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Article

Comparative Fracture Resistance Analysis of Translucent Monolithic Zirconia Dioxide Milled in a CAD/CAM System

Cristian Abad- Coronel 1,*, Ángeles Paladines 2, Ana Liz Ulloa 2, César A. Paltán 3 and Jorge I. Fajardo 4

- Faculty of Dentistry. CAD/CAM Materials and Digital Dentistry Research group. Universidad de Cuenca, 10107 Cuenca, Ecuador
- ² Faculty of Dentistry, Universidad de Cuenca, 010107. Cuenca, Ecuador, maria.paladinesd@ucuenca.edu.ec_(A.P); ana.ulloaw@ucuenca.edu.ec (A.U).
- ³ New Materials and Transformation Processes Research Group GiMaT, Universidad Politécnica Salesiana, Cuenca 170517, Ecuador; cpaltan@ups.edu.ec
- ⁴ New Materials and Transformation Processes Research Group GiMaT, Mechanical Enginnering Faculty, Universidad Politécnica Salesiana, 170517 Cuenca, Ecuador, jfajardo@ups.edu.ec
- * Correspondence: cristian.abad@ucuenca.edu.ec

Abstract: The aim of this study was to evaluate and compare the fracture resistance of definitive zirconia dioxide restorations obtained using a computer-aided design and manufacturing (CAD/CAM) system. Methods: Two groups of ten samples were analyzed for each material (n: 20), the first group was Zolid Gen X Amann Girrbach (ZGX) and the second group was Cercon HT Dentsply Sirona (CDS). The restorations were designed with identical parameters and milled with a CAD/CAM system. Each specimen was load tested at a speed of 0.5 mm/min with a direction parallel to the major axis of the tooth and with an initial preload of 10N until fracture using a universal testing machine (Universal/Tensile Testing Machine, Autograph AGS-X Series) equipped with a 20 kN load cell. The results obtained were recorded in Newtons (N), using software connected to the testing machine. Results: Statistically significant differences were found, and the fracture toughness of the monolithic zirconia crowns was lower in the CDS group (1744.84 \pm 172.8 N), compared to the ZGX group (2387.41 \pm 516 N). Conclusions: The monolithic zirconia CAD-CAM zirconia crowns showed sufficient fracture strength to be used in posterior molar and premolar zones with either material as they withstood fracture loads greater than the maximum masticatory force.

Keywords: zirconia; monolithic; multilayer zirconia; fracture resistance; CAD/CAM materials

1. Introduction

In dentistry, the introduction of technological advances such as digital flow and CAD/CAM (computer-aided design/computer-aided manufacturing) systems have enabled the fabrication of fixed dental prostheses using ceramic blocks (1). CAD/CAM blocks were introduced in the dental market in 1980 (2), while the production of restorations using zirconia blocks started in the late 1990s (3).

After the production and purification process, pure zirconia can be presented in 3 phases due to its chemical structure: monoclinic, tetragonal and cubic. The cubic phase crystallizes at a temperature of 2680°C and transforms at 2370°C into the tetragonal phase. At a temperature of 1170°C it transforms to monoclinic, with a volume increase of approximately 4-5 %. The addition of yttrium oxide leads to the formation of the metastable tetragonal phase and also of the cubic portions of the structure simultaneously, maintaining the stability of the crystalline form at room temperature (4)(5). Thus, the different generations from yttria-stabilized tetragonal zirconia oxide (Y-TZP) appear: The first generation, 3Y-TZP, contains 3% in moles of yttrium and 0.25% in weight of aluminum oxide, being a more robust material, with a bending strength of up to 1200 MPa. The second generation, 3Y-TZP 3% in moles of yttrium and 0.05 wt.% of aluminum oxide, was created with the purpose of

improving translucency, reducing the alumina content of the first generation, however, it was not yet suitable for aesthetic areas, having to be layered with ceramic (6).

In 2015, a new ceramic system was introduced to the market: the tetragonal zirconia polycrystal stabilized with 5% moles of yttrium improving translucency, thus developing the third generation of 5Y-TZP. Its cubic phase reaches approximately 50% of the structure, the size and number of crystals, which are larger than 3Y-TZP, favor light transmission, reducing the refraction effect and giving better translucency with better optical properties, but with lower fracture toughness. In 2017, the fourth generation appears containing tetragonal zirconia polycrystals stabilized with 4 % moles of yttrium, increasing fracture toughness and fracture toughness than the third generation and with higher translucency than the first generation (7). In general, it has been stated that increasing the yttrium content increases the translucency of the material but decreases the flexural strength of zirconia (8) (9).

The improved mechanical properties, its biocompatibility and greater resistance to corrosion are advantages of zirconia. Its challenge is to present esthetics similar to natural dentition (10). Currently, monolithic translucent zirconia merges fracture resistance and color enhancement (11), evolving from an original white and opaque appearance to translucent, chromatic and polychromatic (multilayer) forms, which combine the favorable properties of different zirconia generations (3Y-TZP, 4Y-TZP and 5Y-TZP) (12).

Monolithic zirconia restorations became popular with the development of new CAD/CAM technologies (13) (14). It appears that monolithic translucent restorations improve survival compared to porcelain veneers with lower fracture resistance. It is a simplified procedure to make monolithic total coronal restoration, and it is the first choice compared to layered restorations avoiding the risk of chipping (15). In addition, the mechanical properties of monolithic zirconia materials are superior to those of all-ceramic restorative materials (4). In in vitro studies, monolithic zirconia single crowns showed a higher fracture resistance than layered zirconia crowns and could withstand the stresses that occur in the molar region during mastication (between 441 and 981 N) (16) (17).

Zirconia restorations can be milled in a fully sintered state (hard-state material) or pre-sintered (soft-state material). (18) In addition, high-speed sintering allows the production of zirconia restorations in a single appointment using a chairside workflow. These new rapid sintering protocols do not show a negative influence on flexural strength (19). After milling, zirconia prostheses should be sintered to achieve higher density and maximum strength (20) (21).

Monolithic Zirconia

The first multilayer monolithic zirconia system had the same yttrium content and cubic fraction in the different layers of the material, with the only difference in the pigment composition, which caused differences in shade, but not in translucency (22). Modi-fications in composition, structure and fabrication method have resulted in multilayered and precolored monolithic zirconia discs considered universal, with a balance between flexural strength and translucency, presenting a wider range of indications for single anterior and posterior crowns up to plural fixed prostheses. The most versatile combination was achieved using 4Y-TZP (fourth generation zirconia) with a more intense chroma in the base or cervical layer and 5Y-TZP (third generation zirconia) more translucent in the upper or incisal layer (23).

Monolithic zirconia dioxide can be presented with various types of translucency: low, medium, high, super and ultra, achieving different gradients of color and translucency desired for each clinical case. The grain size influences these translucent presentations, grains up to 80 nm result in a translucency similar to dental porcelains (24). Therefore, monolithic zirconia minimizes the risk of restoration failure due to chipping and incompatibility between the veneering ceramic and the zirconia ceramic (25).

1.1. Zirconia Cercon HT Dentsply-Sirona (CDS)

According to its manufacturer, because of its mechanical and esthetic properties, CDS can be applied in multi-unit crowns and bridges with a maximum of two pontics between stacked crowns in anterior and posterior regions. It is composed of yttrium-stabilized zirconia (Y-TPZ). It can be used

2

 $\leq 0.1\%$

3

as a fully anatomical restoration or as a framework to be veneered with feldspathic ceramics. Due to their composition (Table 1) they have high strength, corrosion resistance, biological compatibility and translucency (26).

Materials % Components $ZrO_2+HfO_2+Y_2O_3$ ≥94.0 % Y_2O_3 5 % **CDS** Al_2O_3 ≤1% Fe₂O₃ $\leq 0.01\%$ Other oxides \leq 0.2 % $ZrO_2+HfO_2+Y_2O_3$ ≥99.0 % Y_2O_3 6 - 7 % ZGX Al₂O₃ ≤ 0.5% Fe_2O_3 $\leq 0.5\%$

Table 1. Composition of multilayer monolithic zirconia dioxide.

1.2. Zirconia Zolid Gen-X Amann Girrbach (ZGX)

It is a highly translucent and highly resistant multilayer monolithic zirconia oxide material, with a chromatic transition that improves its efficiency and esthetics, blending well with natural teeth. It is virtually divided into four horizontal layers to adapt perfectly to the color gradient, simplifying the choice of material for its multiple indications such as fully anatomical crowns and bridges from 4 pieces and anatomically reduced crown structures (Table 1).

Other oxides

Monolithic zirconia has been continuously developing and it is necessary to know properties such as fracture resistance of these new materials. Compared to other ceramic materials, monolithic zirconia significantly reduces the space required for the preparation of the restoration and, therefore, contributes to a prosthetic restoration that preserves the greatest amount of tooth structure (19). Therefore, the objectives of this research were to evaluate and compare the fracture resistance of two CAD-CAM materials, zirconia dioxide (CDS) and (ZGX), stating as null hypothesis that there would be no significant differences in fracture resistance between the zirconia dioxide restorations studied.

2. Materials and Methods

2.1. Materials

Two translucent monolithic zirconia dioxide materials (CDS and ZGX) were selected. A typodont was used with a preparation to make a full crown, following the following parameters: 2 mm occlusal reduction, 1.0 mm axial reduction, chamfered termination line, parallelism between axial walls of 6 degrees and rounded edges. A digital file of the preparation was obtained with a high power structured light scanner (PrimeScanTM, Dentsply-Sirona TM, New York, USA).

2.2. Digitalization of the model and design

Once the model was digitized, the restoration was designed in an integrated design software (InLAB SW 22.0, Dentsply-SironaTM, Bensheim, Germany) (Figure 1). For milling, the information was transferred to an integrated milling machine (CEREC InLab MCXLTM, York, Pennsylvania, USA). Twenty restorations were made in two groups of 10 specimens for each material (Figure 2).

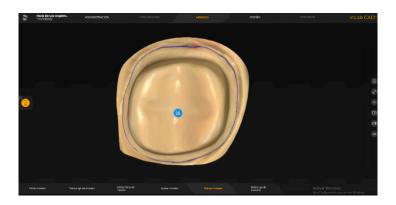


Figure 1. Digitization of the model.





Figure 2. Restorations on CAD-CAM disks of zirconia dioxide before sintering.

2.3. Sinterization

Sintering of the zirconia dioxide restorations was carried out in a slow sintering furnace (InFire HTC, CEREC SpeedFire, Dentsply-Sirona, Bensheim, Germany) with a sintering time of 8 hours at a maximum temperature of $1500\,^{\circ}$ C on a preset pro-gram for the material.

2.4. Fracture test

A cast metal master die (Figure 3 [a]) was obtained from the initial scan of the original dowel type, suitable for load testing. The specimens were supported with non-cemented metal die and placed on the platform of the universal testing machine (Universal/Tensile Testing Machine, Autograph AGS-X Series).



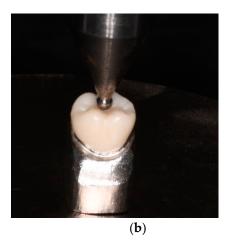


Figure 3. (a) Master die in cast metal. (b) Load of the punch in tempered steel on the sample seated in the cast metal die.

The specimen was load tested at a rate of 0.5 mm/min with a direction parallel to the major axis of the tooth with an initial preload of 10N (Figure 3 b) equipped with a 20kN load cell. The load was applied through a hardened steel pilot punch with a radius of 3mm applied in the central pit of the crown until fracture occurred. The force/displacement of the specimens was determined using the built-in software (TRAPEZIUM LITE X Software). The results were expressed in newtons (N).

2.5. Evaluation of the fracture mode

The fracture surface of the samples after loading was observed and analyzed using a high-resolution stereomicroscope (Olympus; SZX7, USA).

3. Results

3.1. Descriptive Analysis

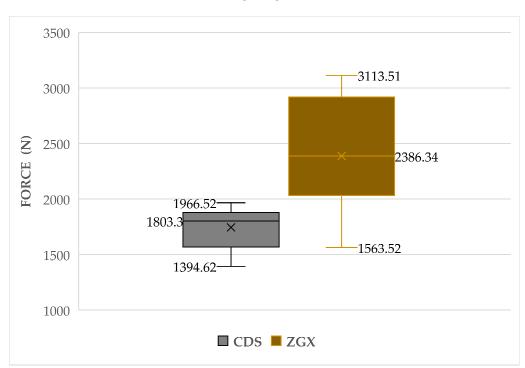
Table 2 shows the descriptive statistics of the fracture toughness of materials used in this study.

Table 2.

CAD/CAM material	Media (SD)	CI 95%	CV	Minimum	Maximum
CDS	1744,84 (172,80)	(1628,75;1860,93)	9,9%	1394,60	1563,50
ZGX	2387,41 (516,10)	(2018,23;2756,59)	21,6%	1966,50	3113,50

Note: Fracture strength expressed in Newtons. SD: standard deviation, CV: coefficient of variation.

The ZGX material showed higher average fracture resistance with 2387.41 (SD = 516.10) N, the 95% confidence interval for the mean was (2018.23;2756.59) N, the coefficient of variation value indicated a mean dispersion (CV=21.9%), with a minimum and maximum strength of 1966.50 N and 3113.50 N, respectively. In comparison, the values reported with the CDS material yielded lower average fracture toughness with 1744.84 (SD = 172.80) N, the 95% confidence interval for the mean was (1628.75;1860.93) N, the dispersion was low (CV = 9.9%), and the observations were between Min = 1394.60 N and Max= 1563.50 N (Table 2). Figure 4 shows the quartiles, maximum and minimum values. From the comparison it was observed that the maximum value reached with the CDS material was lower than Quartile 1 (25%) of ZGX, showing a higher resistance.



6

Figure 4. Box and whisker diagram for fracture resistance of CAD/CAM materials in zirconia dioxide.

Figure 5 shows the average fracture resistance of the materials. ZGX presented higher values than CDS.

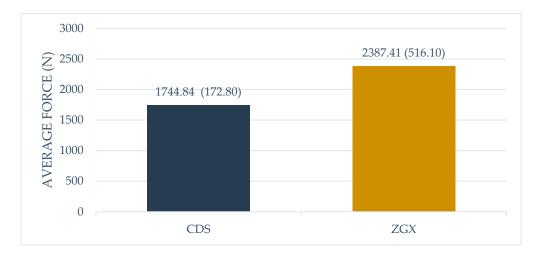


Figure 5. Bar chart for average fracture strength of CAD/CAM materials in zirconia dioxide.

3.2. Inferential analysis

With the results in Table 3, the null hypothesis that the fracture toughness measurements are normally distributed was not rejected, with the Shapiro-Wilk statistic (p-value > 0.05), and the null hypothesis of equality of variances (p-value < 0.05) was rejected by Levene's test. Consequently, to evaluate the research hypothesis, the parametric test was used, with Student's t-statistic for independent samples assuming different variances.

Table 3. Normality and Levene test (verification of assumptions).

	CAD/CAM material	Shap	Shapiro-Wilk			Levene	
		Statistic	gl	P-value	F	P-value	
CDS		0,92	10	0,33	7,15	0,02	
ZGX		0,95	9	0,71			

Note: Significance level 5%.

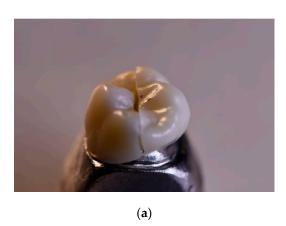
According to Table 4, the null hypothesis was not accepted (t=-3.75, p-value = 0.003<0.05). It was then determined, with a significance level of 5%, that there were significant differences between CDS and ZGX.

Table 4. Descriptive statistics of fracture resistance of CAD/CAM materials in Zirconia Dioxide.

CAD/CAM material	Media (DE)	Statistical T-de Student	P-value
CDS	1744,84 (172,80)	-3,75	0,003<0.05
ZGX	2387,41 (516,10)		

Note: Significance level 5%, Average testing for independent samples.

From the fractographic analysis, it is observed that the two materials under study present a brittle fracture. Once the critical stress value is reached, brittle materials present unstable cracks, that is, do not require an increase in stress for the spontaneous propagation of the crack and catastrophic failure occurs (Figure 6).



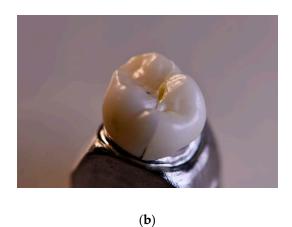


Figure 6. Images of the fracture surfaces of the different materials studied: (a) CDS; (b) ZGX.

4. Discussion

The all-ceramic crown is a common restorative method for a tooth that has lost much of its structure (27). Compared with the metal-ceramic crown, it has excellent biocompatibility and esthetic appearance, magnetic resonance imaging compatibility, and superior refractive index and transparency (28). Currently, materials used in all-ceramic crowns include mainly feldspathic, silicabased and yttria-stabilized tetragonal zirconia polycrystals (Y-TZP) ceramics (29). Full-contour zirconia restorations are gaining popularity in the market at the expense of multilayer systems (30). CAD/CAM applications offer a standardized fabrication process with a reliable and predictable workflow for single and complex restorations on teeth (31). Monolithic zirconia crowns have high flexural strength and fracture toughness (32). Mechanical properties such as fracture resistance would be affected by the different composition of each material. However, if these properties exceed the masticatory forces, they are clinically favorable for application in the posterior sector. Therefore, materials such as zirconium dioxide with high toughness, due to their fully crystalline microstructure and thanks to the presence of a resistive transformation mechanism, exhibit superior fracture toughness values in relation to other ceramic materials by preventing fracture propagation (33).

Therefore, the objective of this research was to compare, through an in vitro study, the fracture resistance of zirconium oxide crowns of two different commercial brands (CDS and ZGX). The null hypothesis was rejected, and it was concluded that there are differences in average fracture resistance between both CAD/CAM materials. In addition, mean fracture strengths of 1744.84 ± 172.8 N were observed for CDS and a higher strength of 2387.41 ± 516.1 N for ZGX, This differs from that reported in a study, where they compared the fracture load of four brands of zirconia, whose reported mean fracture loads were, 4804.94 ± 70.12 N, 3317.76 ± 199.80 N, 3086.54 ± 441.74 N and 2921.87 ± 349.67 N for Cercon HT, Cercon XT, Zolid Gen X and Vita YZ XT, respectively, the crowns were sandblasted before cementing to increase bond strength. Zolid Gen X had the most cracks overall, while Cercon HT crowns had the fewest cracks. Concluding that, Cercon HT presented the best strength properties, the highest fracture load and no visible cracks and that Zolid Gen X presented the lowest strength properties (34). In contrast to our study the crowns were not cemented; in a study by Sorrentino et al. who cemented the restorations with a dual-curing self-adhesive universal resin cement to simulate a real clinical situation, the formation of an adhesive layer probably contributed to increase the fracture toughness, allowing the cement to act as an elastic stress adsorbent and compensating the stiffness of the zirconia core, this could strengthen the restoration, allowing to dissipate occlusal loads over the entire surface of the crowns.(35)

Bulut in his study concluded that the occlusal thickness and the type of cement significantly affected the fracture resistance of the crowns, but the occlusal thickness was more significant. Samples of 0.5, 1.0 and 1.5 mm were made, the 1.5 mm crowns cemented with a resin cement showed higher fracture resistance compared to the other thicknesses however no significant differences were found therefore posterior zirconia crowns can withstand physiological occlusal forces even with a thickness as low as 0.5 mm (36). Corroborating with this, Sorrentino et al. similarly suggested that

8

the occlusal thickness could be reduced to 0.5 mm without affecting fracture resistance, the crowns exhibited high fracture resistance at this 0.5 mm thickness, with a fracture load of 1400 NW being clinically acceptable. In a literature review on zirconium dioxide-based restorations, the results showed a performance similar to that of this study in terms of fracture resistance, being a resistant material suitable for this purpose both in areas with high functional load, as well as in esthetic areas of the patient (37).

An important aspect to mention is that the production of the restorations in this study involved several stages such as milling and sintering, therefore, some self-report certain limitations of the material as the production of the restorations involves several processing steps that could cause defects in the finished product (38). Therefore, there are currently studies that analyze whether variables in the production process could affect the clinical success of monolithic zirconia crowns (39) (40) (41).

An in vitro study by Kauling (42) evaluated the properties of 3-unit zirconia monolithic fixed dental prostheses (FPD) after rapid sintering and compared the properties with conventional sintering. They found that the fast-sintering FPDs had a better marginal and occlusal fit than the conventionally sintered FPDs. In addition, no significant differences in fracture load values were found due to the sintering procedure, but artificial aging was found to significantly affect the fracture load values. In general, fast sintering FPDs had equal and better values for fracture set and fracture load than conventional sintering FPDs. However, other authors concluded that there was no significant difference between the two groups, and the mechanical strength of the material was not affected, which would imply clinical and laboratory time savings when performing rapid sintering on translucent monolithic zirconium dioxide restorations. However, rapidly sintered restorations have limited reliability depending on the case (43).

In another study, the flexural strength of different kinds of multilayered zirconia in enamel and dentin layers was evaluated. The strength was similar for that of both layers and the multilayer restoration accumulated the highest strength, followed by the translucent super multilayer and the ultra-translucent multilayer. However, the strength of the transverse multilayer was lower than that of the enamel or dentin layers due to weak interfaces. In addition, it was mentioned that, when measuring strength by bending, there may be errors due to friction and accuracy in determining the distances of the loading spans (44). The result of resistance to fracture shown with CDS in this research was similar to that obtained in a study where they compared the resistance to fracture between a group of crowns made to measure and a group of prefabricated crowns, both made of Cercon HT Dentsply-Sirona Zirconia (34); yielding an average resistance of 1987.38 \pm 414.88 N for the crowns made to measure and 1793.54 \pm 423.82 N for the prefabricated ones, finding no significant differences between the two. According to Ottawa: (Canadian Agency for Drugs and Technologies in Health) the average resistance to initial fracture shown with Zolid Gen-X was 2634 \pm 106.2 N and after aging in a chewing simulator it was 2087 \pm 126.1 N, showing similar values to those reported in the present investigation (27).

Table 5. Comparative of fracture resistance of CAD/CAM materials in Zirconia Dioxide.

Materials		Results	
CDS	Abad C. 1744,84 ± 172,80 N	Kongkiatkamon S. (1987,38 ± 414,88 N)	
ZGX	Abad C. 2387,41 ± 516,10 N	Ottawa 2634 ± 106,20 N	

It should be noted that, during the load test that was performed in the first instance, a printed resin die was used and during the process the initial failure was of the die, so it was chosen to perform it in a more resistant material. In this case, a cast metal cobalt-chromium die with higher elastic modulus and fracture resistance, however a natural tooth could have replicated the clinical environment more accurately if it had been chosen as an abutment, however natural teeth have different sizes, shapes and qualities, and therefore the preparation material would be difficult to standardize (45).

Laboratory tests apply static loads until the material breaks by means of a universal machine, representing its behavior in a force-displacement curve and recording the maximum load applied. These tests provide information on the strength of the material, the potential risk of failure and the deformation of the material. However, they cannot sufficiently predict the long-term performance of dental restorations. Badawy et al. (46) mentioned in their study the importance of knowing the fracture toughness of dental ceramics, which by nature are brittle and have an increased susceptibility to fracture under stress. A restorative material with high fracture toughness presents better fracture resistance and longevity. Being an in-vitro study, one of the limitations of this research is that the behavior of these materials under cyclic fatigue was not analyzed. Fracture toughness testing, using a single unidirectional compressive load, provides only limited insight into clinically relevant mechanisms of crown damage under forces with different directions and cyclic loading. (43) Future research needs to analyze the cyclic fatigue and clinical behavior of this material over time, as well as to analyze the material cemented with different adhesive techniques. Therefore, experimental settings that reproduce situations similar to intraoral conditions are needed. More evidence from long-term clinical studies is needed to verify the fracture performance of monolithic zirconia CAD/CAM materials for indirect full-coverage restorations.

5. Conclusions

- It was found that the ZGX material, obtained higher fracture resistance compared with the CDS.
- The crown fracture loads of the two materials were in the acceptable range. In comparison with the maximum bite force, the materials showed an acceptable load-to-fracture value.
- The monolithic zirconia crowns showed a favorable mechanical property to withstand the occlusal load at 0.5 mm thickness.

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9

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