

1 Article

## 2 Application-specific oxide-based and metal-dielectric 3 thin film materials prepared by RF magnetron 4 sputtering

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10 **Abstract:** We report on the development of several different thin-film functional material systems  
11 prepared by RF magnetron sputtering at Edith Cowan University nanofabrication labs. We conduct  
12 research on the design, prototyping, and practical fabrication of high-performance magneto-optic  
13 (MO) materials, oxide based sensor components, and heat regulation coatings for advanced  
14 construction and solar windows.

15 **Keywords:** thin films; coatings; magneto-optics; sensors; glass; heat regulation.

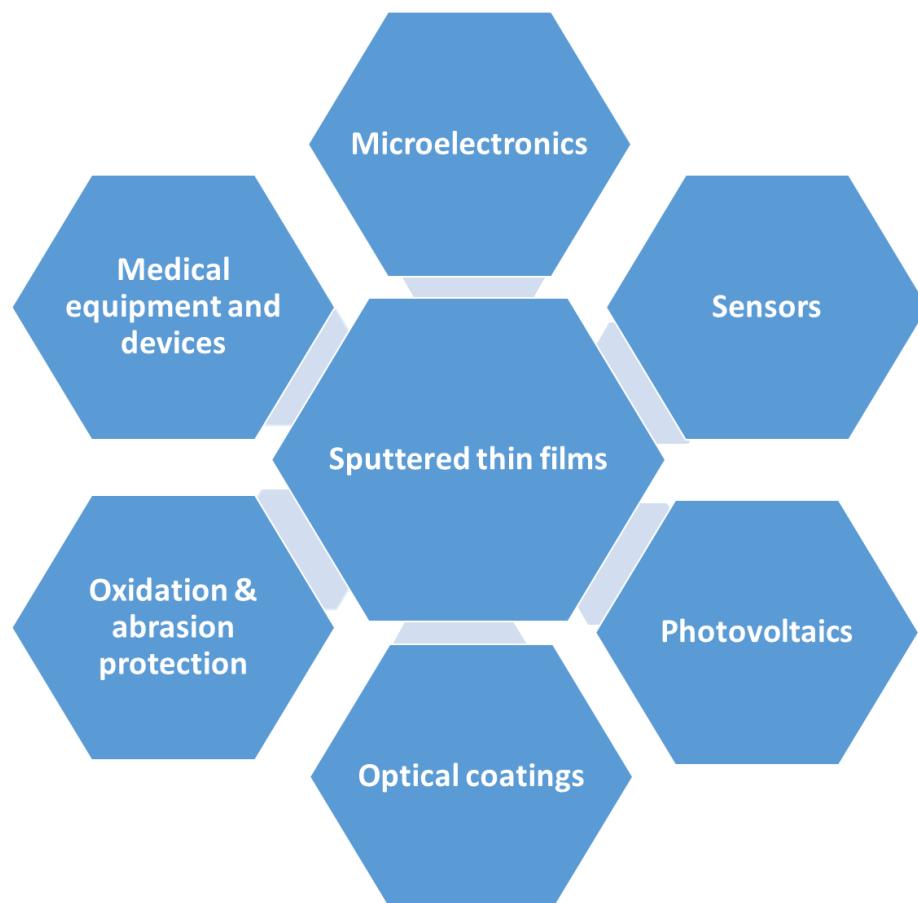
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### 17 1. Introduction

18 Among all the physical vapor deposition techniques, magnetron sputter deposition is one of the  
19 most common technologies used to grow thin film materials and coatings for various existing and  
20 modern nano-technological applications. Sputter deposition of thin films has a long track record of  
21 development history in vacuum technology since 1800s [1-10]. Many dedicated research groups and  
22 scholars were involved in the development of the modern phase of magnetron sputtering technology,  
23 although the journey of the magnetron sputtering process is still considered far from its ultimate  
24 development [6, 8]. However, nowadays the magnetron sputtering is considered one of the most  
25 effective processes for the deposition of a wide range of high-quality thin-film materials either in  
26 single or multilayer form, including metals, dielectrics, metal oxides of complex stoichiometry, and  
27 nanoparticles. A vast number of sputtered material types were shown to be suitable for various  
28 existing and emerging nanotechnology-related applications, and attractive for many rapidly growing  
29 diverse market sectors. Sputtering processes allow to deposit thin-film materials either on bare  
30 substrates or on top of any structured systems, e.g. photonic or magneto-photonic crystals, usually  
31 without having any unpredictable thickness uniformity or stoichiometry issues with the grown films.  
32 Thin-film materials, especially radio frequency (RF) magnetron sputtered thin films were originally  
33 considered useful mainly in electronics and semiconductor devices, however, sputtered thin films  
34 have also been found to be applicable within a wide range of fields such as optoelectronics, energy,  
35 mechanical/chemical, optical coatings, life sciences, and others [9-29]. In this nano-technological era,  
36 the sputter-deposition of thin films becomes a rather ubiquitous and actively growing field of human  
37 endeavour, integrating the fundamental and important scientific areas of research, process  
38 development, deposition-system design, and new product manufacturing. This trend is expected to  
39 continue into the periods extending far into the foreseeable future. The reasons behind the rapid  
40 growth of the sputtering industry over other thin film manufacture techniques include (i) possibility  
41 of using large-area sputtering targets that provide uniform film thickness over large-area substrates;  
42 (ii) flexibility of growing thin or extremely ultra-thin film materials of various composition types  
43 (even complex stoichiometry types, e.g. oxide-mix-based iron garnet precursors) on different  
44 substrate types; (iii) ease of controlling the film thickness by calibrating the deposition run times and

45 other parameters; (iv) better layer-to-substrate adhesion quality, compared to techniques such as  
46 thermal evaporation. Also, the successful establishment of deposition technologies for thin polymer  
47 films and metal/plasma polymer nano-particles fabrication using polymer or metal-polymer  
48 composite targets in RF magnetron sputtering systems by optimizing the process gas chemistries (e.g.  
49 argon, nitrogen), shows the diversity of thin-film types grown by RF magnetron sputtering [30-33].  
50 Figure 1 presents a wide range of possible application areas of sputtered thin films for the continued  
51 exploration by future generations.  
52



53  
54

55 **Figure 1.** Spectrum of modern nano-technological application areas reliant on sputtered thin-film materials.  
56

57 Based on the current and possible future emerging applications, the global market of sputtered  
58 thin films can be subdivided into many segments. According to the report [34] made by PR Newswire  
59 in 2017, the sputtered thin films market volume including sputtering-related equipment, raw  
60 materials, and services, amounts to approximately one-quarter of the total estimated (over US \$70  
61 billion) value of global markets of thin-film technologies in 2016, and is expected to grow at a  
62 significant rate. However, according to the MarketWatch report published in 2018, the thin film  
63 materials market is expected to witness a substantial growth from 2018 to 2024, due to the demand  
64 for miniaturization of thin-film related technologies, devices, and products. In addition, the  
65 increasing number of applications and end-use industry practices are also expected to propel the  
66 growth of the thin-films product markets in the near future [35].  
67

68 In this paper, we discuss the experimental results selected from a decade-long lab-based work,  
69 during which the RF sputtering synthesis of different thin-film material types and multilayer  
70 structures have been explored extensively. We also present and discuss the specific material  
71 development results and functional material properties of interest for several specific applications.  
72 The organization of the article is as follows. Section 2 introduces the background study of Bi-  
73 substituted iron garnet thin-film materials and multilayers together with some very recently obtained

74 optical properties for highly bismuth-substituted iron garnets of composition type  $\text{Bi}_2\text{Dy}_1\text{Fe}_4\text{Ga}_1\text{O}_{12}$  (BiDyIG). These garnet composition types (with bismuth substitution levels above about 1.8) can only  
75 be prepared using physical vapour deposition techniques (e.g. sputtering), and have not been  
76 reported synthesized by crystal growth techniques such as liquid-phase epitaxy. Section 3 describes  
77 the design, fabrication and characterization of ruthenium oxide ( $\text{RuO}_2$ ) thin films grown on rigid and  
78 flexible substrates, for sensor applications. Section 4 describes the fabrication techniques and process  
79 parameters used for growing metal-dielectric nano-composite (MDC) layers and MDC layers  
80 contained within multilayer structures for use in next-generation environment-friendly highly  
81 durable optical coatings for solar and thermal radiation control. The optical properties of these MDC  
82 thin-films and multilayer building blocks containing nanocomposite-type materials are presented in  
83 this section.  
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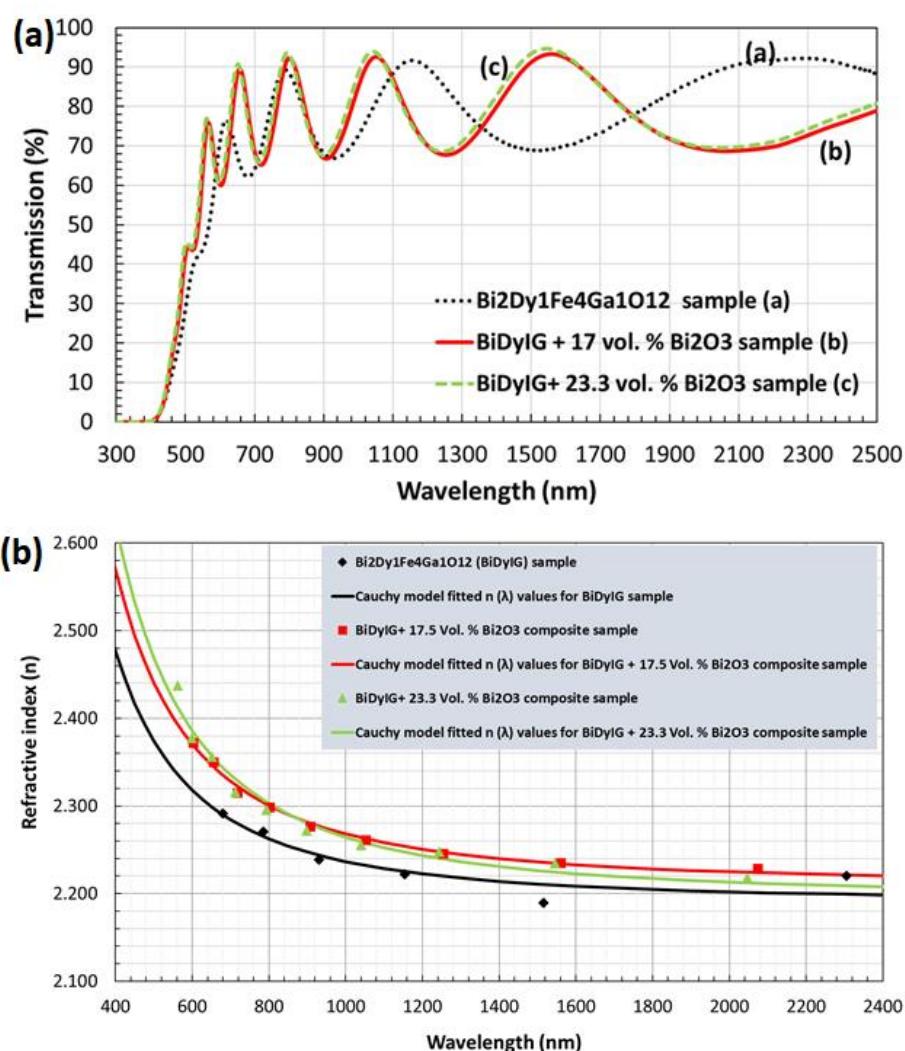
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## 86 **2. Garnets, garnet-oxide composites, and multilayer structures manufactured by sputtering**

87 Natural garnets are popular as gemstones, but when they are engineered either by modifying their  
88 stoichiometry or by adjusting the fabrication process, they can possess extra-ordinary multifunctional  
89 properties that make them attractive for various applications e.g. integrated photonic circuits and  
90 devices. Through nano-engineering, garnet thin films can be controlled, at the atomic level, to attain  
91 naturally-unachievable photonic and magnetic properties that open the way towards the  
92 development of magnetophotonic and magneto-plasmonic crystals (MPCs) for a wide range of  
93 applications, including telecommunication, biomedicine, digital forensics, sensing and data  
94 processing. Thin-film garnets have a long history that started since these were developed in 1960 for  
95 the first time for use in bubble memory device applications [36-55]. The properties of thin garnet films  
96 are always dependent on their fabrication methods, process parameters and especially on the  
97 stoichiometry of the material. By varying the materials compositional constituents together with their  
98 optimized fabrication process parameters in RF magnetron sputtering systems, the magnetic and  
99 magneto-optic properties of garnet thin films can be tailored for specific applications. Multiple  
100 research groups worldwide [56-65] have conducted a significant number of research works using  
101 only RF magnetron sputtering to synthesize, develop and improve many garnet thin-film material  
102 systems. Since the last decade, a number of highly bismuth (Bi) substituted iron garnet thin-film  
103 material systems including garnet-oxide and garnet-garnet nano-composite derivatives, have been  
104 synthesized, their sputtering process parameters optimized, and many studies of the optical,  
105 magnetic and magneto-optical properties were reported by our group at ECU [66-73]. We have  
106 reported obtaining nano-crystalline garnet thin-film materials with high Faraday rotation across the  
107 visible spectral range, a record-high magneto-optic quality, very low coercive force with  
108 perpendicular magnetization and almost in-plane magnetization types. Also, a rather unconventional  
109 magnetic switching properties have recently been demonstrated in all-garnet multilayer thin film  
110 structures. In this section, we present the recently obtained results on the optical constants of RF  
111 sputtered highly Bi-substituted iron-garnet precursors of nominal composition type  $\text{Bi}_2\text{Dy}_1\text{Fe}_4\text{Ga}_1\text{O}_{12}$   
112 (BiDyIG) and garnet-oxide composites (GOC), together with a glimpse of the previously best-  
113 achieved MO properties in thin garnet films of similar compositions. The unconventional hysteresis  
114 loop shapes observed in GOC-based all-garnet multilayer structures are also presented.

115 Figure 2(a) shows the measured transmission spectra of as-deposited  $\text{Bi}_2\text{Dy}_1\text{Fe}_4\text{Ga}_1\text{O}_{12}$  (BiDyIG)  
116 garnet and BiDyIG:  $\text{Bi}_2\text{O}_3$  (17 & 23.3 vol. %) composite thin film layers prepared on glass substrates  
117 by using RF magnetron co-sputtering process. These particular garnet types possessed MO garnet  
118 compositions (and optical properties) of special importance in common application areas, e.g.  
119 Faraday rotators, ferromagnetic resonance-based microwave devices, MPCs, and MO imagers. In the  
120 co-sputtering process, two separate oxide-mix-based ceramic targets ( $\text{Bi}_2\text{Dy}_1\text{Fe}_4\text{Ga}_1\text{O}_{12}$ , and  $\text{Bi}_2\text{O}_3$ )  
121 were used and the materials volumetric fraction ratios were controlled and calculated from their  
122 partial deposition rates. The details of several GOC layer deposition technologies and sputtering  
123 process parameters are described in Refs. [66, 68-70]. From the thickness-dependent transmission-

124 wave interference fringes intensities (measured over a wide range of wavelengths in all samples, Fig  
 125 2a), using a new combinatorial approach, the optical constants of amorphous garnet-precursor layers  
 126 are calculated and refined, together with the film thickness confirmation [73]. This combinatorial  
 127 approach employs a custom-built spectrum-fitting software in conjunction with Swanepoel envelop  
 128 method (SWEM). The following operational steps are conducted for the evaluation of optical  
 129 constants: (i) calculation of the refractive index data and film thickness using the SWEM method[74];  
 130 (ii) use of the calculated index data (from SWEM), in conjunction with least-square fitting to derive  
 131 the real part of index from Cauchy's formula ( $n(\lambda) = a + b/\lambda^2$ ); (iii) use of the refractive index data  
 132 (derived from Cauchy's formula) in magnetic photonic crystal (MPC) analysis software [75] to model  
 133 and fit the measured transmission spectra, and (iv) from this fitting process, reconfirm the film  
 134 thicknesses and derive the absorption coefficient spectra of the films. The wavelength-dependent  
 135 index ( $n$ ) data (calculated based on Cauchy's dispersion formula) for the amorphous garnet and  
 136 garnet-oxide precursor thin layers deposited on glass (Corning Eagle XG, 0.5 mm thick) substrates,  
 137 yields the following spectral dependency for BiDyIG sample,  $n = 2.1906 + 0.0459/\lambda^2$ , and for BiDyIG:  
 138  $\text{Bi}_2\text{O}_3$  (17 vol. %) composite sample,  $n = 2.2105 + 0.0576/\lambda^2$ ; for BiDyIG:  $\text{Bi}_2\text{O}_3$  (23.3 vol. %) composite  
 139 sample, index dispersion function  $n = 2.1961 + 0.0683/\lambda^2$  was obtained.

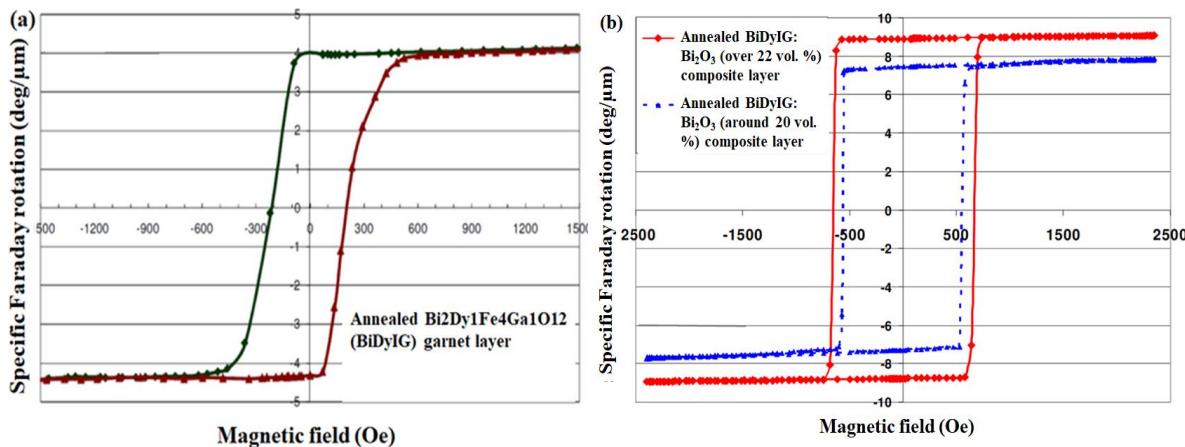


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141 **Figure 2.** (a) Measured transmission spectra of as-deposited  $\text{Bi}_2\text{Dy}_1\text{Fe}_4\text{Ga}_1\text{O}_{12}$  (BiDyIG) and BiDyIG:  $\text{Bi}_2\text{O}_3$  (17 &  
 142 23.3 vol. %) composite thin films, (b) derived refractive index dispersion spectra for  $\text{Bi}_2\text{Dy}_1\text{Fe}_4\text{Ga}_1\text{O}_{12}$  (BiDyIG)  
 143 and BiDyIG:  $\text{Bi}_2\text{O}_3$  (17 & 23.3 vol. %) composite thin films where the solid curves were determined according to  
 144 Cauchy dispersion relationship.

145 The calculated refractive indices at different wavelengths derived from Cauchy's relation as well  
 146 as the calculated refractive index data points using the SEWM method were plotted and compared  
 147 (as shown in Fig. 2b). It can be noted that the refractive index (n) is in the range of 2.2-2.6 in the visible  
 148 region and decreases with increasing wavelength. In the long-wavelength region (above 1600 nm),  
 149 the refractive index seems to be asymptotically approaching a constant value. The volumetric fraction  
 150 of excess  $\text{Bi}_2\text{O}_3$  introduced into the BiDyIG system helps increase the refractive index of the composite  
 151 films, however, this also shifts the absorption edge towards the shorter wavelength region (as seen  
 152 in Fig. 2a). Note that there are always significant differences that exist between the optical constants  
 153 of the crystallized garnets and oxide-mix-based amorphous precursor layers. Therefore, it is also  
 154 important to check the conformity of layer(s) to their designed spectral transmission specifications  
 155 before annealing, especially when developing functional multilayer structures, such as MPC.

156 In our previous work, we have observed the effects of excess  $\text{Bi}_2\text{O}_3$  addition to core materials  
 157 within each garnet-related oxide mix (a generic composition type can be defined using a formula  
 158 description such as  $(\text{Bi},\text{Y},\text{Dy},\text{Lu},\dots)_3(\text{Fe},\text{Al},\text{Ga},\dots)_5\text{O}_{12}$ ) on their annealing crystallization behaviour,  
 159 and the final optical/MO properties. It was reported that an optimized amount of extra  $\text{Bi}_2\text{O}_3$  content  
 160 addition, can significantly improve the specific Faraday rotation, optical transparency and optical  
 161 absorption coefficient across the visible spectral range, thus leading to achieving record-high MO  
 162 quality factors in suitably annealed garnet-oxide composite thin films [66, 68]. Figure 3 shows the  
 163 typical magnetic hysteresis loop properties of annealed garnet and GOC films measured through  
 164 specific Faraday rotation at 532 nm using a Thorlabs PAX polarimeter system in conjunction with a  
 165 custom-made calibrated electromagnet. Noteably, the annealed BiDyIG sample showed a nearly  
 166 square-shaped hysteresis loops of Faraday rotation (Fig. 3a), whilst the annealed GOC films often  
 167 showed practically perfectly "square" shapes of hysteresis loop (Fig. 3b) with perpendicular  
 168 magnetic anisotropy, high (close to 100 %) remnant magnetization, and very sensitive magnetic  
 169 switching behaviour.

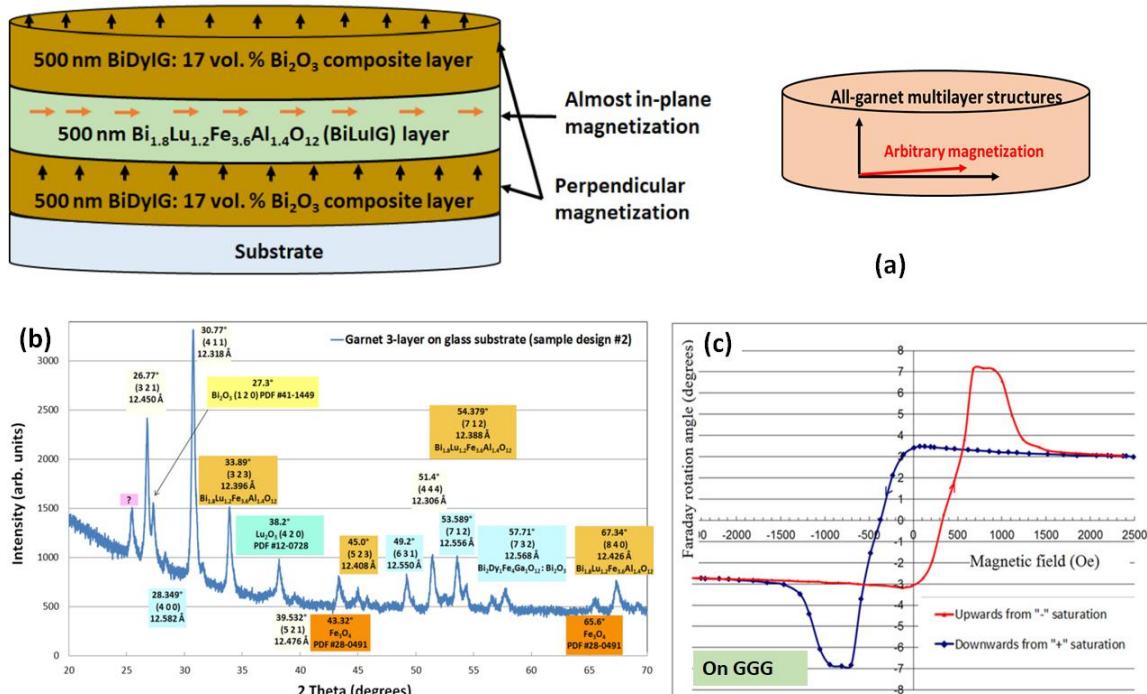


170  
 171 **Figure 3.** Hysteresis loops of specific Faraday rotation at 532 nm measured in sputtered garnet films. (a)  
 172 Annealed (nanocrystalline)  $\text{Bi}_2\text{Dy}_1\text{Fe}_4\text{Ga}_1\text{O}_{12}$  (BiDyIG) sample, and (b) annealed BiDyIG:  $\text{Bi}_2\text{O}_3$  composite-type  
 173 oxide-diluted thin films [66].

174 The strong uniaxial magnetic anisotropy in BiDyIG:  $\text{Bi}_2\text{O}_3$  nano-composite films together with some  
 175 degree of control over the coercive force and switching field properties (as shown in Fig. 3b) and  
 176 excellent optical and magnetic properties, make them very attractive and promising for a large range  
 177 of optoelectronic, photonics-related, sensing, and MO imaging applications.

178 We observed somewhat unconventional and remarkable magnetic switching properties for the  
 179 first time in RF magnetron sputtered all-garnet multilayer thin-film structures, in which magneto-  
 180 soft layers were sandwiched in-between two magneto-hard garnet material layers of identical  
 181 composition type [76]. Both garnet material types possessed very large specific Faraday rotation

182 across the visible spectral range ( $\approx 6^\circ/\mu\text{m}$  at 532 nm and  $\sim 1.6^\circ/\mu\text{m}$  at 635 nm [66, 68]) and high  
 183 magneto-optic (MO) quality. The magnetic switching behavior of trilayers (illustrated in Fig. 4a),  
 184 were characterized by way of measuring their Faraday rotation hysteresis loops. The samples were  
 185 prepared on glass (Corning Eagle XG) and also GGG (111) substrates; the sputtering deposition was  
 186 followed by post-deposition annealing crystallization (heat treatment process, 1 h at 570 °C)  
 187 conducted in air atmosphere. The amount of extra bismuth oxide content co-sputtered from a  
 188 separate target (17 vol. %) was selected to facilitate a notable increase in the specific Faraday rotation  
 189 whilst at the same time avoiding a significant reduction in the upper limits of the annealing  
 190 temperature range. X-ray diffraction (XRD) measurements (performed in the range of 2θ angles  
 191 between 20° and 70°, as shown in Fig. 4b) revealed the body-centered cubic lattice structure of  
 192 different constituent garnet materials present inside annealed trilayers. Their microstructure type has  
 193 been identified as being nanocrystalline on both substrate types. A notable and unexpected feature  
 194 of hysteresis loop behavior (Fig. 4c) was the presence of an “intermediate saturation” state exhibiting  
 195 the maximum Faraday rotation, which then was followed by conventional magnetization saturation  
 196 state with reduced Faraday rotation, at increasing external magnetic fields above about 1 kOe. The  
 197 final saturated Faraday rotation was observed at near 1.6 kOe, at below 50% of the maximum Faraday  
 198 rotation angle seen at smaller fields. To the best of our knowledge, no prior (or later) reports of similar  
 199 magnetic switching behaviours observed in any thin-film materials, relative to Ref. 76, can be found  
 200 in the published literature. These exchange-coupled all-garnet multilayer structures demonstrated an  
 201 attractive combination of optical and magnetic properties, and are of interest for emerging  
 202 applications in optical sensors and isolators, ultrafast nanophotonics, magneto-plasmonics and  
 203 possibly spintronics.



204

205 **Figure 4.** The schematic diagram of all-garnet multilayer structures together with the predicted layer-specific  
 206 magnetization vector directions (a); XRD analysis results obtained from a multilayer garnet structure prepared  
 207 on a glass substrate (b); the unconventional magnetic hysteresis loop of Faraday rotation (°) measured using  
 208 green laser light source.

209 The objective of making this all-garnet trilayer structure was to investigate the potential of  
 210 obtaining and controlling these special magnetic switching properties observed in the described  
 211 trilayer types that are not attainable normally in any single-layer magnetic thin films. We note that  
 212 the unconventional magnetic behavior has only been observed in trilayers employing co-sputtered

213 nanocomposite-type outer magneto-hard layers. Further studies are on-going, aimed at achieving  
214 better control over the magnetic properties (e.g. coercive force, switching field(s), and saturation  
215 magnetization) in garnet multilayer structures having different combinations of high-performance  
216 garnet materials of various optimized thicknesses as well as stoichiometry types. Other active areas  
217 of ongoing research within our group include the investigations of the effects of the post-deposition  
218 oxygen plasma treatment of amorphous-phase garnet-precursors on the final magnetic and MO  
219 properties observed in crystallized films. Initial findings indicate that there exist optimized oxygen  
220 plasma post-treatment regimes, which lead to observing strong improvements in the MO quality of  
221 annealed thin garnet layers.

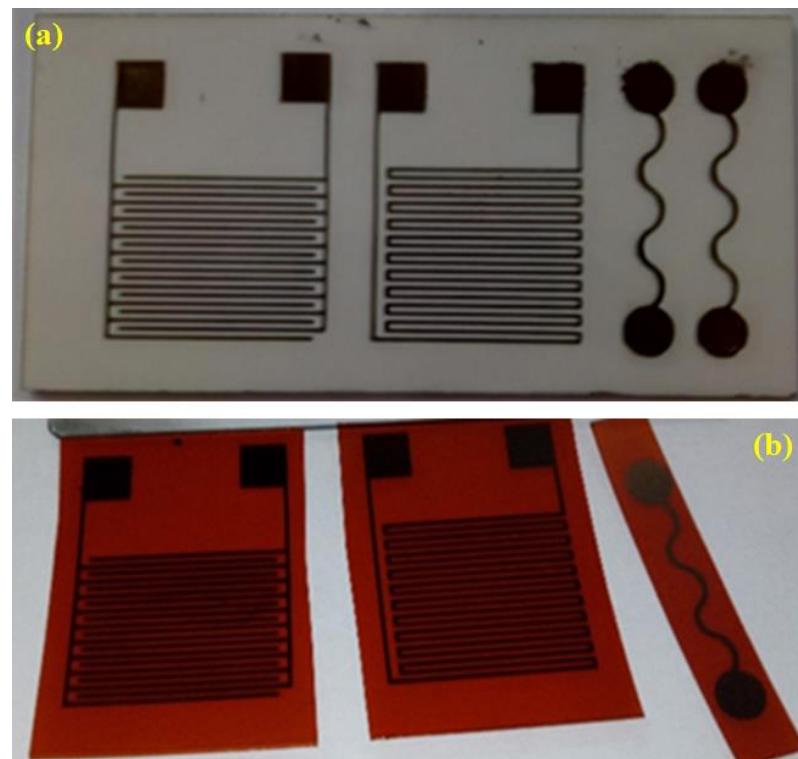
222 **3. Ruthenium-oxide thin-films grown on flexible and rigid substrates for cost-effective sensor  
223 electrodes**

224 Sputter-deposition process parameters such as total or partial gas pressure(s), process gas  
225 chemistry, substrate type, substrate-stage heating temperature, substrate-stage rotation rate,  
226 substrate-to-target distance, target rotation rate, and RF powder densities, are well-known to affect  
227 the growth and properties of thin-film materials. There are many reports published in the literature  
228 describing the necessity of sputter-deposition process parameter optimization for many application-  
229 specific oxide-based and other thin-film materials [78-88]. For example, sputter-deposition process  
230 parameters were studied and optimized to deposit ruthenium oxide ( $\text{RuO}_2$ ) thin films with strong  
231 adhesion properties for manufacturing durable sensing electrodes [84, 88]. For the manufacture of  
232 sensors, it is important to control the material properties in order to obtain the desired functionality  
233 [89]. In this section, we present optimized R.F. sputter-deposition process parameters for the  
234 manufacture of highly-durable  $\text{RuO}_2$  thin-film electrodes on flexible and rigid substrates, along with  
235 the pH and temperature sensing performance of these electrodes.

236 Ruthenium oxide thin films feature very attractive properties for use in various sensing devices,  
237 such as pH sensing, cryogenic temperature sensing, and even bio-sensing applications [90-92]. In  
238 order to manufacture durable and therefore cost-effective electrodes, it is important to have strong  
239 adhesion of  $\text{RuO}_2$  to its substrate material. This requires optimization of multiple sputter-deposition  
240 process parameters, to overcome sputter-chamber pressure-dependent adhesion properties of  $\text{RuO}_2$   
241 layers fabricated on different substrates [90].

242  
243 *3.1. Experimental*  
244

245  $\text{RuO}_2$  thin-film electrodes (potentiometric, interdigitated and resistive) were deposited directly  
246 onto two different substrate materials (alumina and polyimide), as shown in Figure 5. In summary,  
247 100 nm thick layers of  $\text{RuO}_2$  were deposited using RF magnetron sputtering from a metal-oxide ( $\text{RuO}_2$ )  
248 target (99.95% purity) with 110 W sputter power, at room temperature, with 4 mTorr chamber  
249 pressure and 5:5 sccm Ar: $\text{O}_2$  gas flow rate. Electrode patterns were achieved using a standard  
250 photolithographic process.  
251

252  
253254 **Figure 5.** 100nm thick potentiometric, interdigitated and resistive RuO<sub>2</sub> electrodes sputter deposited on alumina  
255 (a) and polyimide (b) substrates.

256

257 Potentiometric measurements were made using an Atlas Scientific ORP EZO circuit connected  
258 to PC via an Electrically Isolated USB EZO Carrier Board, with a commercially available glass  
259 Ag|AgCl|3M KCl reference electrode (Sigma). Resistive electrodes were characterized with an  
260 Agilent 34410A high performance digital multimeter, using a 2-wire set-up to measure resistance.  
261 Measurements were made using commercially available buffer solutions (Rowe Scientific), for pH.  
262 Whilst, temperature was controlled using a thermoelectric device and insulation.

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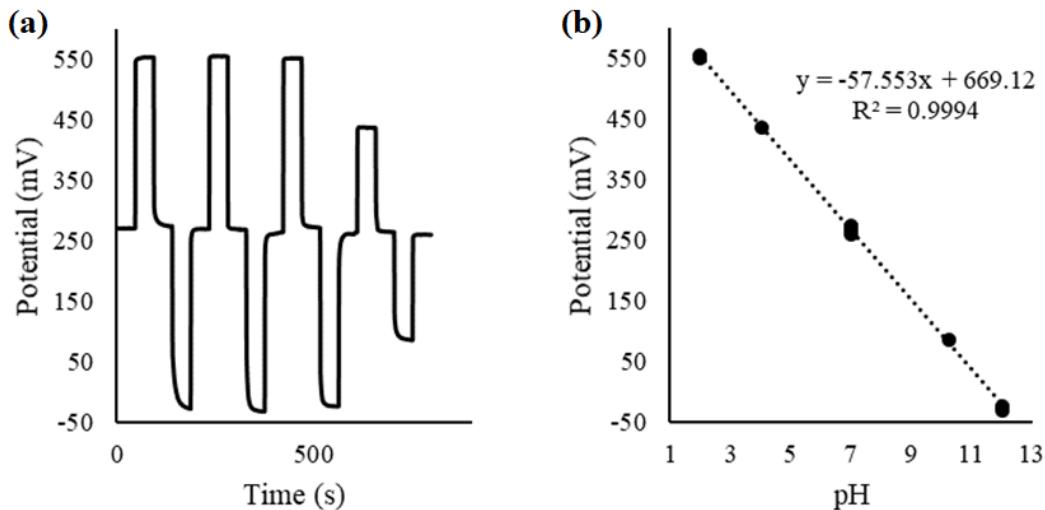
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### 3.2. Results and comparison

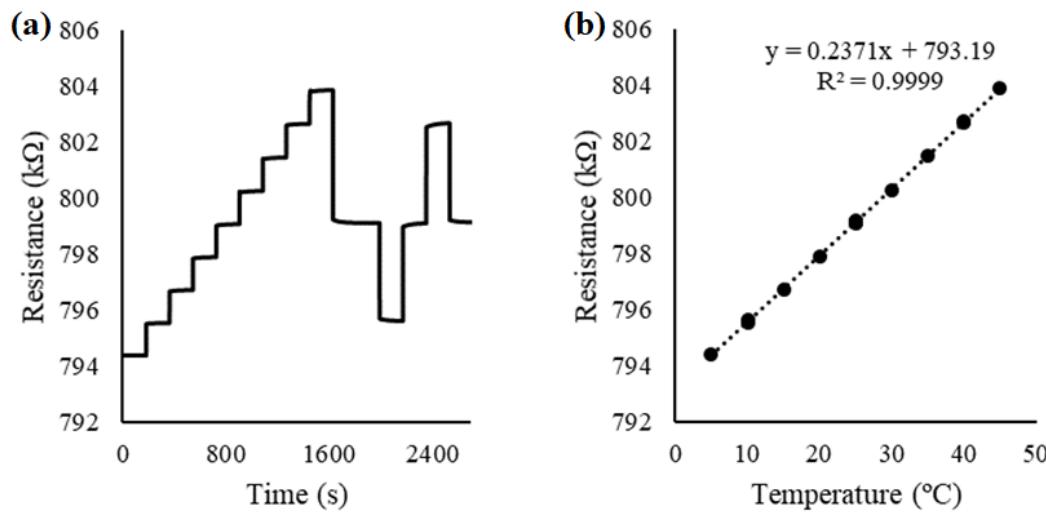
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RuO<sub>2</sub> films sputter deposited directly onto flexible polyimide substrates can be a cost-effective choice for use as a potentiometric electrode. It has been found experimentally that the polyimide-based electrodes prepared using a 4 mTorr chamber pressure and 1:1 Ar: O<sub>2</sub> gas ratio, showed excellent performance when used as potentiometric pH electrode (vs. Ag|AgCl|KCl reference electrode), exhibiting a reversible ( $\pm 3.9$  mV), linear ( $R^2=0.9994$ ) and Nernstian (57.5 mV/pH) pH response, as shown in Fig. 6. The obtained result is comparable to previously reported RuO<sub>2</sub> pH electrodes prepared on alumina substrates, which also exhibited a reversible ( $\pm 1.8$  mV), linear ( $R^2=0.9999$ ) and Nernstian (59.1 mV/pH) pH response [90]. The polyimide resistive and interdigitated electrodes failed when used as conductivity and temperature sensors, due to gradual delamination. However, the alumina-based resistive temperature sensor exhibited reversible ( $\pm 0.01$  °C) linear ( $R^2=0.9999$ ) response, which is comparable to some commercially available sensors as shown in Fig. 7.

279  
280281 Figure 6. Electric potential recorded vs. a Ag|AgCl|KCl reference electrode for the potentiometric RuO<sub>2</sub>  
282 electrode on polyimide substrate, in pH 2, 4 7, 10 and 12 buffers (a), and the reversible linear Nernstian pH  
283 response of the electrode (b).

284

285  
286287 Figure 7. Electric resistance variations recorded for a RuO<sub>2</sub> electrode on alumina substrate, at 5 to 45 °C (a), and  
288 the reversible linear temperature response of the electrode (b).

289

290 To summarize, durable metallic RuO<sub>2</sub> thin films could only be deposited with a chamber  
291 pressure  $\geq 4$  mTorr with argon: oxygen content in the chamber. RuO<sub>2</sub> films deposited at pressures  
292 lower than 4 mTorr produced powdery films that rapidly delaminate from all substrates. The  
293 improved durability of these RuO<sub>2</sub> electrodes allows for the development of reliable sensors,  
294 potentially for miniaturised applications or where conventional glass probes are not suitable, such as  
295 biomedical applications.

296

297 Other RF sputtered metal oxide materials investigated by our group included rare-earth oxide  
298 compositions such as Er<sub>2</sub>O<sub>3</sub>, Dy<sub>2</sub>O<sub>3</sub>, Gd<sub>2</sub>O<sub>3</sub>, and other, e.g. Zr<sub>2</sub>O<sub>3</sub>, TiO<sub>2</sub>, SnO<sub>2</sub>, and Al<sub>2</sub>O<sub>3</sub>. Intended  
299 applications included the scratch-proof and hydrophobic film layers, sensing applications, diffusion  
300 protection layers, and generic multilayer constituents. Two principal categories of deposition  
301 processes were explored with oxide materials: sputtering in pure-argon plasma and the processes  
302 run using argon-oxygen plasma mixes. Substantial differences in the resulting oxide material  
303 properties were observed, dependent on the deposition process type used. The main reason for the

304 observed property differences was the oxygen loss occurring during sputtering deposition, which  
305 has often been possible to recover using high-temperature oven annealing processes.

306 **4. Metal-dielectric nanocomposite-based multilayer building blocks for transparent solar and**  
307 **thermal regulation coatings**

308 The development of modern energy-efficient glass and window products requires specialized  
309 thin-film coatings containing silver (Ag) layer(s) to filter or reflect the infrared and far-infrared  
310 (thermal) radiation components of the solar spectrum, thus reducing the energy consumption in  
311 buildings. Also, surface plasmon resonance-based optical sensors require noble metal-dielectric  
312 interfaces, and have numerous commercial applications in gas, biochemical and chemical sensing  
313 due to their high sensitivity to the refractive index changes in a dielectric medium placed on top of  
314 ultra-thin metallic (Ag) films [93-96]. The deposition of the ultra-thin Ag layers with low surface  
315 roughness and high uniformity is the key to achieving the required application-specific optical  
316 properties. However, the deposition of ultra-thin (less than 20 nm) Ag layers often results in forming  
317 morphologically uneven nano-islands, even when using the fine-tuned deposition processes, such as  
318 RF magnetron sputtering [97, 98]. The formation of these Ag nano-islands significantly affects the  
319 optical performance of multilayer metal-dielectric thin-film structures. Typically, reduced reflectivity  
320 across the near-infrared range results from the imperfect metal layer morphologies. Also, dielectric  
321 material layer deposited on top of these island-shaped ultra-thin Ag layers tend to “sink” into the  
322 spaces between these silver nano-islands, leading to strong optical property deviations from the  
323 designed response. Another issue associated with Ag is that it oxidizes very quickly, therefore the  
324 Ag layer has to be protected from oxidation even during the deposition of the next material layer in  
325 the thin-film multilayer sequence. Researchers have proposed and trialled the preparation of  
326 nanocomposites to overcome these issues related to the difficulties of forming ultra-thin Ag layers.  
327 Most of the relevant success stories were about depositing metal-dielectric nano-particle based  
328 composites [99-103].

329 We have prepared co-sputtered metal-dielectric nanocomposites (MDC) by developing a co-  
330 sputtering process for Ag-MgF<sub>2</sub> system, with various volumetric contents of the dielectric phase  
331 added to the metal. We have also developed MDC-containing multilayer structures, and their  
332 characterisation results suggest that MDC layers can replace the pure-metal layers in multilayer  
333 optical coatings, thus offering a new possibility to design and fabricate highly durable and  
334 environmentally-stable coatings on glass suitable for solar and thermal regulation technologies [104].  
335 In this section, we present the growth process details for thin-film single-layer MDC and newly  
336 developed MDC-containing multilayer coatings. Their measured optical characteristics are also  
337 reported. The transmission spectrum features of these newly-developed MDC-based multilayer  
338 building blocks appear to be promising for manufacturing cost-effective solar and thermal heat  
339 regulation coatings for the construction industry, in the near future.

340  
341 *4.1 Deposition of MDC layers and multilayer structures*  
342

343 Several batches of MDC (Ag+MgF<sub>2</sub>) films were deposited onto glass substrates by using the co-  
344 sputtering process in an RF magnetron sputtering system. The volumetric fraction of dielectric (MgF<sub>2</sub>)  
345 phase was controlled by adjusting the RF power densities applied to the MgF<sub>2</sub> sputtering target  
346 during the co-sputtering process, after carefully calibrating the partial deposition rates for both MgF<sub>2</sub>  
347 and Ag. The thicknesses of ultrathin composite films trialled were in the range between 12 - 25 nm.  
348 After the successful growth of MDC layers, we prepared several multilayer structures introducing  
349 the optimized MDC layers along with surrounding oxide layers. Table 1 summarizes the deposition  
350 process parameters used to fabricate these metal-dielectric nanocomposite layers and MDC  
351 containing multilayer building blocks. The transmission and reflection spectra of MDC layers were  
352 measured just after the deposition using an Agilent Cary 5000 UV-VIS-NIR spectrophotometer. The  
353 reflection spectrum measurements were carried out using a custom-built reflection-mode optical

354 measurement module mounted inside the spectrophotometer, which contained four mirrors adjusted  
 355 at 45-degree tilts to form a periscope-type device as shown in Fig. 8.  
 356

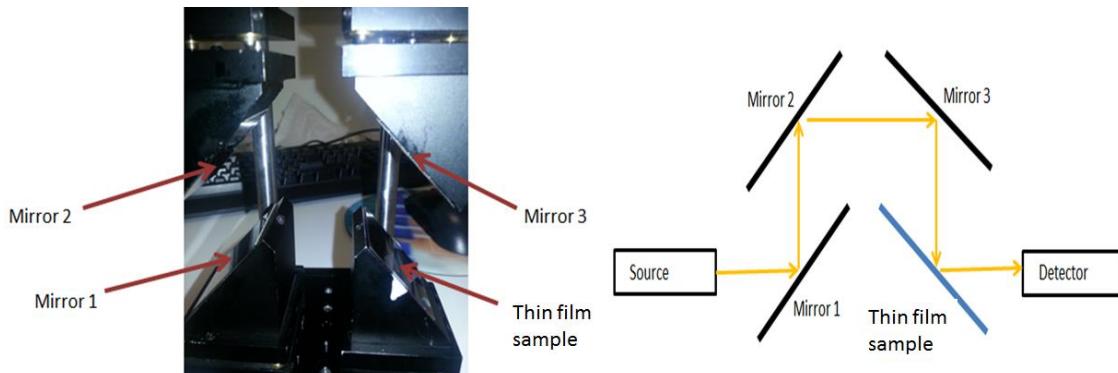
357 **Table 1.** Sputtering process parameters used to deposit MDC single layer and MDC containing multilayer  
 358 building blocks.

359

Process parameters	Layer structure (single layer MDC)	Layer structure (multilayers containing MDC layer)
Sputtering targets	Ag, MgF <sub>2</sub>	Al <sub>2</sub> O <sub>3</sub> , Zr <sub>2</sub> O <sub>3</sub> , Ag, MgF <sub>2</sub>
RF Power	Ag (55-65 W), MgF <sub>2</sub> (83-95 W)	Al <sub>2</sub> O <sub>3</sub> (190 - 195 W), Ag (55 - 65 W), MgF <sub>2</sub> (83 - 95 W)
Base pressure (Torr)	$5 \times 10^{-6}$	$5 \times 10^{-6}$
Process gas	Ar	Ar
Process pressure	2-3 mTorr	1-3 mTorr
Substrate temperature (°C)	Room temperature	Room temperature
Post deposition heat treatment	No	Up to 500°C for 1-10 hours

360

361



362

363

364 **Figure 8.** Schematic diagram of the optical system used in Cary 5000 spectrophotometer to measure the  
 365 reflection spectrum of the thin film coatings on glass substrates.

366

367 Since our primary motivation for MDC materials development was to broaden the range of  
 368 possible high-performance designs of heat-mirror-type coatings, and because the reflectivity of these  
 369 coating types across the near-infrared range is their main performance indicator, developing both the  
 370 transmission and reflection spectral measurements was necessary.

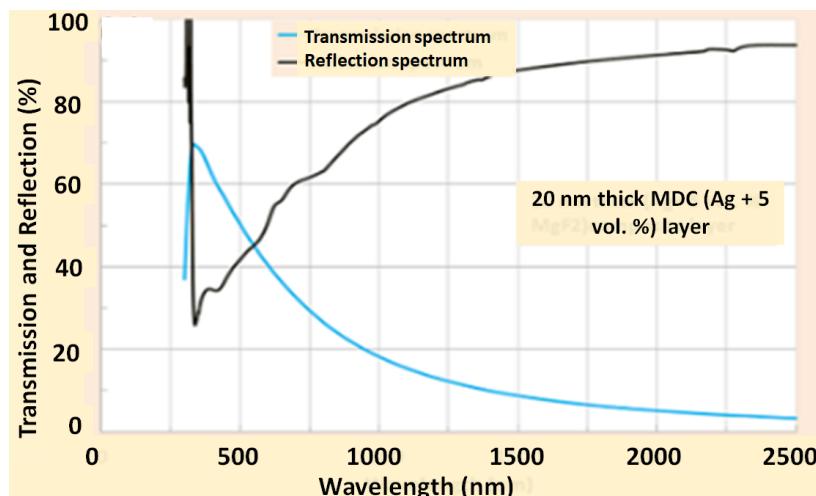
371

#### 372 4.2 Optical characteristics of MDC thin films and MDC-containing multilayer structures

373

374 Figure 9 shows an example of the measured transmission and reflection spectrum of Ag+MgF<sub>2</sub>  
 375 (5 vol. %) composite (~20 nm) thin-film. The transmission peak in this Ag+MgF<sub>2</sub> composite layer  
 376 exhibited short-wavelength transmission and reflection features similar to the Ag layer of the same  
 377 thickness. The optical absorption was calculated by subtracting the transmittance and reflectance of  
 378 the composite layers using the formula  $A=1-T-R$  (%), where A is the absorbed power fraction, T is the  
 379 power transmission coefficient, and R is the power reflectivity. It was found that the Ag+5 vol. %  
 380 MgF<sub>2</sub> sample had a comparatively lower absorption (less than 9 % by power) in the UV-Visible  
 381 spectral range, which is close to that of the pure Ag layer. This indicates that the addition of 5 vol. %  
 382 MgF<sub>2</sub> into the Ag layer during the co-sputtering process can potentially improve the coating adhesion  
 383 and stability aspects without compromising the plasmonics metal properties.

384



385

386

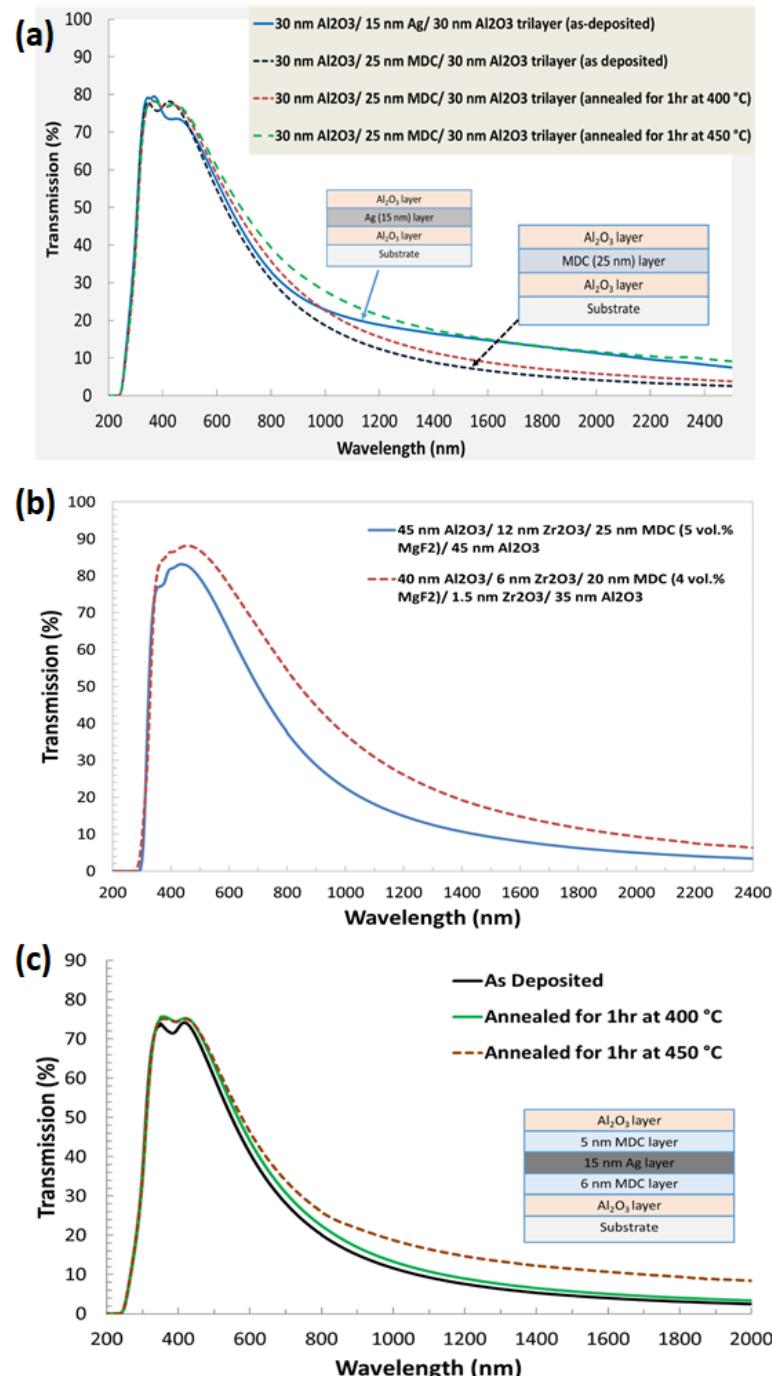
387 **Figure 9.** Measured transmission and reflection spectra of ~ 20 nm thick Ag + 5 vol. % MgF<sub>2</sub> composite layer,  
388 deposited onto glass substrate.

389

390 Several trilayer structures containing at least one MDC layer were deposited on clear glass  
391 substrates using one continuous sputtering run, and their optical performance was characterized.  
392 Figure 10 (a) shows the transmission spectrum of as-deposited multilayer coatings, where the layer  
393 structure consists of at least one MDC (Ag + 4-5 vol. % MgF<sub>2</sub>) in comparison to that of a typical tri-  
394 layer pure metal (Ag) based DMD-type coating. It can be noted that the use of a 25 nm MDC layer  
395 instead of a pure 15 nm Ag layer resulted in better thermal radiation filtering performance without  
396 compromising the visible spectral transmission, whilst avoiding any potential layer morphology-  
397 related issues that usually affect ultrathin (thinner than about 17 nm) layers. Experimental  
398 investigations revealed that the co-sputtered MDC (even comparatively thicker) layers with high  
399 metal volume content can be embedded into any type of multilayer structures for possibly improving  
400 the spectrally-selective transparency control, and structural properties of the coating whilst allowing  
401 significant design flexibility. Particularly important is the possibility of depositing MDC-type layers  
402 onto practically any underlying film layers, almost regardless of surface energy-related layer  
403 interface compatibility considerations. The MDC based structures also demonstrated much lower  
404 thermal emissivity whilst maintaining the same superior visible transmission compared to the silver-  
405 based coatings, as shown in Fig. 10(a).

406

407



408  
409

410 **Figure 10.** Measured transmission spectra of multilayer thin film structures containing a single (or double)  
411 metallic or MDC layer. (a) Transmission of a tri-layer MDC structure compared to that of a typical Ag layer  
412 within a DMD structure; thermal performance stability test results are also shown for the tri-layer MDC structure;  
413 (b) transmission spectra of multilayer structures containing MDC layer of different volumetric fractions of added  
414 dielectric, and (c) thermal performance stability test results for a complex DMD-type multilayer structure  
415 containing both the MDC outer-bracket sublayers and an ultra-thin pure-Ag core layer.  
416

417 In order to investigate the design variations, material intercompatibility, durability and thermal  
418 stability properties of the MDC-based coatings, several different types of test multilayers (up to five-  
419 layer structures) were developed, as shown in Fig. 10 (b, c). Figure 10 (b) shows the optical  
420 performance of an elementary (five layer-based) thin-film coating building blocks composed of a  
421 center MDC layer, surrounded by thin oxide-based “bracket layers” deposited by pure-argon  
422 sputtering process from a ceramic oxide target of Zr<sub>2</sub>O<sub>3</sub>. The addition of these ultrathin rare-earth

423 oxide layers has led to broadening the structure design possibilities in terms of improving the peak  
424 transmission and spectral selectivity. The optical performance variations observed in this particular  
425 five layer-based coatings confirmed the possibility of engineering a broader range of optical coatings  
426 for future solar and thermal regulation application in comparison with a simple dielectric-metal-  
427 dielectric (DMD) trilayers or multilayers of similar spectral response. Figure 10(c) presents a more  
428 complex generalized MDC-type multilayer building block, which was subjected to extensive thermal  
429 stability (dry heat exposure) tests. The performance of the developed structure (before and after heat  
430 exposure in an air-filled lab oven) shows that the optical properties are comparable to some of the  
431 conventional multilayer structures containing pure Ag layers [105, 106]. It can be seen clearly that the  
432 transmission spectra were found to be only slightly changed at temperatures near 400 °C, which is a  
433 very encouraging result, and confirms that the very thin MDC barrier layers can play a vital role in  
434 protecting the ultra-thin core Ag layers within the multilayer structures. This confirms that the MDC  
435 layers can be used to enable arbitrarily complex high-stability low-E, heat-mirror, or filter-type  
436 optical coating designs of high spectral selectivity, on a range of optical substrates. Additionally, it is  
437 possible to engineer a broader range of reflected or transmitted colour properties, compared to pure  
438 metal-based designs, which are much more limited in terms of the optical materials selection.  
439

## 440 5. Conclusions

441 We demonstrate a range of material system design possibilities for multiple practical  
442 applications provided by fine-tuning the RF magnetron sputtering technologies. We established  
443 numerous sputtering-based thin-film material synthesis processes at ECU, aiming at incorporating  
444 these optical materials into functional devices for sensing, optical spectra shaping, polarisation  
445 control, magnetic switching, and magnetic field visualization, among others. Three functionally  
446 different categories of thin-film material systems have been discussed, such as MO garnets, metal  
447 oxides, and metal-dielectric nanocomposites, and results have been presented describing their  
448 growth processes and relevant parameters, physical properties, and behavior. All of the characteristic  
449 results obtained from these material system types are of interest for use in practical field-specific  
450 applications in optics, magneto-optics, sensing, and renewable energy.  
451

452 **Author Contributions:** All authors have made nearly equal contributions to the study and manuscript. M. N. A.  
453 planned and designed the manuscript. M. N. A., W. L., and M. V. discussed the contents and wrote the  
454 manuscript, K. A. revised the manuscript, and edited it further, contributing to the final group discussion  
455 outcome regarding the manuscript.

456 **Funding:** This research work is supported by Electron Science Research Institute, Edith Cowan University, WA,  
457 Australia. No external funding was received.

458 **Acknowledgments:** The authors would like to acknowledge Dr. Yamna El-Mouedden for making some  
459 characterization experiments with MDC-based thin films and for generating the results presented in Figure 9  
460 also Fig. 8.

461 **Conflicts of Interest:** The authors declare no conflict of interest.

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