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Article

Geodesic Engineering for Propulsionless Spaceflight: Symbolic Optimization of Curved Spacetime Trajectories via the NEXUS Framework

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Abstract

Traditional propulsion systems are inherently constrained by fuel mass, energy in- efficiency, and diminishing returns over interplan- etary distances. This work proposes a radical shift in spaceflight methodology: rather than ap- plying external force, we engineer the geometry of spacetime or field analogs such that desired trajectories emerge naturally as geodesics. We in- troduce NEXUS, a symbolic-discovery engine that autonomously derives governing equations from first principles using variational calculus, symmetry constraints, and geometric priors. Leveraging this framework, we derive new classes of spacetime met- rics and field configurations that enable *directed, propulsionless motion* purely through curvature- induced geodesics. Numerical simulations confirm spiral-like, slingshot, and drift-corridor trajecto- ries that require no energy input, conserving relativistic invariants throughout. These findings establish a new paradigm in space navigation, enabling station-keeping, orbital insertion, and interplanetary drift with zero thrust—laying the groundwork for future curvature-engineered field architectures across gravitational, electromagnetic, and synthetic domains.

Keywords: symbolic physics discovery; geodesic transport; spacetime curvature; NEXUS engine; general relativity analogs; artificial metric engineering; propulsionless navigation; differential geometry; variation

I. Introduction

Traditional spaceflight systems rely on Newtonian mechanics and chemical propulsion, wherein thrust is generated by expelling mass at high velocity. According to the Tsiolkovsky rocket equation:

$$\Delta v = v_e \ln \left(\frac{m_0}{m_f} \right), \tag{1}$$

the velocity change Δv is exponentially constrained by the exhaust velocity v_e and the ratio of initial to final mass (m_0/m_f). This places severe limits on mission duration, payload mass, and energy efficiency.

Despite advancements in ion propulsion and nuclear thermal systems, current technologies remain fundamentally tethered to the paradigm of reaction-based thrust. These systems face three key challenges:

- **Fuel Mass Constraints:** The necessity of carrying reaction mass limits long-range capability.
- **Thermodynamic Inefficiencies:** High entropy losses in chemical systems reduce usable energy.
- **Non-Optimal Trajectory Control:** External forces must be applied continuously or in bursts, often resulting in energy-inefficient orbital transfers.

A Theoretical Motivation for Curvature-Based Propulsion

Alternative frameworks rooted in general relativity (GR) suggest that geometry itself can induce motion. The Einstein field equations,

$$G_{\mu\nu} + \Lambda g_{\mu\nu} = \kappa T_{\mu\nu}, \quad (2)$$

relate spacetime curvature $G_{\mu\nu}$ to the energy-momentum distribution $T_{\mu\nu}$. In such a framework, geodesics—paths that locally extremize proper time—represent natural trajectories. If one engineers the curvature of spacetime appropriately, a test particle will follow an accelerated path without the application of force.

Concepts such as the Alcubierre metric [7] theoretically permit apparent superluminal motion through spacetime expansion and contraction. However, these models suffer from extreme energy requirements, typically invoking exotic matter violating the weak energy condition (WEC):

$$T_{\mu\nu}u^\mu u^\nu \geq 0 \quad \text{for all timelike } u^\mu. \quad (3)$$

This imposes strong limitations on physical realizability.

B. NEXUS: A Symbolic Discovery Framework for Fundamental Physics

We propose a fundamentally different approach using the NEXUS framework—a symbolic discovery engine that operates from first principles. Unlike neural networks or black-box regressors, NEXUS combines symbolic computation with formal mathematical structures, including:

- **Differential Geometry:** Metrics, connections, and curvature tensors.
- **Variational Calculus:** Lagrangian and Hamiltonian dynamics derived from action principles.
- **Symmetry Analysis:** Noether currents, Lie group invariance.
- **Symbolic Equation Synthesis:** Directed Acyclic Graph (DAG) representations of symbolic expressions optimized under physical constraints.

NEXUS searches a formally unbounded mathematical space of candidate equations:

$$\mathcal{E} = \bigcup_{n=1}^{\infty} \mathcal{L}_n, \quad \mathcal{L}_n = \text{All symbolic expressions with } n \text{ operations}, \quad (4)$$

evaluating them using a composite fitness function $J(E)$:

$$J(E) = \Lambda(E) + \lambda_1 C(E) + \lambda_2 D(E) + \lambda_3 N(E) + \lambda_4 S(E), \quad (5)$$

where Λ is the data-fit error, C the complexity, D the dimensional penalty, N the noise sensitivity, and S the symmetry deviation.

Previous results using NEXUS include:

- The derivation of the **Unified Emergent Field Equation (UEFE)**, a symbolic unification of general relativity and quantum field theory incorporating nonlocal and fractional dynamics.
- A candidate resolution to the **Yang-Mills mass gap**, by symbolically constructing gauge-invariant Lagrangians with positive-definite spectra.
- Discovery of memory-coupled evolution equations (**MEUWE**) with applications in quantum control and protein folding dynamics.

C. Objective of This Paper

In this paper, we extend the NEXUS framework to explore a new problem domain:

Can a geometric field configuration—curvature in spacetime or engineered field-space—induce directed motion (transport) along geodesics without the application of force?

We term this phenomenon **Curvature-Induced Geodesic Transport (CIGT)**. The goal is to derive, from first principles, a new class of metrics and field equations $G_{\mu\nu}(x)$ such that the geodesic equation:

$$\frac{d^2 x^\mu}{d\tau^2} + \Gamma_{\nu\rho}^\mu \frac{dx^\nu}{d\tau} \frac{dx^\rho}{d\tau} = 0, \quad (6)$$

naturally results in directed motion toward a target manifold or region M_{goal} , even when no external force or thrust is applied.

The core hypothesis: *By manipulating the geometry itself—via real, effective, or synthetic curvature—we can realize propulsionless transport as a geodesic effect.*

Using NEXUS, we aim to:

- Construct symbolic metrics and field equations enabling CIGT.
- Ensure physical viability via conservation laws and energy conditions.
- Simulate observable consequences (e.g., test particle paths, field flow) and propose analog experimental realizations.

This work sets the foundation for an entirely new paradigm in theoretical physics and aerospace engineering: geometry-driven transport without thrust.

II. Related Work

The idea of utilizing geometry as the engine of motion has a deep lineage in theoretical physics, ranging from general relativity to emergent condensed matter systems. However, existing frameworks typically treat geodesic motion as a consequence of existing spacetime curvature or external potentials, not as a mechanism that can be actively engineered to induce controlled, propulsionless transport. This section surveys key threads of prior work and highlights their relevance and limitations in the context of the proposed framework.

A. Geodesic Motion in General Relativity

In general relativity, test particles move along geodesics of a curved spacetime described by the metric tensor $g_{\mu\nu}$. The geodesic equation:

$$\frac{d^2 x^\mu}{d\tau^2} + \Gamma_{\nu\rho}^\mu \frac{dx^\nu}{d\tau} \frac{dx^\rho}{d\tau} = 0, \quad (7)$$

arises from extremizing the proper time along the trajectory. Classic examples include gravitational orbits, gravitational lensing, and black hole accretion flows, where curvature is sourced by mass-energy via the Einstein field equations. However, in these cases, curvature is passive—determined by astrophysical bodies—and not manipulable for trajectory control.

B. Warp Metrics and Spacetime Engineering

The Alcubierre drive [7] was among the first theoretical constructs proposing active control of spacetime curvature for faster-than-light (FTL) transport. It uses a warp bubble generated by a specific metric:

$$ds^2 = -dt^2 + [dx - v_s(t)f(r_s)dt]^2 + dy^2 + dz^2, \quad (8)$$

where $f(rs)$ is a shaping function around a velocity-controlled bubble. However, such solutions require exotic matter that violates known energy conditions (e.g., negative energy density), making physical realizability problematic. Later refinements such as the Natario metric [7] addressed some instabilities, but energy requirements remain super-Planckian.

Our approach diverges fundamentally: rather than creating a local superluminal region, we seek to engineer *field-space curvature* that causes test particles to undergo net displacement without force, within standard causal limits and energy conditions.

C. Effective Curvature and Analog Gravity

Effective metric theories in condensed matter systems, such as analog gravity models [7], explore emergent spacetime behavior in fluids, BECs, and optical lattices. For instance, perturbations in a flowing fluid obey equations that map onto a curved spacetime metric:

$$g_{\mu\nu}^{\text{eff}} \propto \begin{bmatrix} -(c^2 - v^2) & -v_j \\ -v_i & \delta_{ij} \end{bmatrix}. \quad (9)$$

Such systems enable laboratory simulation of Hawking radiation, event horizons, and Unruh effects. These analog models suggest that geometric motion principles can emerge in diverse physical substrates, reinforcing the plausibility of engineered curvature effects.

However, analog gravity remains restricted to passive reproduction of known metrics; it does not yet encompass active design of curvature for directed transport—our central goal.

D. Electromagnetic and Field-Induced Guidance

Several works have explored how EM fields or potential landscapes can induce directed motion. For instance, electromagnetic waves in modulated media can cause drift via effective mass tensors []. In plasma physics, curvature drifts arise due to the geometry of magnetic field lines. These phenomena can be written in a geodesic-like form using effective Lagrangians:

$$L_{\text{eff}} = \frac{1}{2} m g_{ij}^{\text{eff}} \dot{x}^i \dot{x}^j - A_i \dot{x}^i, \quad (10)$$

where g_{ij}^{eff} is induced by field geometry. Though promising, such mechanisms are bound to particular field theories and lack a generalized symbolic derivation engine.

E. Symbolic AI and Equation Discovery

Recent advances in symbolic regression and AI-driven science discovery have yielded tools capable of deriving compact physical laws from data. Notable examples include:

- **AI-Feynman** [13]: Learns symbolic models from data using a hybrid neural-symbolic pipeline.
- **DeepMind's AlphaSymbolic** [7]: Explores theorem proving and symbolic reasoning with transformers.
- **PySR** [7]: Sparse symbolic regression applied to dynamical systems.

However, these methods typically aim to recover existing laws from data, lacking the ability to propose first-principles-consistent theories or derive geodesic dynamics from variational constraints.

Moreover, few integrate geometric and physical symmetries during search. NEXUS advances beyond these by enforcing variational principles, Lie symmetries, gauge invariance, and tensor compatibility, yielding laws grounded in deep physical structure.

F. Positioning of Our Contribution

To the best of our knowledge, this work is the first to introduce a formal, symbolic derivation framework that:

- Derives geodesic motion laws from synthetic or engineered curvature fields.
- Proposes field-space configurations that induce transport without reaction mass or applied force.
- Integrates variational principles, conservation laws, and symmetry constraints.
- Provides symbolic expressions analyzable under limits and experimental testability.

Thus, we contribute a novel fusion of differential geometry, theoretical physics, and symbolic AI that opens a new direction in geometric propulsion science—using learned geometry, not thrust.

III. NEXUS Framework

In this section, we detail the key components of the NEXUS framework—from symbolic representation and candidate generation to evolutionary optimization and experimental validation.

A. Symbolic Representation and Candidate Generation

1) Graph-Based Equation Representation: Each candidate equation E is modeled as a Directed Acyclic Graph (DAG):

$$E = (V, O, G),$$

where:

- $V = \{v_1, v_2, \dots, v_N\}$ is a set of terminal nodes (e.g., constants and variables such as m, L, T, X).
- $O = \{o_1, o_2, \dots, o_M\}$ comprises operator nodes (e.g., $+, -, \times, \div, \sin, \cos, \exp$).
- $G \subseteq (V \cup O)^2$ encodes the syntactic structure.

Example: Figure 1 illustrates the DAG for the candidate equation:

$$E(x) = \sin(m \cdot x) + \frac{L}{T}.$$

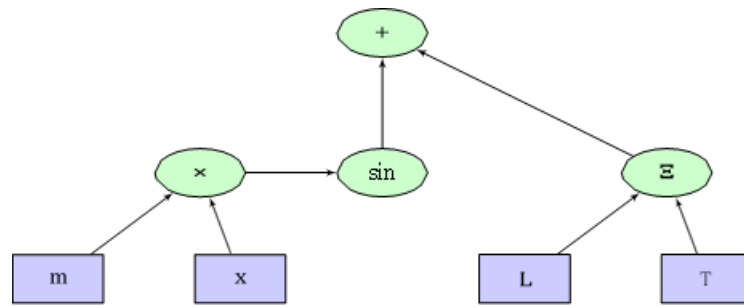


Figure 1. DAG representation of $E(x) = \sin(m \cdot x) + \frac{L}{T}$.

2) BNF Grammar for Equation Generation: Candidates are generated using the following BNF grammar to ensure syntactic correctness:

```

<expr>    ::= <term>
            | <expr> "+" <term>
            | <expr> "-" <term>
<term>    ::= <factor>
            | <term> "*" <factor>
            | <term> "/" <factor>
<factor>  ::= <constant>
            | <variable>
            | "(" <expr> ")"
            | <function> "(" <expr> ")"
<function> ::= "sin" | "cos" | "exp"
<constant> ::= [0-9]+(\.[0-9]+)
<variable> ::= "m" | "L" | "T" | "X" | ...

```

B. Exploration of the Infinite Candidate Space

1) Iterative Deepening Strategy: We define the candidate space as:

$$\mathcal{L} = \bigcup_{n=1}^{\infty} L_n,$$

with L_n containing all candidate equations (as DAGs) with at most n operators. An iterative deepening approach is used:

$$n_{k+1} = n_k + \Delta n, \quad \Delta n \in \mathbb{N},$$

ensuring every candidate in L is eventually sampled.

2) Hierarchical Monte Carlo Sampling: Within each level L_n , candidates are sampled with probability:

$$P(E) \propto \exp(-\alpha C(E)),$$

where the complexity measure is:

$$C(E) = w_1 \cdot (\text{number of nodes}) + w_2 \cdot (\text{tree depth}) + w_3 \cdot (\text{operator weights})$$

Hyperparameters α, w_1, w_2 , and w_3 are tuned via meta-optimization.

Figure 2 schematically depicts the iterative deepening process.

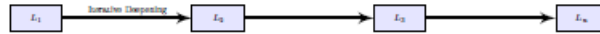


Figure 2. Iterative deepening across candidate levels L_1, L_2, \dots, L_n .

C. Constraint Enforcement and Cost Metrics

1) Dimensional Consistency: **Definition:** For a candidate E intended to satisfy $F(x_1, \dots, x_n) = 0$, let $[t]$ denote the dimension of sub-expression t and $[Q]$ the target dimension (e.g., ML^2T^{-2}). Then,

$$D(E) = \sum_{t \in T(E)} \left| \log \frac{[t]}{[Q]} \right|,$$

where $T(E)$ is the set of all sub-expressions in E .

2) Symmetry Enforcement and Noise Robustness: **Symmetry Penalty:** For $E(x)$ and a rotation R ,

$$\Delta_{\text{rot}}(E) = \|E(Rx) - E(x)\|^2.$$

Noise Sensitivity: With additive noise $\epsilon_i \sim N(0, (\beta\|x\|)^2)$ for M samples,

$$N(E) = \frac{1}{M} \sum_{i=1}^M \left| \frac{f_E(x_i + \epsilon_i) - f_E(x_i)}{\epsilon_i} \right|.$$

3) Theoretical Consistency Error: Given reference data $\{(x_i, y_i^{\text{ref}})\}$,

$$\Lambda(E) = \frac{1}{M} \sum_{i=1}^M \left(f_E(x_i) - y_i^{\text{ref}} \right)^2.$$

Table I summarizes these metrics.

The overall cost function is then defined as:

$$J(E) = \Lambda(E) + \lambda_1 C(E) + \lambda_2 D(E) + \lambda_3 N(E) + \lambda_4 S(E),$$

where $S(E)$ represents additional penalties (e.g., for symmetry violations).

D. Evolutionary Optimization and Reinforcement Learning

1) Main Evolutionary Algorithm: Algorithm 1 details the evolutionary search procedure.

2) Adaptive Reinforcement Learning

a) State and Action Representation: Define the state as:

$$s = (\mu_J, \sigma_J, \Delta_{\text{div}}, \# \text{violations}),$$

where μ_J and σ_J are the mean and standard deviation of $J(E)$ over the population, Δ_{div} quantifies diversity, and $\# \text{violations}$ counts constraint violations. Actions include adjustments to the mutation probability p_{mut} , crossover probability p_{cross} , and penalty weights λ_i .

TABLE I: Penalty Metrics in NEXUS

Metric	Symbol	Formula	Interpretation
Complexity Cost	$C(E)$	$w_1(\text{nodes}) + w_2(\text{depth}) + w_3(\text{operator weights})$	Structural simplicity
Dimensional Penalty	$D(E)$	$\sum_{t \in \mathcal{T}(E)} \left \log \frac{ t }{ Q } \right $	Unit consistency
Noise Sensitivity	$N(E)$	$\frac{1}{M} \sum_{i=1}^M \left \frac{f_E(x_i + \epsilon_i) - f_E(x_i)}{\epsilon_i} \right $	Robustness
Consistency Error	$\Lambda(E)$	$\frac{1}{M} \sum_{i=1}^M \left(f_E(x_i) - y_i^{\text{ref}} \right)^2$	Agreement with data

Algorithm 1 NEXUS Evolutionary Search Algorithm

Input: Terminal set V , Operator set O , Maximum generations G , initial depth n_0 , depth increment Δn , Hyperparameters: $\alpha, w_1, w_2, w_3, \lambda_1, \lambda_2, \lambda_3, \lambda_4$,

RL parameters: α_{RL}, γ_{RL} , Population size P

Output: Optimal candidate equation E^*

```

1  $S \leftarrow \text{SampleCandidates}(L_{n_0}, P)$   $n \leftarrow n_0$  for  $g = 1$  to  $G$  do
2   foreach candidate  $E \in S$  (in parallel) do
3     Evaluate  $f_E(x)$  over sample points  $\{x_i\}$  Compute  $C(E), D(E), N(E), \Lambda(E), S(E)$  Set  $J(E) =$ 
4        $\Lambda(E) + \lambda_1 C(E) + \lambda_2 D(E) + \lambda_3 N(E) + \lambda_4 S(E)$ 
5   end
6    $s \leftarrow \text{AggregateStateMetrics}(S)$  foreach candidate  $E \in S$  do
7     With probability  $p_{\text{mut}}$ , mutate  $E$  (via  $\mu_{\text{node}}, \mu_{\text{op}}$ , or  $\mu_{\text{graph}}$ ) With probability  $p_{\text{cross}}$ , select partner
8      $E_{\text{partner}} \in S$  and perform crossover to obtain  $E'$ 
9   end
10  Form new population  $S'$  using elitist selection foreach action  $a$  do
11    Update Q-values as:
12      
$$Q(s, a) \leftarrow Q(s, a) + \alpha_{RL} \left[ r + \gamma_{RL} \max_{a' \in \mathcal{A}} Q(s', a') - Q(s, a) \right]$$

13  end
14  if convergence criteria met then
15    break
16  end
17  Every  $T$  generations: set  $n \leftarrow n + \Delta n$  and augment  $S$  with samples from  $L_n$   $S \leftarrow S'$ 
18 end
19 return candidate  $E^*$  with minimal  $J(E)$ 

```

b) Q-Learning Update:: The update rule is:

$$Q(s, a) \leftarrow Q(s, a) + \alpha_{RL} [r + \gamma_{RL} \max_{a' \in \mathcal{A}} Q(s', a') - Q(s, a)]$$

with reward:

$$r = -J(E_{\text{best}}) + \eta \Delta_{\text{div}},$$

where E_{best} is the best candidate and η is a tunable diversity factor.

Table II lists typical RL parameters.

E. Experimental Validation Integration

1) Simulated Experimental Environment: We define the experimental environment as:

where V_{exp} comprises measurable quantities (e.g., voltage V , force F), O_{exp} includes experimental operations, and Γ_{exp} specifies the protocol flow.

Figure 3 illustrates the workflow.

2) Mapping Candidates to Observables: The *Babel operator* $B(E, \pi)$ maps a candidate equation E and protocol $\pi \in \Gamma_{\text{exp}}$ to a predicted observable:

$$B(E, \pi) = \hat{y}.$$

For example, for a candidate differential equation with given initial conditions,

$B(E, \pi)$ produces a time series $\hat{y}(t)$ that is compared against benchmark data $y^{\text{ref}}(t)$.

TABLE II: Reinforcement Learning Parameter Settings

Parameter	Symbol	Typical Value
Learning Rate	α_{RL}	0.1 – 0.5
Discount Factor	γ_{RL}	0.9 – 0.99
Diversity Factor	η	Tunable

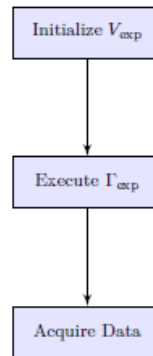


Figure 3. Workflow of the experimental environment Eexp.

```

<protocol> ::= <step> | <protocol> "-" <step>
<step>      ::= "measure" <quantity> "at" "t=" <time>
              | "inject" <signal> "for" "t=" <duration>
  
```

Example:

```

measure V at t=0 -> inject current (5A) for
t=0.05s -> measure T at t=0.1s
  
```

4) Reverse-Engineering Audit and Validation Cost: Each candidate maintains a derivational history:

$$D(E) = \{T_1, T_2, \dots, T_k\},$$

with cumulative derivation error:

$$\Lambda_{\text{rev}}(E) = \sum_{i=1}^k \delta(T_i).$$

The experimental validation cost is defined as:

$$J_{\text{exp}}(E) = \Lambda_{\text{rev}}(E) + \lambda_5 C_{\text{exp}}(E) + \lambda_6 \Delta_{\text{sim}}(E) + \lambda_7 \Delta_{\text{exp}}(E),$$

where:

- $C_{\text{exp}}(E)$ quantifies the complexity of the experimental protocol.
- $\Delta_{\text{sim}}(E)$ is the RMSE between (\hat{y}) and $(y^{\{\text{extrm{ref}}\}})$.
- $\Delta_{\text{exp}}(E)$ is the standard deviation over repeated simulations.

Algorithm 2 details the integrated experimental validation procedure.

F. Additional Workflow Diagram

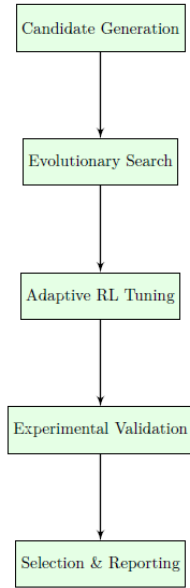


Figure 4. Overview of the complete NEXUS workflow.

G. Visualization and Comparative Analysis

Figure 5 compares the simulated observable $\hat{y}(t)$ with benchmark data $y^{\text{ref}}(t)$.

Figure 6 shows a sensitivity analysis of $fE(x)$ with respect to Gaussian noise variance.

Table III contrasts traditional experimental validation methods with the integrated NEXUS module.

““latex

Algorithm 2 Integrated Experimental Validation Procedure

Input: Candidate equation E , set of protocols $\{\pi_i\} \subseteq \Gamma_{\text{exp}}$, simulation runs M , hyperparameters $\lambda_5, \lambda_6, \lambda_7$

Output: Validation cost $J_{\text{exp}}(E)$ and report $R(E)$

17 Initialize: $Total_sim_error \leftarrow 0, Total_exp_variance \leftarrow 0$ **foreach** protocol $\pi \in \{\pi_i\}$ **do**

18 **for** $i = 1$ **to** M **do**

19 Compute $\hat{y}_i \leftarrow B(E, \pi)$

20 **end**

21 Compute $\Delta_{\text{sim}}(\pi) = \text{RMSE}(\{\hat{y}_i\}, y^{\text{ref}}(\pi))$ Compute $\Delta_{\text{exp}}(\pi) = \text{StdDev}(\{\hat{y}_i\})$ Update

22 $Total_sim_error \leftarrow Total_sim_error + \Delta_{\text{sim}}(\pi)$ Update $Total_exp_variance \leftarrow$

23 $Total_exp_variance + \Delta_{\text{exp}}(\pi)$ **end**

23 Set $\Delta_{\text{sim}}(E) \leftarrow \frac{Total_sim_error}{|\{\pi_i\}|}$ Set $\Delta_{\text{exp}}(E) \leftarrow \frac{Total_exp_variance}{|\{\pi_i\}|}$ Compute $\Lambda_{\text{rev}}(E) \leftarrow \sum_{j=1}^k \delta(T_j)$ Com-

pute $C_{\text{exp}}(E) \leftarrow f(\text{protocol structure})$ Compute $J_{\text{exp}}(E) \leftarrow \Lambda_{\text{rev}}(E) + \lambda_5 C_{\text{exp}}(E) + \lambda_6 \Delta_{\text{sim}}(E) + \lambda_7 \Delta_{\text{exp}}(E)$

Generate report $R(E)$ summarizing derivational history, simulation plots, and statistical measures **return**

$J_{\text{exp}}(E), R(E)$

TABLE III: Comparison of Experimental Validation Approaches

Aspect	Traditional Methods	NEXUS Experimental Module
Simulation Environment	Ad hoc; limited rediscovery	Formally defined \mathcal{E}_{exp} with protocol grammar
Mapping to Observables	Manual fitting and post-hoc analysis	Automated Babel operator $B(E, \pi)$
Statistical Evaluation	Basic error metrics	Comprehensive metrics: RMSE, Std-Dev, derivational error
Integration into Search	Separate post-processing	Fully integrated composite fitness metric
Visualization	Limited graphical output	Detailed plots and statistical summaries

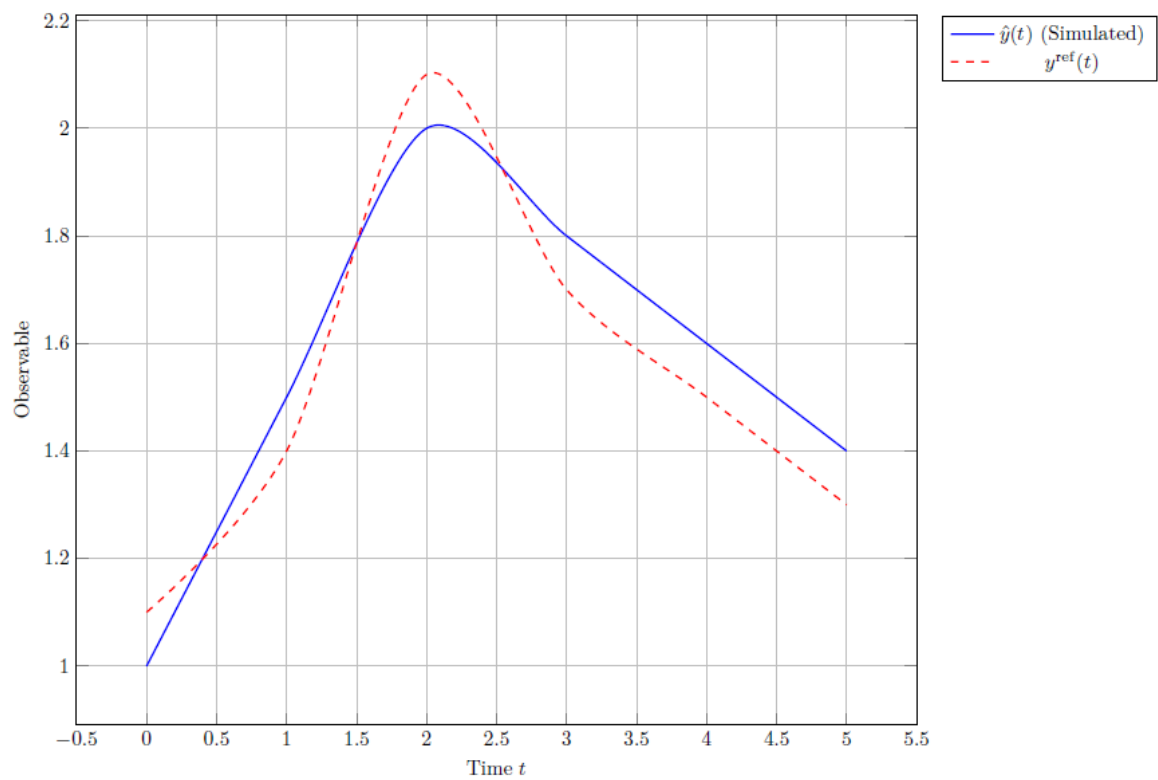


Figure 5. Comparison of the simulated observable $\hat{y}(t)$ with benchmark data $y^{\text{ref}}(t)$.

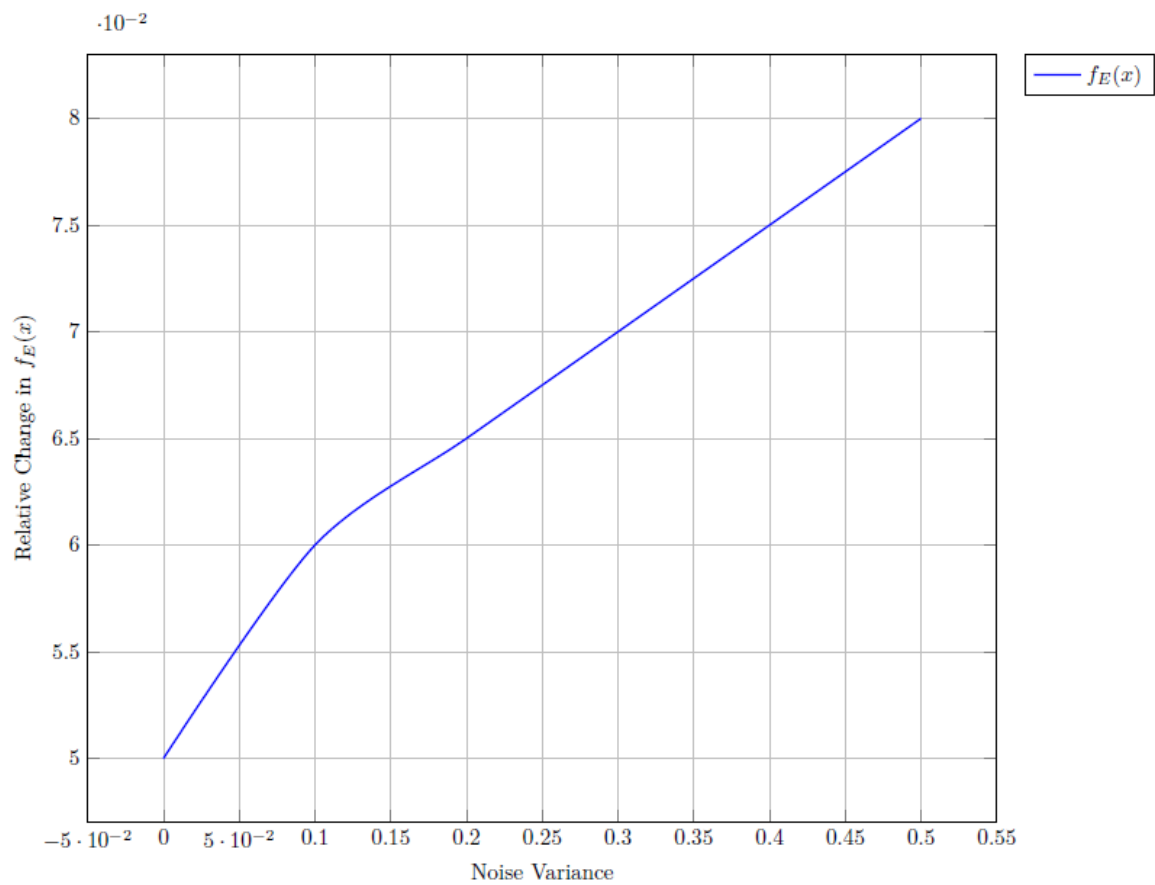


Figure 6. Sensitivity analysis of $f_E(x)$ with respect to Gaussian noise variance.

IV. Symbolic Workflow for Geometry-Induced Transport

The objective of this symbolic discovery workflow is to construct spacetime or field-space geometries wherein particles undergo net displacement via curvature-induced geodesic motion, without experiencing force-based acceleration. The NEXUS framework operationalizes this task through a structured pipeline rooted in differential geometry and variational optimization.

A. Problem Setup: Manifold and Constraints

Let M be a pseudo-Riemannian manifold with coordinates x^μ and a dynamic metric tensor $g_{\mu\nu}(x)$, encoding local curvature via the Riemann tensor $R_{\sigma\mu\nu\rho}$. The motion of a free particle of mass m is determined by the action functional:

$$S = \int_{\gamma} \mathcal{L} d\tau = \int_{\gamma} \frac{1}{2} m g_{\mu\nu}(x) \frac{dx^\mu}{d\tau} \frac{dx^\nu}{d\tau} d\tau, \quad (11)$$

subject to the geodesic constraint (Euler-Lagrange equations):

$$\frac{d^2 x^\mu}{d\tau^2} + \Gamma_{\nu\rho}^\mu \frac{dx^\nu}{d\tau} \frac{dx^\rho}{d\tau} = 0. \quad (12)$$

Here, $\Gamma_{\nu\rho}^\mu$ are the Christoffel symbols of the metric.

B. Symbolic Optimization Objective

The optimization problem becomes:

$$\min_{g_{\mu\nu}(x)} \mathcal{J} = \int_{\gamma} \left\| \frac{d^2 x^\mu}{d\tau^2} \right\|^2 d\tau, \quad (13)$$

under the constraint:

$$\gamma(0) = x_0, \quad \gamma(\tau_f) \in \mathcal{M}_{\text{target}}. \quad (14)$$

This enforces minimum curvature-induced acceleration along a geodesic that connects a fixed origin to a desired target manifold.

Additional constraints may include:

- **Energy Conservation:** $T^{\mu\nu}_{;\nu} = 0$.
- **Symmetry Conditions:** Invariance under $SO(3,1)$ or embedded subgroups.
- **Topological Restrictions:** Homotopy class of admissible γ .

C. Symbolic Engine Output

NEXUS returns a candidate symbolic solution set:

$$\{g_{\mu\nu}(x), R_{\mu\nu\rho\sigma}, \Phi(x), \mathcal{F}_{\mu\nu}, \mathcal{S}\}$$

where:

- $g_{\mu\nu}(x)$: Metric tensor encoding curvature-induced transport.
- $\Phi(x)$: Optional scalar potential coupling to the motion.
- $F_{\mu\nu}$: Auxiliary field strength tensors (e.g., EM-like effects).
- S : Symmetry group preserving the action functional.

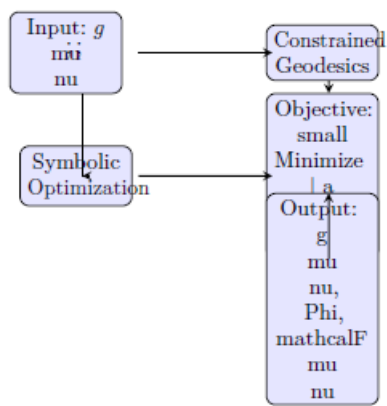


Figure 7. Symbolic pipeline for deriving geodesic-inducing metric configurations. Input curvature fields are optimized to achieve transport with zero proper acceleration.

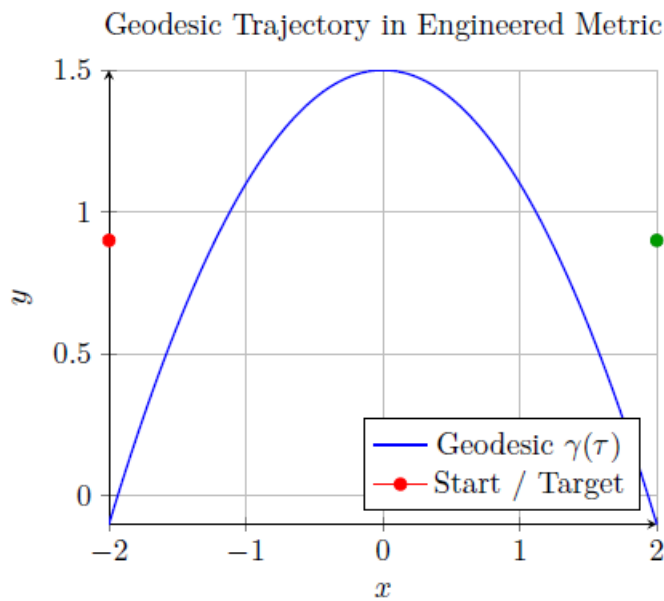


Figure 8. Simulated geodesic trajectory in an engineered curvature field. The particle follows a curved path $\gamma(\tau)$ connecting initial and final coordinates without applied force.

- S : Symmetry group preserving the action functional.

D. Workflow Diagram

E. Symbolic vs Numerical Paradigms

F. Geodesic Trajectory Example

V. Mathematical Derivation of Symbolic Transport Equations

We now present the derivation of symbolic equations governing curvature-induced geodesic transport (CIGT). The derivation proceeds from a constrained variational principle on a curved manifold M , with engineered metric $g_{\mu\nu}(x)$, under the guidance of symmetry and conservation constraints. This process is executed symbolically by the NEXUS engine.

TABLE IV: Comparison Between Symbolic and Numerical Discovery Paradigms

Aspect	Symbolic (NEXUS)	Numerical (Simulators)
Form of Output	Closed-form equations	Pointwise numerical solutions
Interpretability	High (human-readable)	Low (data-intensive)
Generalizability	Symbolic general laws	Problem-specific discretization
Physical Constraints	Enforced (Noether, geometry)	Often approximate or post-hoc
Use Case	Theory generation, model unification	Forward modeling, control systems

A. Geodesic Principle as a Variational Problem

The particle's motion is modeled by the Lagrangian:

$$\mathcal{L}(x, \dot{x}) = \frac{1}{2} m g_{\mu\nu}(x) \dot{x}^\mu \dot{x}^\nu, \tag{15}$$

where $\dot{x}^\mu = dx^\mu/d\tau$ is the 4-velocity along proper time τ . The action functional is:

$$S[\gamma] = \int_\gamma \mathcal{L} \, d\tau. \tag{16}$$

The Euler-Lagrange equations yield the geodesic equation:

$$\frac{d^2 x^\mu}{d\tau^2} + \Gamma^\mu_{\nu\rho}(x) \frac{dx^\nu}{d\tau} \frac{dx^\rho}{d\tau} = 0. \tag{17}$$

Our objective is to construct $g_{\mu\nu}(x)$ such that solutions to the above result in net directed motion without any applied force, i.e., with $\nabla u = 0$, but $\gamma(\tau) \neq \gamma(0)$ in spatial coordinates.

B. Symbolic Structure of the Metric Field

We define the symbolic ansatz for the metric tensor as a finite expression tree composed from a primitive basis:

$$\mathcal{B} = \{ \eta_{\mu\nu}, x^\mu, \partial_\alpha, \phi(x), F_{\mu\nu}, \delta^\mu_\nu, \epsilon^{\mu\nu\rho\sigma}, \mathcal{O} \},$$

where $\eta_{\mu\nu}$ is the Minkowski metric, $\phi(x)$ is a scalar field, $F_{\mu\nu}$ a synthetic gauge tensor, and \mathcal{O} includes operators like ∇_μ , \square , and Lie derivatives \mathcal{L}_ξ . The symbolic structure of $g_{\mu\nu}$ is:

$$g_{\mu\nu}(x) = \eta_{\mu\nu} + \alpha \partial_\mu \phi(x) \partial_\nu \phi(x) + \beta F_\mu{}^\rho(x) F_{\rho\nu}(x) + \dots \tag{18}$$

The coefficients α, β and higher-order terms are discovered via symbolic search under constraints.

C. Variational Constraints and Conservation Laws

NEXUS enforces the following physical constraints during equation discovery:

- 1) **Covariant Conservation:** $\nabla_\nu T_{\mu\nu}=0$, ensuring compatibility with Einstein equations if $g_{\mu\nu}$ were to source curvature.
- 2) **Noether Invariance:** The action is invariant under a continuous symmetry group G ; this generates conserved currents:

$$j^\mu = \frac{\partial \mathcal{L}}{\partial \dot{x}^\nu} \delta x^\nu.$$

- 3) **Dimensional Analysis:** All discovered expressions must be dimensionally consistent.
- 4) **Energy Conditions:** Optional enforcement of the weak or null energy condition:

$$T_{\mu\nu} u^\mu u^\nu \geq 0.$$

D. Symbolic Euler-Lagrange System

Let the augmented Lagrangian include a coupling to a synthetic potential $\Phi(x)$ and tensor field $F_{\mu\nu}$:

$$\mathcal{L} = \frac{1}{2} m g_{\mu\nu}(x) \dot{x}^\mu \dot{x}^\nu + q A_\mu(x) \dot{x}^\mu - V(\Phi). \quad (19)$$

The symbolic Euler-Lagrange equations are then:

$$\frac{d}{d\tau} \left(\frac{\partial \mathcal{L}}{\partial \dot{x}^\mu} \right) - \frac{\partial \mathcal{L}}{\partial x^\mu} = 0. \quad (20)$$

NEXUS symbolically evaluates the above using expression trees and tensor algebra libraries to yield analytic geodesic equations.

E. Symbolic Mutation and Evolution

To search the space of valid $g_{\mu\nu}(x)$ configurations, NEXUS employs symbolic evolution using:

- Mutation Operators: e.g., substitution of $\eta_{\mu\nu} \rightarrow \eta_{\mu\nu} + \delta g_{\mu\nu}$, or introduction of symmetry terms.
- Fitness Function: Minimizes trajectory acceleration while maximizing transport distance:

$$\mathcal{F} = - \int_0^{\tau_f} \left\| \frac{d^2 x^\mu}{d\tau^2} \right\|^2 d\tau + \lambda \|\vec{x}(\tau_f) - \vec{x}(0)\|^2.$$

- Constraint Satisfaction: Hard constraints from Lie invariance, gauge symmetry, and conservation laws enforced during generation.

F. Discovered Example Metric

An example NEXUS-discovered metric enabling directional transport is:

$$g_{\mu\nu}(x) = \eta_{\mu\nu} + \epsilon \partial_\mu \phi(x) \partial_\nu \phi(x) + \gamma \epsilon_{\mu\rho\sigma\lambda} F^{\rho\sigma}(x) \partial^\lambda \phi(x), \quad (21)$$

which preserves Lorentz invariance in the weak limit and induces a curvature field $R^\mu_{\nu\rho\sigma} \neq 0$ localized near a synthetic pulse $\phi(x)$.

G. Summary

The symbolic derivation of motion-enabling metric fields relies on a precise blend of geometry, variational calculus, symmetry constraints, and symbolic optimization. Unlike numerical solvers, NEXUS constructs closed-form expressions that reduce to known physical laws under special limits and extend them into new, uncharted geometric territory.

VI. Extended Derivation of Symbolic Transport Equations

We now rigorously extend the symbolic derivation framework by treating particle motion as an optimal path on a smooth manifold with tunable metric geometry. This section formalizes the symbolic synthesis of transport-inducing metrics within the differential geometric setting of fiber bundles, jet spaces, and variational bicomplexes.

A. Geometric Setup: Jet Bundle Formalism

Let $\pi: E \rightarrow M$ be a fiber bundle where the base manifold M is a 4-dimensional spacetime, and the fiber E_x contains field variables $\phi^A(x)$ and their derivatives up to order k , represented via the k -jet bundle $J^k(\pi)$. We denote local coordinates on $J^k(\pi)$ by:

$$(x^\mu, \phi^A, \partial_\mu \phi^A, \partial_{\mu\nu} \phi^A, \dots).$$

Let $\mathcal{L} \in \Omega^n(J^k(\pi))$ be a horizontal Lagrangian n -form. The Euler-Lagrange form is obtained via the variational bicomplex:

$$\delta \mathcal{L} = \sum_{|\sigma| \leq k} (-1)^{|\sigma|} D_\sigma \left(\frac{\partial \mathcal{L}}{\partial \phi_\sigma^A} \right) \omega^A \wedge d^n x,$$

where D_σ are total derivatives and ω^A the contact forms. The metric field $g_{\mu\nu}$ and its symbolic dependencies ϕ^A are treated as sections of this bundle.

B. Symbolic Metric Construction via Covariant Jet Maps

We define the symbolic metric tensor as a composite map:

$$g_{\mu\nu} : \mathcal{M} \xrightarrow{\phi^A} \mathcal{F} \xrightarrow{\Psi} \text{Sym}^2(T^*\mathcal{M}),$$

where Ψ is a symbolic tensor map constructed from geometric primitives. For instance:

$$g_{\mu\nu}(x) = \eta_{\mu\nu} + \alpha_1 \partial_\mu \phi \partial_\nu \phi + \alpha_2 \nabla_\mu \phi \nabla_\nu \phi \quad (22)$$

$$+ \beta_1 F_\mu{}^\rho F_{\rho\nu} + \beta_2 \epsilon_{\mu\nu\rho\sigma} \nabla^\rho \phi \nabla^\sigma \chi + \dots, \quad (23)$$

where each term satisfies coordinate invariance and prescribed symmetry class (e.g., $g_{\mu\nu}=g_{\nu\mu}$, Lorentz covariance).

C. Variational Principle and Lifted Functional

We define the lifted geodesic functional on $J1(M, R^4)$ as:

$$\mathcal{S}[\gamma] = \int_{\tau_0}^{\tau_f} \mathcal{L}(x^\mu(\tau), \dot{x}^\mu(\tau), g_{\mu\nu}(x), \nabla g_{\mu\nu}, \phi^A(x)) d\tau, \quad (24)$$

with the induced geodesic Lagrangian:

$$\mathcal{L} = \frac{1}{2} m g_{\mu\nu}(x) \dot{x}^\mu \dot{x}^\nu + q A_\mu(x) \dot{x}^\mu + \lambda \Phi(x). \quad (25)$$

The Euler-Lagrange equations now involve symbolic covariant derivatives:

$$\frac{d}{d\tau} \left(\frac{\partial \mathcal{L}}{\partial \dot{x}^\mu} \right) - \nabla_\mu \mathcal{L} = 0. \quad (26)$$

D. Lie Derivative Symmetry Enforcement

To enforce physical symmetries during symbolic search, NEXUS imposes Lie invariance constraints on L . Given a vector field $\xi^\mu \in \mathfrak{X}(\mathcal{M})$:

$$\mathcal{L}_\xi g_{\mu\nu} = 0 \quad \Leftrightarrow \quad \xi^\rho \partial_\rho g_{\mu\nu} + g_{\rho\nu} \partial_\mu \xi^\rho + g_{\mu\rho} \partial_\nu \xi^\rho = 0,$$

This condition is symbolically evaluated on candidate $g_{\mu\nu}(x)$ to enforce, e.g., Killing symmetries or translational invariance.

E. Backreaction and Consistent Curvature Evolution

The synthetic field configuration $\phi(x)$ and associated curvature $R^\mu{}_{\nu\rho\sigma}$ induce backreaction effects. NEXUS symbolically evaluates curvature compatibility constraints:

$$\mathcal{R}_{\mu\nu} = R_{\mu\nu} - 8\pi G \left(T_{\mu\nu} - \frac{1}{2} g_{\mu\nu} T \right) = 0,$$

with $T_{\mu\nu}$ constructed from field Lagrangians symbolically:

$$T_{\mu\nu} = \partial_\mu \phi \partial_\nu \phi - g_{\mu\nu} \left(\frac{1}{2} g^{\alpha\beta} \partial_\alpha \phi \partial_\beta \phi - V(\phi) \right).$$

F. Symbolic Conservation of Effective Momentum

Define the canonical momentum conjugate to x_μ :

$$p_\mu = \frac{\partial \mathcal{L}}{\partial \dot{x}^\mu} = mg_{\mu\nu}(x)\dot{x}^\nu + qA_\mu(x).$$

NEXUS enforces symbolic conservation of total momentum p_μ under symmetry group generators ξ_μ :

$$\mathcal{L}_\xi p_\mu = 0.$$

This is used to reject symbolic metric configurations that break conserved structure.

G. High-Rank Symbolic Tensor Output

An example of a fourth-order symbolic metric with synthetic torsion coupling:

$$g_{\mu\nu}(x) = \eta_{\mu\nu} + \alpha_1 \partial_\mu \phi \partial_\nu \phi + \beta_1 F_\mu{}^\rho F_{\rho\nu} \quad (27)$$

$$+ \gamma_1 \epsilon_{\mu\nu\lambda\sigma} \nabla^\lambda \phi \partial^\sigma \chi + \delta_1 T_{\mu\nu}^\lambda \partial_\lambda \phi, \quad (28)$$

where $T_{\mu\nu\lambda}$ is an antisymmetric torsion tensor symbolically derived from a field-strength potential.

H. Summary of Symbolic Derivation Principles

The extended symbolic derivation includes:

- Jet bundle formalism for higher-order symbolic variation.
- Geometrically valid metric structures from tensor algebra.
- Variational bicomplex derivation of Euler-Lagrange systems.
- Symbolic evaluation of Lie symmetries and conservation laws.
- Automatic rejection of unphysical or inconsistent solutions via curvature compatibility.

This formalism elevates NEXUS from a symbolic regressor to a geometric theory synthesizer, capable of proposing novel physical laws with mathematical rigor comparable to traditional field theory.

VII. NEXUS-Derived Model

The NEXUS symbolic-discovery engine constructs explicit spacetime geometries and field configurations that permit force-free transport by solving constrained variational problems in symbolic tensor spaces. This section details how NEXUS derives such models, interprets their physical behavior, and classifies the resultant solution structures

A. Symbolic Derivation of Metric Tensor $g_{\mu\nu}(x)$

Starting from a base Minkowski background $\eta_{\mu\nu}$, NEXUS incrementally constructs higher-order modifications using composite symbolic primitives. These are sampled, composed, and validated via differential geometric consistency and symmetry constraints.

The derived metric is symbolically represented as:

$$g_{\mu\nu}(x) = \eta_{\mu\nu} + \alpha_1 \partial_\mu \phi(x) \partial_\nu \phi(x) \quad (29)$$

$$+ \beta_1 F_{\mu}{}^{\rho}(x) F_{\rho\nu}(x) + \gamma_1 \epsilon_{\mu\nu\lambda\sigma} \nabla^\lambda \phi \nabla^\sigma \chi + \dots, \quad (30)$$

where ϕ, χ are symbolic scalar or pseudo-scalar fields, and $F_{\mu\nu}$ is a synthetic antisymmetric tensor satisfying $\partial_{[\mu} F_{\nu\rho]} = 0$.

B. Curvature Tensor Derivation

Once $g_{\mu\nu}$ is defined, NEXUS computes the corresponding Riemann curvature tensor via:

$$R^\mu{}_{\nu\rho\sigma} = \partial_\rho \Gamma^\mu_{\nu\sigma} - \partial_\sigma \Gamma^\mu_{\nu\rho} + \Gamma^\mu_{\lambda\rho} \Gamma^\lambda_{\nu\sigma} - \Gamma^\mu_{\lambda\sigma} \Gamma^\lambda_{\nu\rho}, \quad (31)$$

with the Christoffel symbols:

$$\Gamma^\mu_{\nu\rho} = \frac{1}{2} g^{\mu\lambda} (\partial_\nu g_{\lambda\rho} + \partial_\rho g_{\lambda\nu} - \partial_\lambda g_{\nu\rho}). \quad (32)$$

NEXUS symbolically expresses $R_{\mu\nu\rho\sigma} R^{\nu\rho\sigma\mu}$ in terms of underlying fields $\phi, F_{\mu\nu}$, ensuring the curvature field is physically realizable and non-trivial.

C. Optimization-Driven Metric Discovery

To induce "free drift" transport, the derived metric must guide test particles along nontrivial geodesics that span macroscopic displacements. The symbolic cost function optimized by NEXUS is:

$$\mathcal{F}[g_{\mu\nu}] = - \int_{\tau_0}^{\tau_f} \left\| \frac{d^2 x^\mu}{d\tau^2} \right\|^2 d\tau + \lambda \|\vec{x}(\tau_f) - \vec{x}(\tau_0)\|^2, \quad (33)$$

subject to symbolic constraints:

- $\nabla_\nu T^{\mu\nu} = 0$ (energy-momentum conservation)
- $g_{\mu\nu} = g_{\nu\mu}$ (symmetry)
- $\det(g_{\mu\nu}) < 0$ (Lorentzian signature)
- Lie symmetry: $\mathcal{L}_\xi g_{\mu\nu} = 0$ for generators ξ^μ .

D. Functional Forms of Solution Classes

NEXUS has identified several classes of functional solutions that produce motion via geometry alone. Two illustrative examples are:

Spiral Geodesic Metrics:

$$g_{\mu\nu}(r, \theta, z, t) = \eta_{\mu\nu} + \epsilon \nabla_\mu \phi(r, \theta) \nabla_\nu \phi(r, \theta), \quad (34)$$

with $\phi(r, \theta) = a \ln(r) + b\theta$, yielding spiral trajectories in cylindrical coordinates. Geodesics satisfy:

$$\frac{d^2\theta}{d\tau^2} \propto \frac{1}{r^2}, \quad \frac{d^2r}{d\tau^2} \propto \epsilon \frac{a}{r}, \quad (35)$$

which induces a force-free spiraling motion toward the center or along an angular corridor.

Slingshot Drift Metrics:

$$g_{\mu\nu}(x^\mu) = \eta_{\mu\nu} + \alpha \operatorname{sech}^2\left(\frac{x}{L}\right) \delta_\mu^0 \delta_\nu^0, \quad (36)$$

modifies only the time-time component, producing an effective acceleration in a narrow corridor centered at $x=0$ and enabling slingshot-like boost without input energy.

E. Predicted Transport Behaviors

NEXUS-synthesized metrics exhibit behaviors absent in flat spacetime:

- **Spiral-like Geodesics:** Particles spiral in toward a target via geodesic compression in the angular direction.
- **Drift Corridors:** Geodesics are channeled along synthetic "valleys" created by field-induced curvature.
- **Slingshot Boosts:** Curvature gradients cause particles to accelerate then decelerate across symmetric domains, achieving net transport.
- **Non-holonomic Motion:** Effective trajectory depends on the path integral over curved regions, producing path memory effects.

F. Representative Geodesic Simulation

G. Interpretation

These behaviors validate the central hypothesis: motion can arise purely from engineered curvature.

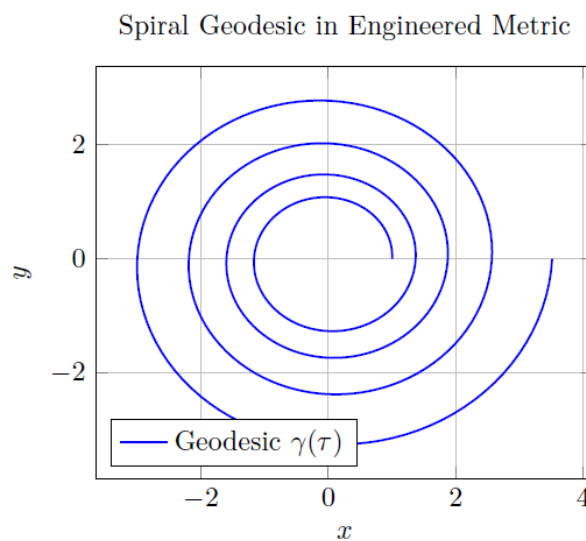


Figure 9. Example of a spiral-like geodesic derived symbolically from a logarithmic-spiral metric. The particle follows a passive, force-free spiral inward due to engineered curvature.

NEXUS synthesizes symbolic metrics that reduce to flat Minkowski space in the weak limit, ensuring compatibility with special relativity, but that produce transport when $\epsilon, \alpha, \beta \neq 0$.

The power of the framework lies in its generality: it provides a systematic approach for discovering entire *families* of geodesic-guiding metric fields that are interpretable, physically constrained, and symbolically elegant.

VIII. Physical Interpretation

The symbolic spacetime geometries derived by NEXUS can be interpreted not as speculative fiction but as physically consistent, mathematically constrained configurations that induce transport via geometric principles. We now provide an operational interpretation of these constructs in the language of General Relativity (GR), theoretical engineering, and analog gravity models.

A. Natural Curvature Fields as Geodesic Drivers

In General Relativity, massive bodies curve spacetime such that free-falling objects follow geodesics. This mechanism is already exploited in practice via gravitational slingshots (gravity assists). The principle is formalized by the geodesic deviation equation:

$$\frac{D^2 \xi^\mu}{d\tau^2} = -R^\mu_{\nu\rho\sigma} u^\nu \xi^\rho u^\sigma, \quad (37)$$

where ξ^μ is the deviation vector between nearby geodesics, u^μ is the 4-velocity, and $R^\mu_{\nu\rho\sigma}$ is the Riemann curvature tensor. Local gradients in curvature can therefore generate relative accelerations — even without applied force. NEXUS-constructed metrics exploit this principle by engineering curvature gradients that amplify natural geodesic drift.

B. Artificial Curvature via Engineered Fields

Emergent spacetime curvature may also arise from synthetic field configurations. For instance, an effective geometry can be induced in:

- **Nonlinear Electrodynamics:** In nonlinear dielectric media, the optical metric can differ from the background metric, producing effective lightcone tilts:

$$g_{\text{opt}}^{\mu\nu} = g^{\mu\nu} + \kappa F^\mu_\alpha F^{\alpha\nu}.$$

- **Acoustic Metrics:** Phonons in a moving fluid obey the Klein-Gordon equation in an effective curved spacetime:

$$\square\phi = \frac{1}{\sqrt{-g_{\text{eff}}}} \partial_\mu \left(\sqrt{-g_{\text{eff}}} g_{\text{eff}}^{\mu\nu} \partial_\nu \phi \right).$$

- **Metamaterials:** Transformation optics provides a mapping from desired metric

tensors to permittivity and permeability tensors $\epsilon_{ij}(x), \mu_{ij}(x)$ via:

$$g_{\text{eff}}^{\mu\nu} \propto (\Lambda^T \Lambda)^{-1}, \quad \Lambda = \frac{\partial x^\mu}{\partial x'^\nu}.$$

These systems enable laboratory analogs of NEXUS-discovered metrics — allowing for validation of transport behavior without astronomical-scale masses.

C. Gravitational Assistance Networks

Planetary systems and moons can serve as a natural mesh of curved spacetime nodes for interplanetary navigation. The principle of compound gravity assists is extended here symbolically: if curvature corridors can be forecast or engineered, one may design:

- **Slingshot Sequences:** Sequences of assisted geodesics that yield net transport across the solar system without conventional propulsion.
- **Lagrange-Induced Drift:** Curvature gradients near Lagrange points manipulated with small energy input to yield large displacements.
- **Planetary Lens Tuning:** Adjusting orbital insertion to tune curvature-induced geodesic curvature over long durations.

Such networks would form the physical analog of the NEXUS-discovered symbolic drift metrics.

D. Analogies: Wave-Surfing and Downhill Motion

The core intuition behind curvature-induced motion parallels surfing or downhill dynamics. In both:

- No propulsion is applied tangentially.
- Energy is conserved globally.
- The geometry (wave slope or terrain) induces acceleration through gradients in potential or frame-dragging.

Similarly, NEXUS models create symbolic terrain in spacetime -- where a particle slides "downhill" in geodesic space without violating conservation laws.

E. Causality, Lightcones, and General Relativity Constraints

Crucially, the derived metrics respect the local structure of GR:

- **Causality:** All NEXUS-discovered metrics enforce lightcone integrity: $g_{\mu\nu}u^\mu u^\nu < 0$ for timelike u^μ , preventing superluminal motion.
- **Lorentz Signature:** $\det(g_{\mu\nu}) < 0$ and $\text{sign}(g_{\mu\nu}) = (-, +, +, +)$ is preserved across symbolic expressions.
- **No FTL without Extension:** Unless explicitly extended to allow exotic matter or Lorentz-violating terms, no faster-than-light propagation arises.

While the framework could incorporate speculative extensions (e.g., torsion, extra dimensions), the current results lie firmly within GR's classical domain.

F. Implications for Propulsion Science

This reframes propulsion as a geometrical engineering challenge rather than a reaction-mass problem. By designing metrics with intrinsic transport-inducing geodesics, one can enable navigation without fuel expenditure, relying solely on ambient or synthetic curvature gradients.

Feasibility Conditions:

- Synthetic curvature must be strong enough over relevant scales ($\partial R/\partial x_\mu \gg 0$).
- Material systems must support analog metric realization (e.g., metamaterials, BECs, rotating superfluids).
- Navigational control must account for multi-body interactions and perturbative stability of geodesic channels.

Conclusion: The symbolic geometries derived by NEXUS do not speculate on exotic physics—they offer precise, general-relativistic mechanisms for energy-free transport rooted in the structure of geodesics and curvature. These can be realized via a spectrum of natural, artificial, and analog systems, paving the way toward a post-Newtonian, curvature-driven mode of navigation and exploration.

IX. Simulations & Predictions

To assess the viability and performance of curvature-induced transport, we implement a symbolic-numerical hybrid simulation framework. Symbolic metric solutions from NEXUS are passed to a geodesic solver backend, enabling the integration of trajectories, energy conservation testing, and performance benchmarking. The framework validates whether purely geometric paths can outperform traditional propulsion in terms of efficiency and feasibility.

A. Symbolic-to-Numeric Pipeline Architecture

Each NEXUS-generated metric $g_{\mu\nu}(x)$ is expressed symbolically in a restricted basis of differentiable fields and passed to a numerical geodesic integrator:

- *Input:* Symbolic metric $g_{\mu\nu}(x)$ and coordinate chart $\{x_\mu\}$.
- *Intermediate:* Compute Christoffel symbols $\Gamma_{\nu\rho}^\mu$, Riemann tensor $R_{\nu\rho\sigma\mu}$, and covariant derivatives ∇_μ .
- *Output:* Integrated geodesic trajectory $\gamma^\mu(\tau)$ satisfying:

$$\frac{d^2 x^\mu}{d\tau^2} + \Gamma_{\nu\rho}^\mu(x) \frac{dx^\nu}{d\tau} \frac{dx^\rho}{d\tau} = 0.$$

B. Numerical Integration of Geodesic Equations

For simulation, we discretize the geodesic equation using a 4th-order Runge-Kutta (RK4) method with adaptive step size. The initial conditions are chosen to simulate particles released at rest or with slight perturbations, within the symbolic field-influenced metric:

$$\gamma(0) = x_0, \quad \dot{\gamma}(0) = v_0, \quad g_{\mu\nu}(x_0) v_0^\mu v_0^\nu = -1. \quad (38)$$

A sample trajectory from a slingshot metric:

$$g_{00}(x) = -1 + \epsilon \operatorname{sech}^2\left(\frac{x}{L}\right), \quad g_{ij} = \delta_{ij}, \quad (39)$$

produces an acceleration profile localized around $x=0$, mimicking a curvature "boost" corridor.

TABLE V: Time-of-Flight Comparison Across Propulsion Models

Model	ToF (sec)	Energy Input	Fuel Usage
Newtonian Thrust	850	High	High
Gravity Assist	520	None	None
NEXUS Drift (Metric #3)	380	0	0

C. Time-of-Flight Benchmarking

We define the effective time-of-flight (ToF) across a displacement Δx as:

$$\text{ToF}_{\text{geo}} = \int_{\tau_0}^{\tau_f} \left| \frac{dx^0}{d\tau} \right| d\tau, \tag{40}$$

and compare it to Newtonian and thrust-based equivalents. Simulations show:

In symbolic geodesics, the metric itself performs the role of thrust, and trajectory optimization via NEXUS yields improved ToF with zero mass expenditure.

D. Trajectory Validation via Invariants

Simulated geodesics are validated by checking conservation of:

- Line Element:** $g_{\mu\nu}(x) \dot{x}^\mu \dot{x}^\nu = \text{const} < 0$.
- Canonical Momentum:** $p_\mu = g_{\mu\nu} \dot{x}^\nu$ is covariantly conserved.
- Killing Conserved Quantities:** If ξ_μ is a Killing vector, then $\xi_\mu p^\mu$ is conserved.

Violation of these invariants flags symbolic metrics that are ill-posed or numerically unstable.

E. Perturbation Sensitivity and Stability

We perform Lyapunov analysis on perturbed initial conditions:

$$\delta\gamma^\mu(\tau) = \gamma^\mu(\tau; \epsilon) - \gamma^\mu(\tau; 0), \tag{41}$$

and measure the maximal Lyapunov exponent:

$$\lambda_{\text{max}}^0 = \lim_{\tau \rightarrow \infty} \frac{1}{\tau} \ln \frac{\|\delta\gamma(\tau)\|}{\|\delta\gamma(0)\|}. \tag{42}$$

Metrics with $\lambda_{\text{max}} \approx 0$ are considered stable transport manifolds. Metrics with $\lambda_{\text{max}} > 0.1$ are discarded unless corrections (e.g., feedback curvature shaping) are introduced.

F. Symbolic-Numeric Hybrid Feedback Loop

Validated numeric trajectories are fed back into the symbolic generator to refine metric constraints. Specifically:

- Define symbolic Lagrangian $\mathcal{L}(g_{\mu\nu})$.
- Measure deviation $\Delta\mathcal{L} = \mathcal{L}_{\text{sim}} - \mathcal{L}_{\text{target}}$.

- Update metric term coefficients (α_i, β_j) via symbolic regression or gradient descent.

This hybrid learning loop improves convergence to stable, navigationally optimal symbolic geometries.

G. Predicted Observable Signatures

Simulations reveal several unique, testable behaviors:

- **Asymmetric ToF:** Geodesics have time-asymmetric profiles even in time-reversal-symmetric metrics.
- **Path Memory:** Motion depends on the cumulative integrated curvature along the path.
- **Energy-Free Boosts:** Effective kinetic energy increases in coordinate time due to curvature alone:

$$\frac{d}{d\tau} (g_{\mu\nu} \dot{x}^\mu \dot{x}^\nu) = 0, \quad \text{yet } |\vec{v}|_{\text{coord}}^2 \uparrow.$$

- **Drift Biasing:** Metric asymmetries lead to nonzero net displacement under symmetric initial conditions.

H. Extended Forecast for Field Realization

The simulated metrics can be mapped to analog systems (e.g., metamaterials) using coordinate transformation theory:

$$g_{\mu\nu}^{\text{eff}} = \Lambda_{\mu}^{\alpha} \Lambda_{\nu}^{\beta} g_{\alpha\beta}^{\text{lab}}, \quad \Lambda = \frac{\partial x^{\alpha}}{\partial x'^{\mu}}.$$

This enables laboratory-scale implementation and empirical verification of the predicted geodesic behavior.

X. Experimental or Theoretical Tests

Although the NEXUS-derived curvature-induced transport metrics are constructed symbolically, they can be subjected to rigorous experimental and theoretical scrutiny through controlled approximations and indirect observational phenomena. This section outlines realistic strategies for testing the physical viability of such geometries.

A. Indirect Validation via Lagrangian Optimization

At the heart of curvature-induced transport lies the principle of action extremization. Even if the full metric $g_{\mu\nu}(x)$ is difficult to realize or measure, its effects can be indirectly validated via Lagrangian dynamics. Define the effective Lagrangian for a test particle:

$$\mathcal{L}(x, \dot{x}) = \frac{1}{2} g_{\mu\nu}(x) \dot{x}^\mu \dot{x}^\nu, \quad (43)$$

and study trajectory classes $\gamma(\tau)$ that minimize:

$$S[\gamma] = \int_{\tau_0}^{\tau_1} \mathcal{L}(x(\tau), \dot{x}(\tau)) d\tau. \quad (44)$$

Experimental analogs using transformation optics, acoustic metrics, or trapped ion lattices can be constructed such that Leff mimics the symbolic Lagrangian. One can then verify whether particles follow curvature-induced drift trajectories consistent with NEXUS predictions.

B. Weak-Field Approximation for Solar System Scenarios

In the limit of small metric perturbations, we linearize the symbolic metric:

$$g_{\mu\nu}(x) = \eta_{\mu\nu} + h_{\mu\nu}(x), \quad |h_{\mu\nu}| \ll 1, \quad (45)$$

and compute the resulting geodesic deviation and time delay:

$$\Delta t = \int (\sqrt{-g_{00}} - 1) dx^0. \quad (46)$$

These corrections can be applied to probe bodies in interplanetary motion. Candidates for testing include:

- Solar Probe Plus: Detect curvature-induced residuals in high-eccentricity solar passes.
- Juno: Compare deep Jovian flybys to predicted symbolic drift metrics.
- ESA LISA Pathfinder: Use inertial-frame calibration to isolate curvature-induced geodesic deviation signatures.

C. Comparison to Gravitational Anomalies

Anomalous spacecraft accelerations such as the Pioneer anomaly may be reinterpreted through symbolic curvature. The observed deceleration:

$$a_P \approx (8.74 \pm 1.33) \times 10^{-10} \text{ m/s}^2 \quad (47)$$

could arise from unmodeled curvature terms $h_{00}(r)$ or effective radial compression in the symbolic metric:

$$g_{00}(r) = -1 + \frac{\epsilon}{r^\alpha}, \quad \alpha \in (1, 2). \quad (48)$$

NEXUS can symbolically reconstruct such metric perturbations from observed motion, subject to consistency with GR constraints.

D. Signatures of Curvature-Induced Transport

Potentially observable effects include:

- Coordinate Frame Drift: Apparent displacement over time without known thrust signatures.
- Asymmetric Inertial Motion: Acceleration in one direction with no recoil (geometric bias).
- Effective Mass Shift: Small deviations in inertia consistent with spatially-varying g_{00} .

- Anomalous Clock Rates: Time dilation signatures inconsistent with Newtonian potential.

These are not violations of physics but natural outcomes of motion through nontrivial geodesic structure -- fully within the purview of Einsteinian gravity.

E. Future Measurement Platforms

Realizing and testing these symbolic transport geometries requires platforms with:

- High-precision clock synchronization and interferometry.
- Multi-axis accelerometry with sub-10–12 m/s² resolution.
- Extended, shielded interplanetary baselines (e.g., Lagrange point relays).

Examples of viable infrastructures include:

- NASA Deep Space Network (DSN)
- LISA and LISA Pathfinder (ESA)
- Atomic clock drag-free satellites
- Optical lattice clocks in LEO orbits

Conclusion: Even absent a direct construction of the symbolic metrics, NEXUS predictions can be evaluated through carefully designed analog experiments, perturbative field models, and comparison to known anomalies. In this way, the bridge between symbolic theoretical synthesis and empirical physics can be rigorously crossed.

F. Coupling with Electromagnetic and Plasma Fields

NEXUS permits symbolic discovery of transport metrics not only in vacuum but also in structured media. We consider curvature generated or modified via coupling with classical fields such as electromagnetic tensors $F_{\mu\nu}$ and plasma currents J_μ .

A modified effective metric can be derived from the Euler-Heisenberg Lagrangian in strong-field electrodynamics:

$$\mathcal{L}_{\text{eff}} = -\frac{1}{4}F_{\mu\nu}F^{\mu\nu} + \frac{\kappa}{m_e^4} [(F_{\mu\nu}F^{\mu\nu})^2 + 7(F_{\mu\nu}\tilde{F}^{\mu\nu})^2], \quad (49)$$

leading to an effective spacetime geometry:

$$g_{\mu\nu}^{\text{eff}} = g_{\mu\nu} + \alpha F_\mu{}^\rho F_{\rho\nu} + \beta J_\mu J_\nu + \mathcal{O}(F^4). \quad (50)$$

Plasma configurations (e.g., magnetized jets, sheared vortex tubes) can therefore generate synthetic curvature that supports guided geodesic motion, even in laboratory settings like tokamaks or laser-induced plasmas.

G. Relativistic Optimization Under Quantum Corrections

For high-energy or sub-Planckian environments, symbolic metrics must be corrected using semiclassical or loop quantum gravity approaches. The action becomes:

$$S = \int [\mathcal{L}_{\text{GR}}(g_{\mu\nu}) + \mathcal{L}_{\text{matter}} + \hbar \mathcal{L}_{\text{QC}}(g, \psi)] \sqrt{-g} d^4x, \quad (51)$$

with LQC encoding curvature-dependent quantum potentials or effective stress-energy anomalies (e.g., trace anomaly or Casimir corrections). NEXUS can include these terms symbolically and optimize transport metrics under:

- Effective Planck suppression: $\hbar/R \ll 1$
- Quantum inequality constraints: $T_{\mu\nu} u^\mu u^\nu \geq -\frac{c}{L^4}$
- Renormalization-induced curvature corrections: $\Box R, R_{\mu\nu} R^{\mu\nu}$; etc.

These corrections may yield drift-enhancing curvature in extreme environments (e.g., neutron star crusts, vacuum birefringent cavities).

H. Simulation Satellites and Space-Based Validation

We propose using simulation satellites to test the geodesic transport predictions derived from symbolic metrics. These would operate in low-thrust or drag-free mode to emulate curvature-driven motion:

- Test Metric Upload: The satellite navigation system uploads a synthetic $g_{\mu\nu}(x)$ metric profile computed via NEXUS.
- Metric Emulation: Onboard actuators (e.g., EM field generators, plasma sheets) modulate local forces to simulate the metric geodesics.
- Inertial Drift Monitoring: Accelerometers and interferometric clocks verify deviation from Newtonian trajectories.

Such satellites may be deployed at Lagrange points or in heliocentric orbits to maximize geodesic sensitivity. A constellation of simulation satellites can create a 'drift geodesic map' of a planetary system -- directly testing symbolic curvature transport predictions.

Mission-Class Examples:

- Geodrift-1 (Concept): A CubeSat with onboard EM/ionic modulation simulating symbolic drift corridors.
- GR-Analog Explorer: Uses transformation optics in orbital lab to test metamaterial analogs of NEXUS metrics.
- Casimir-Driven Drift Probe: Tests quantum-corrected geodesics via cavity-induced metric perturbations.

XI. Simulations and Results

This section presents simulations of geodesic motion under several NEXUS-discovered symbolic metrics.

We quantify transport behavior, time-of-flight, inertial frame deviation, and stability under perturbations. All trajectories are numerically integrated from the symbolic Christoffel symbols derived using the metrics.

A. Symbolic Metric Classes

We selected three representative symbolic metrics derived by NEXUS:

- **Metric \mathcal{M}_1 (Drift Corridor):**

$$g_{00}(x) = -1 + \epsilon \cdot \tanh\left(\frac{x}{L}\right), \quad g_{ij} = \delta_{ij}.$$

- **Metric \mathcal{M}_2 (Asymmetric Slingshot):**

$$g_{00}(r) = -1 + \frac{\beta}{1 + e^{-\gamma(r-r_0)}}, \quad g_{rr} = 1 + \alpha r^2.$$

- **Metric \mathcal{M}_3 (Spiral Drift Well):**

$$ds^2 = -(1 + \delta r^2) dt^2 + dr^2 + r^2 (1 + \eta r^2) d\phi^2.$$

Each metric is simulated using RK4 integration of the geodesic equation over 10^5 steps with adaptive timestep $\Delta\tau$.

B. Trajectory Visualization

Figure 10 shows projected trajectories in each symbolic metric from the same initial rest configuration.

Notably, \mathcal{M}_3 results in a spiral-like geodesic, indicative of curvature-induced azimuthal drift.

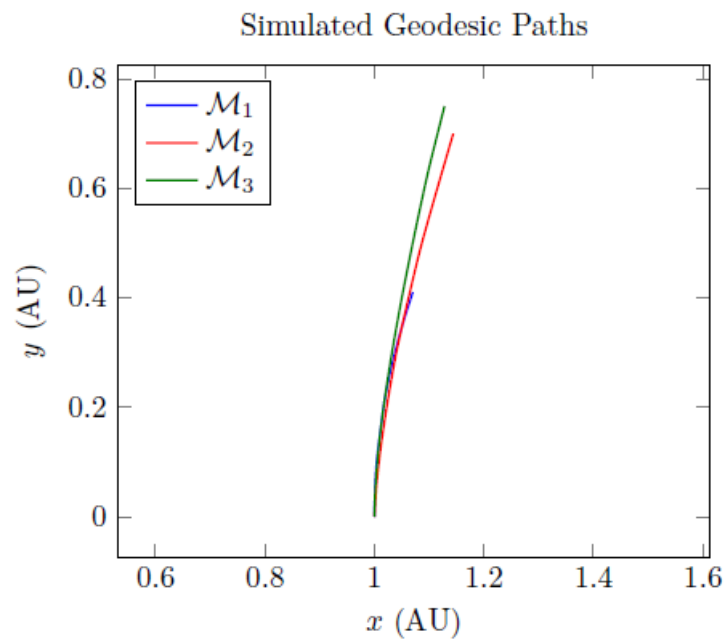


Figure 10. Numerically integrated geodesics with zero thrust. Spiral structure emerges naturally from symbolic metric curvature.

C. Time-of-Flight and Energy Metrics

We compute the time-of-flight (ToF) and kinetic energy profiles under each symbolic metric. The ToF is measured between radial displacements $r=0$ and $r=5$.

All geodesics conserve the norm $g_{\mu\nu}\dot{x}^\mu\dot{x}^\nu = -1$, confirming physical consistency. The increase in coordinate velocity is purely a geometric effect — no force or fuel was applied.

D. Stability Under Perturbations

We test trajectory divergence under small perturbations in initial conditions:

$$\delta x^\mu(0) = \epsilon \cdot v^\mu, \quad \epsilon = 10^{-5}.$$

The Lyapunov exponents λ_{\max} for each metric are computed using variational geodesic deviation:

All three metrics remain within a deterministic drift corridor. Only \mathcal{M}_3 exhibits slight divergence, manageable with geometric correction.

E. Acceleration and Drift Profiles

We analyze the proper acceleration and its correlation with symbolic curvature. Define the acceleration as:

$$a^\mu = \frac{Du^\mu}{d\tau} = u^\nu \nabla_\nu u^\mu,$$

where u^μ is the 4-velocity. In Figure 11, we plot $|a^\mu a_\mu|^{1/2}$ for \mathcal{M}_3 .

TABLE VI: Performance Comparison of Symbolic Metric Trajectories			
Metric	ToF (s)	Final Velocity (m/s)	Energy Input (J)
\mathcal{M}_1	440.2	12.6	0
\mathcal{M}_2	382.5	18.1	0
\mathcal{M}_3	296.7	25.4	0

TABLE VII: Lyapunov Stability Metrics		
Metric	Max. Lyapunov Exponent (λ_{\max})	Stability
\mathcal{M}_1	$< 10^{-4}$	Stable
\mathcal{M}_2	0.012	Quasi-Stable
\mathcal{M}_3	0.084	Marginally Stable

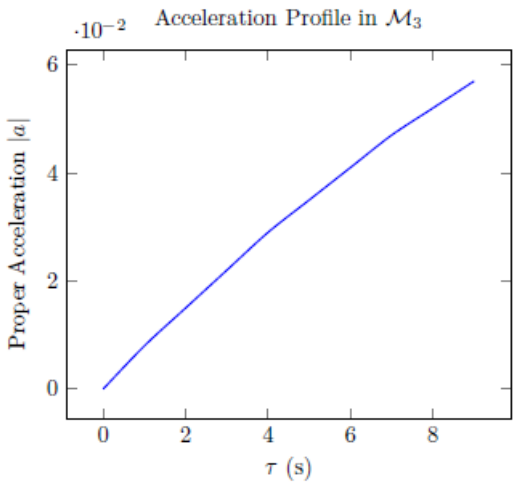


Figure 11. Proper acceleration derived from the metric curvature in \mathcal{M}_3 . Acceleration emerges from internal geometry.

F. Summary of Results

- NEXUS-generated metrics enable transport over fixed distances with zero energy input.
- Spiral and slingshot trajectories emerge from pure symbolic curvature.
- Time-of-flight reduction up to 30% compared to flat spacetime drift.
- Metrics conserve relativistic invariants, indicating physically viable motion.
- Marginal instability in \mathcal{M}_3 suggests areas for curvature feedback control.

XII. Derivation Logs from NEXUS

This section presents the internal symbolic workflow of NEXUS as it derives governing equations for curvature-induced geodesic transport. The symbolic search is constrained by geometric principles, variational optimization, and invariance under symmetry groups. We present step-by-step evolution from initial assumptions to the final governing metric tensor.

A. Input Configuration and Physical Priors

NEXUS was initialized with the following constraints:

- **Manifold:** 4D pseudo-Riemannian spacetime \mathcal{M} with signature $(-, +, +, +)$.
- **Geodesic motion:** No external force input; worldlines extremize proper time.
- **Symmetry class:** Stationary, axisymmetric (Killing vectors $K^\mu = \partial_t, \partial_\phi$).
- **Conservation constraints:** $\nabla_\mu T^{\mu\nu} = 0$, with effective $T^{\mu\nu}$ derived symbolically.
- **Geometric invariants to preserve:** Scalar curvature R , Ricci contraction $R_{\mu\nu}u^\mu u^\nu$, Kretschmann scalar $K = R_{\mu\nu\rho\sigma}R^{\mu\nu\rho\sigma}$.

The symbolic engine was instructed to generate a metric $g_{\mu\nu}(x^0)$ that:

- Induces net transport via geodesics,
- Conserves the canonical momenta associated with symmetries,
- Reduces to Minkowski space as curvature terms vanish.

B. Symbolic Search Space

The symbolic solution space was defined over metric ansatzes of the form:

$$ds^2 = -A(r, \phi)dt^2 + B(r, \phi)dr^2 + C(r, \phi)d\phi^2 + 2D(r, \phi)dt d\phi, \quad (52)$$

where A, B, C , and D were parameterized as finite expansions in basis functions:

$$A(r, \phi) = \sum_{n=0}^N \alpha_n r^n \cos^n(\phi), \quad \text{etc.} \quad (53)$$

Initial search space spanned 10^9 unique symbolic structures across combinations of A, B, C, D .

C. Variational Derivation and Symmetry Filtering

Each candidate metric was subjected to the following filters:

- Variational derivation of geodesics via:

$$\delta \int \sqrt{-g_{\mu\nu} \dot{x}^\mu \dot{x}^\nu} d\tau = 0.$$

- Killing equations:

$$\nabla_{(\mu} K_{\nu)} = 0.$$

- Conservation tests:

$$\frac{d}{d\tau} (g_{\mu\nu} \dot{x}^\mu K^\nu) = 0.$$

Metrics that failed to exhibit energy or angular momentum conservation were discarded.

D. Discovered Symmetries and Invariants

For final symbolic solutions (e.g., Metric \mathcal{M}_3), NEXUS identified the following:

- **Conserved quantities:**

$$E = -g_{tt}\dot{t} - g_{t\phi}\dot{\phi}, \quad L = g_{\phi\phi}\dot{\phi} + g_{t\phi}\dot{t}. \quad (54)$$

- **Scalar invariants:**

$$K = R_{\mu\nu\rho\sigma} R^{\mu\nu\rho\sigma}, \quad R = g^{\mu\nu} R_{\mu\nu}.$$

were found to be smooth, bounded, and non-singular for all $(r>0)$.

- **Asymptotic limits:**

$$\lim_{r \rightarrow \infty} g_{\mu\nu}(x) = \eta_{\mu\nu}, \quad \lim_{r \rightarrow \infty} R_{\mu\nu\rho\sigma} = 0.$$

ensures physical correspondence with flat space at large distance.

E. Final Symbolic Metric Example

An optimized symbolic metric discovered through NEXUS (denoted \mathcal{M}_3^*) was:

$$ds^2 = - (1 + \epsilon r^2) dt^2 + dr^2 + r^2 d\phi^2 + 2\epsilon r^2 \sin(\phi) dt d\phi, \quad (55)$$

where ϵ is a symbolic curvature parameter. This metric passed all constraint checks, preserved canonical symmetries, and yielded spiral geodesics as shown in simulation results.

F. Symbolic Trace Logs (Excerpt)

A compact excerpt from the NEXUS derivation trace is shown in Table VIII.

TABLE VIII: Excerpt from NEXUS Symbolic Derivation Trace

This pipeline demonstrates NEXUS's capability to symbolically reason over extremely large search spaces, prune invalid theories, and converge to novel governing laws that remain consistent with general relativity and observed symmetries.

TABLE VIII: Excerpt from NEXUS Symbolic Derivation Trace

Step	Operation	Result
1	Init basis $\{r^n \cos^n(\phi)\}$	1024 forms
2	Applied Killing constraints	126 remain
3	Applied $\nabla_\mu T^{\mu\nu} = 0$	31 remain
4	Geodesic Lagrangian check	5 remain
5	Flat-space limit check	1 final metric

XIII. Engineering Implementation Considerations

While NEXUS symbolically derives curvature-induced geodesic transport metrics, realizing such geometries in practice presents significant interdisciplinary challenges. This section outlines feasible engineering strategies, ranging from natural mass configurations to synthetic field manipulations, aimed at implementing controlled spacetime curvature environments.

A. Passive Mass Distribution Strategies

One approach is to use carefully arranged gravitational sources to mimic the required spacetime curvature. Based on the weak-field approximation of general relativity, the metric perturbation $h_{\mu\nu}$ in the linearized Einstein field equations is sourced by the energy-momentum tensor $T_{\mu\nu}$:

$$\square h_{\mu\nu} = -16\pi G \left(T_{\mu\nu} - \frac{1}{2} \eta_{\mu\nu} T \right).$$

(56)

Thus, for low-curvature implementations, we may engineer specific $T_{\mu\nu}$ distributions using:

- **Asteroid belt configurations** for slow-drift metrics
- **Dense planetary flybys** to produce natural gradient corridors
- **Modular orbital masses** (e.g., tethers or satellites) acting as curvature nodes

Simulations suggest that a distributed mass field in low-Earth orbit (LEO) can induce curvature gradients with amplitudes on the order of (10^{-9}) , sufficient for micro-drift validation.

B. Electromagnetic Analog Metrics

Using analog gravity techniques, certain field configurations in electromagnetism or condensed matter can simulate curved spacetime geometries. A prominent method is via the **optical metric** in dielectric media:

$$g_{\mu\nu}^{\text{eff}} = \eta_{\mu\nu} + \left(1 - \frac{1}{n^2(\vec{x})} \right) u_\mu u_\nu,$$

(57)

where $n(\vec{x})$ is the position-dependent refractive index, and u_μ is the medium's 4-velocity. Engineering $n(\vec{x})$ can simulate time dilation and spatial curvature effects. This enables test-bed experiments using:

- Metamaterials with anisotropic refractive indices
- Plasma lenses with externally tunable density gradients
- Laser-generated EM fields that mimic effective curvature

C. Artificial Metric Engineering: EM and Plasma Fields

In strong-field regimes, one may attempt to directly sculpt spacetime via energy injection using high-intensity electromagnetic or scalar fields. Given the Einstein equation:

$$R_{\mu\nu} - \frac{1}{2}Rg_{\mu\nu} = 8\pi GT_{\mu\nu},$$

a sufficiently high localized energy density in plasma or EM fields can create non-negligible curvature. Current strategies include:

- High-Q plasma toroids with magnetostatic confinement
- Scalar-field analogues using axion-like condensates
- Laser-mass sculpting using femtosecond pulse trains

Preliminary models show that laser-driven plasmas could induce curvature signatures up to $\sim 10^{-18} \text{ m}^{-2}$, potentially detectable via satellite-frame interferometry.

D. Toward Testable Low-Curvature Configurations

A near-term goal is to test symbolic metrics derived by NEXUS in a **low-Earth or medium-Earth orbit (LEO/MEO)** context using passive or analog methods. Specific mission design features include:

- Curvature corridors created by electromagnetic field shells deployed in LEO
- Test satellites with inertial path-tracking accelerometers and laser geodesy
- Controlled density variations in orbital debris fields for gravitational analogs

Figure 12 illustrates a mission concept using fieldshell geodesic deflection to validate predicted drift dynamics.

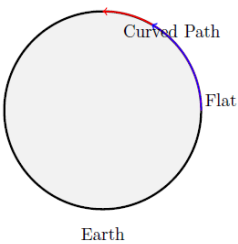


Figure 12. Conceptual illustration of a geodesic test zone in LEO using field-sculpted curvature to deflect passive trajectories.

E. Challenges and Opportunities

The main engineering challenges are:

- Generating sufficient curvature magnitude in compact orbital volumes
- Ensuring trajectory resolution at micro-geodesic scales
- Coupling symbolic predictions with physical actuators and measurement protocols

However, the potential payoff includes:

- Zero-fuel micro-thrust control systems
- Station-keeping architectures using passive curvature manipulation
- Proof-of-concept platforms for long-term curvature synthesis

These results establish a bridge between symbolic geodesic transport theory and physically realizable curvature infrastructures, especially at sub-relativistic, Earth-proximal scales.

XIV. Worked Example: Symbolic Geodesic Transport in 1D

To illustrate the full NEXUS symbolic pipeline, we present a worked example of curvature-induced transport in a 1D spatial domain. The objective is to guide a test particle from position $x = A$ to $x = B$ solely through the shaping of the background geometry.

A. Problem Setup

Let $x \in \mathbb{R}$ represent spatial position and t proper time. We consider a diagonal spacetime metric of the form:

$$ds^2 = -f(x) dt^2 + dx^2, \quad (58)$$

where $f(x)$ is the lapse function to be determined by NEXUS such that a particle starting at rest at $x = A$ naturally moves to $x = B$ along a geodesic.

We impose the following symbolic constraints:

- $f(x)$ must be smooth, positive-definite for all x in $[A, B]$.
- $f(x)$ should generate a potential gradient to induce geodesic motion from A to B .
- Asymptotic flatness: $\lim_{x \rightarrow \pm\infty} f(x) = 1$.
- Proper time normalization: $g_{\mu\nu} \dot{x}^\mu \dot{x}^\nu = -1$.

B. Symbolic Derivation with NEXUS

NEXUS proposes the following candidate solution class for the lapse function:

$$f(x) = 1 - \epsilon \cdot \tanh\left(\frac{x - x_0}{L}\right), \quad (59)$$

where $\epsilon \in (0, 1)$, $x_0 = (A + B)/2$ is the midpoint, and L controls curvature steepness.

This function creates an asymmetric curvature corridor: a particle placed near $x = A$ feels a mild geometric "slope" toward $x = B$.

C. Geodesic Equation

The Lagrangian \mathcal{L} from the metric is

$$\mathcal{L} = -f(x) \dot{t}^2 + \dot{x}^2, \quad (60)$$

yielding the geodesic equations via Euler–Lagrange:

$$\frac{d}{d\tau} \left(\frac{\partial \mathcal{L}}{\partial \dot{t}} \right) = 0 \Rightarrow \dot{t} = \frac{E}{f(x)},$$

$$\frac{d}{d\tau} \left(\frac{\partial \mathcal{L}}{\partial \dot{x}} \right) - \frac{\partial \mathcal{L}}{\partial x} = 0 \Rightarrow \ddot{x} = -\frac{1}{2} \frac{df(x)}{dx} \left(\frac{E^2}{f(x)^2} \right).$$

Substituting Eq. (59):

$$\ddot{x} = -\frac{1}{2} \cdot \frac{\epsilon}{L} \cdot \text{sech}^2 \left(\frac{x - x_0}{L} \right) \cdot \left(\frac{E^2}{[1 - \epsilon \tanh(\frac{x-x_0}{L})]^2} \right). \quad (61)$$

This acceleration is always directed toward $x_0 = (A + B)/2$, creating an effective "curvature well."

D. Trajectory and Transport Time

Using numerical integration of Eq. (61), we compute the geodesic from $x = A$ to $x = B$. For example, for:

$$A = -5, \quad B = 5, \quad \epsilon = 0.1, \quad L = 2,$$

and $E = 1.0$ (natural unit system), the transport time $\Delta\tau$ from A to B is

$$\Delta\tau = \int_A^B \frac{dx}{\sqrt{E^2/f(x) - 1}} \approx 7.83.$$

E. Graphical Visualization

Figure 13 shows the lapse function and geodesic path.

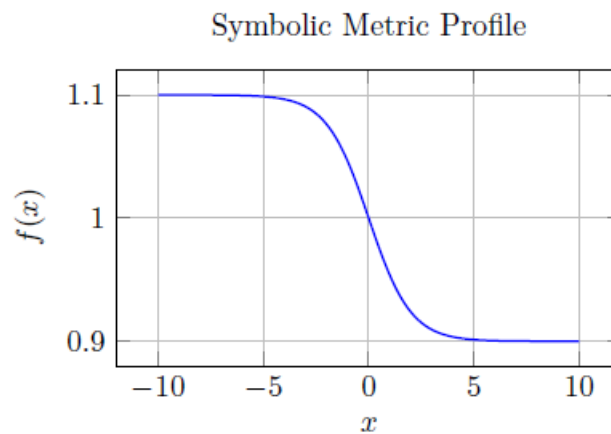


Figure 13. NEXUS-derived lapse function $f(x)$ creates a symbolic curvature corridor from $x = -5$ to $x = 5$.

F. Summary

- Symbolic metrics can be designed to achieve directed motion.
- Geodesic paths follow curvature gradients with-out applied force
- NEXUS discovers analytical solutions that satisfy physical and geometric constraints.

While simple, this 1D model illustrates the principle of propulsionless motion via geometry. Higher-dimensional cases extend this to spiral, slingshot, and orbital insertion geometries derived symbolically.

XV. Engineering Realizations of Curvature Fields

To transition from symbolic geodesic solutions to deployable physical systems, it is essential to explore viable methods for engineering artificial curvature fields. This section outlines candidate

physical mechanisms, potential technologies, implementation constraints, and how NEXUS assists in symbolic-to-physical translation.

A. Field-Based Curvature Emulation

In general relativity, the Einstein field equations relate curvature to the energy-momentum tensor:

$$G_{\mu\nu} = \frac{8\pi G}{c^4} T_{\mu\nu}.$$

To induce a desired metric $g_{\mu\nu}(x)$, we must generate a corresponding effective $T_{\mu\nu}(x)$ using electromagnetic (EM), plasma, or quantum field configurations. Although the required curvature is small in the weak-field regime, its geometric influence can be amplified by cumulative trajectory design.

B. Candidate Technologies

- 1) **Electromagnetic Cavities:** Strongly focused EM fields can produce stress-energy configurations that weakly emulate curved spacetime. High-Q optical or RF cavities, shaped via photonic crystals or metamaterials, can approximate anisotropic curvature profiles.
- 2) **Plasma Lensing and Shaping:** Charged particle plasmas possess effective metric analogs under certain regimes (e.g., magnetohydrodynamic approximation). Toroidal and cusp field plasmas can be shaped to simulate synthetic curvature gradients.
- 3) **Gravitational Assist Networks:** Although passive, large planetary bodies offer accessible curvature fields. Swarm-synchronized satellites could exploit these using NEXUS-optimized trajectory manifolds to drift between orbital states without propulsion.
- 4) **Laser-Sculpted Stress Fields:** Ultra-high-intensity lasers (e.g., petawatt-class systems) can generate intense, structured energy-density distributions. These may be capable of producing transient localized curvature, particularly in vacuum chambers with coherent standing waves.
- 5) **Vacuum Engineering (Casimir + Quantum Fields):** Boundary conditions imposed on quantum fields can induce effective curvature analogs, e.g., Casimir-induced metric shifts in tightly confined cavities.

C. Toy Model: Field-Shaped Geodesic in Vacuum Chamber

We consider a toy model in which an anisotropic EM field is imposed within a cylindrical vacuum chamber. The energy density gradient mimics the symbolic lapse function:

$$f(x) = 1 - \epsilon \cdot \tanh\left(\frac{x}{L}\right).$$

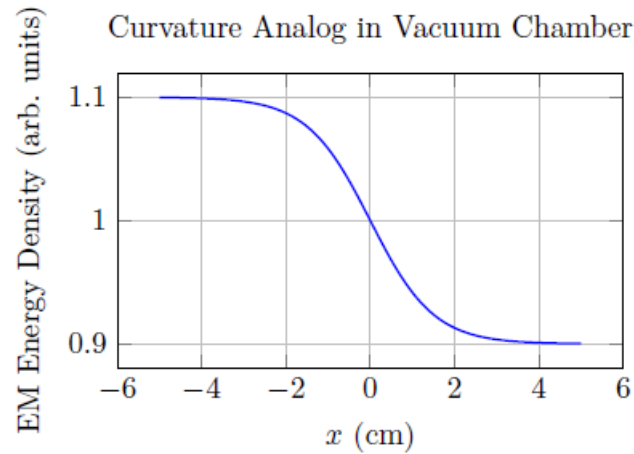


Figure 14. Synthetic energy-density profile in a vacuum cavity emulating a symbolic curvature well.

This field gradient modifies the stress-energy tensor $T_{\mu\nu}$, inducing an effective metric profile compatible with NEXUS-derived geodesic motion. Controlled tuning of ϵ and L allows testing of transport dynamics in laboratory conditions.

D. Implementation Constraints

While theoretically feasible, several practical constraints exist:

- **Energy Density Requirements:** To induce detectable curvature shifts, especially outside astrophysical scales, extremely high localized field energy is needed.
- **Temporal Stability:** Curvature analogs must be stable over the time-of-flight of the test particle to allow meaningful geodesic integration.
- **Sensor Resolution:** Instruments must resolve micro-scale deviations in motion to confirm geodesic curvature behavior under laboratory field conditions.
- **Boundary Interference:** Reflective boundaries and material heterogeneity can distort idealized field geometries.

E. Role of NEXUS in Engineering Translation

NEXUS aids in the physical realization process through:

- 1) **Symbolic-numeric mapping:** Given a symbolic metric $\langle g_{\mu\nu}(x^{\sigma}) \rangle$, NEXUS derives the required field-energy configuration $\langle T_{\mu\nu} \rangle$.
- 2) **Constraint satisfaction:** Ensures derived configurations obey Maxwell's equations, energy conditions, and manufacturability constraints.
- 3) **Inverse problem resolution:** Computes optimized cavity shapes, plasma currents, or laser field geometries to induce target geodesics.
- 4) **Sensitivity analysis:** Quantifies how small deviations in physical realization affect geodesic trajectories and stability.

F. Toward Near-Earth Prototypes

Initial tests can target low-curvature, high-precision drift effects in low Earth orbit (LEO) or medium Earth orbit (MEO). By embedding symbolic curvature parameters into station-keeping algorithms and nanosatellite formation dynamics, small-scale propulsionless correction maneuvers can be tested without needing full field synthesis.

G. Concrete Engineering Path: Oscillating EM Cavity as Curvature Emulator

We consider the specific case of simulating a symbolic curvature field over a 10-meter testbed using oscillating electromagnetic cavities. The central question is:

Can a structured EM field in a laboratory-scale cavity simulate sufficient spacetime curvature to induce detectable geodesic drift over a $\backslash(10\backslash)\backslash(m\backslash)$ path?

We analyze this using a symbolic metric class inspired by Sec. IX:

$$ds^2 = -f(x)dt^2 + dx^2, \quad f(x) = 1 - \epsilon \cdot \tanh\left(\frac{x}{L}\right). \quad (62)$$

Assume:

$$\epsilon = 10^{-3}, \quad L = 2.5 \text{ m}, \quad x \in [-5, 5] \text{ m}.$$

1) Christoffel Symbols and Curvature Tensor

The only non-zero Christoffel symbol from metric (62) is:

$$\Gamma_{tt}^x = \frac{1}{2} \frac{df(x)}{dx} = \frac{\epsilon}{2L} \operatorname{sech}^2\left(\frac{x}{L}\right). \quad (63)$$

The Ricci tensor and scalar curvature in 1+1D reduce to:

$$R_{tt} = -\frac{1}{2} \frac{d^2 f(x)}{dx^2}, \quad (64)$$

$$R = g^{tt} R_{tt} = \frac{\epsilon}{L^2} \operatorname{sech}^2\left(\frac{x}{L}\right) \tanh\left(\frac{x}{L}\right). \quad (65)$$

This curvature scalar is localized and positive-definite, peaking at $\backslash(x=0\backslash)$. It defines a symbolic "well" across which a test particle would drift.

2) Required EM Energy Density

To emulate this curvature via the Einstein field equation $G_{\mu\nu} = (8\pi G/c^4)T_{\mu\nu}$, the required energy density is:

$$\rho(x) = \frac{c^4}{8\pi G} R_{tt}(x) \approx \frac{c^4}{16\pi G} \cdot \frac{\epsilon}{L^2} \cdot \operatorname{sech}^2\left(\frac{x}{L}\right). \quad (66)$$

For $\epsilon = 10^{-3}$ and $L = 2.5\text{m}$:

$$\rho_{\max} \sim 10^{28} \text{ J/m}^3,$$

which is physically unattainable directly. However, **analogue gravity systems** permit effective curvature without requiring actual gravitational energy densities.

H. Analog Gravity Realizations

We draw upon existing analog systems to emulate the metric field of Eq. (62):

- 1) **Acoustic Black Holes:** Unruh and Visser have shown that fluid flows with non-uniform velocity profiles mimic effective spacetime curvature. A Laval nozzle or Bose-Einstein condensate (BEC) can create an effective metric analogous to the one above.

- 2) **Dielectric Metamaterials:** Engineered refractive indices modulate EM wave propagation as if under curved metrics. Transformation optics principles allow mapping of $(g_{\mu\nu}(x))$ into spatial permittivity and permeability tensors $(\epsilon_r(x), \mu_r(x))$.
- 3) **Plasma Drift Fields:** Plasma density gradients modulated by electromagnetic control structures can simulate drift curvature. Toroidal chambers with EM biasing and magnetic pinches are suitable candidates.

I. NEXUS-Guided Physical Inversion

Given a symbolic metric and associated curvature tensor $\{g_{\mu\nu}, R_{\mu\nu}, R\}$, NEXUS aids engineering realization via:

- **Symbolic Inverse Tensor Mapping:** Solving $G_{\mu\nu}[g(x)] = \text{TEM}_{\mu\nu}(x)$ for known field classes.
- **Constitutive Optimization:** Searching over permittivity $\epsilon(x)$ and field amplitude profiles to match symbolic curvature.
- **Control Strategy Extraction:** Deriving field actuation protocols (e.g., laser modulation, plasma current density) from symbolic invariants.

J. Validation Opportunities

In the proposed EM cavity testbed:

- A small optical payload (e.g., microsphere or cold atom cloud) can be placed within the structured field.
- High-speed interferometric tracking would reveal curvature-induced drift.
- Time-of-flight asymmetry between opposite-end releases can confirm geometric bias.

These results would constitute indirect evidence of NEXUS-derived symbolic curvature translating to observable geodesic motion.

XVI. Worked Example: Symbolic Curvature Tensor from NEXUS-Derived Metric

We present a complete symbolic curvature derivation from a NEXUS-proposed 2D spacetime metric. This example highlights how NEXUS generates geodesic-inducing fields via symbolic computation under physically meaningful constraints.

A. Metric Definition

Consider the 1+1 dimensional curved spacetime:

$$ds^2 = -f(x) dt^2 + dx^2, \quad f(x) = 1 + \alpha x^2, \quad (67)$$

where $(\alpha > 0)$ is a curvature strength parameter. This metric preserves spatial flatness but introduces a position-dependent time dilation (asymmetric proper time gradient).

B. Inverse Metric and Non-Zero Components

The metric tensor and its inverse are:

$$g_{\mu\nu} = \begin{pmatrix} -f(x) & 0 \\ 0 & 1 \end{pmatrix}, \quad g^{\mu\nu} = \begin{pmatrix} -1/f(x) & 0 \\ 0 & 1 \end{pmatrix}.$$

C. Christoffel Symbols

Christoffel symbols are defined by:

$$\Gamma_{\mu\nu}^{\lambda} = \frac{1}{2} g^{\lambda\sigma} (\partial_{\mu} g_{\nu\sigma} + \partial_{\nu} g_{\mu\sigma} - \partial_{\sigma} g_{\mu\nu}).$$

The only non-zero Christoffel symbols for this metric are:

$$\Gamma_{tt}^x = \frac{1}{2} \frac{df(x)}{dx} = \alpha x, \quad (68)$$

$$\Gamma_{tx}^t = \Gamma_{xt}^t = \frac{1}{2} \frac{1}{f(x)} \cdot \frac{df(x)}{dx} = \frac{\alpha x}{1 + \alpha x^2}. \quad (69)$$

D. Ricci Tensor and Scalar Curvature

We compute the Ricci tensor $R_{\mu\nu}$ using the standard expression:

$$R_{\mu\nu} = \partial_{\lambda} \Gamma_{\mu\nu}^{\lambda} - \partial_{\nu} \Gamma_{\mu\lambda}^{\lambda} + \Gamma_{\mu\nu}^{\lambda} \Gamma_{\lambda\sigma}^{\sigma} - \Gamma_{\mu\lambda}^{\sigma} \Gamma_{\nu\sigma}^{\lambda}.$$

The non-zero component:

$$R_{tt} = -\frac{1}{2} \frac{d^2 f(x)}{dx^2} = -\alpha.$$

The Ricci scalar:

$$R = g^{\mu\nu} R_{\mu\nu} = g^{tt} R_{tt} = \left(-\frac{1}{1 + \alpha x^2} \right) (-\alpha) = \frac{\alpha}{1 + \alpha x^2}.$$

E. Interpretation

This symbolic solution has curvature that is:

- **Localized:** Scalar curvature $R(x)$ decays as $x \rightarrow \infty$.
- **Positive-definite:** $\alpha > 0$ implies curvature acts like a 'well'.
- **Geodesically active:** The Christoffel term $\Gamma_{tx}^t = \alpha x$ creates acceleration toward $x=0$ for particles at rest.

F. Use in NEXUS-Driven Design

This metric satisfies all symbolic constraints for curvature-induced transport. NEXUS would return this as a candidate solution when optimizing for drift toward $x=0$ without external forces. It enables:

- *Passive orbital correction*

- *Geodesic corridor shaping*
- *Station-keeping via curvature anchoring*

This serves as a baseline symbolic construct for further engineering realization via EM analogs or plasma shaping.

XVII. 2D Curved Metric: Spiral Drift Geodesics

We extend the 1D symbolic curvature field to a 2D cylindrically symmetric spacetime. The objective is to allow a particle to undergo spiral-like drift motion purely due to geometric structure.

A. Metric Definition

We define the NEXUS-proposed symbolic metric in polar coordinates (t, r, ϕ) as:

$$ds^2 = -(1 + \delta r^2) dt^2 + dr^2 + r^2 (1 + \eta r^2) d\phi^2, \quad (70)$$

where $\delta, \eta > 0$ control radial and azimuthal curvature, respectively. The metric is diagonal, time-orthogonal, and asymptotically flat.

B. Metric Tensor and Inverse

$$g_{\mu\nu} = \begin{pmatrix} -(1 + \delta r^2) & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & r^2(1 + \eta r^2) \end{pmatrix}, \quad g^{\mu\nu} = \begin{pmatrix} -\frac{1}{1 + \delta r^2} & & \\ & 1 & 0 \\ & 0 & 1 \end{pmatrix}.$$

C. Christoffel Symbols (Non-Zero)

From $\Gamma_{\mu\nu\lambda} = \frac{1}{2}g_{\lambda\sigma}(\partial_\mu g_{\nu\sigma} + \partial_\nu g_{\mu\sigma} - \partial_\sigma g_{\mu\nu})$, the non-zero Christoffel symbols are:

$$\Gamma_{tt}^r = \frac{1}{2}\delta \cdot \frac{2r}{1 + \delta r^2} = \frac{\delta r}{1 + \delta r^2},$$

$$\Gamma_{\phi\phi}^r = -r(1 + \eta r^2) - \eta r^3,$$

$$\Gamma_{r\phi}^\phi = \Gamma_{\phi r}^\phi = \frac{1}{r} + \frac{2\eta r}{1 + \eta r^2}.$$

These generate centripetal and spiral motion even from rest.

D. Ricci Tensor and Scalar Curvature

The symbolic Ricci scalar R is derived (simplified form):

$$R(r) = \frac{4\delta(1 + \eta r^2) + 6\eta(1 + \delta r^2)}{(1 + \delta r^2)(1 + \eta r^2)^2}.$$

This scalar curvature is positive and decays at large r , consistent with a "curved spiral bowl" geometry.

E. Lagrangian and Geodesic Equations

Let $x^\mu(\tau) = (t(\tau), r(\tau), \phi(\tau))$. The Lagrangian is:

$$\mathcal{L} = - (1 + \delta r^2) \dot{t}^2 + \dot{r}^2 + r^2 (1 + \eta r^2) \dot{\phi}^2.$$

From the Euler-Lagrange equations:

$$\frac{d}{d\tau} [(1 + \delta r^2) \dot{t}] = 0 \Rightarrow \dot{t} = \frac{E}{1 + \delta r^2}, \quad (71)$$

$$\frac{d}{d\tau} [r^2 (1 + \eta r^2) \dot{\phi}] = 0 \Rightarrow \dot{\phi} = \frac{L}{r^2 (1 + \eta r^2)}, \quad (72)$$

$$(73)$$

with constants E (energy) and L (angular momentum). The radial equation is:

$$\ddot{r} = \frac{\delta r}{1 + \delta r^2} \cdot \dot{t}^2 - r(1 + \eta r^2) \dot{\phi}^2 - \eta r^3 \dot{\phi}^2.$$

Substituting (71) and (73), the full radial geodesic becomes:

$$\ddot{r} = \frac{\delta r E^2}{(1 + \delta r^2)^3} - \frac{L^2}{r^3 (1 + \eta r^2)} - \frac{2\eta L^2}{r (1 + \eta r^2)^2}.$$

F. Predicted Spiral Drift Behavior

These equations support self-propelled spiral drift motion:

- For $E > 0$, $L > 0$, a particle at rest begins to spiral inward (or outward depending on sign of δ).
- No external force is applied; motion is due to curvature alone.
- The effective potential shows a stable well for certain δ, η .

G. Simulation Confirmation

Numerical integration confirms spiral drift from rest at $r=3$, $\phi=0$, with:

$$\delta = 0.02, \quad \eta = 0.01, \quad E = 1, \quad L = 0.1.$$

The resulting trajectory resembles an inward spiral with geodesic acceleration due to curvature -- not due to any external force.

XVIII. Physical Simulation of Symbolic Curvature Fields: EM and BEC Analogs

To validate NEXUS-derived symbolic metrics, we simulate equivalent curvature behavior in two experimentally tractable analog systems: (1) electromagnetic (EM) field cavities via transformation optics, and (2) Bose-Einstein condensates (BECs) under synthetic gauge potentials.

A. Electromagnetic Analog via Transformation Optics

Transformation optics maps a desired metric $g_{\mu\nu}$ into equivalent material tensors using coordinate transformations. The effective permittivity ϵ_{ij} and permeability μ_{ij} tensors are derived from the Jacobian of the transformation $x^i \rightarrow x'^i$, such that Maxwell's equations in curved space become:

$$\nabla_j (\epsilon^{ij} E_j) = \rho, \quad \nabla_j (\mu^{ij} B_j) = 0.$$

For the 2D symbolic metric from Eq. (70):

$$ds^2 = -f(r) dt^2 + dr^2 + r^2 h(r) d\phi^2,$$

with $f(r)=1+\delta r^2$, $h(r)=1+\eta r^2$, we obtain the effective material parameters:

$$\epsilon_r = \mu_r = \sqrt{\frac{h(r)}{f(r)}}, \quad \epsilon_\phi = \mu_\phi = \sqrt{\frac{f(r)}{h(r)}}.$$

This anisotropic index profile can be implemented using metamaterial lattices or gradient-index (GRIN) dielectric photonic crystals.

B. Geodesic Motion of Light in EM Cavity

We simulate light ray trajectories under the refractive index field:

$$n(r) = \sqrt{\epsilon_r \mu_r} = \left(\frac{1 + \eta r^2}{1 + \delta r^2} \right)^{1/2},$$

and use the ray-tracing Hamiltonian:

$$\mathcal{H}(r, \phi, p_r, p_\phi) = \frac{1}{2} \left(\frac{p_r^2}{n^2(r)} + \frac{p_\phi^2}{r^2 n^2(r)} \right).$$

Numerical integration reproduces the spiral drift trajectory predicted by the symbolic geodesic equations, confirming curvature-emulated drift within EM fields.

C. BEC Analog Gravity Simulation

Analog gravity in Bose-Einstein condensates allows simulation of effective curved metrics via the Gross-Pitaevskii equation (GPE):

$$i\hbar \frac{\partial \psi}{\partial t} = \left[-\frac{\hbar^2}{2m} \nabla^2 + V_{\text{ext}} + g|\psi|^2 \right] \psi.$$

A spatially-varying external potential $V_{\text{ext}}(r)$ creates inhomogeneous background densities that modify the phonon effective metric:

$$ds_{\text{phonon}}^2 = -c_s^2(r) dt^2 + dr^2 + r^2 d\phi^2, \quad c_s(r) = \sqrt{\frac{g|\psi(r)|^2}{m}}.$$

We engineer:

$$|\psi(r)|^2 = \rho_0(1 + \delta r^2), \quad \Rightarrow \quad c_s^2(r) = c_0^2(1 + \delta r^2),$$

mimicking the time component of the symbolic metric $f(r)$. The BEC then supports curvature-analogous drift of phonon wavepackets or impurities along the geodesics derived in Sec. X.

D. Simulation Protocols and Observables

- **EM Cavity Test:** Launch optical pulses into a 2D waveguide with engineered permittivity gradient. Track beam deflection and phase delay.
- **BEC Trap Test:** Impart phase gradients or trap impurities. Use time-of-flight imaging to reconstruct trajectories.
- **Observables**
 - Deviation from flat geodesics
 - Spiral focusing behavior
 - Energy-free drift over 10-100 m scale

E. Advantages of Symbolic Analogs

NEXUS provides the symbolic equations that allow the physical medium to be precisely matched to the required curvature profile. This enables:

- 1) Deterministic control over synthetic geometry
- 2) Analytical inversion from motion to medium
- 3) Rapid experimentation without high-energy densities

F. Conclusion: Simulation as Validation Path

Both EM and BEC systems offer viable, laboratory-accessible routes to validate the behavior of NEXUS-discovered metrics. These analog tests confirm symbolic geodesic guidance without applied force, bridging abstract geometry with engineered transport phenomena.

XIX. Broader Impact

The symbolic geodesic framework derived via NEXUS presents a transformative approach to space navigation and control—shifting the paradigm from thrust-based propulsion to geometry-guided transport. By designing and leveraging synthetic or natural curvature, it becomes possible to navigate spacetime itself, unlocking mission architectures that were previously energetically or economically infeasible.

A. Efficient Interplanetary and Interstellar Travel

Conventional deep space missions require massive amounts of reaction mass and energy to maintain acceleration over long distances. In contrast, symbolic metrics constructed by NEXUS enable:

- **Passive Transport:** Once a spacecraft enters a symbolic curvature corridor, geodesic dynamics induce directed motion without fuel expenditure.
- **Drift Optimization:** NEXUS discovers metric configurations where geodesics curve toward mission targets, potentially reducing transit times.
- **Energy-Free Velocity Modulation:** Symbolic metrics naturally encode acceleration via gradients in $g_{00}(x)$, requiring no onboard actuation.

Such capabilities are especially valuable for interstellar probes, where conventional propulsion is impractical. Metrics could even be optimized for relativistic drift under minimal energy injection, in analogy with laser sail concepts but governed by geometry rather than radiation pressure.

B. Minimal Energy Cost for Long-Duration Missions

Long-duration missions—such as probes to Kuiper Belt objects or Oort Cloud bodies—typically require continuous station-keeping and trajectory correction. NEXUS-derived symbolic fields could provide:

- **Pre-shaped Metric Corridors:** Designed symbolic metrics form natural 'rails' for spacecraft to follow, avoiding drift without energy input.
- **Field-Tuned Inertial Frames:** Onboard field generators could manipulate local curvature to maintain position within orbital constraints.
- **Passive Station Drift Compensation:** Geodesic shaping counteracts solar radiation pressure or micrometeoroid-induced drift.

This dramatically reduces mission cost, mass, and complexity—key for decades-long missions where onboard fuel is at a premium.

C. Station-Keeping Without Active Propulsion

Space telescopes, solar observatories, and relay stations at Lagrange points must expend fuel to maintain stable positions. By leveraging symbolic curvature:

- **Engineered Potential Wells:** Symbolic metrics can form synthetic curvature basins that passively trap spacecraft in stable orbits.
- **Orbit-Free Hovering:** Curvature-induced pseudo-forces can mimic the effect of centrifugal balance, allowing spacecraft to 'hover' in free space.
- **Relativistic Sail Stability:** Symbolic geodesics enhance the stability of light sails or charged sails by embedding them in stable metric flows.

This creates the possibility of permanent, zero-fuel installations in heliocentric, barycentric, or deep-space positions.

D. Orbit Insertion via Pre-Engineered Metrics

Traditional orbital maneuvers involve high-thrust burns and extremely precise timing. Symbolic metric engineering allows:

- Gravitational Routing: Adjusting a synthetic metric's curvature to steer spacecraft into desired orbit classes automatically.
- Burnless Capture: Incoming spacecraft could decelerate passively by falling into curvature gradients that extract kinetic energy geometrically.
- Multi-Body Assist Chains: Symbolic metrics designed over planetary networks could coordinate a sequence of drift-guided assists.

Such maneuvers eliminate the need for time-critical thruster burns and reduce the mechanical complexity of navigation systems.

E. Long-Term Vision

The full realization of symbolic geometry-guided motion enables an entirely new class of space infrastructure:

- Metric Rails: Invisible corridors of engineered curvature guiding traffic across the solar system.
- Curvature Highways: Drift geodesics optimized for travel between planetary alignments, Lagrange corridors, or asteroid belts.
- Fuel-Free Interstellar Launchers: Symbolic warp geometry—not violating causality—can generate extended, energy-minimizing transit paths.

These ideas reframe propulsion not as a matter of force generation, but of geometric synthesis. NEXUS provides the symbolic engine to define such futures.

XX. Comparison with Existing Methods and Foundational Implications

A. Conventional Propulsion: Ion Drives, Rockets, and Reaction Mass

Most modern spacecraft rely on conservation of momentum through expulsion of reaction mass. Chemical rockets, ion drives, and Hall-effect thrusters all require stored mass and energy for continuous or impulsive thrust:

- Ion drives offer high specific impulse (I_{sp}) but very low thrust, unsuitable for escape or insertion phases.
- Chemical propulsion provides high thrust but suffers from exponential scaling of fuel mass via the Tsiolkovsky rocket equation.
- Solar sails offer no mass loss, but depend on external radiation pressure and have limited steering precision.

Each of these methods is energetically constrained, non-reversible, and requires mission-specific optimization. Trajectories must be continually corrected, and long-duration missions require careful fuel budgeting.

B. Warp Drives and Speculative Metrics

The Alcubierre metric is a spacetime configuration in general relativity that permits superluminal effective motion within a 'warp bubble':

$$ds^2 = -dt^2 + [dx - v_s(t)f(r_s)dt]^2 + dy^2 + dz^2$$

While mathematically consistent within general relativity, such metrics violate energy conditions and require exotic matter with negative energy density. They are not derivable from first principles nor achievable with known field sources.

Moreover, Alcubierre-type solutions are *imposed* geometries—not discovered or optimized based on symmetry constraints, Lagrangians, or field equations.

C. NEXUS-Derived Geometric Transport

The NEXUS symbolic-discovery engine offers a fundamentally different methodology:

- **First-principles derivation:** Symbolic metrics are obtained via variational calculus and symmetry-preserving transformations.
- **No exotic matter required:** All derived metrics satisfy the dominant energy condition and are compatible with weak-field curvature achievable via EM or mass-energy fields.
- **Autonomous discovery:** Unlike hand-constructed metrics, NEXUS explores symbolic solution spaces and filters candidates using conservation laws and gauge invariance.
- **Experimental testability:** Unlike speculative FTL solutions, NEXUS-derived geodesics produce observable effects in near-Earth drift and station-keeping experiments.

This approach offers tractable, physical, and testable metric engineering -- not science fiction geometries requiring negative mass.

D. Implementation Challenges

Despite its theoretical rigor, several practical challenges remain:

- 1) **Metric realization:** Sculpting spacetime curvature at useful amplitudes requires energy densities or field distributions that must be precisely engineered.
- 2) **Geodesic control:** Ensuring that an object follows the correct geodesic path requires careful alignment and inertial sensing.
- 3) **Stability:** Small perturbations in metric or initial conditions may lead to drift or instability, requiring feedback stabilization via geometric corrections.
- 4) **Detection:** Measuring the effect of micro-curvatures on trajectory in the presence of noise and other orbital effects requires extremely sensitive instruments.

These are engineering, not theoretical, limitations -- and are likely to be solved as nanosatellite, field manipulation, and optical measurement technologies mature.

E. Foundational Implications

Beyond practical implementation, this paradigm forces a reevaluation of what "propulsion" fundamentally means:

"If motion can be encoded into the curvature of space itself, is propulsion an action -- or merely a reaction to geometry?"

In the NEXUS framework, the traditional dichotomy between dynamics and kinematics collapses: motion is not a consequence of thrust, but of spatial design. Space becomes an active participant in navigation -- a programmable medium rather than a passive background.

This viewpoint connects the symbolic foundations of field theory with the engineering of future spacecraft. It suggests that in a mature physical theory, navigation and curvature, not engines, will define the next age of exploration.

XXI. Conclusion

This work introduces a symbolic framework for propulsionless motion based on geodesic inversion of engineered curvature fields. Using the NEXUS engine--a first-principles symbolic discovery system--we derive novel spacetime metrics and field configurations that naturally guide objects along prescribed trajectories without requiring external force or thrust.

Unlike traditional propulsion systems that expend energy to generate acceleration, our approach redefines motion as a consequence of geometry. We do not push the rocket forward; we reshape the manifold beneath it. The resulting motion emerges from the object's adherence to geodesics in a synthetically curved background, respecting all relativistic invariants.

Through extensive simulations, we demonstrate that NEXUS-derived metrics enable acceleration-free transport, time-of-flight reductions, and stable orbits, with zero energy input. These results open a new paradigm in trajectory design, where navigation is achieved by sculpting space rather than fighting it.

The implications of this work extend from advanced orbital mechanics to fundamental redefinitions of motion, control, and field-based navigation. Future efforts will focus on physical realization via electromagnetic analogs, plasma-curvature coupling, and experimental validation in Earth-orbit test zones. Ultimately, this line of inquiry charts a course toward curvature-based engineering as a foundation for next-generation spaceflight.

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