

Article

Optimization Design Analysis of Movable Rotating Plate Type Grading Device for Potato

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Abstract: Given the existing movable rotating plate type grading device for potatoes with a high safety factor and heavy mass, the body frame of the grading device and movable rotating plate were optimized and a lightweight design was carried out. Based on ANSYS Workbench 2022, the static analysis of the body frame before and after improvement was compared, and it was verified that the strength and deformation of the optimized body frame met the design requirements, and the weight of the optimized body frame was reduced by 32.3%. Based on the direct optimization module of ANSYS Workbench 2022, the plate length, width, and height were used as design variables for the lightweight design of the movable rotating plate. The MOGA algorithm was used to generate sixty design solutions, and the optimal combination of size parameters for the plate was 610 mm, 95mm, and 1.2 mm. Compared with the whole grading device before optimization, the total mass was reduced by 22.86% after optimization. The research of this article provides a reference for the structural design and optimization analysis of potato grading devices.

Keywords: movable rotating plate; potato; grading; optimization; ANSYS Workbench

1. Introduction

Potato is one of the world's most important food crops. China's potato cultivation area is located in the world's first, but the potato mechanization production degree is low. Potato mechanization research has been urgent with the potato staple food strategy promoted [1-3]. Potato grading devices are necessary equipment in potato harvesting, and related scholars have conducted extensive research. Currently, there are roller shaft-type, screen-type, and drum-type grading devices for potatoes [4]. These three grading devices in the grading process on the potato damage, grading grade less and grade adjustment is more complicated, seriously affecting the efficiency of potato grading [5-7]. Therefore, we researched and designed the movable rotating plate type grading device for potatoes, which adopted a movable rotary plate with an adjustable gap, high grading efficiency, and three grading levels. Still, the grading device has a high safety factor and heavy mass, which needs to be optimized and improved.

The traditional optimization mode, which requires changes to the physical object, is time-consuming and costly. In contrast, the virtual simulation optimization design method can shorten the design cycle and save costs to a large extent [8]. There are more reports on virtual simulation optimization in China and abroad. Krasnyuk A. M. et al. [9] used optimality criterion based on ANSYS software for the topology-optimized design of axial fan blades with a 60% reduction in blade mass. Yan[10] conducted the lightweight design of the frame of a tensile machine based on ANSYS Workbench, the equivalent force and total deformation of the optimized model were reduced, and the weight was reduced by 7.11%. Ma et al. [11] optimized the frame of a light truck based on ANSYS using the homogenization method to obtain an optimized frame topology that satisfied the volume constraint and minimized the total flexibility. Gadwala William Kery et al. [12] carried out the optimization of a sports car rim using ANSYS Workbench finite element analysis, which identified carbon fiber as a feasible material for manufacturing the sports car rim. Jackis Aukah et al.[13]

optimized a husked corn dryer using ANSYS Workbench, and found that the air velocity at the collector inlet and biomass heat exchanger outlet should be increased to 3m/s and 2.8m/s, respectively. Muhammad Aisha et al. [14] used the finite element method in ANSYS Workbench to optimize the topology of a steering knuckle, and the optimization determined the mass to be removed. Similarly, Sharma M P et al. [15] used CREO2.0 in combination with ANSYS workbench to optimize the shape of the automotive steering knuckle. Jha et al. [16] used CATIA in combination with ANSYS Workbench to optimize and improve the steering knuckle. Li et al. [17] improved and optimized the base structure of the welding robot based on ANSYS Workbench. The original model was analyzed and compared with the improved and optimized solution, and the expected optimization objectives were achieved. Feng et al. [18] used ANSYS Workbench to optimize the design of the fan base of the motor, and the structural stresses under various operating conditions were simulated and verified. Li Chuchen et al. [19] used ANSYS Workbench's response surface optimization for the lightweight design of a particular vehicle's on-board lens, and the lens's total mass was reduced by 20.69% after optimization. Li Xiang et al. [20] optimized the potato excavator suspension based on ANSYS Workbench and the response surface method and obtained the optimized suspension thickness, which can effectively reduce the deformation.

The analysis of the existing studies shows that the virtual simulation optimization design method, which can be cost-saving and high efficiency, has rarely been reported for the optimization design of potato grading devices. Therefore, given the problems of high safety factor and heavy mass of the existing movable rotating plate type grading device for potatoes, this article uses the virtual simulation optimization method based on ANSYS Workbench 2022 to optimize the design of the body frame and movable rotating plate to reduce the weight while the strength and deformation meet the design requirements.

2. Materials and Methods

2.1. Movable rotating plate type grading device for potato

A movable rotating plate type grading device for potatoes (shown in Figure 1), according to the movable rotating plate gap size as a way to grade potatoes, shows its grading principle schematic diagram in Figure 2. The movable rotating plate moves in a cycle with the conveying chain, and the bottom is in contact with the slide rails on both sides. With the change in the tilting angle of the slide rails, the gap between adjacent rotating plates gradually increases. Potatoes of different sizes fall into the potato-collecting device from different gaps.



Figure 1. Movable rotating plate type grading device for potato.

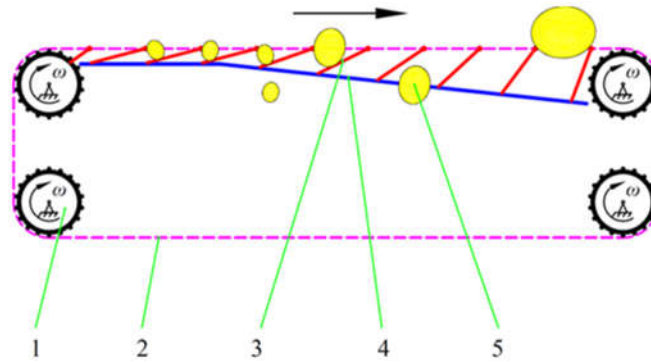


Figure 2. Schematic diagram of potato grading principle. 1. Sprocket. 2. Chain. 3. Movable rotating plate. 4. Slide. 5. Potato.

The body frame (shown in Figure 3) is composed of the chain fixing part and the base. The chain fixing part mainly plays the role of fixing the chain and the movable rotating plate assembly, which is made of square steel pipe welded together, and the steel plate is welded on the steel pipe to fix the bearing seat. The size of the square steel pipe is 40×40×4(mm), and the thickness of the steel plate is 8mm. The base is made of rectangular steel pipe welded together, which is 40×30×3(mm).

The size of the body frame is 1400×896×780 (mm), and the total mass is 157.82 kg. Given its high safety factor and large overall mass, it is designed to be lightweight.

The movable rotating plate (shown in Figure 4) consists of a rotating plate movable shaft, rotating plate, and rotating plate friction shaft, which are connected by welding. The rotating plate movable shaft is the central part that connects the rotating plate and the chain. It is connected to the bracket on the chain part and drives the movement of the rotating plate. The rotating plate friction shaft is in contact with the slide rail, and its main role is to avoid direct contact between the rotating plate and the slide rail, resulting in the wear deformation of the rotating plate.

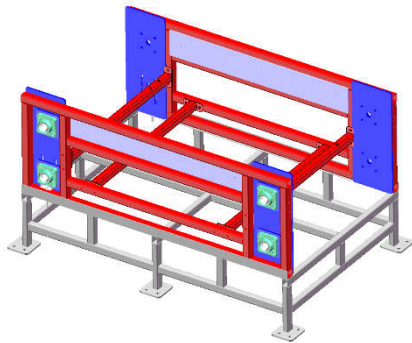


Figure 3. Grading device frame.

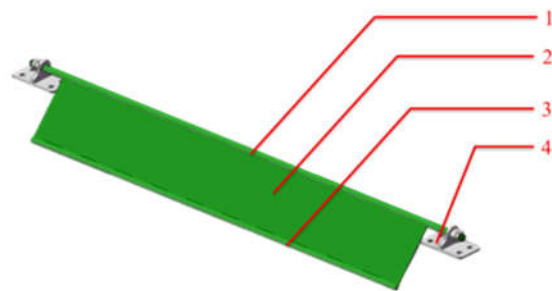


Figure 4. Movable rotating plate 1. Rotating plate movable shaft. 2. Rotating plate. 3. Rotating plate friction shaft. 4. Bracket.

The size of the existing rotating plate is 640×95×2 (mm) in length, width, and thickness, respectively, and the total mass of the single movable rotating plate is 1.7449kg. There are 32 groups of movable rotating plates in the machine, which causes the heavy mass and inconvenient for operation.

2.2. Static analysis of existing body frame

2.2.1. Analysis of load on the body frame

The total mass of the chain and movable rotating plate assembly (shown in Figure 5) is 134.23 kg, and the total mass of the potatoes when the grading device is fully loaded (shown in Figure 6) is 16.153 kg. Therefore, the force applied to the body frame is as follows.

$$0$$

$$F=(134.23+16.153) \times 9.8=1473.75\text{N}$$

$$(1)$$

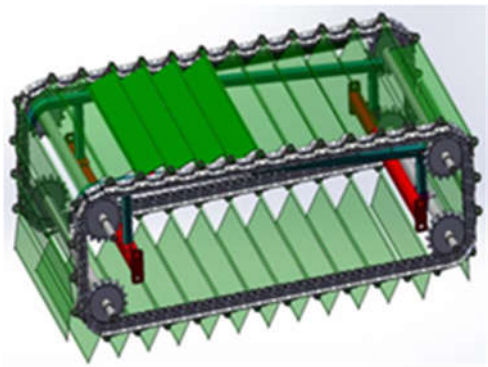


Figure 5. Diagram of chain and movable rotating plate assembly.



Figure 6. A full load of grading device.

2.2.2. Pre-processing of the static Analysis of the body frame

According to the design requirements, the material of the body frame is Q235, and the material properties are shown in Table 1.

Table 1. Material properties.

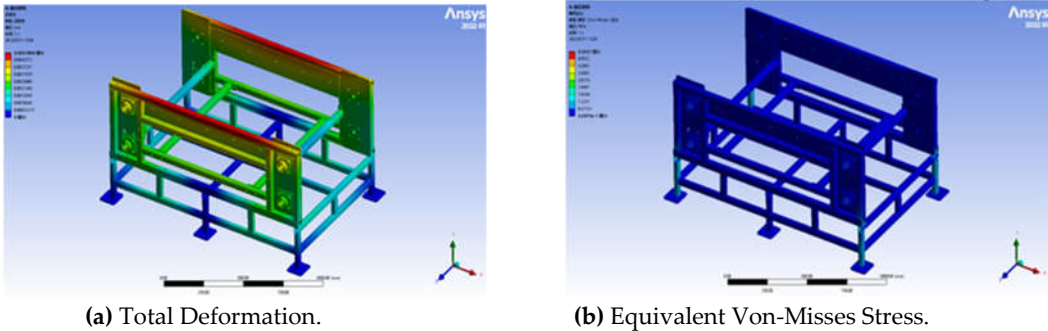
Materials	Density(Kg/m³)	Young's Modulus/Pa	Poisson's Ratio	Yield Strength/Pa	Tangential Modulus/Pa
Q235	7850	2.12×10 ¹¹	0.288	2.35×10 ⁸	6.1×10 ⁹

The parts of the body frame are welded and bolted together, so the contact setting is "binding." When analyzing in ANSYS, the mesh division's size and the mesh division's quality at key locations will directly affect the accuracy of the analysis results [21]. The dense the mesh division, the more accurate the calculation results, but the calculation volume will increase [22]. The overall tetrahedral meshing method is adopted for the frame, the order of the elements is selected as second order, and the mesh cell size is set to 8mm. The critical position of the force contact is in the bearing seat, so the mesh cell size is set to 3mm. The completed meshing generates 1628000 nodes and 888646 cells.

Fixed supports are set on the bottom surface of the six foot seats of the body frame and force are applied to the eight bearing surfaces with a total combined force of 1473.75 N, i.e., 184.21875 N on each surface, and the direction is vertically downward.

2.2.3. Solving

The total deformation and equivalent Von-Misses stress of the body frame were solved and the clouds of the total deformation and equivalent Von-Misses stress were shown in Figure 7.



(a) Total Deformation. **(b)** Equivalent Von-Misses Stress.

Figure 7. Analysis diagram of the rack before optimization.

The total deformation cloud diagram showed that the deformation at the upper steel tube of the body frame was more significant, the overall deformation gradually decreased from top to bottom, and the maximum deformation was 0.0047894 mm. The equivalent stress cloud diagram showed that

the stress was mainly concentrated on the eight bearing positions and the four vertical beams of the base, and the maximum stress value was 5.5037 MPa.

Based on the above analysis results, it was seen that the existing body frame met the strength requirements, the safety factor was relatively high, and the redundancy is high. Therefore, there was a large space for the lightweight optimization of the body frame.

2.3. Static Analysis of existing movable rotating plate

2.3.1. Calculation of the Load on the movable rotating plate

During the movement of the rotating plate, the angle between the rotating plate and the horizontal plane is continuously changing from 0 to 90 degree. When the rotating plate is parallel to the horizontal plane, the maximum load is applied. To obtain the maximum load, the whole surface of the rotating plate is covered with potatoes (Figure 8) and the total mass is 2.63 kg, which equals to 25.8N.



Figure 8. Single movable rotating plate covered with potatoes.

2.3.2. Statics analysis pre-processing of movable rotating plate

According to the design requirements, the material of the movable rotating plate is Q235, and the material-related parameters are the same as the body frame.

The movable shaft, the friction shaft, and the rotating plate are welded together so they are "bound" to each other. The mesh division method is "automatic", the mesh cell size is set to 2mm, and the mesh division generates 426133 nodes and 250562 cells.

During the static analysis, the fixed constraints are applied to the connection between the rotating plate and the chain, as well as the contact position with the slide rail. The force applied to the movable rotating plate is 25.8N, and the direction is perpendicular to the rotating plate downward.

2.3.3. Solving

The total deformation and equivalent Von-Mises stress were analyzed in the solution option, and the clouds of the total deformation and equivalent Von-Mises stress were derived, as shown in Figure 9.

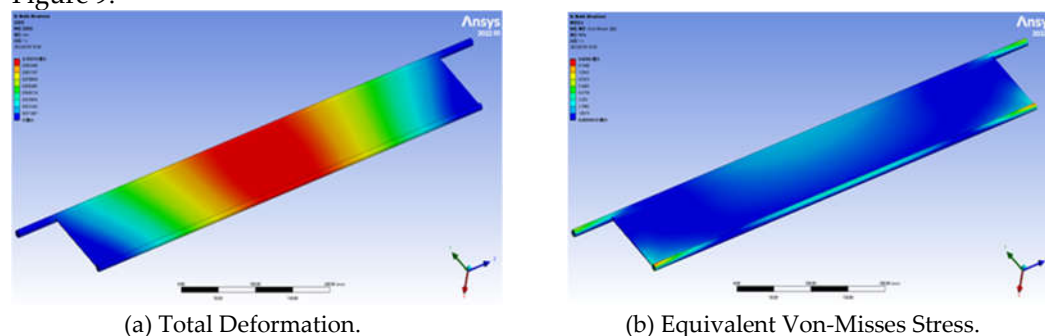


Figure 9. Analysis clouds of the rotating plate before optimization.

The total deformation obtained from the simulation results showed that the deformation mainly occurred in the middle part of the rotating shaft, rotating plate, and friction shaft. The overall

deformation increased gradually from the two ends of the movable rotating plate to the middle part, reaching the maximum deformation of 0.10513mm in the central part.

The analysis of the equivalent Von-Misses stress diagram showed that the stress was mainly concentrated in the two ends of the rotating shaft and the friction shaft. The main reason was that the two ends of the movable rotating plate shaft were connected to the bracket, which caused the stress concentration during the movement. However, the friction shaft was contacted with the sliding rail, and there was also stress concentration during the movement. The maximum stress was 9.8396MPa, which was less than the material yield strength of 235MPa.

According to the above analysis results, it can be seen that the movable rotating plate met the strength requirements, and the design can be optimized from the perspective of dimensional parameters.

3. Results and Discussion

3.1. Body frame optimization design

3.1.1. Body frame structure improvement

The wall thickness of the square steel pipe, which is composed of the body frame, is an essential factor affecting the quality of the structure, so the wall thickness is changed from 4mm to 2mm. The overall body frame has six 8mm thick side plates, which are mainly used to fix the bearing seat and chain brace. Considering its high safety factor, the wall thickness of the side plates is changed to 5mm. The base is an important part bearing the whole machine, and the structure is also improved for optimization. The optimized body frame is shown in Figure 10, and the total mass is 106.84kg.



Figure 10. Optimized body frame.

3.1.1. Static analysis of improved body frame

The optimized body frame was subjected to static structural analysis with the same mesh division, fixed supports, and load constraints as the body frame before optimization, and the total deformation and equivalent Von-Misses stress analysis results were obtained, which were shown in Figure 11.

The maximum total deformation of the final optimized rack is 0.0063963mm, and the maximum equivalent Von-Misses stress is 4.8083MPa. The deformation was still in the middle part of the steel tube above the frame, but the total deformation was minor. The stress was concentrated on the bearing position and the vertical beam of the frame base, and the stress was much smaller than the yield stress.

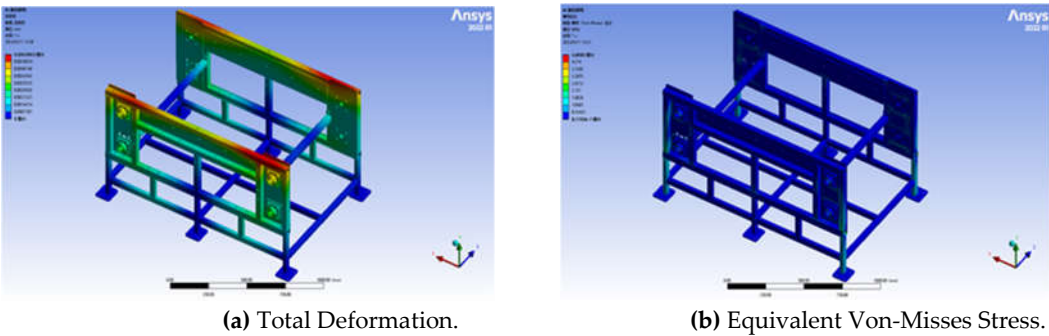


Figure 11. Clouds of optimized body frame analysis results.

In summary, the optimized body frame met the strength requirements and the machine's total mass reduced significantly. A comparison of the relevant parameters before and after the optimization of the body frame was shown in Table 2, and the total mass was reduced by 32.3% compared with the pre-optimized frame.

Table 2. Comparison of relevant parameters before and after frame optimization

Projects	Steel pipe wall thickness/mm	Side plate thickness/mm	The total mass of frame/kg
Before optimization	4	8	157.82
After optimization	2	5	106.84

3.2. Optimized design of the movable rotating plate.

3.2.1 Rotating plate friction shaft improvement

The existing rotating plate friction shaft is $\Phi 9\text{mm}$ in diameter and 640mm in length. In view of its contact position with the slide rail only at the two ends, the friction shaft can be split into two sections, and the length of each section is 50mm. The schematic diagram of the improved friction shaft is shown in Figure 12.

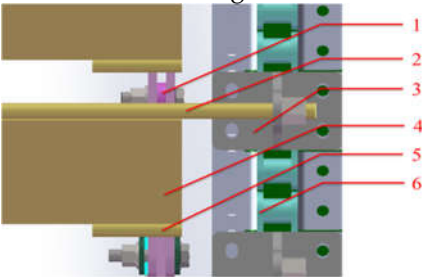


Figure 12. Schematic diagram of the improved friction shaft of the rotating plate. 1. Slide rail. 2. Rotating plate movable shaft. 3. Bracket. 4. Rotating plate. 5. Rotating plate friction shaft 6. Chain.

3.2.2 Size optimization of rotating plate

To facilitate optimization and simplification of the model, the rotating plate friction shaft of the rotary plate was not modeled for the time being. The improved model of movable rotating plate was established in SolidWorks, and the length, width, and thickness of the rotating plate was define as the design variables based on the configuration requirements of the Workbench optimization module[23,24], as shown in Table 3.

Table 3. Design variable parameterization.

Design variable name	Size / mm	Meaning of variables
DS_D1@ thin-stretch1	640	the length of the rotating plate
DS_D2@ sketch2	95	the width of the rotating plate

DS_D3@thin-stretch1

2

the thickness of the rotating plate

The improved model can be imported directly into Workbench using the interface between SolidWorks and Workbench for static structural analysis. According to the design requirements, Q235 was selected as the material for the movable rotating plate. The design variables were selected in the Design Modeler, and the model was then ready for static structural analysis.

The rotating shaft and rotating plate were welded, so they were "bound" contact. The mesh division method used "Automatic." The mesh cell size was set to 2mm, and 211,015 nodes and 80,593 cells were generated by grid division. The grid quality of the movable rotating plate met the requirements through the verification of grid evaluation statistics provided by Workbench.

The fixed restraint and load applied to the movable rotating plate were the same as in the previous section.

The model's total deformation and equivalent Von-Mises stress were analyzed in the solution option, and the clouds of the total deformation and equivalent Von-Mises stress were derived, as shown in Figure 13.

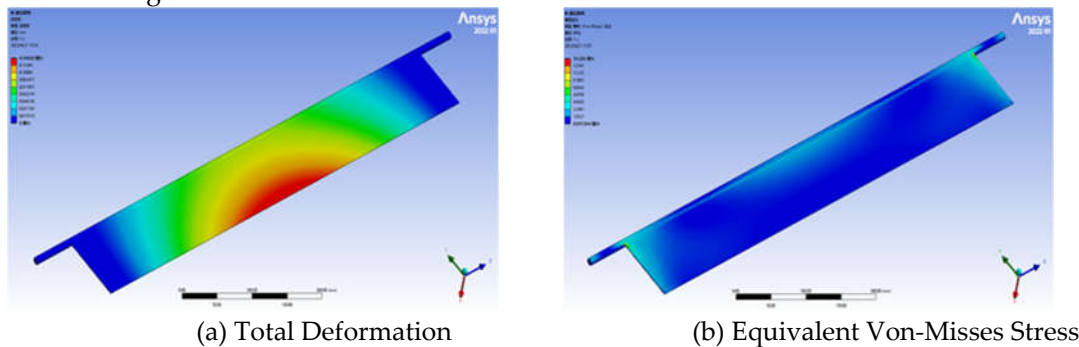


Figure 13. Analysis clouds of the movable rotating plate before optimization.

The total deformation cloud obtained from the simulation results showed that the main deformation occurred in the middle part of the rotating plate and the central part of the rotating shaft, and the maximum deformation was 0.14022 mm. The results of the equivalent Von-Mises stress showed that the maximum stress value was 14.556 MPa.

3.2.3 Build the mathematical optimization model

Structural optimization is usually done by varying the design variables to optimize the structure without affecting its performance and to satisfy the constraints[25]. By changing the dimensional parameters of the rotating plate, the mass is reduced as much as possible while ensuring that the deformation and stresses are within the safety factor.

This optimization design uses the direct optimization module in Workbench to optimize the design and seek the optimal combination of the dimensional parameters of the rotating plate. Therefore, the length P_1 , width P_2 , and thickness P_3 of the rotating plate are design variables, and the setting of size range was mainly determined based on usage and manufacturing requirements. The maximum deformation P_4 , the maximum equivalent force P_5 and the mass P_6 are used as the optimization objectives, where the stress is taken as a safety factor of 1.5 to obtain the allowable stress of 156 MPa, i.e., the minimum stress must not exceed 156 MPa. The following mathematical model for optimization design is derived:

$$\left\{ \begin{array}{l} \min \left\{ \begin{array}{l} p_4 = f_1(p_1, p_2, p_3) \\ p_5 = f_2(p_1, p_2, p_3) \leq 156 \text{ MPa} \\ p_6 = f_3(p_1, p_2, p_3) \end{array} \right. \\ \text{s.t.} \left\{ \begin{array}{l} p_1 \in (610, 616, 620, 640) \\ p_2 \in (95, 98, 100) \\ p_3 \in (1, 1.2, 1.5, 1.8, 2) \end{array} \right. \end{array} \right. \quad (2)$$

3.2.4 Building a direct optimization model

The optimization algorithm must first be defined to establish a direct optimization model. Based on the optimization requirements of multiple independent variables and multiple objective functions in this article, the MOGA algorithm was used for optimization analysis, which supported multiple objectives and constraints, required continuous input parameters, and was well suited for calculating global maxima or minima, to find the global optimum while circumventing the pitfalls of local optima [26,27]. In the MOGA algorithm setup, the initial sample capacity was set to 100, the number of samples generated per iteration was 50, the maximum number of iterations was 20, and the maximum number of candidates was 3.

The objectives and constraints were set based on the above mathematical model for the rotating plate's length P_1 , width P_2 , and thickness P_3 . The optimization scheme was updated after the parameter setting, and then the solution started.

The total deformation, equivalent Von-Misses stress, and mass of the model for the different cases of length, width, and thickness of the rotating plate were obtained by analyzing the generated 60 sets of design solutions, as shown in Table 4.

Table 4. Raw optimization data

Serial number	P_1 / mm	P_2 / mm	P_3 / mm	P_4 / mm	P_5 / MPa	P_6 / kg
1	610	95	1	0.335376	31.37097	0.924593
2	616	95	1	0.33314	31.54316	0.929073
3	620	95	1	0.338713	31.4189	0.93206
4	640	95	1	0.343188	33.55511	0.946994
5	610	98	1	0.353951	31.02046	0.938977
6	616	98	1	0.351401	31.18514	0.943598
7	620	98	1	0.357154	31.05804	0.946679
8	640	98	1	0.36119	33.17132	0.962085
9	610	100	1	0.366924	30.81309	0.948566
10	616	100	1	0.364175	30.97273	0.953282
11	620	100	1	0.370046	30.84402	0.956426
12	640	100	1	0.373807	32.94609	0.972146
13	610	95	1.2	0.247201	26.80225	1.01569
14	616	95	1.2	0.246619	26.99724	1.021066
15	620	95	1.2	0.250821	26.8091	1.024651
16	640	95	1.2	0.25723	28.43592	1.042571
17	610	98	1.2	0.258042	26.48829	1.032951
18	616	98	1.2	0.257254	26.67827	1.038497
19	620	98	1.2	0.261565	26.4883	1.042194
20	640	98	1.2	0.267701	28.09787	1.060681
21	610	100	1.2	0.265646	26.29697	1.044458
22	616	100	1.2	0.26473	26.48342	1.050117
23	620	100	1.2	0.269111	26.29202	1.05389
24	640	100	1.2	0.275079	27.8929	1.072754
25	610	95	1.5	0.178684	21.59502	1.152336
26	616	95	1.5	0.179551	21.69055	1.159057
27	620	95	1.5	0.1823	21.58057	1.163537
28	640	95	1.5	0.189913	22.48546	1.185938
29	610	98	1.5	0.184138	21.33209	1.173912
30	616	98	1.5	0.184898	21.4249	1.180844
31	620	98	1.5	0.187684	21.31408	1.185466
32	640	98	1.5	0.195152	22.20793	1.208575
33	610	100	1.5	0.188006	21.16695	1.188296
34	616	100	1.5	0.1887	21.25752	1.19537

35	620	100	1.5	0.19151	21.14581	1.200086
36	640	100	1.5	0.198891	22.03336	1.223666
37	610	95	1.8	0.140836	17.79926	1.288982
38	616	95	1.8	0.142329	17.86102	1.297047
39	620	95	1.8	0.14429	17.78071	1.302423
40	640	95	1.8	0.15203	18.18255	1.329304
41	610	98	1.8	0.143799	17.57471	1.314873
42	616	98	1.8	0.145232	17.63877	1.323192
43	620	98	1.8	0.147198	17.55431	1.328738
44	640	98	1.8	0.154848	17.94952	1.356468
45	610	100	1.8	0.145937	17.43167	1.332134
46	616	100	1.8	0.147335	17.49638	1.340623
47	620	100	1.8	0.149304	17.40931	1.346282
48	640	100	1.8	0.156902	17.80011	1.374578
49	610	95	2	0.129303	14.27097	1.38008
50	616	95	2	0.131227	14.31895	1.38904
51	620	95	2	0.132632	14.2965	1.395014
52	640	95	2	0.140215	14.55594	1.424882
53	610	98	2	0.131863	14.06587	1.408847
54	616	98	2	0.133774	14.11403	1.418091
55	620	98	2	0.135171	14.08991	1.424253
56	640	98	2	0.142727	14.34426	1.455064
57	610	100	2	0.133604	13.93621	1.428026
58	616	100	2	0.135506	13.9844	1.437458
59	620	100	2	0.1369	13.95889	1.443746
60	640	100	2	0.14444	14.20926	1.475186

3.2.5 Analysis of optimization results

The optimization state converged in 1 iteration with 0 failure points, and three sets of optimal solutions were obtained, as shown in Table 5.

Table 5. Optimized design points.

Candidate points	P ₁ / mm	P ₂ / mm	P ₃ / mm	P ₄ / mm	P ₅ / MPa	P ₆ / kg
1	610	95	1.2	0.2472	26.802	1.0157
2	616	95	1.2	0.24662	26.997	1.0211
3	620	95	1.2	0.25082	26.809	1.0247

Candidate point 1 was selected as the final optimization solution. Comparing the design variables and target variables before and after optimization, it can be seen that the mass is reduced by 28.7%, although the deformation was increased by 0.1mm. The stress was increased by 12MPa. It was still within the design allowance and met the strength requirements of the movable rotating plate. The reliability and safety were all in line with the requirements, and the comparison of the parameters before and after the optimization of the rotating plate was shown in Table 6.

Table 6. Comparison of the parameters before and after the optimization of the rotating plate.

Projects	P ₁ / mm	P ₂ / mm	P ₃ / mm	P ₄ / mm	P ₅ / MPa	P ₆ / kg
Before optimization	640	95	2	0.140215	14.55594	1.424882
After optimization	610	95	1.2	0.2472	26.802	1.0157

As described in the previous section, ANSYS workbench for the optimized design of the movable rotating plate, the rotating plate friction shaft was not modeled and optimized, but the structure was improved directly, so after the optimization of the rotating plate, the rotating plate

friction shaft was added for finite element analysis, and the final optimized results of the movable rotating plate were obtained, as shown in Figure 14.

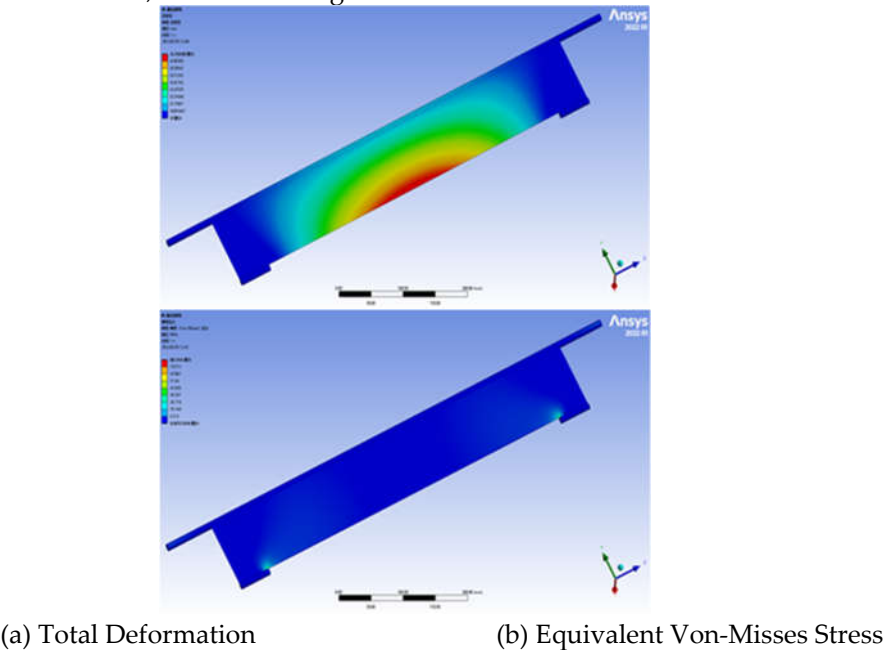


Figure 14. Analysis clouds of the movable rotating plate after optimization.

According to the results of static analysis, the maximum deformation of the final optimized movable rotating plate was 0.76938mm, the maximum stress value was 86.144Mpa, and the minimum safety factor was 2.9718. The more considerable deformation is still in the middle part of the rotating plate, but it still meets the safety strength requirements. The stress was mainly concentrated on the rotating plate movable shaft and the rotating plate friction shafts of the rotating plate. Considering the real situation, the rotating plate movable shaft need to be bolted, and the friction shaft of the Rotating plate friction shaft has friction with the slide rail, but the maximum stress was still less than the allowable stress of the material. The minimum safety coefficient also meets the design requirements.

4. Conclusions

The comparison of static structural analysis of the frame and movable rotating plate before and after optimization was shown in Table 7.

Table 7. Comparison of static Analysis of frame and movable rotating plate before and after optimization

Optimization Project		Mass / kg	Total deformation / mm	Equivalent Stress / MPa
Body frame	Before optimization	157.82	0.0047894	5.5037
	After optimization	106.84	0.0063963	4.8083
Movable rotating plate	Before optimization	1.7449	0.10513	9.8396
	After optimization	1.0657	0.76938	86.144

The total mass of the movable rotating plate before optimization was 1.7449kg, and the total mass of the movable rotating plate after optimization was 1.0657kg, which reduced the mass by 38.9% and realized the light weight of the movable rotating plate. The maximum total deformation after optimization was 0.76938mm, which was within the reasonable deformation. The maximum equivalent force was 86.144MPa, which was within the yield limit of the material used and meets the strength requirement.

Before the optimization, the mass of the classifier was 320kg. After the optimization of the body frame and the movable rotating plate, the mass of the classifier was 246.8456kg, which was 22.86% lower than the mass of the whole machine.

Based on the direct optimization module provided by ANSYS Workbench, this article established the finite element model of the movable rotating plate and derived the optimal combination of dimensional parameters through finite element calculation simulation and verification. The accuracy, reliability, and practicality of the optimization method in this article needed more theoretical and practical further verification, and its method provided theoretical guidance for engineering design and structural optimization design, which can effectively avoid the inaccuracy caused by practical design and further save design time.

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