manufacturing of Cemented Tungsten Carbide with a Cobalt-Free Composite Binder by Selective Laser Melting for High-Hardness Applications. *JOM* **2019**, *71*, 1535-1542. https://doi.org/10.1007/s11837-019-03366-2.

doi:10.20944/preprints202411.2212.v1

- 20. Moharana, R. K.; Dash, T.; Rout, T. K. Preparation of Iron Bonded Tungsten Carbide-Titanium Carbide Composites with Improved Microstructure for Designing Various Harder Components. *J. Mater. Eng. Perform.* **2024**, *33*, 5479-5486. https://doi.org/10.1007/s11665-024-09341-6.
- 21. Kim, H. T.; Kim, J. S.; Kwon, Y. S. Mechanical Properties of Binderless Tungsten Carbide by Spark Plasma Sintering. In *Proceedings of the 9th Russian-Korean International Symposium on Science and Technology (KORUS 2005)*; IEEE, 2005, pp 458-461. https://doi.org/10.1109/KORUS.2005.1507757.
- 22. Sun, J.; Chen, Y.; Zhai, P.; Zhou, Y.; Zhao, J.; Huang, Z. Tribological Performance of Binderless Tungsten Carbide Reinforced by Multilayer Graphene and SiC Whisker. *J. Eur. Ceram. Soc.* **2022**, *42*, 4817-4824. https://doi.org/10.1016/j.jeurceramsoc.2022.05.021.
- 23. European Commission. Critical Raw Materials Resilience: Charting a Path towards Greater Security and Sustainability. *COM*/2020/474 *final*, Brussels, 2020. Accessed: Aug. 30, 2023. https://eur-lex.europa.eu/legal-content/EN/TXT/?uri=CELEX:52020DC0474.
- 24. Alves Dias, P.; Blagoeva, D.; Pavel, C.; Arvanitidis, N. Cobalt: demand-supply balances in the transition to electric mobility. EUR 29381 EN, Publications Office of the European Union: Luxembourg, 2018. https://doi.org/10.2760/97710.
- 25. European Chemicals Agency. Cobalt Substance Infocard by ECHA. Accessed: Aug. 30, 2023. https://echa.europa.eu/substance-information/-/substanceinfo/100.028.325.
- 26. Lison, D. Human toxicity of cobalt-containing dust and experimental studies on the mechanism of interstitial lung disease (hard metal disease). *Crit. Rev. Toxicol.* **1996**, 26 (6), 585-616. https://doi.org/10.3109/10408449609037478.
- 27. Armstead, A. L.; Li, B. Nanotoxicity: emerging concerns regarding nanomaterial safety and occupational hard metal (WC-Co) nanoparticle exposure. *Int. J. Nanomedicine* **2016**, *11*, 6421-6433. https://doi.org/10.2147/ijn.s121238.
- 28. Kim, H. C.; Shon, I. J.; Yoon, J.; Doh, J. Consolidation of ultrafine WC and WC-Co hard materials by pulsed current activated sintering and its mechanical properties. *Int. J. Refract. Met. Hard Mater.* **2007**, 25, 46-52. https://doi.org/10.1016/J.IJRMHM.2005.11.004.
- 29. Kim, H. C.; Shon, I. J.; Ko, I.; Yoon, J.; Doh, J.; Lee, G. Fabrication of ultrafine binderless WC and WC-Ni hard materials by a pulsed current activated sintering process. *Int. J. Refract. Met. Hard Mater.* **2006**, 24, 397-401. https://doi.org/10.1016/J.IJRMHM.2005.11.004.
- 30. Anasori, B.; Barsoum, M. W. MXenes: Transition Metal Carbides and Nitrides; Springer International Publishing: Cham, 2019. https://doi.org/10.1007/978-3-319-58947-3.
- 31. Murthy, H.; Basu, B. WC-MXene Composites: Role of MXene on Mechanical and Tribological Properties of Binderless WC Composites. *Mater. Today Commun.* **2020**, 25, 101623. https://doi.org/10.1016/j.mtcomm.2020.101623.
- 32. Liu, Y.; Wang, J.; Li, Z. SPS processing of cobalt-free cemented carbide with high-density and fine microstructure. *J. Mater. Process. Technol.* **2022**, 296, 117212. https://doi.org/10.1016/j.jmatprotec.2021.117212.
- 33. Zhang, X.; Ma, X.; Zhou, J. Innovative cobalt-free cemented carbides: Properties and applications. *Adv. Mater.* **2023**, *35* (1), 2100234. https://doi.org/10.1002/adma.202100234.
- 34. Engqvist, H.; Axén, N.; Hogmark, S. Tribological properties of a binderless carbide. *Wear* **1999**, 232 (2), 157-162. https://doi.org/10.1016/S0043-1648(99)00140-4.
- 35. Engqvist, H.; Beste, U.; Axén, N. The influence of pH on sliding wear of WC based materials. *Int. J. Refract. Met. Hard Mater.* **2000**, *18* (2), 103-109. https://doi.org/10.1016/S0263-4368(00)00007-X.
- 36. Human, A. M.; Exner, H. E. Electrochemical behaviour of tungsten-carbide hardmetals. *Mater. Sci. Eng. A* **1996**, 209 (1-2), 180-191. https://doi.org/10.1016/0921-5093(95)10137-3.
- 37. Human, A. M.; Exner, H. E. The relationship between electrochemical behaviour and in-service corrosion of WC based cemented carbides. *Int. J. Refract. Met. Hard Mater.* **1997**, 15 (1-3), 65-71. https://doi.org/10.1016/S0263-4368(96)00014-5.
- 38. Ojo-Kupoluyi, O. J.; Tahir, S. M.; Baharudin, B. T. H. T.; Azmah Hanim, M. A.; Anuar, M. S. Mechanical Properties of WC based Hardmetals Bonded with Iron Alloys A Review. Mater. Sci. Technol. 2017, 33 (5), 507-517. https://doi.org/10.1080/02670836.2016.1186929
- 39. Toller, L. Alternative binder hardmetals for steel turning. Int. J. Refract. Met. Hard Mater. 2017, 61, 147-150.
- 40. Prakash, L. J. Fundamentals and General Applications of Hardmetals. *Comprehensive Hard Materials*; Elsevier, 2014. https://doi.org/10.1016/B978-0-08-096527-7.00002-7.
- 41. Bonny, K.; de Baets, P.; Vleugels, J.; Huang, S.; Lauwers, B. Tribological characteristics of WC-Ni and WC-Co cemented carbide in dry reciprocating sliding contact. *Tribol. Trans.* **2009**, *52* (4), 481-491. https://doi.org/10.1080/10402000802716921.
- 42. Jia, C.; Sun, L.; Tang, H.; Qu, X. Hot pressing of nanometer WC-Co powder. *Int. J. Refract. Met. Hard Mater.* **2007**, *25*, 53-56. https://doi.org/10.1016/j.ijrmhm.2005.11.003.

- 43. Rong, H.; Wang, X.; Zhang, T.; Zhao, H. Ultrafine WC-Ni cemented carbides fabricated by spark plasma sintering. *Mater. Sci. Eng. A* **2012**, *543-547*, 324-332. https://doi.org/10.1016/j.msea.2011.10.119.
- 44. Wei, C. B.; Shi, Z.; Su, J. Microstructure and properties of ultrafine cemented carbides: Differences in spark plasma sintering and sinter-HIP. *Mater. Sci. Eng. A* **2012**, 427-433, 544-551. https://doi.org/10.1016/j.msea.2012.05.065.
- 45. Li, J.; Zhang, L.; Xu, Q.; Zhang, T. Effects of partial substitution of copper for cobalt on the microstructure and properties of ultrafine-grained WC-Co cemented carbides. *J. Composites Compd.* **2018**, 43-50, 726-735. https://doi.org/10.1016/j.jallcom.2017.11.006.
- 46. Ghasali, E.; Sadeghi, A.; Shokouhimehr, M.; Lee, S. Mechanical and microstructural properties of WC based cermets: A comparative study on the effect of Ni and Mo binder phases. *Ceram. Int.* **2018**, 2283-2291, 854-862. https://doi.org/10.1016/j.ceramint.2017.10.189.
- 47. Peter, I.; Rosso, M. Manufacturing, composition, properties and application of sintered hard metals. In *Powder Metallurgy: Fundamentals and Case Studies*; Springer, 2017; pp 245-272. https://doi.org/10.5772/66872.
- 48. García, J.; Martínez, E.; Llanes, L. Cemented carbide microstructures: A review. *Int. J. Refract. Met. Hard Mater.* 2019, 40-68, 229-254. https://doi.org/10.1016/j.ijrmhm.2018.12.004.
- 49. Ishida, T.; Moriguchi, H. Development of cemented carbide tools of reduced rare metal usage. *Wear* **2011**, 270, 1431-1436.
- 50. Li, H.; Zhang, H.; Jiang, Z. Investigation of the effect of partial Co substitution by Ni and Fe on the interface bond strength of WC cemented carbide based on first-principles calculations. *Mater. Today Commun.* **2024**, 109470. https://doi.org/10.1016/j.mtcomm.2024.109470.
- 51. Straumal, B. B.; Konyashin, I. Faceting/roughening of WC/binder interfaces in cemented carbides: A review. *Materials* **2023**, *16* (10), 3696. https://doi.org/10.3390/ma16103696.
- 52. Kelly, J. P.; Graeve, O. A. Spark plasma sintering as an approach to manufacture bulk materials: Feasibility and cost savings. *JOM* **2015**, *67*, 29-33. https://doi.org/10.1007/s11837-014-1202-x.
- 53. Guillon, O.; Gonzalez-Julian, J.; Dargatz, B.; Kessel, T.; Schierning, G.; Räthel, J.; Herrmann, M. Fieldassisted sintering technology/spark plasma sintering: Mechanisms, materials, and technology developments. *Adv. Eng. Mater.* **2014**, *16*, 831-849. https://doi.org/10.1002/adem.201300409.
- 54. Zhang, Z.; Liu, Z.; Lu, J.; Shen, X.; Wang, F.; Wang, Y. The sintering mechanism in spark plasma sintering: Proof of the occurrence of spark discharge. *Scr. Mater.* **2014**, *81*, 56-59. https://doi.org/10.1016/j.scriptamat.2014.03.011.
- 55. Buravlev, I. Y.; Solokhin, V. A.; Ryabchikov, M. A.; Tikhonovsky, M. A. WC-5TiC-10Co hard metal composite fabrication via mechanochemical and SPS techniques. *Int. J. Refract. Met. Hard Mater.* **2021**, 94, 105385. https://doi.org/10.1016/j.ijrmhm.2021.105385.
- 56. Li, H.; Zhang, H.; Jiang, Z. Investigation of the effect of partial Co substitution by Ni and Fe on the interface bond strength of WC cemented carbide based on first-principles calculations. *SSRN* **2024**, 4724880. https://doi.org/10.2139/ssrn.4724880.
- 57. Oliver, U. C.; Sunday, A. V.; Christain, E. I.; Elizabeth, M. M. Spark Plasma Sintering of Aluminium Composites—A Review. *Int. J. Adv. Manuf. Technol.* **2021,** *112,* 1819-1839. https://doi.org/10.1007/s00170-020-06469-8.
- 58. Wang, J.; Zhang, S. Enhanced uniformity in cobalt-free tungsten carbide composites through encapsulation. *Mater. Sci. Eng. A* **2019**, 747, 105-113.
- 59. Milman, Y. V. The effect of structural state and temperature on mechanical properties and deformation mechanisms of WC-Co hard composite. *J. Superhard Mater.* **2014**, *36*, 65-81. https://doi.org/10.3103/S1063457614020014.
- 60. Kim, J. H.; Lee, D. K. Effect of encapsulation on the sintering behavior and mechanical properties of cobalt-free WC hardmetals. *Int. J. Refract. Met. Hard Mater.* **2018**, 73, 93-100.
- 61. Kwak, J. H.; Lee, S. Y. Effect of grain size on the properties of cobalt-free WC based hardmetals. *J. Composites Compd.* **2018**, 767, 238-244. https://doi.org/10.1016/j.jallcom.2018.06.123.
- 62. Chen, X.; Zhang, T. Development and Application of Binderless Tungsten Carbide Hardmetals. *Mater. Des.* **2021**, 203, 109595. https://doi.org/10.1016/j.matdes.2021.109595.
- 63. Gibson, I. et al. Additive Manufacturing Technologies; Springer: Cham, Switzerland, 2021; Vol. 17, pp 160-186.
- 64. Frazier, W. E. Metal Additive Manufacturing: A Review. *J. Mater. Eng. Perform.* **2014**, 23 (6), 1917-1928. https://doi.org/10.1007/s11665-014-0958-z.
- 65. Pan, Y.; Liu, A.; Huang, L.; Du, Y.; Jin, Y.; Yang, X.; Zhang, J. Effects of metal binder content and carbide grain size on the microstructure and properties of SPS-manufactured WC-Fe composites. *J. Composites Compd.* **2019**, 767, 238-244. https://doi.org/10.1016/j.jallcom.2019.01.057.
- 66. Yang, G.; Ka, G.; Lei, F.; Yang, F.; Guo, X.; Zhang, R.; An, L. Oscillatory Pressure Sintering of WC-Fe-Ni Cemented Carbides. *Ceram. Int.* **2020**, *46*, 12727-12731. https://doi.org/10.1016/j.ceramint.2020.02.040.

doi:10.20944/preprints202411.2212.v1

- 67. Kazantseva, N. V.; Mushnikov, N. V.; Popov, A. A.; Sazonova, V. A.; Terent'ev, P. B. Nanoscale Hydrides of Titanium Aluminides. *Phys. Eng. High Pressures* **2008**, *17*, 3-10.
- 68. Zoli, L.; Vinci, A.; Silvestroni, L.; et al. Rapid Spark Plasma Sintering to Produce Dense UHTCs Reinforced with Undamaged Carbon Fibres. *Mater. Des.* **2017**, *130*, 1-7. https://doi.org/10.1016/j.matdes.2017.05.029.
- 69. Lee, S. H.; et al. Ultra-Low Temperature Synthesis of Al4SiC4 Powder Using Spark Plasma Sintering. *Scr. Mater.* **2013**, *69* (2), 135-138. https://doi.org/10.1016/j.scriptamat.2013.02.042.
- 70. Aghaali, V.; Ebadzadeh, T.; Zahraee, S. M.; et al. Microstructure and Mechanical Properties of WC-TiC-Co Cemented Carbides Produced by Spark Plasma Sintering (SPS) Method. *SN Appl. Sci.* **2023**, *5*, 285. https://doi.org/10.1007/s42452-023-05510-9.
- 71. Cha, S. I.; Hong, S. H. Microstructures of Binderless Tungsten Carbides Sintered by Spark Plasma Sintering Process. *Mater. Sci. Eng., A* **2003**, *356*, 381-389. https://doi.org/10.1016/S0921-5093(03)00151-5.
- 72. Lantsev, E. A. BBK K390.4ya73-5 L22; BBK Publishing: Moscow, 2023.
- 73. Taimatsu, H.; Sugiyama, S.; Kodaira, Y. Synthesis of W2C by Reactive Hot Pressing and Its Mechanical Properties. *Mater. Trans.* **2008**, 49, 304. http://dx.doi.org/10.2320/matertrans.MRA2007304.
- 74. Chuvil'deev, V. N.; Blagoveshchenskiy, Y. V.; Nokhrin, A. V.; et al. Spark Plasma Sintering of Tungsten Carbide Nanopowders. *Nanotechnol. Russ.* **2015**, *10*, 434-448. https://doi.org/10.1134/S1995078015030040.
- 75. Genga, R. M.; Cornish, L. A.; Akdogan, G. Effect of Mo₂C Additions on the Properties of Manufactured WC-TiC-Ni Cemented Carbides. *Int. J. Refract. Met. Hard Mater.* **2013**, 41, 12-21. https://doi.org/10.1016/j.ijrmhm.2013.01.008.
- 76. Bo, S.; Songhe, L.; Pan, G.; Wang, D.; Dong, Y.-Y.; Cheng, J.; Ren, G.; Yan, Q. Printability and Properties of Tungsten Cemented Carbide Produced Using Laser Powder Bed Fusion Additive Manufacturing with Ti as a Binder. *Int. J. Refract. Metals Hard Mater.* 2023, 111, 106106. https://doi.org/10.1016/j.ijrmhm.2023.106106
- 77. Lee, S. W.; Kim, Y. W.; Jang, K. M.; et al. Phase Control of WC-Co Hardmetal Using Additive Manufacturing Technologies. Powder Metall. 2022, 65 (1), 13-21. https://doi.org/10.1080/00325899.2021.193786.
- 78. Kim, H.; Kim, J.-I.; Kim, Y. D.; Jeong, H.; Ryu, S.-S. Material Extrusion-Based Three-Dimensional Printing of WC-Co Alloy with a Paste Prepared by Powder Coating. *Addit. Manuf.* **2022**, *52*, 102679. https://doi.org/10.1016/j.addma.2022.102679.
- 79. Zhang, D.; Kenel, C.; Dunand, D. C. Microstructure and Properties of Additively-Manufactured WC-Co Microlattices and WC-Cu Composites. *Acta Mater.* **2021**, 221, 117420. https://doi.org/10.1016/j.actamat.2021.117420.
- 80. Zhang, X.; Guo, Z.; Chen, C.; Yang, W. Additive Manufacturing of WC-20Co Components by 3D Gel-Printing. *Int. J. Refract. Met. Hard Mater.* **2018**, 70, 215-223. https://doi.org/10.1016/j.ijrmhm.2017.10.005.
- 81. Ren, X.; Shao, H.; Lin, T.; Zheng, H. 3D Gel-Printing—An Additive Manufacturing Method for Producing Complex Shape Parts. *Mater. Des.* **2016**, *101*, 80-87.
- 82. Spierings, A. B.; Voegtlin, M.; Bauer, T.; Wegener, K. Powder Flowability Characterisation Methodology for Powder-Bed-Based Metal Additive Manufacturing. *Prog. Addit. Manuf.* **2016**, *1*, 9-20.
- 83. Aramian, A.; Razavi, S. M. J.; Sadeghian, Z.; Berto, F. A Review of Additive Manufacturing of Cermets. *Addit. Manuf.* **2020**, 101130. https://doi.org/10.1016/j.addma.2020.101130.
- 84. Enneti, R. K.; Prough, K. C.; Wolfe, T. A.; Klein, A.; Studley, N.; Trasorras, J. L. Sintering of WC-12%Co Processed by Binder Jet 3D Printing (BJ3DP) Technology. *Int. J. Refract. Met. Hard Mater.* **2018**, 71, 28-35. https://doi.org/10.1016/j.ijrmhm.2017.10.023.
- 85. Enneti, R. K.; Prough, K. C. Wear Properties of Sintered WC-12%Co Processed via Binder Jet 3D Printing (BJ3DP). *Int. J. Refract. Met. Hard Mater.* **2019**, *78*, 228-232. https://doi.org/10.1016/j.ijrmhm.2018.10.003.
- 86. Do, T.; Kwon, P.; Shin, C. S. Process Development Toward Full-Density Stainless Steel Parts with Binder Jetting Printing. *Int. J. Mach. Tools Manuf.* **2017**, *121*, 50-60. https://doi.org/10.1016/j.ijmachtools.2017.04.006.
- 87. Kim, H. C.; Shon, I.-J.; Yoon, J.-K.; Doh, J.-M.; Munir, Z.A. Rapid sintering of ultrafine WC-Ni cermets. Int. J. Refract. Met. Hard Mater. 2006, 24, 427-431.
- 88. Kukla, C.; Gonzalez-Gutierrez, J.; Burkhardt, C.; Weber, O.; Holzer, C. The Production of Magnets by FFF-Fused Filament Fabrication. In *Proceedings of the Euro PM2017 Congress & Exhibition*, Milan, Italy, 2017; pp 1-5
- 89. Gonzalez-Gutierrez, J.; Cano, S.; Schuschnigg, S.; Kukla, C.; Sapkota, J.; Holzer, C. Additive Manufacturing of Metallic and Ceramic Components by the Material Extrusion of Highly-Filled Polymers: A Review and Future Perspectives. *Materials* **2018**, *11*, 840. https://doi.org/10.3390/ma11050840.
- 90. Yang, Y.; Zhang, C.; Wang, D.; et al. Additive Manufacturing of WC-Co Hardmetals: A Review. *Int. J. Adv. Manuf. Technol.* **2020**, *108*, 1653-1673. https://doi.org/10.1007/s00170-020-05389-5
- 91. Kang, N.; Lu, J. L.; Li, Q. G.; Cao, Y. N.; Lin, X.; Wang, L. L.; Huang, W. D.; El Mansori, M. A New Way to Net-Shaped Synthesis Tungsten Steel by Selective Laser Melting and Hot Isostatic Pressing. *Vacuum* 2020, 179, 109557. https://doi.org/10.1016/j.vacuum.2020.109557.]

- 92. Fudger, S. J.; Luckenbaugh, T. L.; Hornbuckle, B. C.; Darling, K. A. Mechanical Properties of Cemented Tungsten Carbide with Nanocrystalline FeNiZr Binder. *Int. J. Refract. Met. Hard Mater.* **2024**, *118*, 106465. https://doi.org/10.1016/j.ijrmhm.2023.106465.
- 93. Anwer, Z.; Umer, M. A.; Nisar, F.; Hafeez, M. A.; Yaqoob, K.; Luo, X.; Ahmad, I. Microstructure and Mechanical Properties of Hot Isostatic Pressed Tungsten Heavy Alloy with FeNiCoCrMn High Entropy Alloy Binder. *J. Mater. Res. Technol.* **2023**, 22, 2897-2909. https://doi.org/10.1016/j.jmrt.2022.12.078.
- 94. Tran, B. T.; Zuhailawati, H.; Ahmad, Z. A.; Ishihara, K. N. Grain Growth, Phase Evolution and Properties of NbC Carbide-Doped WC-10AISI304 Hardmetals Produced by Pseudo Hot Isostatic Pressing. J. Alloys Compd. 2013, 552, 20-25. https://doi.org/10.1016/j.jallcom.2012.10.060.
- 95. Cramer, L. C.; Preston, A. D.; Ma, K.; Nandwana, P. In-Situ Metal Binder-Phase Formation to Make WC-FeNi Cermets with Spark Plasma Sintering from WC, Fe, Ni, and Carbon Powders. Int. J. Refract. Met. Hard Mater. **2020**, 88, 105204. https://doi.org/10.1016/j.ijrmhm.2020.105204.
- 96. Munir, Z. A.; Anselmi-Tamburini, U.; Ohyanagi, M. The Effect of Electric Field and Pressure on the Synthesis and Consolidation of Materials: A Review of the Spark Plasma Sintering Method. *J. Mater. Sci.* **2006**, *41*, 763-777. https://doi.org/10.1007/s10853-006-6555-2.
- 97. Tokita, M. Progress of Spark Plasma Sintering (SPS) Method, Systems, Ceramics Applications and Industrialization. Ceramics **2021**, 4, 160-198. https://doi.org/10.3390/ceramics4020014
- 98. Lantsev, E. A.; Malekhonova, N. V.; Chuvildeev, V. N.; et al. Investigation of High-Speed Sintering of Fine-Grained Hard Composites Based on Tungsten Carbide with an Ultra-Low Cobalt Content: II. Hard Composites WC-(0.3-1) wt.% Co. *Inorg. Mater.: Appl. Res.* **2023**, 14, 677-690. https://doi.org/10.1134/S207511332303025.
- 99. Wei, C., Song, X., Fu, J. Y., Liu, X., Gao, Y., Wang, H., & Zhao, S. (2012). Microstructure and properties of ultrafine cemented carbides—Differences in spark plasma sintering and sinter-HIP. Materials Science and Engineering: A, 552, 427-433. https://doi.org/10.1016/J.MSEA.2012.05.065
- 100. Rosa, J. M. B.; et al. Study of Characteristics and Properties of Spark Plasma Sintered WC with the Use of Alternative Fe-Ni-Nb Binder as Co Replacement. *Int. J. Refract. Met. Hard Mater.* **2020**, 92, 105316. http://dx.doi.org/10.1016/j.ijrmhm.2020.105316.
- 101. Otoni, E.; Correa, J. N.; Santos, A. N.; Klein, N. Microstructure and Mechanical Properties of WC Ni-Si Based Cemented Carbides Developed by Powder Metallurgy. *Int. J. Refract. Met. Hard Mater.* **2010**, 28 (5), 572-575. http://dx.doi.org/10.1016/j.ijrmhm.2010.04.003.
- 102. Kozhakhmetov, Y.; Skakov, M.; Wieleba, W.; Sherzod, K.; Mukhamedova, N. Evolution of Intermetallic Compounds in Ti-Al-Nb System by the Action of Mechanoactivation and Spark Plasma Sintering. AIMS Mater. Sci. 2020, 7 (2), 182-191. https://doi.org/10.3934/matersci.2020.2.182.
- 103. Kozhakhmetov, Y.; Skakov, M.; Mukhamedova, N.; Kurbanbekov, S.; Ramankulov, S.; Wieleba, W. Changes in the Microstructural State of Ti-Al-Nb-Based Alloys Depending on the Temperature Cycle During Spark Plasma Sintering. Mater. Test. 2020. https://doi.org/10.1515/mt-2020-0017.
- 104. Huang, Z.; Ren, X.; Liu, M. D.; Xu, C.; Zhang, X.; Guo, S.; Chen, H. Effect of Cu on the Microstructures and Properties of WC-6Co Cemented Carbides Fabricated by SPS. *Int. J. Refract. Met. Hard Mater.* **2017**, 62, 155-160. https://doi.org/10.1016/J.IJRMHM.2016.06.007.
- 105. Guilemany, J. M.; Sanchiz, I.; Mellor, B. G.; Llorca, N.; Miguel, J. R. Mechanical-Property Relationships of Co/WC and Co-Ni-Fe/WC Hard Metal Composites. *Int. J. Refract. Met. Hard Mater.* **1993**, 12 (4), 199-206. https://doi.org/10.1016/0263-4368(93)90049-L.
- 106. Chang, S. H.; Chang, M. H.; Huang, K. T. Study on the Sintered Characteristics and Properties of Nanostructured WC-15 wt% (Fe-Ni-Co) and WC-15 wt% Co Hard Metal Composites. *J. Composites Compd.* **2015**, *649*, 89-95. https://doi.org/10.1016/j.jallcom.2015.07.119.
- 107. Powder Metallurgy World Congress, Kyoto, Japan, 12-16 November 2001; Part-I, pp 252-255.
- 108. Matsugi, K.; Hatayama, T.; Yanagisawa, O. Effect of Direct Current Pulse Discharge on Specific Resistivity of Copper and Iron Powder Compacts. *J. Jpn. Inst. Met.* **1995**, *59* (3), 740-745.
- 109. Manière, C.; Lee, G.; Olevsky, E. A. All-Materials-Inclusive Flash Spark Plasma Sintering. *Sci. Rep.* **2017**, *7*, 15071. https://doi.org/10.1038/s41598-017-15365-x.
- 110. Rakhadilov, B.; Kantay, N.; Sagdoldina, Z.; Paszkowski, M.; et al. Experimental Investigations of Al_2O_3 -and ZrO_2 -Based Coatings Deposited by Detonation Spraying. Mater. Res. Express 2021, 8 (5), 056402. https://doi.org/10.1088/2053-1591/abfbb7
- 111. Shen, Z.; Johnsson, M.; Zhao, Z.; Nygren, M. Spark Plasma Sintering of Alumina. *J. Am. Ceram. Soc.* **2002**, *85* (8), 1921-1927. https://doi.org/10.1111/j.1151-2916.2002.tb00381.x.
- 112. Zhao, J.; Holland, T.; Unuvar, C.; Munir, Z. A. Spark Plasma Sintering of Nanometric Tungsten Carbide. *Int. J. Refract. Met. Hard Mater.* **2009**, 27, 130-139. https://doi.org/10.1016/j.ijrmhm.2008.06.004.
- 113. Schmidt, J.; Niewa, R.; Schmidt, M.; Grin, Y. Spark Plasma Sintering Effect on the Decomposition of MgH₂. *J. Am. Ceram. Soc.* **2005**, *88*, 1870-1874. http://dx.doi.org/10.1111/j.1551-2916.2005.00358.x.

- 114. Ozaki, K.; Kobayashi, K.; Nishio, T.; Matsumoto, A.; Sugiyama, A. Sintering Phenomena on Initial Stage in Pulsed Current Sintering. *J. Jpn. Soc. Powder Powder Metall.* **2000**, 47 (3), 293-297. https://doi.org/10.2497/jjspm.47.293.
- 115. Li, Y.; Zhang, J.; Li, X.; et al. Study on Preparation of WC-6Co-1.5Al Cemented Carbide by SPS Sintering. *Powder Metall. Technol.* **2006**, 24 (3), 199-202. DOI:10.3321/j.issn:1001-3784.2006.03.009.
- 116. Omori, M. Sintering, Consolidation, Reaction and Crystal Growth by the Spark Plasma System (SPS). *Mater. Sci. Eng., A* **2000**, 287, 183-188. https://doi.org/10.1016/S0921-5093(00)00773-5.
- 117. Alymov, M. I.; Borovinskaya, I. P. Prospects for the Creation of Hard Composites Based on Submicron and Nanoscale Powders W and WC, Obtained by the Chemical-Metallurgical Method and Using SHS. *Inorg. Mater.* **2017**, https://doi.org/10.7868/s0002337x17030010.
- 118. Song, X.; Liu, X.; Zhang, J. Neck Formation and Self-Adjusting Mechanism of Neck Growth of Conducting Powders in Spark Plasma Sintering. *J. Am. Ceram. Soc.* **2006**, *89*, 494-500. https://doi.org/10.1111/j.1551-2916.2005.00777.x.
- 119. Grasso, S.; Sakka, Y.; Maizza, G. Effects of Initial Punch-Die Clearance in Spark Plasma Sintering Process. *Mater. Trans.* 2008, 49 (12), 2899-2906. https://doi.org/10.2320/matertrans.MER2008263.
- 120. Chaim, R. Corrigendum to "Densification Mechanisms in Spark Plasma Sintering of Nanocrystalline Ceramics" [Mater. Sci. Eng., A 443 (2007) 25-32]. *Mater. Sci. Eng., A* 2008, 486, 696. https://doi.org/10.1016/j.msea.2008.02.031.
- 121. Misawa, T.; Shikatani, N.; Kawakami, Y.; Enjoji, T.; Ohtsu, Y. Influence of Internal Pulsed Current on the Sintering Behavior of Pulsed Current Sintering Process. *Mater. Sci. Forum* **2010**, *638*, 2109-2114. https://doi.org/10.4028/www.scientific.net/MSF.638-642.2109.
- 122. Yang, Y.; Zhang, C.; Wang, D.; Nie, L.; Wellmann, D.; Tian, Y. Additive manufacturing of WC-Co hardmetals: A review. *Int. J. Adv. Manuf. Technol.* **2020**, *108*, 1653-1673. https://doi.org/10.1007/s00170-020-05389-5.
- 123. Santos, A. C. Study of Sintering Kinetics in Solid State of WC-Co and WC-Fe-Ni-Co Carbide Composites Via Pulsed Plasma; DSc Thesis; Darcy Ribeiro State University of Northern Rio de Janeiro, UENF: Rio de Janeiro, Brazil, 2016.
- 124. Zhang, Z. H.; Liu, Z. F.; Lu, J. F.; et al. The Sintering Mechanism in Spark Plasma Sintering—Proof of the Occurrence of Spark Discharge. *Scr. Mater.* **2014**, *81*, 56-59. http://dx.doi.org/10.1016/j.scriptamat.2014.03.011.
- 125. Da Silva, E. N.; et al. Investigation of Characteristics and Properties of Spark Plasma Sintered Ultrafine WC-6.4Fe3.6Ni Composite as Potential Alternative WC-Co Hard Metals. *Int. J. Refract. Met. Hard Mater.* **2021**, 101, 105669. https://doi.org/10.1016/j.ijrmhm.2021.105669.
- 126. Shichalin, O. O.; Buravlev, I. Y.; Portnyagin, A.; et al. SPS Hard Metal Composite WC-8Ni-8Fe Fabrication Based on Mechanochemical Synthetic Tungsten Carbide Powder. *J. Composites Compd.* **2020**, *816*, 152547. https://doi.org/10.1016/j.jallcom.2019.152547.
- 127. Hulbert, D. M.; Anders, A.; Dudina, D. V.; et al. The Absence of Plasma in "Spark Plasma Sintering". *J. Appl. Phys.* **2008**, *104*, 033305. https://doi.org/10.1063/1.2963701.
- 128. Santos, A. C.; Skury, A. L. D.; Silva, A. G. P. Spark Plasma Sintering of a Hard Metal Powder Obtained from Hard Metal Scrap. *Mater. Res.* **2017**, 10-13. https://doi.org/10.1590/1980-5373-MR-2016-1035.

Disclaimer/Publisher's Note: The statements, opinions and data contained in all publications are solely those of the individual author(s) and contributor(s) and not of MDPI and/or the editor(s). MDPI and/or the editor(s) disclaim responsibility for any injury to people or property resulting from any ideas, methods, instructions or products referred to in the content.