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## Article

# High-Temperature and Stress Monitoring in Generation IV Nuclear Reactors Using Femtosecond-Inscribed Fiber Bragg Grating Sensors

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**Abstract:** The performance and longevity of next-generation nuclear reactors depend on the implementation of sensing technologies able to withstand extreme conditions. This study evaluates the performance of femtosecond-inscribed Fiber Bragg Grating (fs-FBG) sensors under simulated operating conditions representative of *newcleo*'s Generation IV Lead-cooled Fast Reactors (LFRs). The primary goal of this preliminary test phase is to validate the suitability of fs-FBG sensors for high-temperature (300°C) and mechanical stress monitoring (1-5 kN cyclic tensile force), emphasizing their reliability and accuracy. The experimental campaign involved rigorous thermal and thermo-mechanical testing, conducted in compliance with ASTM standards, to assess key performance metrics such as linearity, repeatability, and precision. The results demonstrate that fs-FBG sensors deliver consistent and reliable measurements in extreme environments, with a temperature sensitivity of 12.62 pm/°C and a displacement sensitivity of 3.954 nm/mm. These findings provide a strong basis for the use of fs-FBG sensors in Generation IV nuclear reactors, highlighting their potential as advanced tools for structural health monitoring.

**Keywords:** Fiber Bragg Grating (FBG); femtosecond-FBGs; high-temperature monitoring; stress monitoring; nuclear reactors; lead-cooled fast reactors; Structural Health Monitoring (SHM)

## 1. Introduction

*newcleo* is a pioneering company that is innovating the nuclear industry to play a fundamental role in climate change mitigation and global decarbonisation. *newcleo* is developing new Generation IV Lead-cooled Fast Reactors (LFRs), which prioritize safety, efficiency, and sustainability. These reactors leverage the unique properties of lead as a coolant, such as superior thermal conductivity, high boiling point, and effective radiation shielding. The design minimizes the risks associated with water-cooled reactors, such as hydrogen production and core meltdown, while enabling operation at atmospheric pressure, simplifying reactor systems, and enhancing safety. Additionally, *newcleo*'s closed fuel cycle allows the recycling of nuclear waste, reducing environmental impact and optimizing fuel utilization.

Advanced monitoring technologies are essential to ensure the safe and efficient operation of these reactors, as they must withstand extreme operating environments characterized by high temperatures (360–550°C, for the vessel), mechanical stress, and radiation (from kGy to few MGy cumulated doses, according to the probe's position). Currently, mechanical and electrical sensors dominate the market due to their broad measurement range, straightforward manufacturing processes, and cost efficiency [1]. However, traditional mechanical sensors often struggle with durability issues, particularly in demanding environments, where their limited displacement range and rigid structures pose challenges. Similarly, electrical sensors require intricate signal processing systems due to the complexity of their

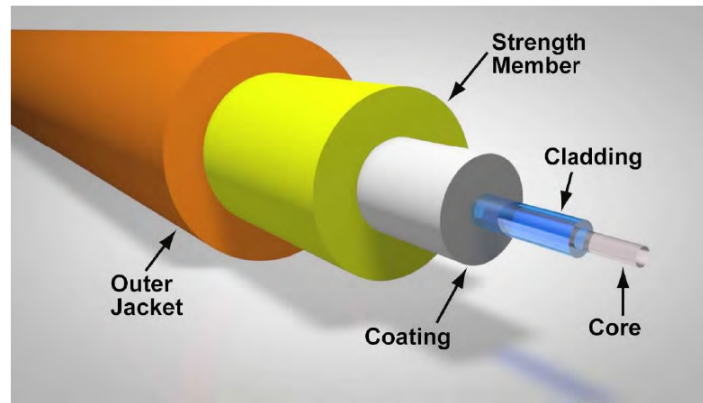
components, circuits, and connections, which can negatively impact measurement accuracy. Moreover, these sensors are highly vulnerable to external disturbances, including static electricity, electromagnetic interference (EMI), and radio frequency interference (RFI) [1,2].

To overcome these limitations, Fiber Optic Sensors (FOSs) have gained widespread adoption for detecting and analyzing various physical and chemical parameters [2–4]. Among these technologies, Fiber Bragg Grating (FBG) sensors [5] have emerged as a promising solution due to their compactness (external coating diameter smaller than 100  $\mu\text{m}$  [6,7]), lightweight design, and ability to integrate seamlessly with reactor components [8], offering significant advantages over conventional technologies thanks to their minimal volume, flexible geometry, and non-invasive deployment [9]. Their high multiplexing capacity allows multiple sensors — up to 13-14 per fiber, and even more [10,11] — to operate on a single optical line, significantly reducing the number of cables and simplifying installation and network complexity. This feature is especially beneficial for long-distance monitoring or scenarios requiring a large number of sensors. FOSs also provide immunity to EMI, making them ideal for environments with high magnetic fields or radiation [2,4]. Additionally, they are explosion-proof, electrically isolated, and capable of safe operation in cryogenic and hazardous atmospheres. Their lightweight and compact design enables deployment in hard-to-reach locations, while remote sensing capabilities ensure reliable performance over significant distances between sensors and interrogators. Unlike traditional sensors, FBGs measure absolute parameters (e.g., Bragg wavelength) independent of power fluctuations, ensuring accuracy without requiring external references. Furthermore, FBGs exhibit remarkable sensitivity across a wide range of measurements, allowing precise detection of minute variations in temperature, strain, and pressure [8]. For instance, they demonstrate a temperature sensitivity of 13  $\text{pm}/^{\circ}\text{C}$  and a strain sensitivity of 1.2  $\text{pm}/\mu\epsilon$  [8,9].

This study investigates the performance of fs-FBG sensors in high-temperature and mechanically stressed environments, replicating conditions found in Generation IV LFRs. FOSs are primarily designed to monitor the structural integrity of *newcleo*'s components, such as reactor vessel, control rods, and steam generator. They can provide real-time monitoring of critical parameters like temperature, stress, and structural integrity, enhancing reactor safety and reliability [12,13]. The research focuses on validating the sensors' linearity, repeatability, and durability under these harsh conditions. To achieve this, a comprehensive testing campaign was conducted, including thermal cycles up to 300°C and thermo-mechanical tests on metallic specimens with FBGs bonded through high-temperature adhesives. This thermal upper limit is due to machine calibration limitations. However, reaching 300°C provides a strong basis for our analyses and tests. Future experiments will include additional testing loops at *newcleo*, specifically on molten lead test platforms, to further evaluate sensor performance and reliability.

## 2. Optical Fiber and FBG Sensors

Optical fibers (illustrated in Figure 1) are cylindrical dielectric waveguides designed to transmit light along their axis through the mechanism of total internal reflection. They are composed of three main structural components [14]: the core, typically made of high-purity silica, sapphire or plastic materials, where light propagates; the cladding, also made of silica but with a lower refractive index to confine light within the core and allow its propagation through the principle of total internal reflection; and the coating, usually composed of polymer materials (e.g., polyimide), which provides mechanical protection and resistance to environmental stress. These fibers are widely utilized in sensing technologies due to their immunity to electromagnetic interference, compact size and multiplexing capability.

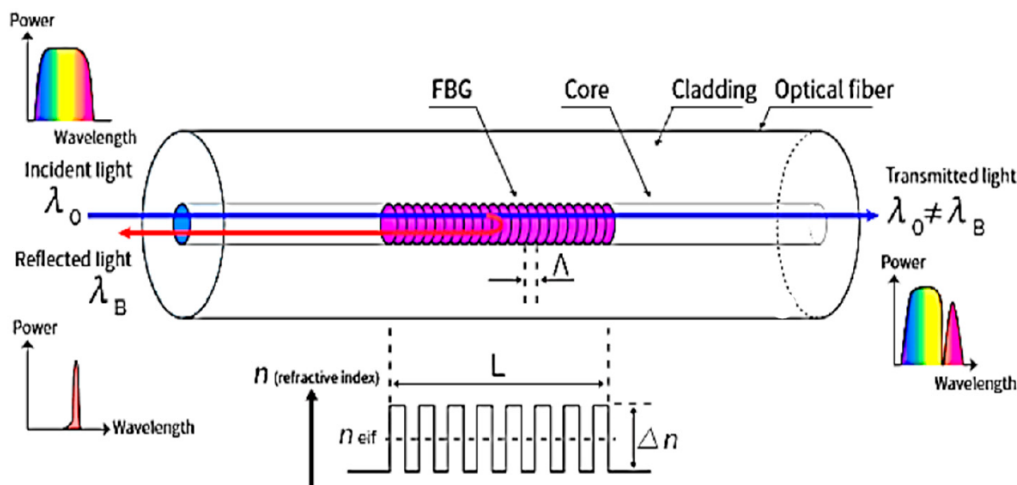


**Figure 1.** Structural components of an optical fiber. Image from <https://stl.tech/blog/types-of-optical-fiber/>.

Fiber Bragg Gratings (FBGs) represent a great advancement in optical sensing technology. These gratings are inscribed within the core of an optical fiber as a periodic modulation of the refractive index. The periodic modulation creates a grating that reflects particular wavelengths of light while allowing others to pass through, thus functioning similar to a highly selective optical filter, as depicted in Figure 2. When light propagates through the fiber, the grating reflects a specific wavelength, known as the Bragg wavelength ( $\lambda_B$ ), while other wavelengths pass through. The Bragg's law is given by:

$$\lambda_B = 2\Lambda n_{\text{eff}}, \quad (1)$$

where  $\Lambda$  is the grating period and  $n_{\text{eff}}$  is the effective refractive index of the fiber core.



**Figure 2.** Scheme of FBG working principle [15].

The fundamental mechanism of FBG sensors is based on the principle of wavelength shift, where external perturbations such as strain, temperature, or pressure induce changes in the grating period ( $\Lambda$ ) and the effective refractive index ( $n_{\text{eff}}$ ). These variations result in a shift in the Bragg wavelength ( $\lambda_B$ ), expressed as:

$$\Delta\lambda_B = 2\Lambda\Delta n_{\text{eff}} + 2n_{\text{eff}}\Delta\Lambda. \quad (2)$$

This relationship shows that the wavelength shift depends on changes in both the grating period and the effective refractive index, enabling precise measurements of external perturbations [5].

The sensitivity of FBGs to external parameters can be analyzed considering a measurand quantity  $X$  (e.g., temperature, strain, or pressure). The dependence of the Bragg wavelength on  $X$  is obtained by differentiating Eq. (2) with respect to  $X$ :



$$\frac{d\lambda_B}{dX} = 2 \frac{d(\Lambda n_{\text{eff}})}{dX} = 2\Lambda \frac{dn_{\text{eff}}}{dX} + 2n_{\text{eff}} \frac{d\Lambda}{dX}. \quad (3)$$

This equation shows that the measurand parameter  $X$  affects either the effective refractive index, the grating period, or both, depending on the nature of the perturbation [5].

For practical applications, this relationship can be simplified by introducing coefficients  $K_T$  and  $K_\epsilon$ , which represent the temperature and strain sensitivity of the sensor, respectively [16]. The simplified expression becomes:

$$\Delta\lambda_B = K_T\Delta T + K_\epsilon\Delta\epsilon, \quad (4)$$

where  $\Delta T$  is the temperature change,  $\Delta\epsilon$  is the strain applied to the fiber,  $K_T = \lambda_B(\alpha + \xi)$ , and  $K_\epsilon = \lambda_B(1 - p_e)$ . Here,  $\alpha$  is the thermal expansion coefficient,  $\xi$  is the thermo-optic coefficient, and  $p_e$  is the photoelastic constant.

The ability to decouple temperature and strain effects [5,8] depends on advanced sensor configurations, such as using multiple FBGs or temperature compensation techniques. These sensors are highly versatile, allowing precise monitoring of key parameters in challenging environments.

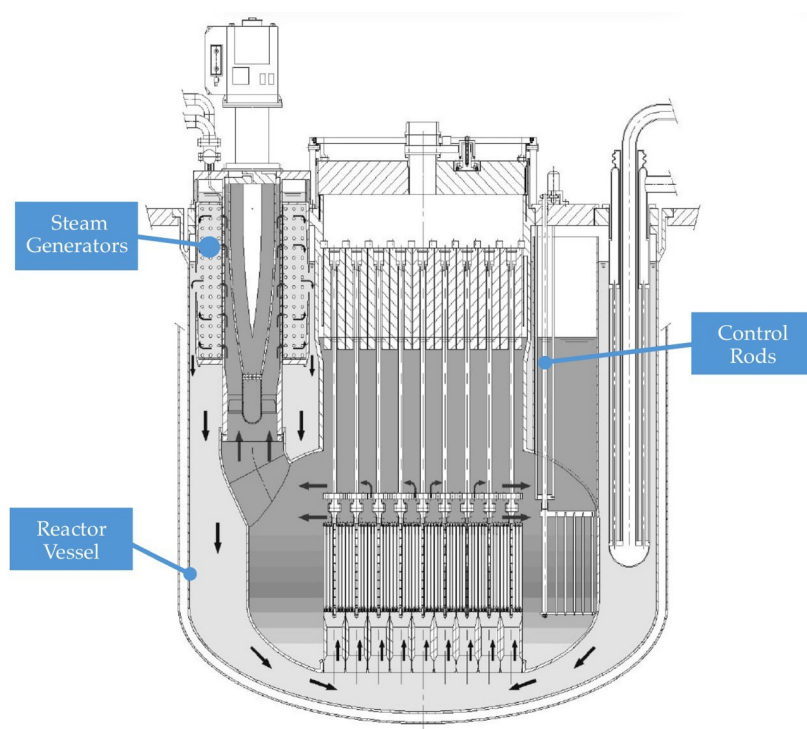
### 2.1. Application of Fiber Optic Sensors

In Structural Health Monitoring (SHM), FOSs enable high-resolution strain, pressure, and temperature measurements. They are used for monitoring underground infrastructure like tunnels [17], assessing landslide stress variations [18], and tracking pore pressure in geohydraulic structures [19]. Additionally, FOSs strengthen structures through fiber-based sensors integrated into carbon materials [20], and enhance leak detection in water infrastructure with active distributed temperature sensing (ADTS) [21]. FBGs can detect pipeline leaks by monitoring temperature and strain [22], while Fabry-Pérot interferometers (FPI) provide precise pressure monitoring in deep-sea oil wells [23]. Fabry-Pérot sensors are particularly valuable in extreme environments, operating at high temperatures (up to 400°C) and under intense radiation in nuclear reactors [24]. Their compact design reduces gamma heating, making them suitable for in-pile experiments [25]. These sensors maintain measurement integrity under harsh conditions, crucial for monitoring during events like Loss of Coolant Accidents (LOCA) [26] and for applications in severe nuclear accidents [27].

FOSs are widely used in the nuclear industry too, for their robustness in extreme environments. Applications include temperature monitoring ensuring safety and process control [28], and detecting pipeline leakages with distributed sensing systems [29]. FBG sensors also demonstrate high radiation tolerance and are under development for next-generation reactors [30,31]. Recent advancements in optical fiber technology have led to the development of radiation-hardened fibers capable of enduring extreme conditions, making them particularly suitable for applications in the nuclear reactors. These fibers are engineered to withstand high temperatures, with studies demonstrating their effectiveness in environments exceeding 300°C [32]. They are also designed to maintain performance under significant radiation exposure, with research highlighting their resilience against fast neutron fluences up to  $10^{20}$  n/cm<sup>2</sup>s [33] and gamma doses reaching 200 kGy [34,35]. The integration of optical fibers in nuclear reactor designs allows for real-time monitoring of parameters like temperature, strain, and radiation dose rates [36,37], with FBGs proving effective for temperature and strain measurements under challenging conditions [38,39]. Furthermore, the development of sensors capable of detecting acoustic signals and vibrations in fuel assemblies enhances the ability to assess structural integrity and monitor reactor dynamics [40,41]. Studies on the effects of radiation-induced attenuation and luminescence [42,43] reveal significant insights into fiber behavior in high-radiation backgrounds, emphasizing the need for ongoing development to enhance their durability and functionality [44–46]. Recent advancements in optical fiber technology not only ensure reliable monitoring in nuclear facilities but also support their potential use in future reactor designs [28,30,47,48].

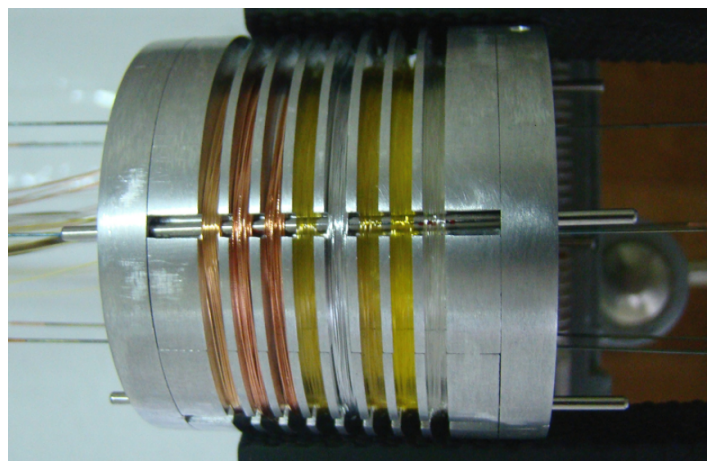
### 3. Case Study: FBGs for Gen. IV Reactors

Part of this study aims to develop an advanced platform for diagnostics and monitoring structural issues in the pre-mentioned Generation IV Nuclear Reactors. The platform will integrate innovative FOSs, specifically engineered to withstand extreme reactor environments — high temperatures (360–550°C), radiation exposure (kGy to MGy), neutron flux (approximately  $10^{12}$  to  $10^{15}$  n/cm<sup>2</sup>s), and mechanical constraints. In addition, it will incorporate software tools that maximize data extraction and make insights accessible to operators. Since developing innovative and effective sensing technologies for LFRs is a central focus for *newcleo*, FOSs have been identified as one of the most promising solutions for continuous monitoring of critical operational parameters and structural integrity. Their selection is also attributed to their high technology readiness level. FOSs are developed mainly for monitoring parameters for the reactor vessel, control rods and steam generator structures, highlighted in Figure 3. An in-depth analysis and testing about how and where to place these sensors, which are going to be integrated with the actual design of the components, is part of this project.



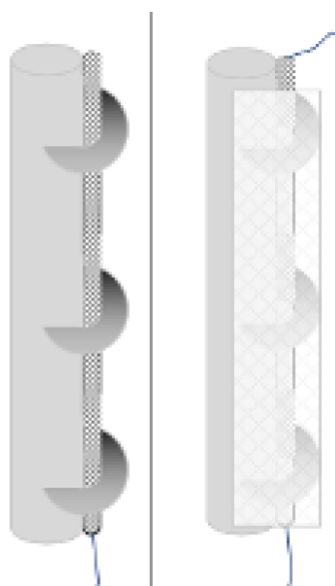
**Figure 3.** Design schematic of *newcleo*'s reactor vessel, control rods, and steam generator, of the LFR-AS-200.

The Reactor Vessel (RV) hosts the core and facilitating coolant circulation. The RV consists of a cylindrical shell with a tori-spherical bottom head. It is located inside the Reactor Building and its flange rests on the support structure all around its circumference. The function is the containment of primary coolant and cover gas. The total height of the vessel is 5140 mm and the wall thickness is 30 mm. Its compact design enhances safety and operability by reducing radioactive waste and eliminating components like shielding and breeding assemblies. Optical fibers with FBG sensors are proposed to be mounted externally on the RV's wall, avoiding in this case direct exposure to molten lead. Temperature, strain, and vibrations on the RV's internal surface are inferred using models that correlate external FBG measurements to internal conditions via thermal conduction and elastic wave propagation [32,41]. For durability, optical fibers can be embedded in grooves machined into the RV wall and secured with high-temperature resin. This method (example shown in Figure 4) ensures robust sensor installation while shielding the fibers from mechanical and environmental stress. Radiation-hardened fibers with protective ceramic coatings are recommended for nuclear environments [40,49].



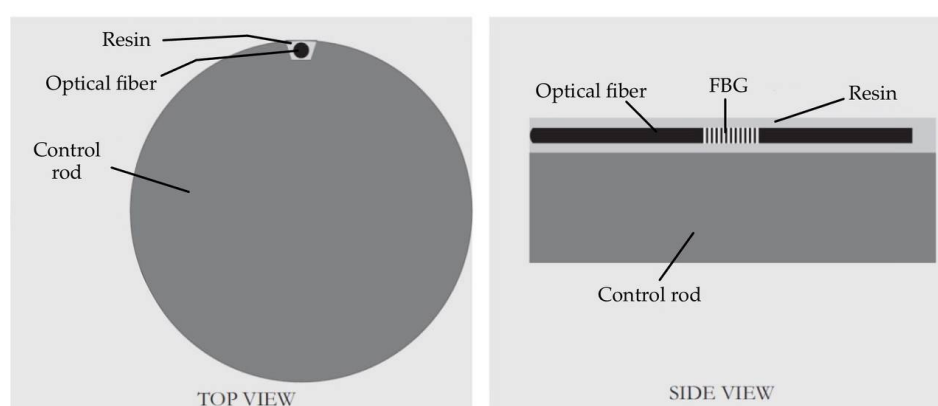
**Figure 4.** Example of integration of optical fiber inside grooves etched on the RV's external wall [49].

The spiral-tube Steam Generator (SG) shows *newcleo*'s commitment to compactness, safety, and reliability. It features a thick plate supporting the SG flange, two perforated shells, and a lower plate to support the tube bundle's weight. The top plate allows vertical tubes to connect to the reactor roof, while the inner perforated shell directs lead flow to the tube bundle and couples with the Amphora-Shaped Inner Vessel (ASIV). The thinner outer shell directs cold lead flow outside the SG. Operating at 140 bars, the steam generator converts heat from liquid lead into superheated steam, ensuring efficient heat transfer and preventing lead-water interactions while enhancing safety and structural stability. Optical fibers can be integrated into the SG design through encapsulation into a stainless-steel housing, and tack-welded [47] onto the tubes, possibly also covered in high-temperature and radiation resistant adhesives [47,50] to ensure perfect adhesion. The methodology is explained by Birri et al., and illustrated in Figure 5. Here, direct contact with molten lead is unavoidable. Alternatively, FOSs can be embedded in grooves machined onto the tube surfaces [32,51], that provides accurate measurements while protecting against molten lead and mechanical damage. High-precision machining or laser technologies shall be used to create the grooves, with fibers secured via laser welding or encapsulated in durable materials like ceramics or metal alloys. Protective sheaths of stainless steel or ceramics [52] enhance durability, shielding fibers from extreme conditions and structural stresses. While this method improves accuracy and robustness, further research is needed to ensure the mechanical integrity of the tubes and long-term fiber protection [31].



**Figure 5.** Fiber fed through tack-welded capillary (left), and fiber fed through tack-welded capillary and taped along length (right) [47].

Concluding, Control Rods (CRs) are used for both reactivity regulation and passive safety. To effectively control the system, six CRs are positioned at the core periphery to manage reactivity changes associated with the transition from cold shutdown to full power, mitigate criticality swings during irradiation cycles due to fuel depletion, and command power variations. These CRs utilize neutron moderation to influence the chain reaction, and their unique flag shape is designed to optimize this control mechanism. Optical fibers can be included into the CRs' design following the same reasoning done for the steam generator. The most promising solution seems to be embedding them within grooves machined onto their surfaces (Figure 6) [32]. The grooves protect the fibers from molten lead and mechanical forces while being filled with high-temperature, radiation-resistant resin to secure and shield the fibers. A stainless steel tube encases the fibers [50], offering enhanced protection against corrosion, thermal shocks, and radiation. A silica micro-capillary tube [53] between the optical fiber and the steel can be further integrated, mitigating thermal expansion mismatches and shielding the fiber from contaminants and stresses. This multi-layered setup ensures mechanical robustness, chemical stability, and accurate long-term performance.



**Figure 6.** Design integration of optical fibers onto the control rods. Image adapted from De Pauw et al. [32].

### 3.1. FOSs in High Temperature Environments

In moderate temperature ranges (0°C to 200°C), FBGs exhibit stable temperature sensitivity, from 11 to 13 pm/°C, due to the thermo-optic effect and fiber thermal expansion [8,9,48]. However, beyond this range, the sensitivity becomes non-linear, requiring polynomial calibration for accurate measurements. Silica fibers, commonly used in FBGs, perform well up to 300°C but degrade at higher temperatures. Above 500°C, hydrogen ingress can destabilize silica, causing fractures on the fiber's surface [54]. Furthermore, between 500°C and 900°C, silica fibers become prone to embrittlement, and their protective coatings, such as polyimide, degrade more rapidly at elevated temperatures [12].

At extreme temperatures, structural integrity becomes a challenge. As the temperature increases, the refractive index contrast in the fiber diminishes, which can lead to shifts in the grating period. At around 700°C, dopants such as germanium (Ge) can escape from the fiber core, erasing the gratings. At temperatures exceeding 900°C, the silica fiber itself becomes thermally unstable, leading to the complete degradation of the gratings [12]. However, this should not be *newcleo's* scenario, since temperatures are expected to be in the range of 360–550°C.

#### 3.1.1. Reinforcement Strategies

FBG fabrication techniques, such as the phase-mask method [8] and femtosecond laser inscription [5,8], play a crucial role in determining the grating's performance. Femtosecond laser inscription, in particular, enables the creation of highly stable gratings in non-photosensitive fibers, making them ideal for applications in high-temperature and radiation-intense conditions. Fs-FBGs are classified into two main types: Type I and Type II [13]. Type I gratings are formed with laser pulses below the glass damage threshold, inducing densification and a positive refractive index change. In contrast, Type II gratings are produced with laser pulses above the damage threshold, resulting in significant



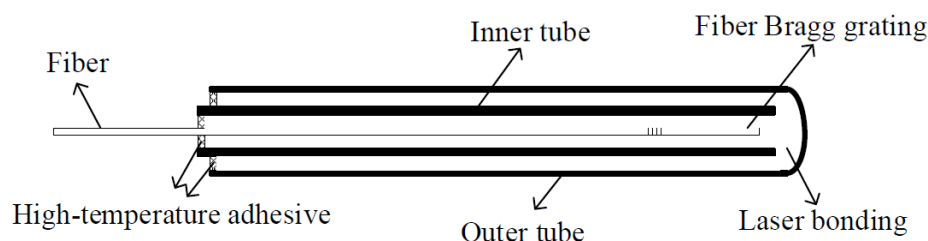
structural changes and enhanced thermal stability, with functionality maintained at temperatures up to 1000°C [13]. The use of femtosecond lasers enables the fabrication of gratings stable up to the glass transition temperature of the fiber material, making them ideal for high-temperature applications [12]. In contrast, UV-inscribed FBGs suffer from limitations such as lower thermal stability and the need for photosensitive fibers [8]. Unlike fs-FBGs, which remain stable up to the glass transition temperature, UV-inscribed gratings degrade at significantly lower temperatures, making them less suitable for high-temperature and radiation-intense applications [5,12].

Regeneration techniques have been shown to enhance the thermal stability of fs-FBGs [13,48]. In particular, regenerating 'seed' FBGs is a promising approach to extending their operational lifetime in high-temperature environments [48,55,56]. This process involves annealing a fully saturated seed grating at high temperatures, up to 950°C [48,56], leading to the formation of regenerated FBGs (RFBGs) with enhanced thermal stability. Factors such as annealing protocol, fiber composition, and hydrogen sensitization determine the reflectivity and mechanical properties of the regenerated gratings [55,57]. Recent advancements have demonstrated significant improvements, with RFBGs achieving mechanical strengths up to four times greater than standard FBGs and showing operational stability even at temperatures exceeding their regeneration point by over 100°C [55,56].

RFBGs have proven capable of operating continuously at temperatures above 1000°C [58], with some demonstrating lifetimes exceeding 9000 hours at 890°C [13,56]. Their dual functionality for temperature and stress-strain monitoring has been confirmed, achieving, respectively, sensitivities of 16.50 pm/°C and 1.25 pm/μ $\epsilon$  [55]. Despite their robustness, challenges remain, including brittleness induced by the relaxation of internal stresses during regeneration and low reflectivity, which limits their dynamic range [48,55]. Future work should focus on improving annealing methods to mitigate brittleness, developing encapsulation techniques for enhanced mechanical protection, and validating long-term performance under combined thermal, mechanical, and radiative stresses [55,56].

Coatings play a fundamental role in enhancing the performance and durability of FOSs in high-temperature environments [51,52]. Polyimide coatings are widely used for their flexibility and thermal stability but degrade beyond 350°C, limiting their long-term use in extreme conditions [51]. Metal coatings, such as titanium and zinc, offer superior thermal and mechanical stability above 400°C, making them more suitable for demanding applications [59]. Titanium-coated FBGs excel in strain sensitivity, while zinc coatings show high sensitivity to temperature, with bimetallic coatings (e.g., Ti/Zn) balancing both properties [59].

For harsher environments, such as nuclear reactors or molten lead-bismuth eutectic (LBE) systems, double-tube protection (Figure 7) and ceramic coatings are preferred. Stainless steel tubular housings shield fibers from corrosion and mechanical stress, while ORMOCER coatings resist LBE-induced damage [50,60]. Additionally, advanced designs using RFBGs with dual-layer protection demonstrate exceptional thermal endurance (up to 1000°C) and enhanced strain sensitivity, making them ideal for extreme conditions [53].



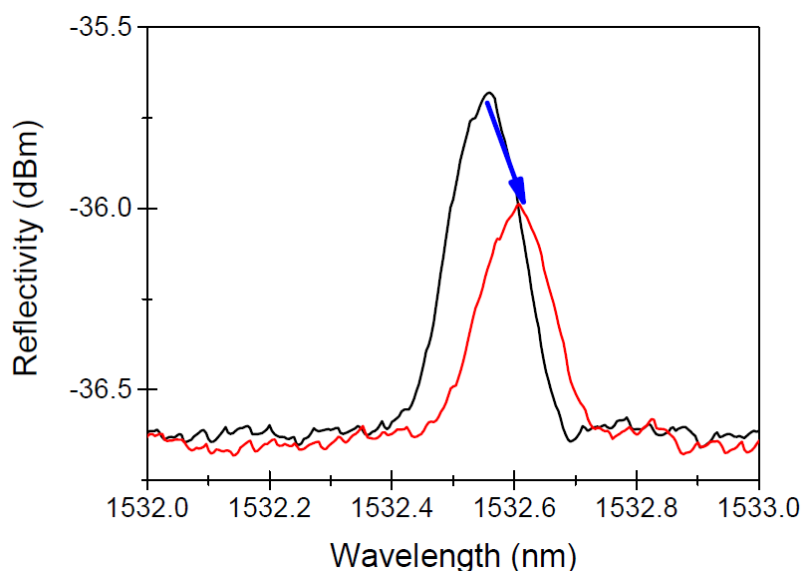
**Figure 7.** Diagram structure of tube packaged fs-FBG high-temperature sensor [50].

### 3.2. FOSs in Radiative Environments

Silica-based optical fibers exhibit varying performance degradation due to radiation effects, such as Radiation-Induced Attenuation (RIA), Radiation-Induced Emission (RIE), and Radiation Induced Refractive Index Change (RIRIC) [36,42,61]. RIA occurs when radiation induces point defects within the

silica matrix, increasing light absorption and signal attenuation [42,61]. Fiber composition, particularly doping elements like germanium, phosphorus, and aluminum, influences the severity of RIA, with pure-silica fibers showing superior resistance [42]. Additionally, fibers doped with elements such as germanium exhibit higher sensitivity to radiation-induced defects, while fluorine-doped fibers tend to resist radiation effects better. RIA can be somewhat mitigated through post-irradiation treatments, like hydrogen loading [42]. RIE, on the other hand, results in the generation of light within the fiber during radiation exposure, which, while useful for dosimetry, can interfere with fiber-based communication systems [42]. RIRIC occurs when radiation alters the refractive index of the fiber due to changes in its glass matrix, potentially affecting fiber performance in sensor applications [42,61]. Neutron irradiation contributes to these changes, with neutron flux inducing compaction in the silica matrix, which leads to an increase in the refractive index, affecting sensor accuracy. The signature of displacement damage typically becomes apparent at neutron fluences of  $10^{16}$ – $10^{17}$  n/cm<sup>2</sup>s, further influencing the fiber's optical properties [33,38,62].

When exposed to radiation, FBGs typically suffer from two primary effects [43]: radiation-induced Bragg wavelength shift (RI-BWS) and signal-to-noise ratio reduction [61], and both effects are shown in Figure 8. These effects stem from changes in the optical properties of the fiber due to radiation interactions with the material's atomic structure. Radiation alters the refractive index of the fiber core, primarily through defect formation in the silica matrix. These defects, sometimes referred to as 'color centers', absorb light and distort the transmission characteristics of the fiber, leading to wavelength shifts that reduce the accuracy of the sensor. The extent of damage depends on fiber composition and pre- or post-inscription treatments. Radiation-resistant fibers, such as hollow-core photonic bandgap fibers, have demonstrated greater resilience, maintaining low levels of attenuation and retaining sensor accuracy under extreme radiation conditions [63]. Notably, FBGs continue to show resilience even under prolonged radiation exposure, maintaining functionality and temperature sensitivity crucial for nuclear reactor monitoring [39,63].



**Figure 8.** An example of the radiation-induced effects on a Bragg peak reflection spectrum, before (black line) and after (red line) X-ray irradiation at 1.5 MGy at room temperature [61].

The performance of optical fibers degrades when exposed to high radiation and temperatures [43,44]. RIA increases as both factors accelerate defect formation, with RIA levels varying based on radiation dose and temperature [64]. Understanding this interplay is fundamental for fiber reliability in extreme environments. Temperature's effect on RIA is dose-dependent. Below 30 kGy, temperature helps anneal defects, but above this threshold, RIA increases with temperature up to 92°C, after which it plateaus [64]. This suggests that higher temperatures may counteract some radiation damage.

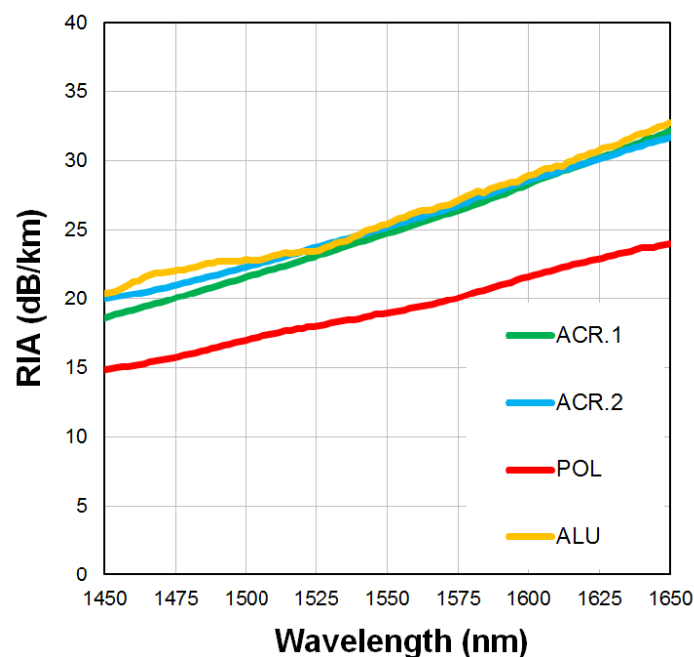
Mechanical properties are also affected. Polyimide-coated fibers, which withstand temperatures up to 300°C, lose mechanical strength when exposed to high radiation doses at elevated temperatures. At 10 MGy(SiO<sub>2</sub>) and 100°C, their tensile strength drops, limiting their long-term reliability [40,64].

### 3.2.1. Reinforcement Strategies

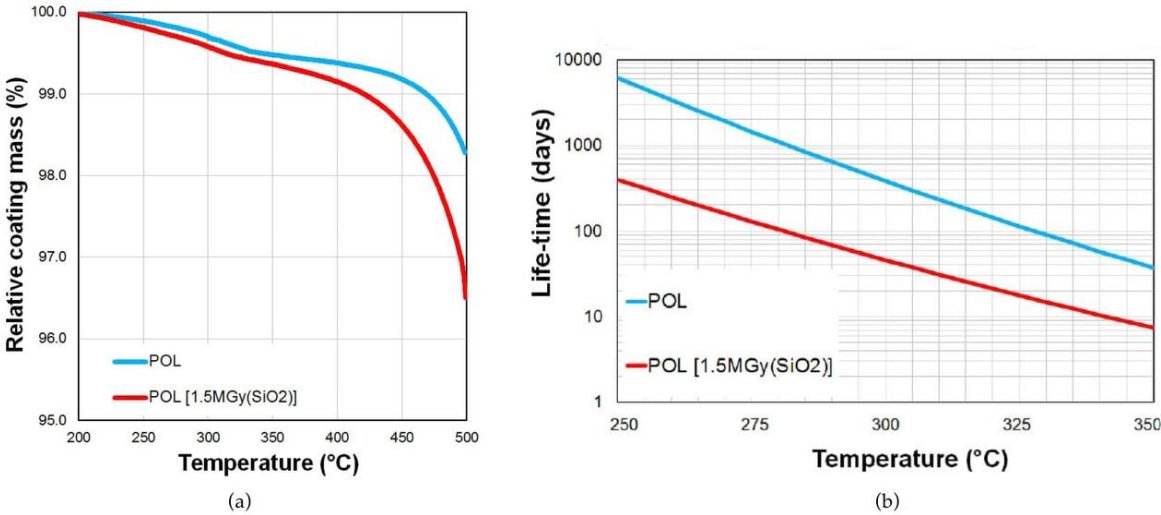
RIA significantly degrades the performance of optical fibers in radiative environments, necessitating the development of radiation hardened fibers [44]. These fibers, typically employing Pure Silica Cores (PSC) or Fluorine-doped cores, minimize color center formation during irradiation and exhibit RIA levels around 10 dB/km at 1550 nm for doses up to several hundred kGy, with reliable operation even at MGy dose levels and neutron fluences of  $10^{20}$  n/cm<sup>2</sup>s [33]. Radiation-tolerant fibers, using Germanium-doped cores, offer a cost-effective solution for environments with lower total ionizing doses, maintaining low RIA values for applications such as short data links or lead fibers [65].

The performance of optical fibers under radiation depends heavily on core composition, dopants, and drawing conditions. While PSC fibers are ideal for telecom applications, their performance in radiative environments varies, with some exhibiting high RIA values of up to 2000 dB/km at doses as low as 2 kGy [33]. Temperature also influences RIA behavior, affecting defect kinetics and recovery, making tailored designs essential for environments with fluctuating radiation and thermal conditions [65].

Coatings are equally crucial for radiation resistance and mechanical integrity. Acrylate coatings degrade rapidly under radiation, while high-temperature acrylates perform better. Polyimide coatings, resilient up to 300°C, degrade under high radiation and temperature, while aluminum coatings offer protection at higher temperatures but increase micro-bending sensitivity [64,65]. Figure 9 shows RIA values, with polyimide demonstrating a slight reduction in RIA compared to acrylates and aluminum due to optimized drawing conditions. Polyimide-coated fibers maintain low RIA at lower radiation doses, but at doses above 10 MGy, particularly at 1625 nm, RIA increases sharply, limiting signal transmission in high-radiation environments [64]. Thermal degradation above 350°C further weakens polyimide coatings, as shown in lifetime predictions in Figure 10 [40].



**Figure 9.** Spectral RIA of the different samples after passive irradiation up to 750 kGy(SiO<sub>2</sub>) at room temperature [40].



**Figure 10.** (a) TGA curves of polyimide coated fiber before/after irradiation. (b) Life-time prediction of polyimide coated fiber before/after irradiation for a 20 wt% mass loss criteria [40].

Rare-earth (RE) doped optical fibers, such as those incorporating Erbium (Er) and Ytterbium (Yb), present unique challenges and opportunities for radiation hardening [66]. The inclusion of codopants like cerium in phosphosilicate-based cores has proven effective in reducing RIA, particularly by mitigating the formation of P1 defects associated with phosphorus. Hydrogen pre-loading further enhances the radiation tolerance of these fibers by suppressing defect precursors and improving RIA behavior, even at cumulative gamma-ray doses of up to 50 krad [45,66]. Hydrogen loading and fluorine doping have been employed as advanced radiation hardening techniques [45]. Hydrogen treated silica fibers have demonstrated significantly reduced RIA, attributed to the suppression of defect precursors like non-bridging oxygen hole centers. This treatment effectively converts these defects into less harmful hydroxyl groups, substantially lowering RIA levels, especially in the visible spectrum. However, challenges such as radiation-induced luminescence remain, particularly under gamma and neutron irradiation [45].

4. Materials and Methods

*newcleo*'s operating environment is characterized by high temperatures (360–550°C) and high cumulated radiation doses (1–10 MGy), combined with a corrosive environment due to molten lead used as coolant. This article presents a comprehensive experimental setup aimed at evaluating, in the first instance, the performance of different FBG sensors under varying thermal and structural conditions. The setup is designed to evaluate the influence of three primary factors — fiber type, wavelength, and gluing technology — on the system's performance. Similar tests, with lower temperature thresholds, were already conducted in Politecnico di Torino by Aimasso et al. [15,16,67].

The testing setup included four optical fibers (single-mode, 1 m length, core diameter of 9 μm, cladding diameter of 125 μm) provided by Télefo S.p.A. FBGs were inscribed with femtosecond laser directly into their cores by the supplier. Coated with polyimide, the fibers' ID and details are listed in Table 1.

**Table 1.** Femtosecond-inscribed FBG specifications for the experimental setup.

FBG ID	Wavelength (nm)	Reflectivity (%)
FBG1	1539.64	54.82
FBG2	1544.03	54.45
FBG3	1548.01	54.02
FBG4	1551.94	53.55

The resin utilized to bond optical fibers to the specimens, during mechanical tests, was WEICON Ceramico W, supplied by WEICON®. All the tests were executed inside the 3119-607 Temperature Controlled Instron chamber of Politecnico di Torino (Figure 13a).

The interrogation system comprised a SmartScan SBI laser interrogator, capable of monitoring four FBGs simultaneously, transmitting a laser beam, and analyzing the reflected wavelengths. The interrogator was developed by the Smart Fibres company (Bracknell RG12 9BG, UK). This setup minimized data misinterpretations and allowed for independent communication with each sensor. The complete laboratory configuration, illustrated in Figure 11, integrated both FBGs and thermocouples for cross-referencing temperature and strain measurements.



**Figure 11.** Laboratory setup: (1) Thermocouple reader, (2) SmartScan SBI interrogator, (3) control PC.

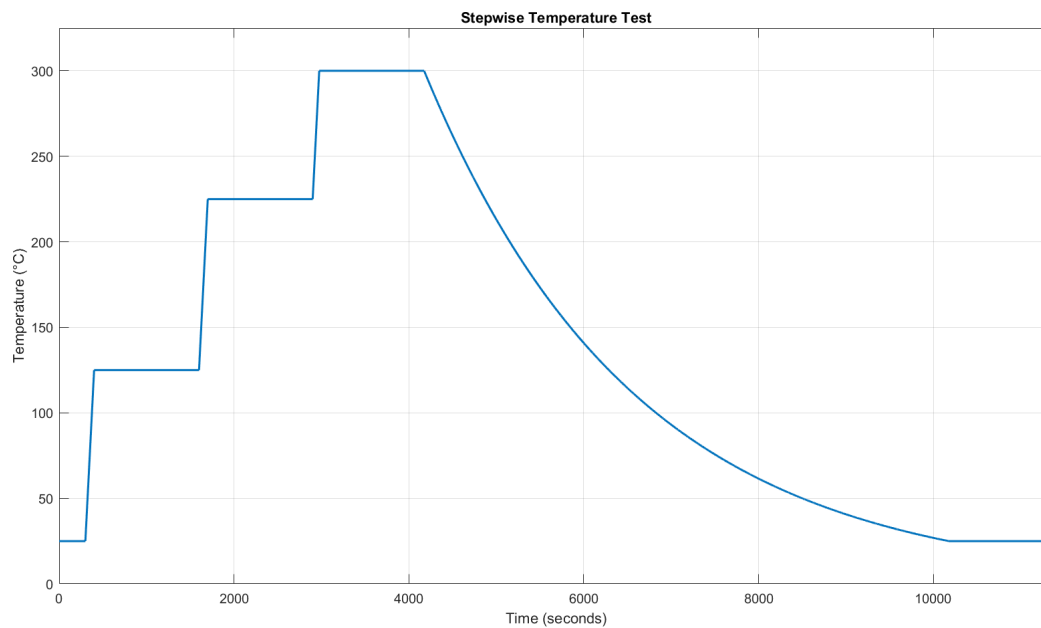
The experimental design involves testing up to four FBGs across multiple wavelengths and gluing methods, under controlled thermal cycling and structural loading conditions: the performance of FOSs can vary significantly depending on the type of fiber, wavelength of operation, and the gluing technology used for sensor integration. The goal is to identify the most promising fiber optic sensors for industrial applications that require high temperature and structural resistance.

Each test is conducted with two repetitions: the first one establishes a baseline for consistency, while the second serves to confirm the reliability of the results. This approach is sufficient for thermal cycles because the nature of thermal processes tends to produce consistent outcomes with minimal variation, as experienced by Madan et al. [51,52]. The relatively stable behavior of materials during thermal cycling means that two repetitions can effectively capture any significant trends or deviations without the need for additional trials. Future research and testing will be conducted, with the main focus on testing fibers in radiative environments [49,54], to evaluate the responsiveness and degradation of the sensors under gamma radiation [12,34,37] and neutron flux [39,62].

#### 4.1. Thermal Testing of Free Fibers

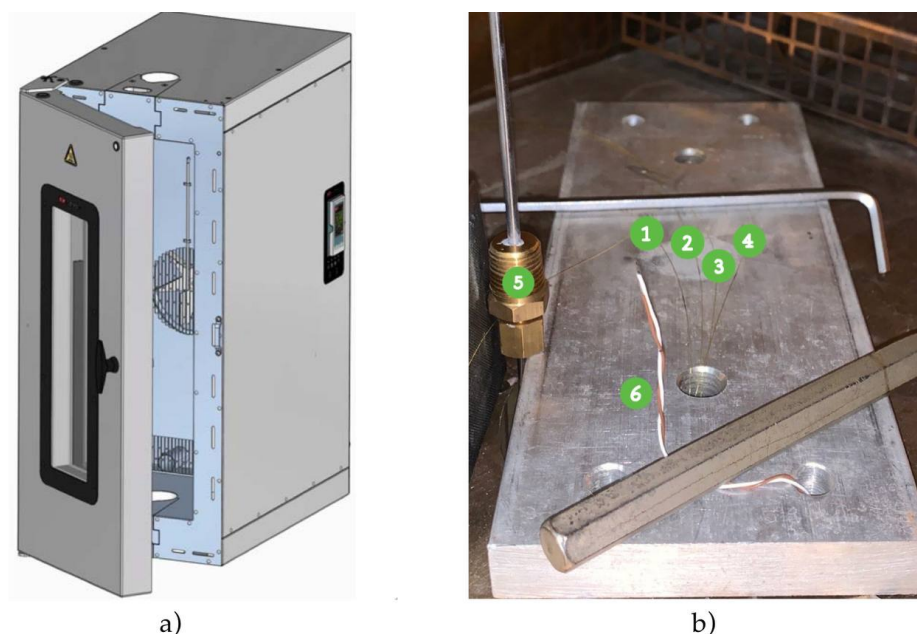
Two thermal tests were conducted inside the Instron thermal chamber, capable of reaching temperatures up to 300°C. Fibers were placed on a neutral platform, as shown in Figure 13b and subjected to step-wise thermal cycles with heating rates of 60°C/min and holding phases of 20 minutes at every 100°C. The ideal thermal cycle to be executed is shown in Figure 12.





**Figure 12.** Stepwise temperature cycle example. Here, it is proposed a thermal test with a heating rate of  $60^{\circ}\text{C}/\text{min}$ , including a holding phase of 20 minutes every  $100^{\circ}\text{C}$ . Once the maximum operating temperature is reached, the chamber will be turned off to allow it to naturally cool down to room temperature (this is an estimate close to the required time for cooling).

The goal is to evaluate the linearity and stability of the FBGs' wavelength response under repeated thermal variations. Our fs-FBGs are expected to have a better linearity along a wider range of temperature [51,52]: the grating structures inscribed using femtosecond lasers have attractive annealing characteristics and may provide a long-term stable operation in high-temperature environment, compared to conventional UV laser written grating structures. K-type and T-type thermocouples were employed as temperature reference sensors. K-type thermocouple has a sensitivity of  $41\ \mu\text{V}/^{\circ}\text{C}$  and an accuracy of  $\pm 2.5^{\circ}\text{C}$ , while the T-type presents a sensitivity of  $43\ \mu\text{V}/^{\circ}\text{C}$  and an accuracy of  $\pm 1.0^{\circ}\text{C}$ . The thermocouples reader sampled data at 1 Hz, with a resolution of  $0.01^{\circ}\text{C}$ . The FBG interrogator acquired data at 2.5 Hz for enhanced precision.



**Figure 13.** (a) 3119-607 Temperature Controlled Instron Chamber. (b) Setup of the optical fibers displaced on a neutral platform, to be inserted inside the Instron chamber. 1) FBG1, 2) FBG2, 3) FBG3, 4) FBG4, 5) K-type thermocouple, 6) T-type thermocouple.

#### 4.2. Thermal-Structural Testing

The second testing phase focused on evaluating the combined effects of thermal and mechanical loads on the performance of fs-FBGs. Optical fibers were bonded to tensile test specimens through resin, and were subjected to cyclic mechanical stress both at room temperature and higher temperatures. Conducted within the Instron thermal chamber, this phase utilized a maximum temperature of 250°C (due to resin's limitation) and tensile forces ranging from 1 kN to 5 kN, corresponding to the maximum amplitude value of applicable force inside the safety limits of the loading cell. These tests were performed under controlled load cycling, allowing us to monitor and apply precise forces, providing insights into the material behavior under specified stress levels. The positional data of the specimens were also recorded to analyze deformation patterns. These data were acquired through the Instron machine, that recorded the vertical movements of its crosshead. Thermal cycles similar to those utilized in the previous phase were employed, allowing for a controlled analysis of sensor response under simultaneous thermal and mechanical stresses.

This specific type of mechanical test was chosen to assess the FBG sensors' ability to withstand and accurately measure mechanical stresses. During reactor operation, components are subjected to dynamic stresses and vibrations due to thermal expansion, mechanical loading, and fluid-induced forces. Simulating these conditions through cyclic mechanical tests provides a preliminary evaluation of the sensors' durability and performance. Additionally, the test partially approximates the impact of molten lead coolant, which can generate both mechanical stress and vibrations [41,68].

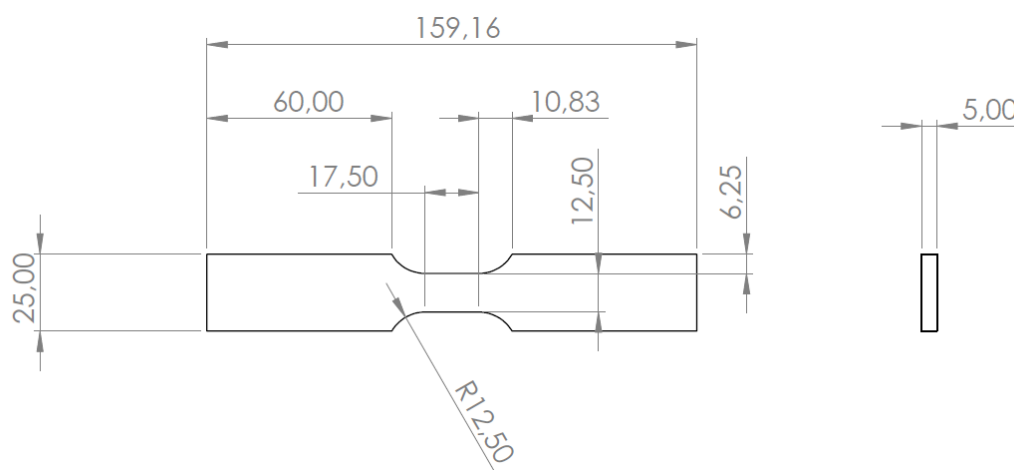
Two main tests were conducted:

- Tests at room temperature: Three sessions of 3,000 cycles at 5 Hz, conducted without heating.
- Tests at elevated temperatures: Six phases, alternating between temperature ramping and stabilization. First, the temperature is gradually increased (mechanical loads consisting of 800 cycles at 1 Hz, with a heating ramp rate of 20°C/min). Once the target temperature is reached, a stabilization phase follows, maintaining the temperature for 3,000 cycles at 5 Hz. This sequence is repeated three times, reaching 100°C, 200°C, and finally 250°C, resulting in a total of three ramp phases and three stabilization phases.

While only two main tests were conducted to limit the number of sensors and specimens, additional repetitions could enhance data reliability. Resin adhesion at high temperatures was crucial to

ensure sensor stability. This testing phase offers valuable insights into the long-term performance of FBG sensors under realistic thermal-mechanical loading conditions.

The test specimens, illustrated in Figure 14 and designed following the ASTM E606 Standard, were fabricated from AISI 316L(N) stainless steel, matching materials used in *newcleo*'s Generation IV reactor components. Optical fibers were bonded on the plane surface of the tensile test specimens using the selected high-temperature resin.

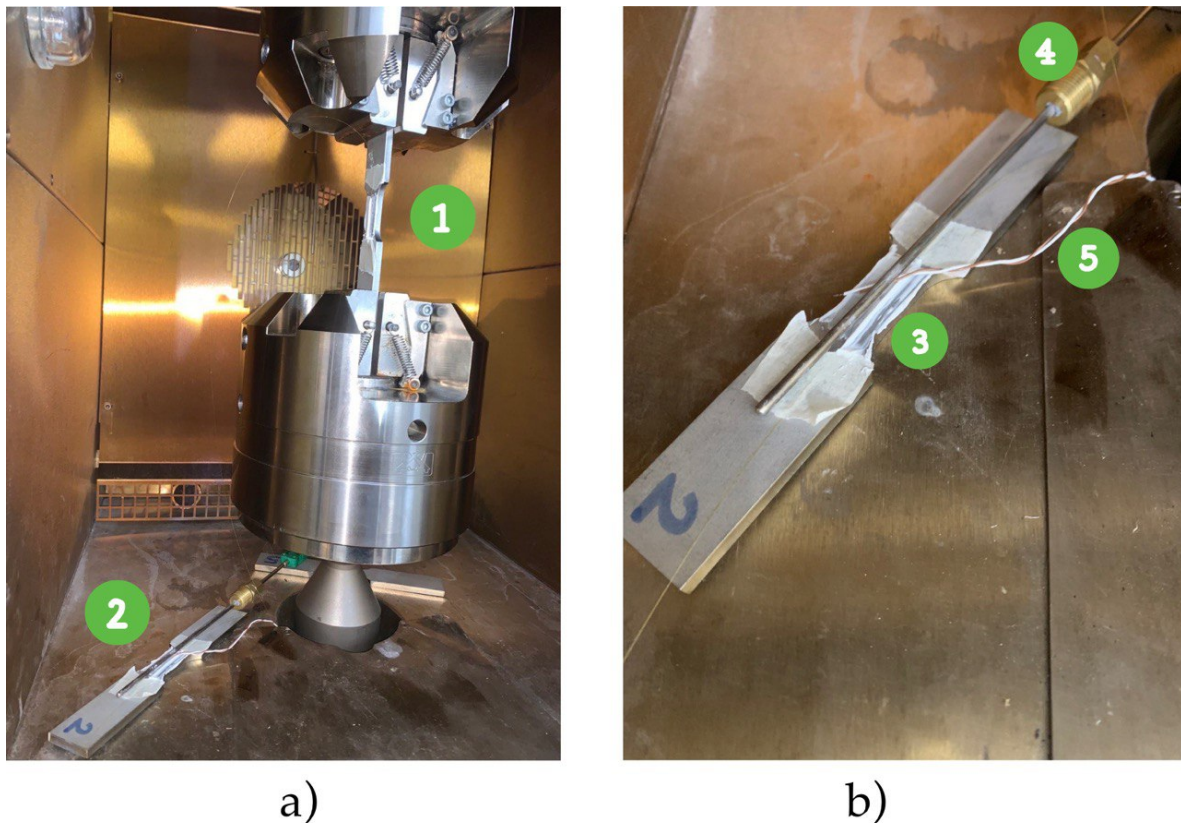


**Figure 14.** Drafting of the dog bone specimen according to the dimensions outlined in the ASTM E606 Standard.

The setup for this testing phase is illustrated in Figure 15. It includes two primary specimens:

- Specimen 1 (labeled as (1) in Figure 15a) is equipped with an optical fiber and undergoes both thermal and mechanical cycling. This specimen is used to study the combined effects of temperature and mechanical stress on the fiber's performance.
- Specimen 2 (labeled as (2) in Figure 15a) has the fiber attached to it with resin and is dedicated to thermal measurements. This specimen serves as a thermal reference, isolated from mechanical stress.

To enhance the accuracy of temperature readings, Specimen 2 is also equipped with K-type and T-type thermocouples (labeled as (4) and (5) in Figure 15b), which provide precise temperature reference values for the measurements from FBG2 (labeled as (3) in Figure 15b). The displacement data acquired from the FBG were compared to that registered from the Instron machine, that registered its crosshead vertical movements with a sensitivity of  $10 \mu\text{m}/\text{kN}$ , along with a resolution of  $1 \mu\text{m}$  and accuracy of  $\pm 0.03\%$  of the reading.



**Figure 15.** Setup for the thermal-mechanical tests: (a) Specimen 1, subjected to both tensile and thermal stresses. (b) Specimen 2, used as thermal reference.

#### 4.3. Resin's Selection

The choice of resin is critical for ensuring the reliable integration of optical fibers with the test specimens. Resins provide a robust bond capable of withstanding high-temperature and mechanical stresses while preserving the optical performance of the sensors. In this study, WEICON Ceramico W (supplied by WEICON®) was selected due to its superior thermal resistance (up to 250°C), high tensile strength (54 MPa), good Young's modulus (9.4–10 GPa) and excellent adhesion properties. The mixture consists of an epoxy base with aluminum oxide as the filler material, mixed in a ratio of 100:25 by weight. The uniform application of the resin, as shown in Figure 16, minimized stress concentrations along the fiber, ensuring accurate and reliable wavelength measurements. The FBG's IDs bonded to the tensile test specimens in Figure 16 are, from left to right, FBG4, FBG2, FBG1.





**Figure 16.** Resin (WEICON Ceramico W) application on the specimens. The FBGs are located at the center of the resin-covered area.

The deposition process was carried out manually, using a fine applicator to ensure an even distribution of the resin along the fiber. Proper resin application is essential, as any inconsistencies — such as uneven thickness, air bubbles, or excessive resin accumulation — can lead to localized stress concentrations [69]. These imperfections may distort the optical signal, reducing the accuracy of the wavelength measurements and introducing errors in temperature and displacement readings. Furthermore, improper resin deposition can compromise the adhesion between the fiber and the specimen, especially under high thermal and mechanical loads, leading to signal drift or even sensor detachment during testing.

## 5. Results and Discussion

In the following sections, the results from the thermal test are discussed, starting with the linear calibration of the FBG sensors, followed by an analysis of temperature estimation using these sensors. In the thermal-structural test section, the correlation between wavelength and displacement is explored, along with a compensation technique for temperature effects. Finally, the displacement estimation through FBG sensors is presented, highlighting how these sensors perform under combined thermal and mechanical stress.

These tests are important because they show how dependable and versatile FBG sensors can be. The results suggest that, with proper calibration, FBG sensors can effectively measure both temperature and strain, making them suitable for high-stress, high-temperature situations. The positive findings also open up possibilities for future studies, which could involve more complex conditions, such as working in a radiative environment.

### 5.1. Thermal Test Results

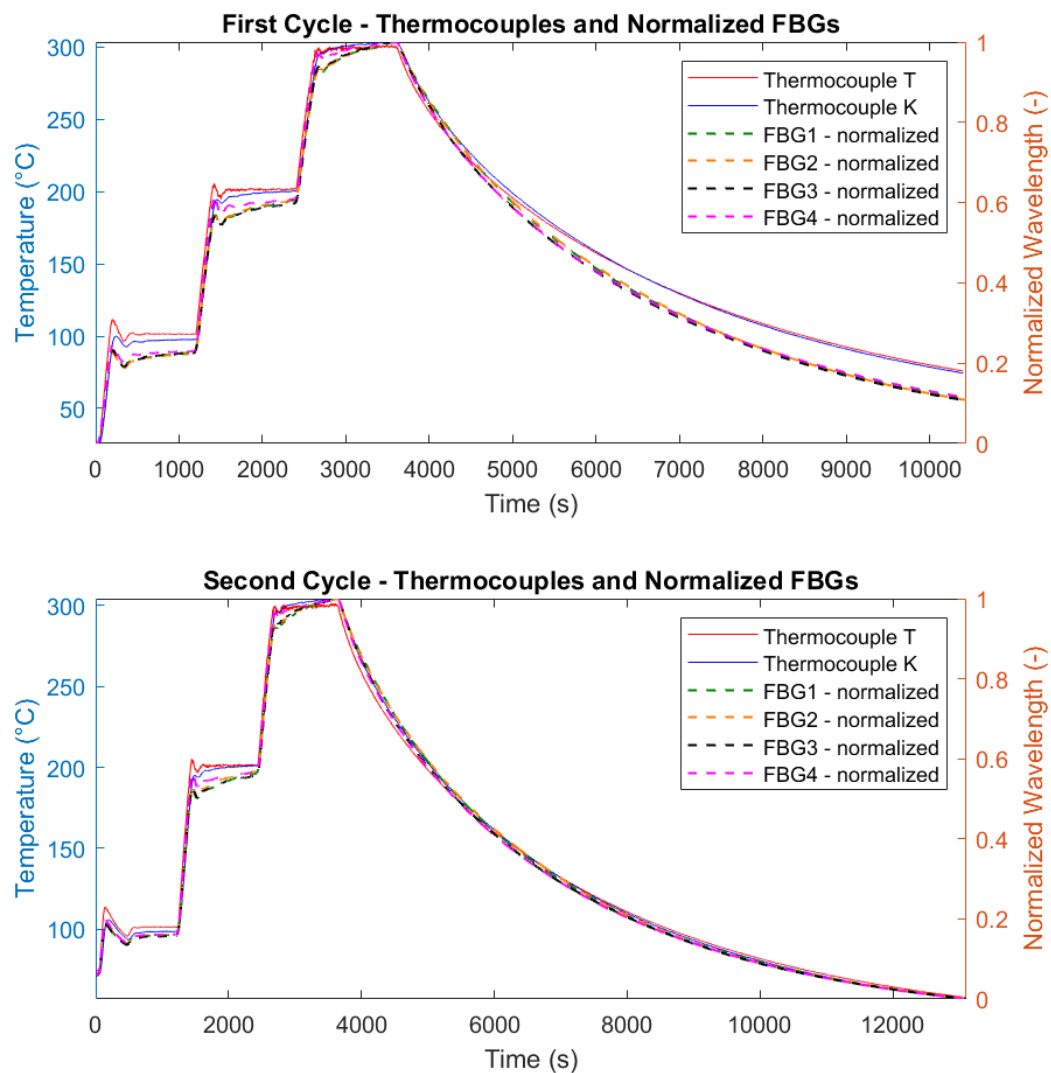
Two stepwise thermal tests were performed, according to Figure 17, to understand the correlation between the Bragg wavelength shifts and temperature variations. The temperature-induced shift in the Bragg wavelength ( $\lambda_B$ ) is described by Equation (1), where both  $n_{\text{eff}}$  and  $\Lambda$  are affected by temperature through thermal expansion and the thermo-optic effect. The simplified relationship between the wavelength shift ( $\Delta\lambda_B$ ) and temperature variations ( $\Delta T$ ) is expressed as:

$$\Delta\lambda_B = K_T \Delta T, \quad (5)$$

where  $K_T$  is the temperature sensitivity coefficient determined through calibration. To standardize the analysis, the wavelength data from the FBGs was normalized and compared to the temperature



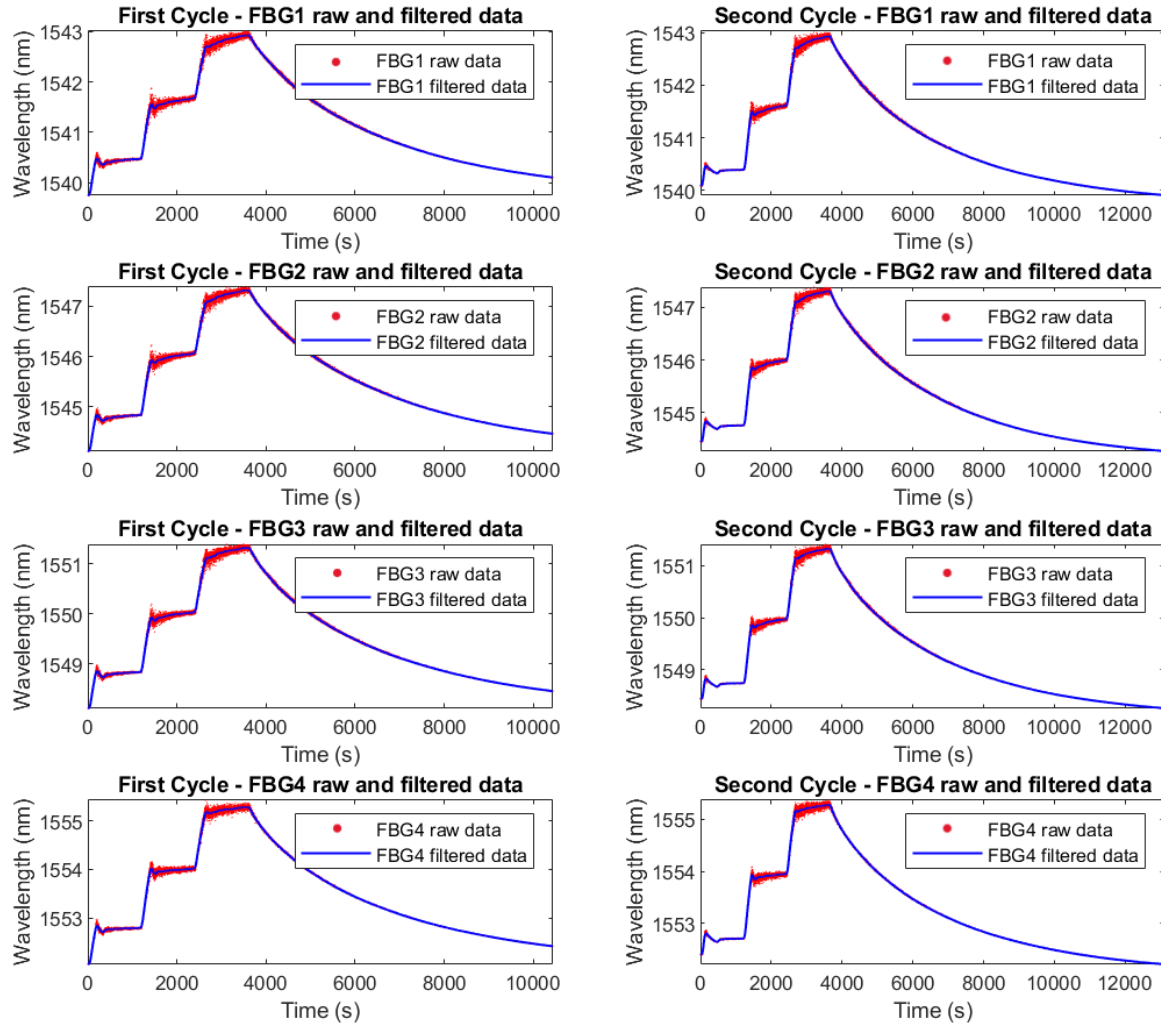
readings from the thermocouples. The results of Figure 17 demonstrated a consistent linear correlation between temperature changes and wavelength shifts.



**Figure 17.** Normalized correlation between temperature changes (solid lines) and wavelength shifts (dashed lines) for the two thermal cycles.

It is important to highlight the influence of the chamber's fan on the FBG measurements. Specifically, during the cooling phase of the first test shown in Figure 17, when the fan was active, a small drift in the FBG wavelengths occurred relative to the temperature readings. In contrast, during the second test, when the fan was turned off, the alignment between the FBG wavelengths and temperature measurements was nearly perfect.

For the experiments, raw wavelength data from the FBGs were processed using a Moving Average Filter (MAF) to reduce noise and enhance data clarity. The MAF was implemented in MATLAB (version 2023a), with a window size of 150 data points used to calculate the smoothed values. Figure 18 illustrates the comparison between raw and filtered data for two thermal cycles.



**Figure 18.** Comparison of raw (red) and filtered (blue) FBG data for the first and second thermal cycles.

#### 5.1.1. Linear Calibration

The scope of this linear calibration is to establish a precise and reliable relationship between temperature and Bragg wavelength shifts, enabling accurate temperature measurements in high-temperature environments. This approach is based on the assumption that the relationship between the Bragg wavelength shift ( $\Delta\lambda_B$ ) and the corresponding temperature change ( $\Delta T$ ) is linear and can be accurately described by Equation (5). Therefore, the aim of the linear calibration is also to determine the temperature sensitivity coefficient  $K_T$ . To validate this assumption and determine  $K_T$ , a controlled thermal environment was established where the FBG sensors and a T-type thermocouple were positioned in close proximity to ensure uniform thermal exposure and minimize spatial temperature gradients. Temperature was increased following the described stepwise thermal cycle (heating phases followed by stabilization phases) up to 300°C, with the thermocouple providing precise reference measurements while the FBG sensors concurrently recorded the corresponding Bragg wavelength shifts,  $\Delta\lambda_B$ . To ensure high measurement accuracy, the T-type thermocouple was selected due to its superior stability and proximity to the FBG sensors during testing, effectively minimizing discrepancies arising from spatial temperature gradients. As depicted in Figure 13, the tip of the T-type thermocouple was positioned only a few millimeters away from the FBGs, whereas the K-type thermocouple was located several centimeters away, leading to potential deviations in recorded temperature values.

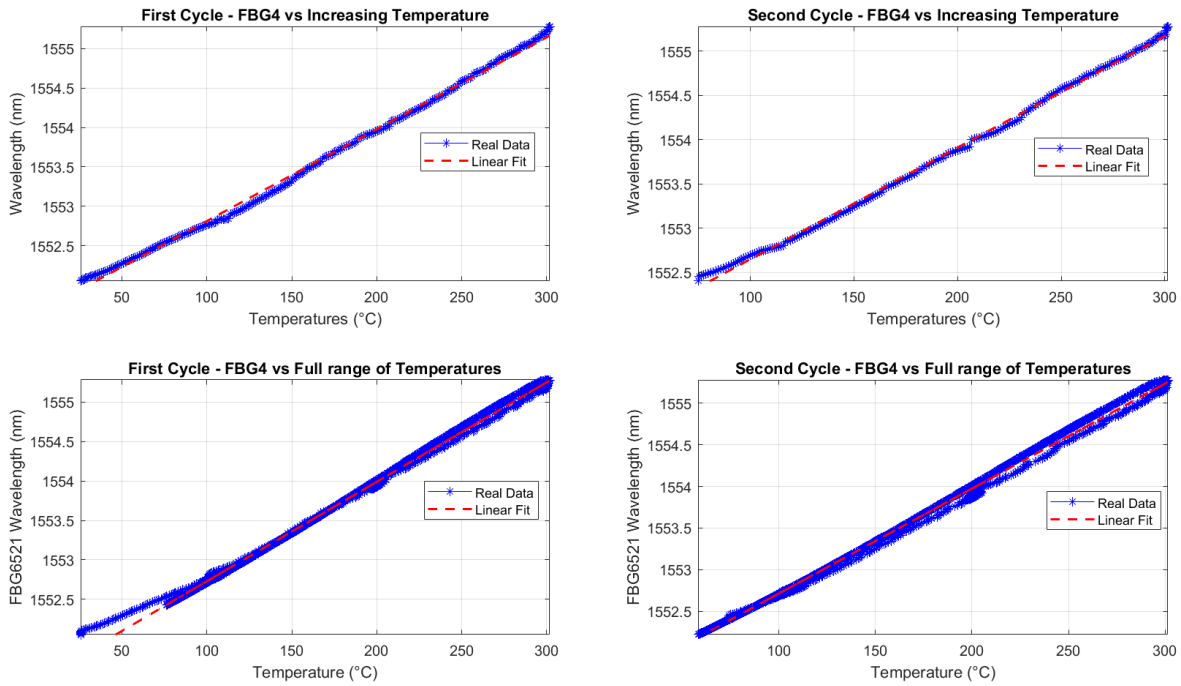
The calibration procedure consisted of plotting the measured wavelength shifts against the temperature variations and performing a linear regression analysis, where the slope of the best-fit line directly provided the value of  $K_T$ . The validity of the linear model was confirmed by a high coefficient of determination ( $R^2 \approx 1$ ), as illustrated in Figure 19. The precision of the fit was further substantiated

by the narrow 95% confidence intervals, as shown in Figure 20, which underscore the reliability of the linear fit, even when extrapolated to higher temperature ranges. The temperature sensitivity coefficients  $K_T$  were determined using temperature readings from the reference thermocouple. Therefore, the wavelength shift of each FBG was correlated with the temperature measured by the T-type thermocouple. This approach eliminates potential biases from the interrogator’s internal calibration, providing a direct sensitivity assessment based on the actual thermal conditions experienced by the sensors. However, this assessment does not account for potential measurement and calibration uncertainties associated with the T-type thermocouple, as these values are not known.

The temperature sensitivities of each FBG, for both First and Second Cycles, are highlighted in Table 2. These sensitivity values are in line with studies and tests for temperature monitoring through FBGs [10,48,51–53,55].

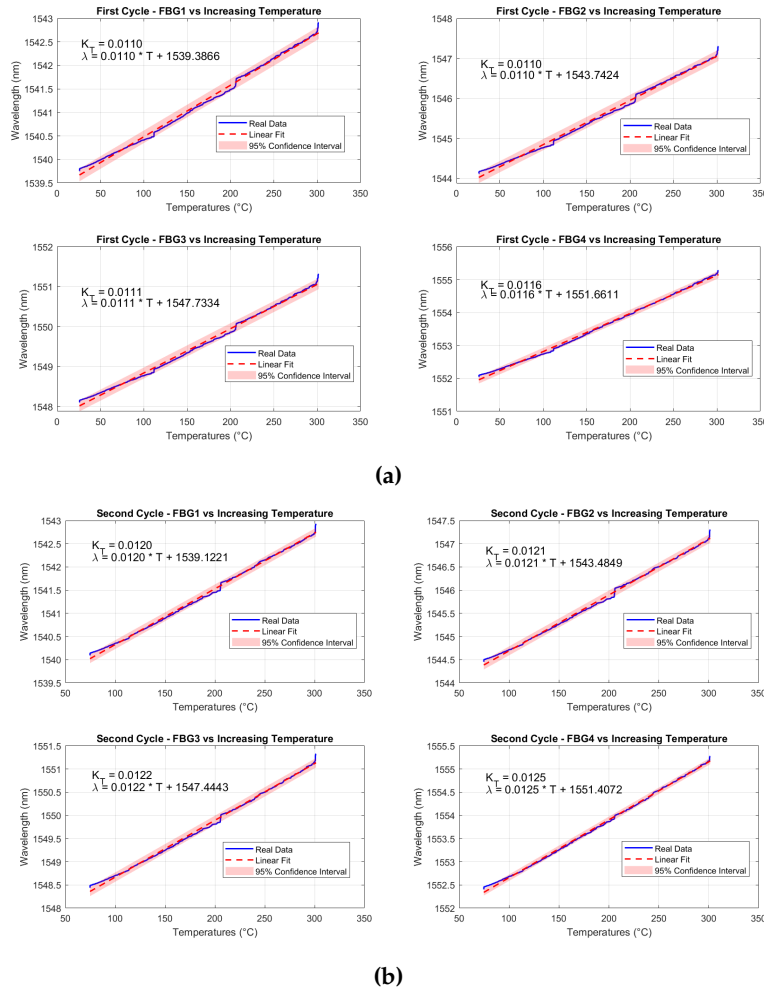
**Table 2.** Temperature sensitivity coefficients  $K_T$  for each FBG sensor.

FBG’s ID	First Cycle $K_T$ (pm/°C)	Second Cycle $K_T$ (pm/°C)
FBG1	12.33	12.37
FBG2	12.43	12.48
FBG3	12.51	12.56
FBG4	12.62	12.61



**Figure 19.** Linear correlation between temperature and wavelength shift for FBG4 during thermal cycles.

Additionally, the use of fs-FBGs, which are known for their enhanced thermal durability, ensured a stable and predictable relationship between temperature and wavelength shifts across the operational range. It is important to note that while the linear calibration remains valid up to approximately 350–400°C, beyond this range, the sensor response may exhibit non-linearity, necessitating the adoption of polynomial regression models to accurately characterize the temperature dependence.



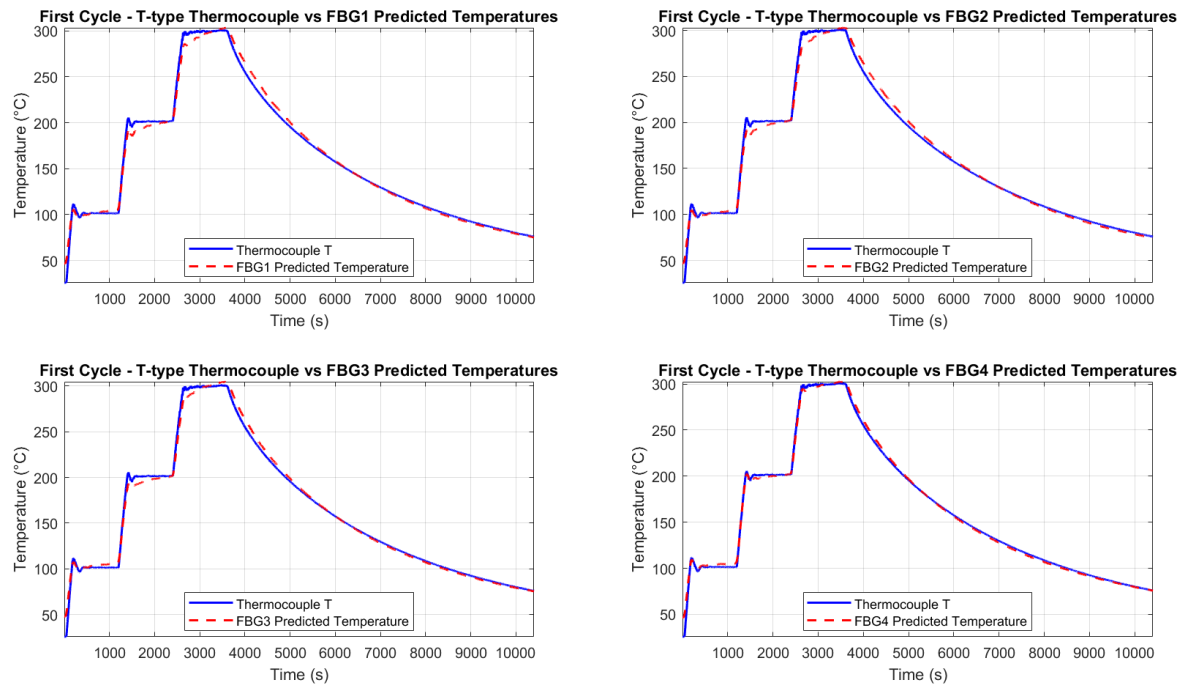
**Figure 20.** Linear fit and 95% confidence interval for: (a) First Cycle. (b) Second Cycle.

### 5.1.2. Temperature Estimation Through FBG Sensors

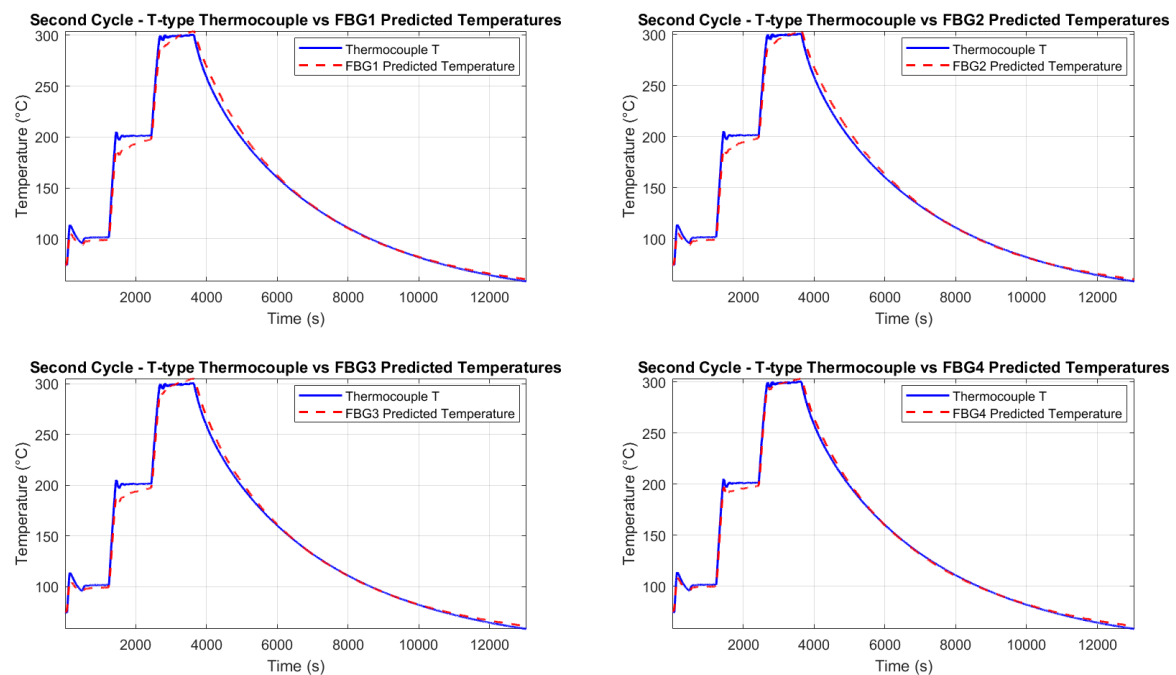
Using the calibrated temperature sensitivity coefficient ( $K_T$ ), FBG sensors can predict temperature values based on the measured wavelength shifts. The predicted temperature is:

$$\Delta T_{\text{predicted}} = \frac{\Delta \lambda_B}{K_T}. \quad (6)$$

Throughout the thermal tests, the predicted temperatures were computed for all FBGs and compared against the reference T-type thermocouple measurements. Figures 21 and 22 show the good agreement between predicted and measured temperatures for both thermal cycles, highlighting the accuracy of the calibration process.



**Figure 21.** Comparison between predicted temperatures (red dashed line) of the 4 FBGs and measured temperatures (blue solid line) from T-type thermocouple, for the first cycle.



**Figure 22.** Comparison between predicted temperatures (red dashed line) of the 4 FBGs and measured temperatures (blue solid line) from T-type thermocouple, for the second cycle.

The alignment with thermocouple measurements confirms the calibration process and the FBG's precision in detecting temperature-induced wavelength shifts. Minor discrepancies in some sections may be attributed to the setup, where the thermocouples and FBGs were not perfectly co-located, and to small vibrations of the fibers caused by the thermal chamber's fan.

## 5.2. Thermal-Structural Test Results

The thermal-structural test evaluated the performance of fs-FBG sensors, in measuring strain and displacement, under combined thermal and mechanical loads, simulating nuclear reactor conditions.



Specimens, made of AISI 316L(N) stainless steel, were subjected to cyclic mechanical stress at room and elevated temperatures (250–300°C) using forces from 1 kN to 5 kN. The tests, performed in the Instron chamber, assessed the sensors' ability to withstand dynamic stresses, vibrations, and thermal expansion. Resin adhesion was crucial for sensor stability, and displacement data of the specimen were recorded to analyze deformation.

Two main test phases, as described in Section 4.2, were conducted: room temperature cycling (3,000 cycles at 5 Hz) and elevated temperature cycling (alternating between gradual heating, 800 cycles at 1 Hz, and constant temperature, 3,000 cycles at 5 Hz). Specimen 1, equipped with an optical fiber, was subjected to both thermal and mechanical cycling, while Specimen 2, used for thermal measurements, served as a reference with K-type and T-type thermocouples. In the first test phase, FBG4 was used for the mechanical tests and was bonded to Specimen 1. In the second test phase, FBG1 replaced FBG4 for the mechanical tests on Specimen 1. Throughout both test phases, FBG2 served as the thermal reference sensor and was bonded to Specimen 2.

### 5.2.1. Correlation Between Wavelength and Displacement

The relationship between the FBG wavelength shift ( $\Delta\lambda_B$ ) and displacement is governed by strain ( $\Delta\epsilon$ ) and temperature ( $\Delta T$ ). For purely mechanical effects, the wavelength shift is expressed as:

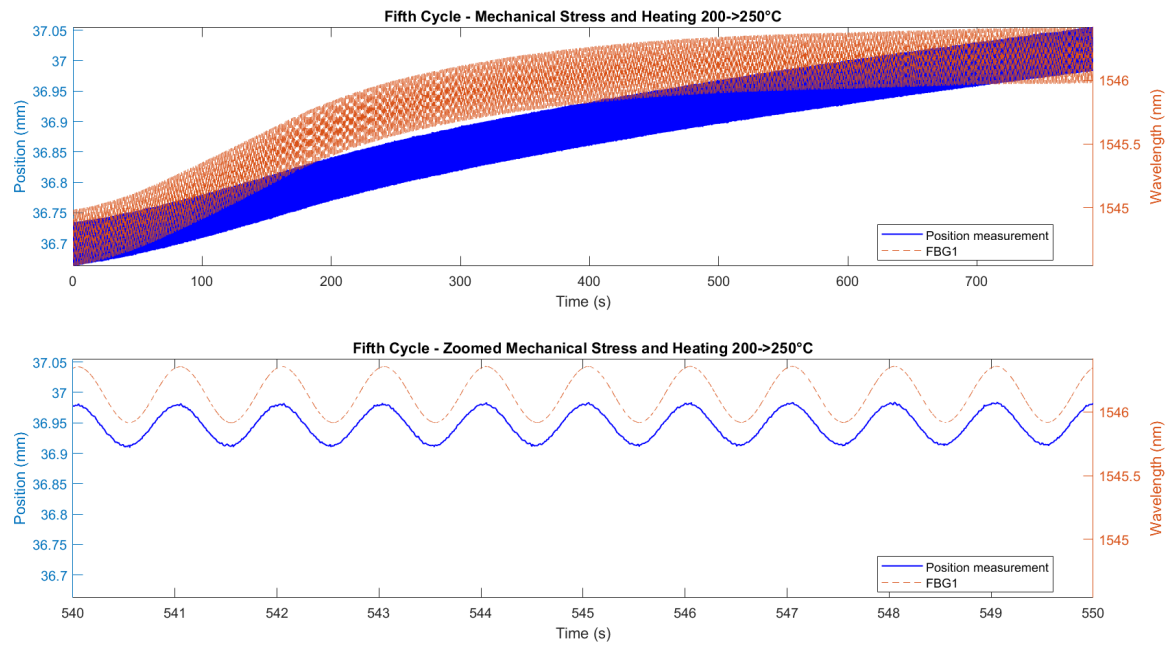
$$\Delta\lambda_B = K_\epsilon \Delta\epsilon, \quad (7)$$

where  $K_\epsilon$  is the strain sensitivity coefficient. Under combined thermal and mechanical conditions, the total shift includes both strain and temperature contributions:

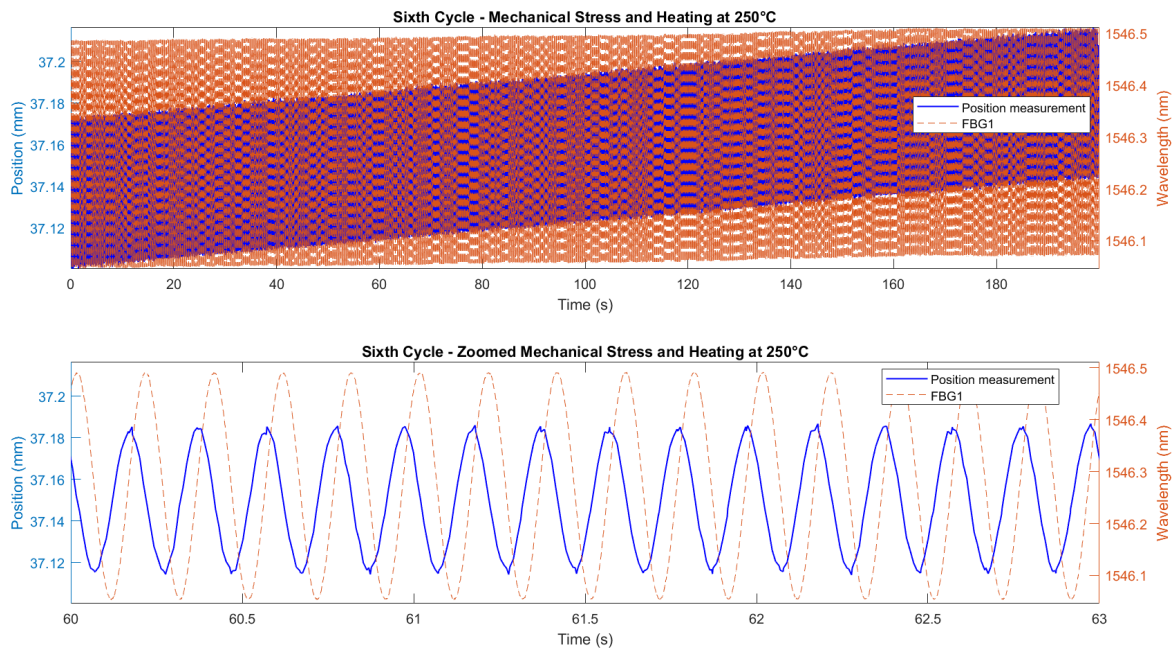
$$\Delta\lambda_B = K_T \Delta T + K_\epsilon \Delta\epsilon, \quad (8)$$

where  $K_T$  is the temperature sensitivity coefficient. The terms  $K_T \Delta T$  and  $K_\epsilon \Delta\epsilon$  represent the respective contributions of temperature and strain, both of which must be considered to ensure accurate displacement measurements.

Figures 23 and 24 demonstrate the correlation between the wavelength shifts of FBG1 and the position measured by the Instron chamber. In the fifth cycle (Figure 23), the temperature increased from 200°C to 250°C under cyclic loading at 1 Hz, while the sixth cycle (Figure 24) maintained a constant temperature of 250°C with cyclic loading at 5 Hz. A minor delay (20–30 ms) between the FBG and Instron measurements was observed, attributed to the resin's mechanical response.



**Figure 23.** Correlation between wavelength from FBG1 and displacement during the fifth cycle (200°C to 250°C) of the second test (1 Hz). A zoomed interval highlights the relationship.



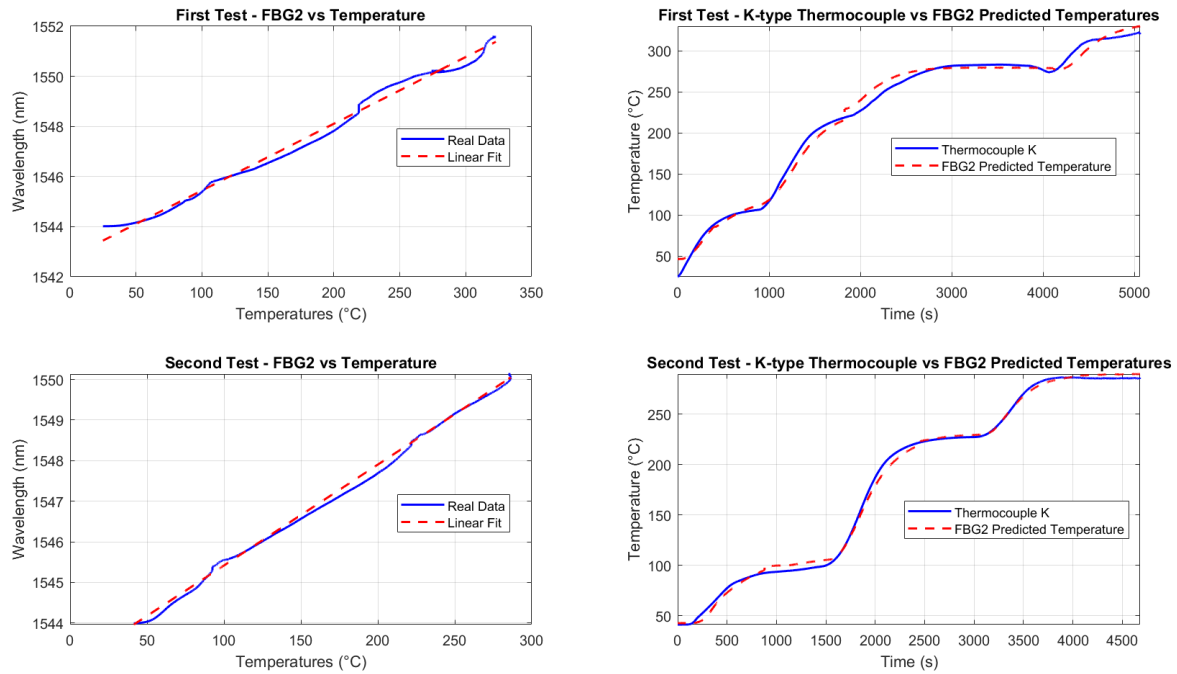
**Figure 24.** Correlation between wavelength from FBG1 and displacement during the sixth cycle (constant temperature at 250°C) of the second test (5 Hz). A zoomed interval highlights the relationship.

### 5.2.2. Temperature-Effect Compensation

To isolate strain-induced wavelength shifts from temperature effects, a second FBG (FBG2) was used as a reference sensor, sensitive only to temperature changes. Positioned on a non-loaded specimen, FBG2 was calibrated using the same procedure followed during the thermal test, with the results shown in Figure 25. The temperature-induced wavelength shift ( $\Delta\lambda_T$ ) measured by FBG2 was used to eliminate the temperature effect from the total wavelength shift of the primary FBG, isolating the strain contribution ( $\Delta\lambda_\epsilon$ ):

$$\Delta\lambda_\epsilon = \Delta\lambda_B - \Delta\lambda_T. \quad (9)$$

This compensation method ensured accurate displacement measurements, independent of thermal variations. Despite minor time delays and damping effects probably introduced by the resin, the deviation between the temperature estimated by the FBGs and the reference thermocouple measurements remained within acceptable limits, validating the robustness of this approach.



**Figure 25.** Left: Correlation between temperature and wavelength shifts of FBG2. Right: Predicted temperatures from FBG2 for both tests.

### 5.2.3. Displacement Estimation Through FBG Sensors

The estimation of displacement using FBGs involves determining the displacement sensitivity coefficient ( $K_L$ ), which relates the strain-induced wavelength shift ( $\Delta\lambda_L$ ) to displacement variations ( $\Delta L$ ), as defined by:

$$K_L = \frac{\Delta\lambda_B - \Delta\lambda_T}{\Delta L}. \quad (10)$$

Here,  $\Delta\lambda_B$  is the total wavelength shift measured by the FBG, and  $\Delta\lambda_T = K_T\Delta T$  represents the thermal contribution, subtracted to isolate the strain-induced shift. The change in notation from  $K_\epsilon$  (strain sensitivity coefficient) to  $K_L$  (displacement sensitivity coefficient) was made to clearly differentiate between strain and displacement sensitivity:  $K_L$  connects the wavelength shift ( $\Delta\lambda_L$ ) directly to the specimen's displacement ( $\Delta L$ ). Once  $K_L$  is determined, displacement variations ( $\Delta L_{\text{predicted}}$ ) are calculated using:

$$\Delta L_{\text{predicted}} = \frac{\Delta\lambda_B - \Delta\lambda_{T,\text{predicted}}}{K_L}, \quad (11)$$

where  $\Delta\lambda_{T,\text{predicted}} = K_T\Delta T_{\text{predicted}}$  is the predicted thermal contribution derived from the reference sensor (FBG2). The accuracy of  $\Delta T_{\text{predicted}}$  depends on the calibration of FBG2, ensuring reliable temperature compensation.

Since no additional stress/strain sensors (e.g., strain gauges) were available on the specimen, comparing the FBG measurements directly to the displacement values measured by the Instron crosshead, rather than stress or strain values, was considered more appropriate. This approach eliminates the risk of introducing additional error through the need to derive stress or strain analytically. The Instron crosshead displacement provided a direct and reliable measurement, ensuring that the FBG-derived displacement values were compared to an accurate reference. The results, shown in

Table 3. Displacement sensitivity coefficients  $K_L$  for each Test’s cycle.

Cycle	First Test	Second Test
	FBG4 $K_L$ (nm/mm)	FBG1 $K_L$ (nm/mm)
1	2.026	3.254
2	2.392	3.415
3	2.55	3.585
4	2.64	3.954
5	2.821	2.790
6	2.36	2.366

Figure 26, demonstrate a good initial agreement between the predicted and measured displacements for all six test cycles.

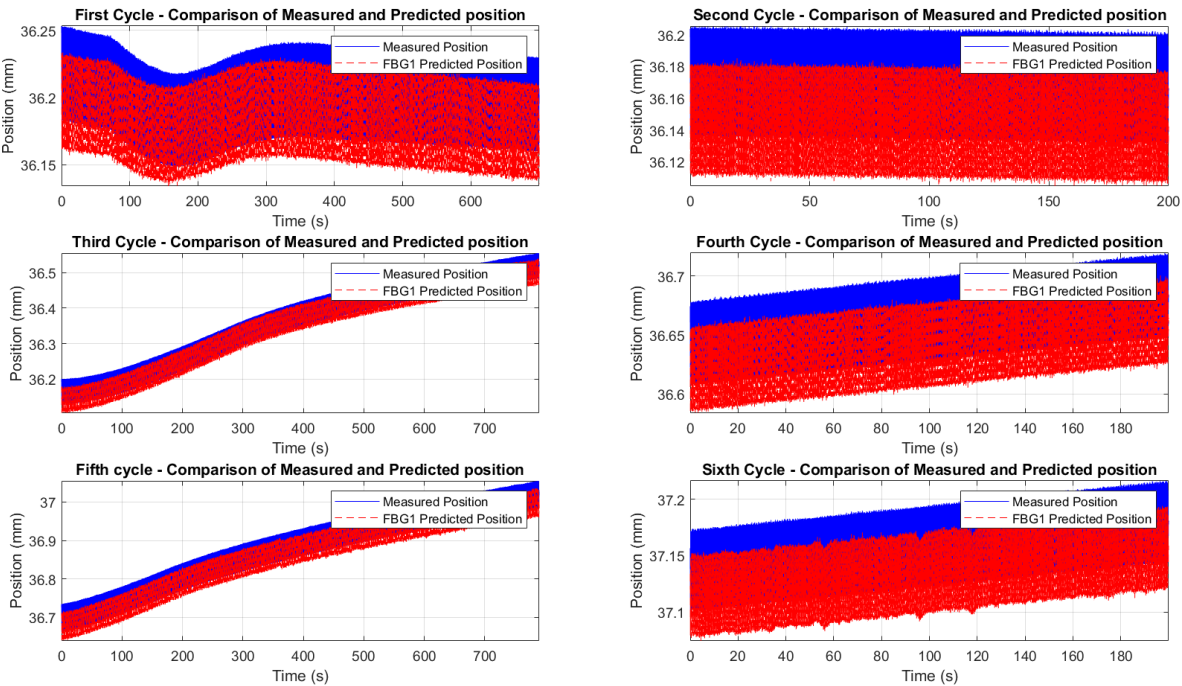
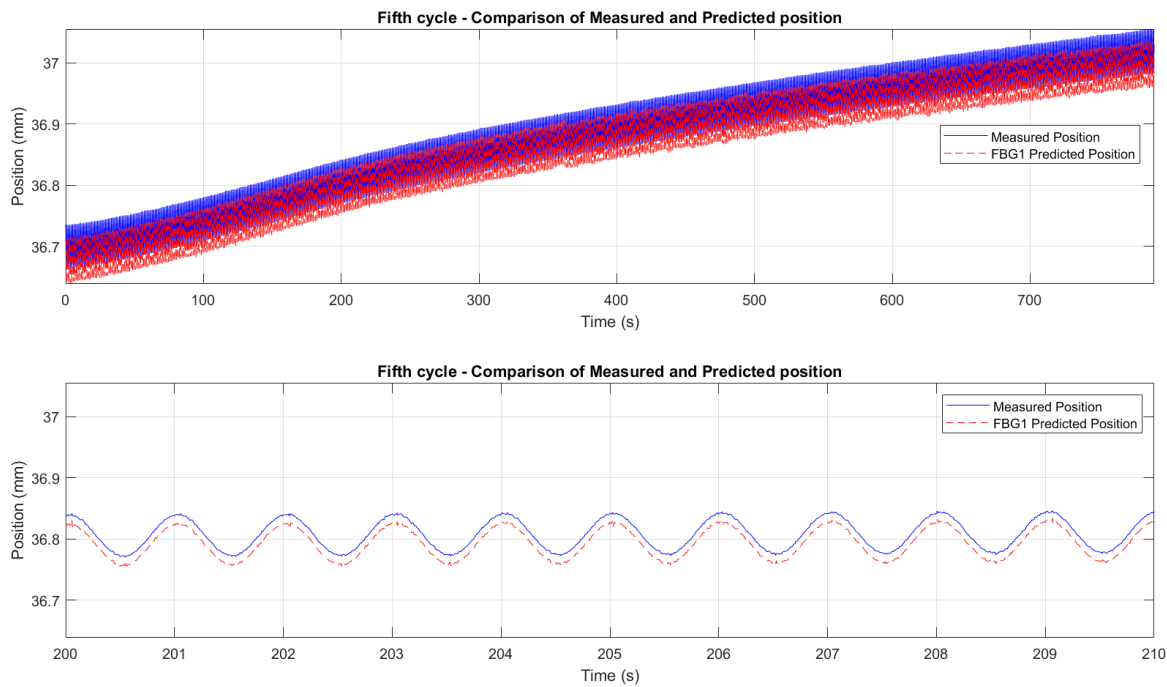


Figure 26. Comparison between measured displacement (blue solid line) and predicted displacement (red dashed line) during the second thermo-mechanical test for all six cycles.

To refine the analysis of the wavelength-to-displacement correlation, Figures 27 and 28 provides zoomed comparisons of the predicted displacement values with measured displacements for the fifth and sixth cycles. These detailed views highlight the accuracy of the prediction process, showcasing how the wavelength shifts were accurately converted into displacement measurements. The displacement sensitivity coefficients were determined using displacement readings from the Instron crosshead. The wavelength shift of each FBG was correlated with the displacement measured by the crosshead. This approach eliminates potential biases from the interrogator’s internal calibration, providing a direct sensitivity assessment based on the actual mechanical conditions experienced by the sensors. The determined values of the displacement sensitivity are highlighted in Table 3, for FBG4 and FBG1 during the First Test and the Second Test, respectively. The obtained sensitivity values are consistent with those reported in studies and tests for displacement estimation using FBGs [59,70,71]. Small  $K_L$  variations across cycles are typical due to factors like misalignments, adhesive behavior, and temperature fluctuations. The resin’s adhesive properties and potential hysteresis may have affected strain transfer, but the overall trends and sensitivity values remain consistent.

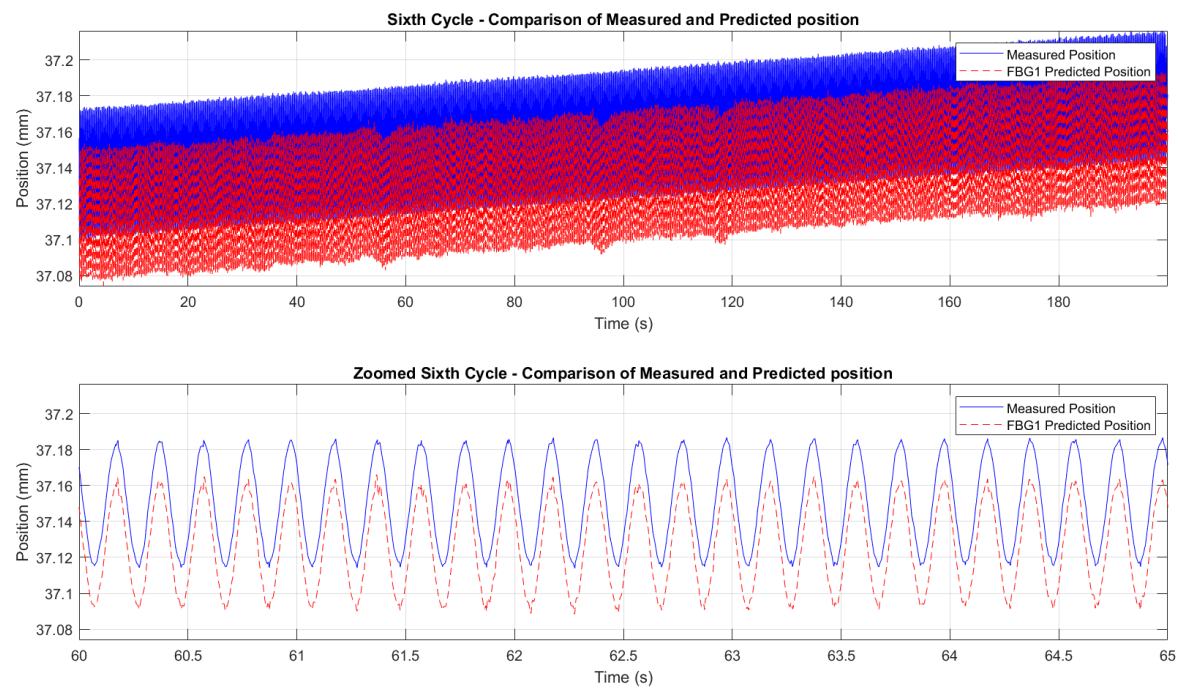
The methodology effectively isolates the strain contribution, leveraging the reference sensor (FBG2) to compensate for temperature-induced shifts. These promising outcomes highlight the

potential of FBGs as displacement sensors, with room for optimization to achieve even greater accuracy. Results from all of the six cycles also highlighted the importance of selecting a resin capable of withstanding high temperatures to ensure no loss of critical information and to maintain perfect adherence of the optical fiber to the specimen. In our case, when the tension cycles peak at 5 kN, they generate a maximum stress of 80 MPa, exceeding the tensile strength of the resin (54 MPa). This induces a plastic hysteresis behaviour of the resin itself, shifting the resin's behavior from elastic to plastic. This can introduce minor hysteresis in the results, such as the mentioned delay of 30 ms. This effect, though minimal, underscores the need for careful selection of materials that can sustain high mechanical loads without compromising the accuracy of the measurement. A better choice of resin, combined with a better resin application, could lead to even better performances.



**Figure 27.** Zoomed comparison between predicted displacements (red dashed line) of FBG1 and measured displacement (blue solid line) from Instron chamber, for the fifth cycle of the second test.





**Figure 28.** Zoomed comparison between predicted displacements (red dashed line) of FBG1 and measured displacement (blue solid line) from Instron chamber, for the sixth cycle of the second test.

6. Precision Evaluation

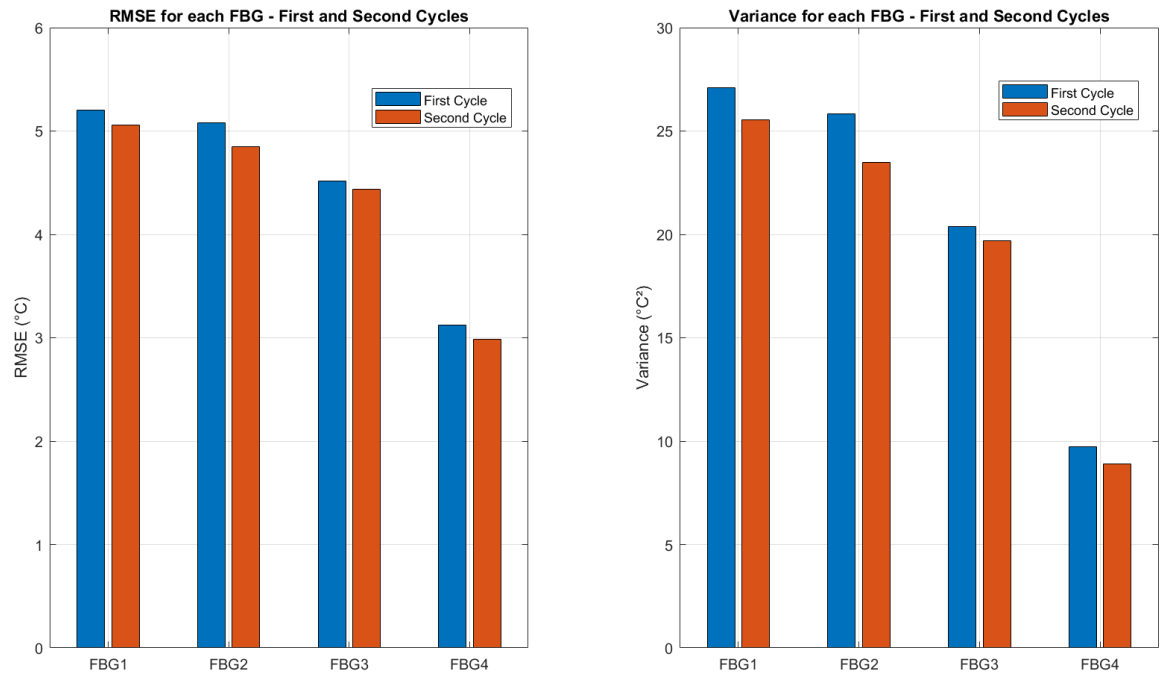
6.1. Error Analysis in FBG-Based Temperature Estimation

The precision of temperature estimation using FBG sensors was evaluated through statistical metrics, including the coefficient of determination ( $R^2$ ) and Root Mean Square Error (RMSE). Table 4 presents these metrics for all FBGs across the two thermal cycles. The high  $R^2$  values ( $> 0.99$ ) and low RMSE values confirm the robustness of the linear calibration and the reliability of the FBG sensors for temperature sensing.

**Table 4.** Error metrics for FBGs in the thermal test.

Sensor	First Cycle		Second Cycle	
	$R^2$	RMSE (°C)	$R^2$	RMSE (°C)
FBG1	0.9946	5.20	0.9946	5.06
FBG2	0.9948	5.08	0.9948	4.85
FBG3	0.9959	4.52	0.9959	4.44
FBG4	0.9981	3.12	0.9981	2.98

Histograms of the RMSE and variance for both cycles, shown in Figure 29, further illustrate the minimal discrepancies across the temperature range. These results confirm that the FBGs, when properly calibrated, are highly precise temperature sensors, even under varying thermal conditions.



**Figure 29.** Histograms of RMSE and variance for the thermal test (first and second cycles).

Precision metrics, such as RMSE, were under 5°C in the 25–300°C range (corresponding to 1,82%) and could be further reduced with an improved testing setup. These results are encouraging for a preliminary trial, showing strong potential for future applications. With additional tests and refined setups, significant improvements in accuracy and reliability can be achieved.

6.2. Error Analysis in FBG-Based Displacement Estimation

The displacement estimation was evaluated by analyzing random errors from both temperature compensation and predicted displacement. The RMSE was used as the primary metric due to its reliability in cycles with minimal temperature variance. Table 5 shows the thermal compensation performance of FBG2 (used as temperature sensor) during the two mechanical tests, compared to the K-type thermocouple readings. Slightly higher errors were observed, likely due to the influence of the resin and the thermal inertia of the specimen.

**Table 5.** Thermal compensation performance of FBG2.

Test	RMSE (°C)	R <sup>2</sup>
First Test	7.28	0.992
Second Test	4.03	0.998

Cycle-specific errors for temperature compensation are detailed in Table 6. Cycles with rapid thermal changes exhibited higher RMSE values, while those with stable conditions showed minimal errors, validating the calibration process under diverse conditions.

**Table 6.** Cycle-specific thermal errors for FBG2.

Cycle	First Cycle - RMSE (°C)	Second Cycle - RMSE (°C)
1	6.35	10.09
2	11.30	5.91
3	9.79	14.29
4	1.40	2.07
5	0.73	5.76
6	1.92	3.98

Finally, Table 7 presents the RMSE values for displacement prediction across both tests. Displacement errors remained consistently low ( $< 0.02$  mm), even during cycles with rapid thermal transitions or high loading frequencies, confirming the reliability of the FBG sensors.

**Table 7.** Position error RMSE evaluation for FBG1 and FBG4 in first and second tests.

Cycle	First Test - FBG4	Second Test - FBG1
	RMSE (mm)	RMSE (mm)
1	0.0117	0.0164
2	0.0076	0.0239
3	0.01525	0.0141
4	0.01605	0.0219
5	0.0112	0.0180
6	0.0125	0.0234

Despite minor errors introduced probably by the resin or residual temperature effects, the results confirm the robustness of FBG sensors for high-precision displacement monitoring under combined thermal and mechanical conditions. The consistent low RMSE values and effective temperature compensation validate the sensors’ accuracy and reliability in complex environments.

7. Conclusions

This study offers a first look at the potential of FBG-based sensors for monitoring key parameters in Generation IV Lead-cooled Fast Reactors. Through early-stage testing and theoretical analysis, the research shows that FBGs are promising candidates for environments with high temperatures and mechanical stress. While further testing, especially in radiative conditions, is needed to fully validate the technology, this work provides a solid starting point for developing durable, integrated fiber optic sensor systems for advanced nuclear reactors.

The analysis of temperature estimation reveals that while the sensors exhibit robust performance, with RMSE values under 5°C, further testing in more controlled environments, using improved setups and more precise equipment, could significantly reduce errors. As seen in the results, factors like fan-induced vibrations, resin properties and thermal inertia of the specimens contribute to some of the discrepancies observed. With a refined experimental setup, accuracy could be enhanced, making FBGs even more reliable. Displacement monitoring also showed encouraging results, with minimal errors (RMSE around 0.015 mm) in cycles with stable thermal conditions. However, the sensors’ performance was slightly affected during rapid thermal changes, likely due to the resin’s influence. These issues could be mitigated with optimized calibration processes, better material choices, and improved sensor integration techniques, ensuring more consistent performance across diverse conditions.

Future research should focus on improving high-temperature resin materials, exploring FBG performance under both radiation and thermal cycling, and carrying out more testing in complex reactor environments. It would be also useful to assess long-term operating temperatures and perform extended cycling evaluations. These steps are crucial for making real-time monitoring and automated diagnostics a reality. Overall, this study highlights how fiber optic sensors have the potential to transform reactor monitoring, improving safety, reliability, and efficiency in the process. Focusing on durability and ease of integration for these sensors represents an important step toward enabling future advancements in nuclear reactor monitoring systems.

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