

Review

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Review

Optimal Conditions for Generation of Runaway Electrons in High Pressure Gases

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Abstract: Runaway electrons (RAEs) generation in high-pressure gases is an important physical phenomenon that influences significantly discharge shapes and properties of initiated plasma. The diffuse discharges formed due to RAEs in air and other gases at atmospheric pressure find wide application. In the present review, theoretical and experimental results that explain the reason for the RAEs occurrence at high pressures are analyzed and recommendations are given on the implementation of conditions under which the runaway electron beam (RAEB) with the highest current can be obtained at atmospheric pressure. Experimental results were obtained using subnanosecond, nanosecond, and submicrosecond generators, including those specially developed for runaway electron generation. The RAEB were recorded by oscilloscopes and collectors with picosecond time resolution. To describe theoretically the phenomenon of continuous electron acceleration, the method of physical kinetics has been used based on the Boltzmann kinetic equation that takes into account the minimum but sufficient number of elementary processes, including shock gas ionization and elastic electron scattering. Results of modeling allowed the main factors to be established that control the RAE appearance, the most important of which is electron scattering on neutral atoms and/or molecules. Theoretical modeling has allowed the influence of various parameters (including the voltage, pressure, gas type, and geometrical characteristics of the discharge gap) to be taken into account. The results of research presented here allow the RAEs accelerators with desirable parameters to be developed and the possibility of obtaining diffuse discharges to be accessed under various conditions. The review consists of the Introduction, 5 Sections, the Conclusion, and the References.

Keywords: runaway electrons; diffuse discharge; high pressure; electron beams

1. Introduction

The possibility of increasing the electron energy of atmospheric discharges to large values was first predicted by C.T.R. Wilson [1] at the beginning of the last century. To substantiate his idea, Wilson used J.J. Thomson's formula [2] according to which the electron energy losses decrease in collisions with particles when the electron velocity increased. Detailed theoretical studies of runaway conditions for electrons and ions in a fully ionized plasma were carried out by R.G. Giovanelli [3] and H. Dreicer [4,5]. Thus, Dreicer has suggested the terms runaway electrons (RAEs) and ions that have become very popular nowadays.

The theory of runaway electrons in gases was further developed by A.V. Gurevich [6,7] who focused on running electrons initiated by high-energy electrons in a weak electric field and possibility of runaway electron breakdown [7]. G.A. Askarjan works [8,9] should also be mentioned that are important for understanding the electron acceleration in gas discharges to energies exceeding those at voltages applied to the interelectrode gap. In these publications, it was shown theoretically that a

part of the runaway electrons could be additionally accelerated in the amplified electric field of the propagating ionization wave front formed by low-energy plasma electrons.

The runaway electrons in the gas discharge at atmospheric pressure, in this case in helium, were first indirectly registered from bremsstrahlung X-ray radiation by S. Frankel *et al.* [10]. Only 40 years after the publication of the first C.T.R. Wilson's idea [1], when testing a new spark camera in work [10] it was revealed that tracks of high-energy particles cannot be detected because of breakdowns initiated along the straight lines perpendicular to flat electrodes. Spark breakdowns short-circuited several successive gaps and did not provide information on a particle track. S. Frankel *et al.* [10] assumed that this is due to runaway electron generation when breakdowns are initiated in the first and subsequent gaps between the spark chamber plates and the next gap is pre-ionized by X-ray bremsstrahlung radiation. To study this phenomenon, the chamber with the cathode of small curvature radius (important improvement for implementation of conditions for RAEs generation) and the flat anode was created. With this chamber filled with helium at atmospheric pressure, the authors managed to register the X-ray film blackening behind the thin-foil anode during the pulse discharge looking like a spark and to register luminophore glow with a PMT. The application of a tip cathode facilitated the transition to the RAEs generation mode in high electric fields at atmospheric pressure and comparatively low high-voltage pulse amplitudes in the gap.

X-ray radiation in air at atmospheric pressure was registered in the next year by Stankevich and Kalinin [11] who increased the voltage pulse amplitude up to ≈ 50 kV and decreased the pulse front duration down to ≈ 2 ns. Similar to work [10], the discharge observed in the gap was a spark. The peculiarity of work [11] was strong blackening of the X-ray film when using the high-voltage tungsten anode. This can be explained by the use of the cathode with a sharp edge from which the discharge was initiated and the runaway electrons were generated. Electrons were decelerated by the flat tungsten anode, thereby leading to an increase in the X-ray bremsstrahlung radiation intensity for positive polarity of the high-voltage electrode.

The next breakthrough in the study of X-ray radiation under the influence of the RAEs for various discharge forms in a non-uniform electric field with cathodes having small curvature radii was generation of diffuse discharges in helium [12] and air [13] at atmospheric pressure. In these works, it was established that the diffuse discharge is formed by the runaway electrons in the presence of x-ray radiation.

Only in 1974 in Russian Scientific and Research Institute of Experimental Physics (RSRIEP), the runaway electron beam (RAEB) was registered behind the anode foil during direct measurements with the help of a shunt [14]. A total of $8 \cdot 10^8$ electrons per pulse were obtained in air at atmospheric pressure. Because of insufficient resolution of sensors and oscilloscope, it was impossible to determine the actual RAEB pulse duration. The results on RAEB registration obtained by this scientific group were not repeated by other scientific groups, institutes, or countries for a long time (for about 30 years), see review [15] and monograph [16] that summarize results of RAEB and x-ray radiation investigations until 2003.

Works on registration of X-ray radiation generation by discharges in high-pressure gases were more successful. X-ray radiation was obtained by several scientific groups from different countries, see [17–23] and the references in these works, including using large facilities [23]. It was shown that x-ray radiation is registered during corona discharge [18]. We do not analyze these studies in our review as the volume of the experimental and theoretical data available in the literature requires a separate review.

Note that in many first theoretical and experimental works (listed below) devoted to the study of the runaway electrons in completely ionized plasma and different gases, there were no references to pioneer C.T.R. Wilson's works [1,24]. Apparently, these works were unknown to the majority of scientists engaged in nanosecond discharges until the 2000s. That is partly why about 50 years passed after the first idea on the possibility of generating runaway electron in high-pressure gases was put forward in work [1] to the direct RAE registration in air at atmospheric pressure using a shunt [14]. Moreover, the number of runaway electrons ($\approx 8 \cdot 10^8$) registered in air at atmospheric pressure behind the anode foil has not increased for the next 30 years, see monograph [16]. This can be explained by

the complexity of physical processes during RAEs generation in gas diodes and the large diameter (30 cm) of the transmission line of the high-voltage pulse generator in the first works (see Figure 5.1.1 of work [16]) and hence, long (> 1 ns) voltage pulse front duration as well as by non-optimal designs of the cathode and gas diode.

Only since 2003, the number of scientific groups studying experimentally RAEB generation at high pressures has started to increase. A large series of investigations was carried out at the High Current Electronics Institute of the Siberian Branch of the Russian Academy of Sciences (HCEI) in which, in particular, the possibility of significant increase in the number of RAEs was shown. The first works were submitted for printing in December, 2002 [25,26], and cycles of investigations were generalized in reviews [27–31] and monograph [32] written in collaboration with colleagues from other Institutes [27,29,30]. Since 2005, the researches have been conducting at the Institute of Electrophysics (IEP) of the Ural Branch of the Russian Academy of Sciences [33,34]; they were preceded by works [35–37] done at the HCEI in collaboration with the IEP. At present, the research team from the IEP continues experimental and theoretical investigations of the RAEs in collaboration with researchers from the P.N. Lebedev Physical Institute of the Russian Academy of Sciences (LPI) [38–40]. The fourth scientific group [41,42] that started to investigate the RAE in collaboration with the HCEI [43–47] is T. Shao research group from the Institute of Electrical Engineering (IEE) of the Chinese Academy of Sciences.

As follows from the above analysis, by the present time the experimental investigations of the RAE at atmospheric pressure and their direct measurements using shunts and collectors have been carried out only by 4 scientific groups. These are the above-mentioned groups at the HCEI, IEP, LPI, and IEE. Also, the experimental and theoretical works are continued in RSRIEP [48–51]. Moreover, as reported in work [52], the researchers failed to increase the beam current amplitude to $\approx 8 \cdot 10^8$ reported in work [14] even when using a modernized system equipped with an output insulator diameter of 10 cm.

The complexity of measuring the parameters of runaway electron beams, primarily, their duration, amplitude, and electron energy distribution should be pointed out, which led to different results obtained by various scientific groups. This point in question is discussed in Section 5 where results of experimental measurements of the RAEB parameters are given.

Modeling of the RAEs generation conditions started from the publication of the first experimental works. Thus, L.P. Babich and I.M. Kutsyk [50] developed a one-dimensional numerical model of high-voltage pulsed discharge in helium at atmospheric pressure. In monograph [53] (see p. 72), the values of the critical field in nitrogen (590 V/(cm·Torr)) and helium (150 V/(cm·Torr)) were obtained at which the first runaway electrons arise. Nowadays, these values are used as criteria in many works. In additions, on p. 77 of the same monograph and in A.V. Kozyrev *et al.* work [54], the critical fields for electron running away were newly calculated taking into account the effect of ionization-induced electron multiplication. These fields turned out to be about 10 times higher in nitrogen (4000 V/(cm·Torr)) and in helium (550 V/(cm·Torr)).

The need to take into account the ionization-induced multiplication of fast electrons to derive the electron runaway criterion was studied in detail in works [55,56] in which the nonlocal electron runaway criterion was used. In addition, in work [57] it was shown that the Townsend electron ionization mechanism remains valid in high fields. The results of modeling the conditions for RAEs generation, obtained by Yakovlenko research group from the Institute of General Physics of the Russian Academy of Sciences, are also presented in the articles cited in the review [27].

The model based on the program MAGIC describing the runaway electrons in helium at atmospheric pressure was developed by W. Jiang and K. Yatsui [58]. As a result of modeling, it was shown that with a tubular cathode, the beam current can reach ~ 1 kA at a voltage of 200 kV. The theoretical models [59–70] developed recently involve more and more factors that affect the runaway electron behavior. However, even now the RAEB generation conditions are modeled only for simplified models. The object of research is very complex and requires various simplifying assumptions, for example, when calculating emission from the cathode with small curvature radius

the surface of which changes for each pulse at high RAE currents due to formation of cathode spots. This process is taken into account together with some others by using various approximations.

Thus, the runaway electrons and X-rays generated by them have been and are being investigated in a large number of experimental and theoretical works devoted to the study of an electric breakdown in gases. RAEs generation in liquids and solids is also beginning to be investigated.

Among the main directions of RAEs and X-rays investigations, considering only a small part of the well-known publications over the last few years, are works [71–73] aimed at obtaining thermonuclear fusion in which the runaway electrons damaged walls of vacuum chambers, thereby limiting plasma heating; works [74–79] considering atmospheric discharges, including high-altitude ones in which X-ray and gamma radiation were registered and reasons for their occurrence were discussed; works [80–85] in which megavolt voltage discharges emitting X-rays and modeling lightning evolution in meter gaps were registered; works [86–89] considering discharges in a uniform electric field at relatively low voltages; and, of course, discharges in a non-uniform electric field registered in centimeter gaps at high voltages in air and other gases for which the runaway electrons were experimentally registered. To confirm the relevance of these studies on electron beam generation, some other works not mentioned above that have been published in 2022–2023 should be mentioned here, including works [90–98] in which the study of the RAEB generation in centimeter gaps was continued. In works [99,100], attention was focused on the study of the RAEs in TOKAMAK-type installations and devices for their diagnostics in these conditions. Works [101–105] studied the RAEs registered in atmospheric discharges, and work [106] investigated the application of the RAE discharges for materials processing.

The purpose of the present review is to analyze the main physical processes leading to generation of the runaway electron beams with maximum currents, to show what electron energies and RAE current pulse durations that can be reached under these conditions, to describe the conditions under which the runaway electron beams with maximum parameters can be most easily registered and to determine how the external conditions change these parameters, and to present results of simplified theoretical modeling of processes in a gas diode to elucidate the most important ones for runaway electron generation and to predict the RAE properties under various conditions.

The Review consists of Introduction, 5 main Sections, and the Conclusion. In Section 2, the theoretical approaches used to calculate the runaway electron beam parameters are briefly described, and the role of the main physical processes influencing the probability of RAEs formation is analyzed. In Section 3, calculated results are presented that allow establishing the mechanism of RAEs generation and predicting their parameters when external conditions change. In Section 4, the scheme of the typical installation used to obtain the RAEB with high currents is described, and in Section 5 influence of various factors on the RAEB parameters are analyzed. Section 6 analyzes the main RAEB parameters and compares the available experimental and calculated data. In the Conclusion, the important role of the RAEs in the formation of diffusion discharges is pointed out, and the need for further studies of the RAEs and RAEBs is substantiated.

2. Theoretical Approaches Used to Calculate the Parameters of the Runaway Electron Beam in High-Voltage Gas Discharges

To establish the main physical processes determining the occurrence of the runaway electrons in various gases, to calculate the RAEB parameters (the beam current and duration and the electron energy distribution), and to forecast their dependences on the change in the external conditions, several theoretical approaches can be formulated.

2.1. Critical electric field strength

As the basis for understanding of the phenomenon of the runaway electrons generated in a weakly ionized low-temperature plasma of high-voltage discharges, an asymptotically decreasing dependence of the deceleration force $F(\epsilon)$ of a fast charged particle (considered to be the electron below) on its kinetic energy ϵ is used [107,108]. Therefore, the equation for the dependence of the

kinetic energy of the fast electron moving through a gas in the uniform electric field of strength E on the coordinate is traditionally written in the form

$$\frac{d\varepsilon}{dx} = eE - F(\varepsilon) = eE - 2\pi N_a \frac{Ze^4}{\varepsilon} \ln\left(\frac{\varepsilon}{I_a}\right). \quad (1)$$

Here e is the elementary electric charge, N_a is the number density of atoms in the gas medium, Z is the atomic number of the gas (the number of bound electrons in the atom), and I_a is the characteristic energy depending on the gas type and very roughly quantitatively estimated to be $I_a \sim 10 \times Z$ eV. Qualitatively, the electron deceleration force in a continuous medium is shown in Figure 1 as a function of the kinetic electron energy.

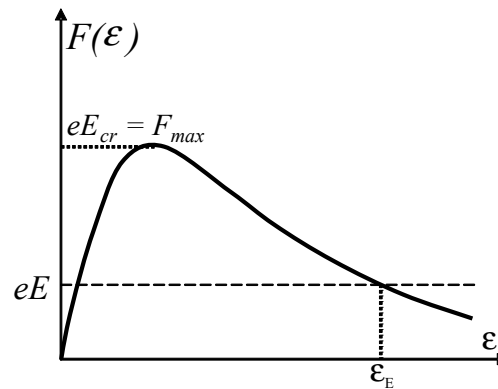


Figure 1. Qualitative dependence of the deceleration force $F(\varepsilon)$ for the electron moving along the force line of the uniform electric field E on the kinetic energy of the electron.

As can be seen from this one-dimensional interpretation, the critical level of the field strength E_{cr} is determined by the maximum deceleration force F_{max} . It is also seen that if the fast electron is injected in the gas with sufficiently high energy $\varepsilon > \varepsilon_E$, it can be continuously accelerated in the field the strength of which is below the critical value $E < E_{cr}$. Such continuous energy-selective mechanism specifies that a physically consecutive theory of the runaway electron phenomenon should be based on the energy distribution function for the electron ensemble. Within the limits of liquid approximation, this effect cannot be described in principle.

The stationary kinetic theory of runaway electrons in a weakly ionized plasma was first developed by Gurevich [6] who defined the probability of plasma electron transition to the continuous acceleration mode by the exponential multiplier $P_{run} \propto \exp(-E_{cr} / 4E)$. As experiments showed, this probability turned out to be highly overestimated when using expression (1) to estimate the critical field strength.

We believe that in real experimental conditions, when high overvoltage across the discharge gap is maintained only for a very short time (of the order of subnanoseconds), conclusions of the stationary theory [6] cannot be used. The matter is that the frequency of scattering collisions of electrons with low energies is many times higher than that of all other processes of electron energy exchange with atomic particles in the gas medium. Therefore, already the first scattering collision deflects the electron trajectory from the direction of action of the electric force, and equation (1) ceases to describe adequately the process of deceleration or acceleration of the scattered electron. Therefore, the decisive factors for the electron transition to the continuous acceleration mode are the scattering collisions, and exactly the transport collision cross section σ^* should estimate numerically the probability of collision of runaway electrons.

It is well known that the transport cross section of scattering of the fast electron with energy ε on a multi-electron atom is determined by the Rezerford cross section of scattering on its nuclear charge, Ze [108]:

$$\sigma^*(\varepsilon) = 2\pi \left(\frac{Ze^2}{\varepsilon} \right)^2 \ln \left(\frac{\varepsilon}{I^*} \right), \quad (2)$$

where I^* is the characteristic energy, generally other than I_a in Eq. (1), but of the same order of magnitude.

As follows from a comparison of Eqs. (2) and (1), the transport cross section decreases with increasing kinetic energy of electron faster than the deceleration force and depends stronger on the atomic number Z of the element. Therefore, equation (1) applies to the electron moving in the uniform electric field E if during movement, it does not scatter at large angles. The probability of this event $P(0)$ (the absence of scattering) even in the gap of infinite length turns out to be finite and can be estimated from the formula (see work [54] and Chapter 3 of work [109])

$$P(0) = \exp \left(- \int_0^\infty \sigma^*(\varepsilon) N_a dx \right) = \exp \left(- \frac{N_a}{eE} \int_0^\infty \sigma^*(\varepsilon) d\varepsilon \right) = \exp \left(- \frac{E_{cr}^*}{E} \right). \quad (3)$$

The characteristic field strength E_{cr}^* so obtained turns out to be significantly higher than the critical strength E_{cr} derived from the Bethe decelerating force. New estimates of the reduced critical field strengths reported on p. 113 of Chapter 2 of work [109] were $E_{cr}^* / p = 210$ V/cm·Torr for helium (He), 1410 V/cm·Torr for nitrogen (N₂), and 6790 V/cm·Torr for sulfur hexafluoride (SF₆). These new values of the critical field strengths E_{cr}^* / p allowed calculating the number of fast electrons under experimental conditions much more accurately than previous ones.

2.2. Kinetic model of the runaway electron effect

As indicated above, the mathematical apparatus of the kinetic Boltzmann equation for the electron velocity (momentum) distribution function should be the main approach to a theoretical description of the runaway electron effect in a pulse discharge. Unfortunately, this problem cannot be solved numerically in the complete formulation (for the 3D3V model) even using modern computers. Therefore, the one-dimensional problem (for the 1D1V model) is conventionally solved [38,66] with field inhomogeneity near the cathode, for example, in the coaxial electrode geometry with current flowing radially between the cathode of small radius and the anode of large radius $r_c \ll r_a$.

In the overwhelming majority of practical situations, the runaway electrons are generated during a very short time (less than one nanosecond), during which the discharge gap can still maintain a high overvoltage. Therefore, in calculations of this short breakdown phase, the movement of ions can be neglected. They appear in the gas due to shock ionization of atoms and remain in the place of their creation. Mathematically, this is expressed through the neglect of ion current when calculating the electric field.

The mathematical problem formulation even in the minimal configuration (nonrelativistic velocities and stationary ions) should describe the evolution of the momentum distribution function $f(r, p, t)$, $p = mv$, of the electron ensemble (here and below, m is the electron mass) and the dynamics of the electric field $E(r, t)$. An example of such minimal model is the kinetic Boltzmann equation (Eq. (4)) and the Maxwell equation (Eq. (5)) for the total current (the particle current plus the bias current) describing the law of conservation of the radial current per unit length $J(t)$ in the coaxial discharge gap:

$$\frac{\partial f}{\partial t} + \frac{p}{m} \frac{\partial f}{\partial r} - eE(r, t) \frac{\partial f}{\partial p} = (-Q_- + Q_+)_{ion} + S_{scatt}, \quad (4)$$

$$r \frac{\partial E}{\partial t} = J(t) + 4\pi e \int_{-\infty}^{\infty} (p/m) f(r, p, t) dp. \quad (5)$$

The two terms in the parentheses on the right-hand side of Eq. (4) describe inelastic electron collisions with atoms, including the ionization-induced multiplication process, and the last term describes the electron scattering effect. Within the limits of the present review, we will not go deep into a description of inelastic collisions, because this complicated question has already been analyzed in detail in our work [66]. For the one-dimensional problem, it is impossible to describe adequately elastic scattering; therefore, the *forward-backward scattering approximation*:

$$S_{scatt} = -N_a(p/m)\sigma^*(p)(f(r, p, t) - f(r, -p, t)) \quad (6)$$

is conventionally used to solve it. To take into account the discharge current $J(t)$, it is necessary to supplement system of equations (4)–(5) with the equation for the current in the external electric circuit. Thus, it is possible either to fix the voltage applied to the gap or to calculate it from the Kirchhoff equation for the circuit.

The initial condition for the formulated problem was to set the initial electron concentration in the gap (uniformly or non-uniformly distributed along the coordinate). The discharge process was initiated by the generator voltage $U_0(t)$ with a given amplitude gradually increasing from zero applied to the gap; what is more, $J(0) = 0$ and $E(r, 0) = 0$.

System of equations (4)–(5) (plus the electric circuit equation) was solved numerically for a uniform coordinate and momentum grid by modern computing methods.

3. Results of modeling

Results of modeling of the high-voltage discharge in nitrogen at atmospheric pressure are presented below. The only characteristics of the gas type were the known parameters of two elementary processes, namely, the shock ionization and transport cross sections [110]. This model does not require any additional semiempirical dependences or correcting parameters.

The voltage pulse with the amplitude $U_0 = 200$ kV, linear leading pulse edge, and 1 ns base duration (shown by the solid curve in Figure 2) from a power source was applied to the coaxial gas-filled diode (with the cathode radius $r_c = 1$ mm, anode radius $r_A = 11$ mm, running length $L = 1$ cm, and nitrogen at a pressure of 760 Torr). The diode was connected in the circuit in series with the ballast resistance $R = 75 \Omega$. We studied the process of multi-electron gas breakdown initiation, assuming an initial electron number density of 10^3 cm^{-3} .

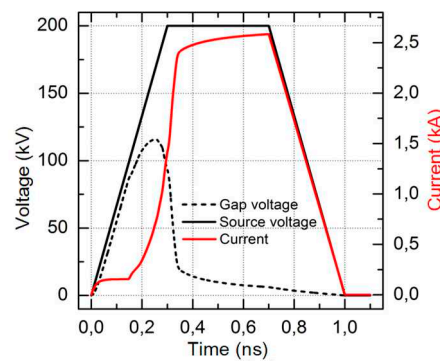


Figure 2. Calculated current and voltage waveforms during the fast breakdown of the coaxial gap filled with nitrogen at atmospheric pressure.

As can be seen from Figure 2, the current in the discharge almost reaches its maximum value of 2.5 kA already within the first 300 ps, but the voltage on the gap does not exceed 120 kV, and the discharge enters the commutation stage in 350 ps.

Basic information on the occurrence of the runaway electrons can be obtained from the calculated electron energy distribution function. Figure 3 shows the instantaneous functions $f(r, p, t_i)$ in the radius-momentum phase plane calculated at three characteristic times of the gap breakdown stage.

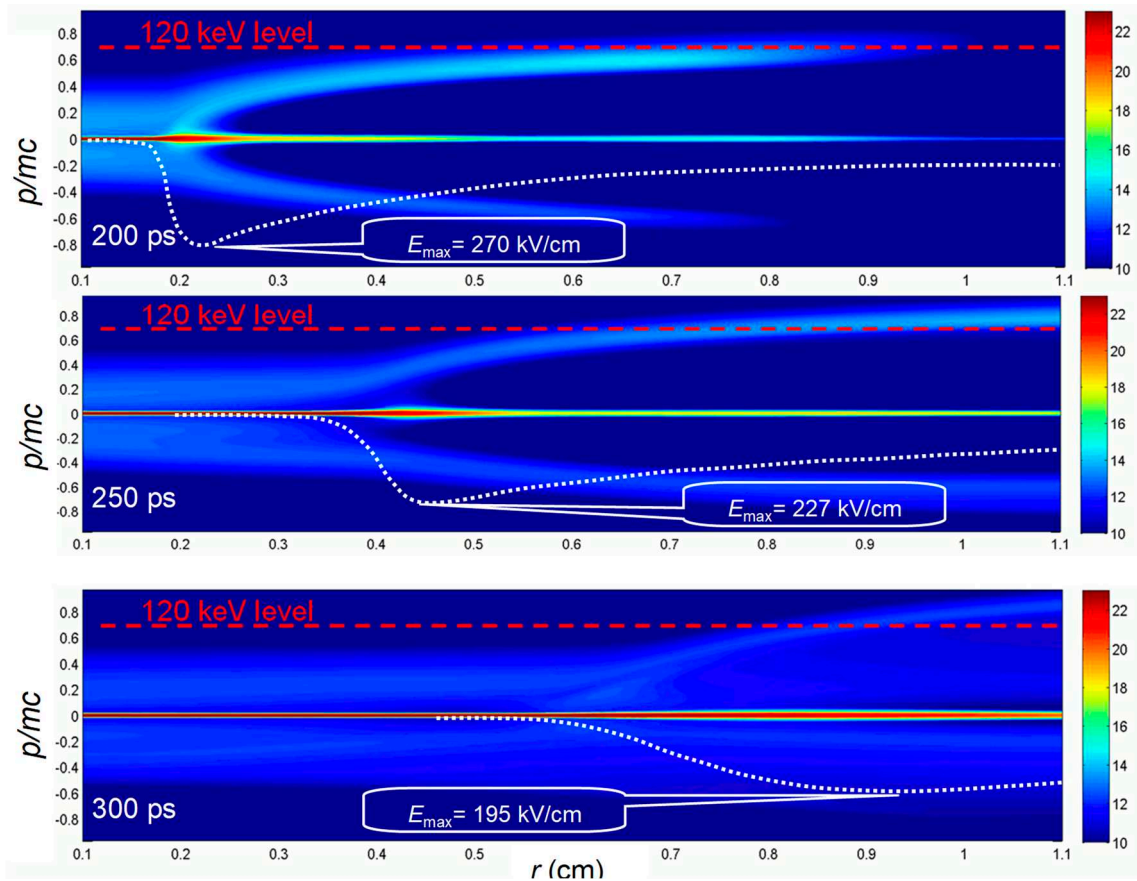


Figure 3. Instantaneous phase portraits of the electron ensemble at indicated times of breakdown evolution in nitrogen (the cathode is on the left, and the anode is on the right). Colors indicate the local distribution density in arbitrary units on logarithmic scale (for example, number 20 means 10^{20}). The dashed curve shows the radial profile of the electric field strength.

The negative momenta in the figure correspond to the scattered electrons moving (toward the cathode) against the electric field force. The dashed straight line at 120 kV is drawn for convenience of our analysis; it corresponds to the voltage amplitude on the discharge gap, as seen from Figure 2.

Under conditions of so fast breakdown, the Maxwell bias current may constitute a significant (and sometimes even main) part of the total current flowing in the discharge circuit. So, at time 200 ps (the top frame in Figure 3), even the runaway electrons have no time to reach the anode, but the current in the circuit reaches 250 A, because a highly conductive dense plasma has already been formed near the cathode (the internal electrode). The highly conductive plasma front is clearly seen on the phase portraits in Figure 3, since the runaway electron flow starts to be formed exactly here. In this local area (quickly moving toward the anode), the maximum field strength (270 kV/cm) is observed, the electron ensemble is strongly heated, and the probability is high that the electrons from the tail of the distribution function go into the continuous acceleration mode.

By the time (250 ps) at which the voltage amplitude is reached in the gap, the runaway electron current on the anode reaches its maximum value, and the maximum energy in their spectrum exceeds the instantaneous value of the applied voltage, as is well seen in the middle frame of Figure 3. By this time, the runaway electrons moving ahead of the dense plasma front due to ionization by collisions have already noticeably ionized the gas in the entire gap, and the first plasma electrons also reach the anode. By that time, the maximum field strength (227 kV/cm) at the dense plasma front already considerably decreases; therefore, the probability of transition to the *runaway* mode greatly decreases as well.

Therefore, in 300 ps the discharge current becomes high enough (greater than 1 kA) so that the voltage across the gap to begin to decrease due to the ballast resistance in the voltage circuit. The

entire gap is filled with the dense plasma, though there is a long tail of few fast electrons in it, as seen in the bottom frame of Figure 3. In the logarithmic color scale, the fast electrons are clearly seen in the picture, but their density did not exceed 10^{-6} of the total number of electrons in the volume. The field strength between the plasma front and the anode is leveled, remaining at a sufficiently high level. This field strongly affects the runaway electrons, accelerating them to anomalously high kinetic energies.

Figure 4 shows the instantaneous power spectra of the electrons arriving at the anode surface at different times. No one electron has time to reach the anode within 220 ps.

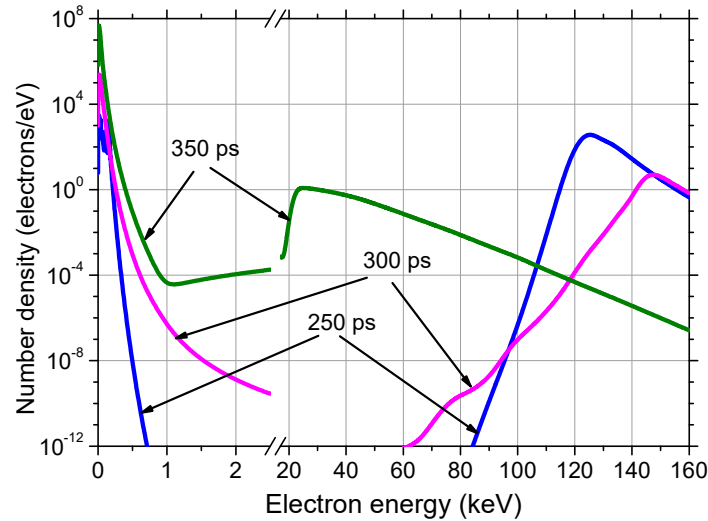


Figure 4. Instantaneous spectra of electrons arriving at the anode at different times.

The runaway electrons are usually registered behind the thin foil placed in the anode plane. Only sufficiently fast electrons passed through this foil to the detector, thereby protecting the detector circuit from a very high plasma electron current. The plasma electrons in Figure 4 have energies below 200 eV, whereas the runaway electrons have energies above 20 keV. We call fast the electrons with energies >200 eV up to few keV; they can reach the anode, but their energy is insufficient to cause them to escape from the gas diode.

To compare with experiments, the current of runaway electrons passing through the Al foil with the thickness $D = 10 \mu\text{m}$ was calculated. In calculations, the electron transmission coefficients $\tau(\epsilon, D)$ from work [111] were used. Figure 5 shows the total spectrum of the electron beam passed through the anode foil in time $T = 1$ ns calculated from the formula $f(\epsilon) = \tau(\epsilon, D) \int_0^T f(r_A, p(\epsilon), t) dt$.

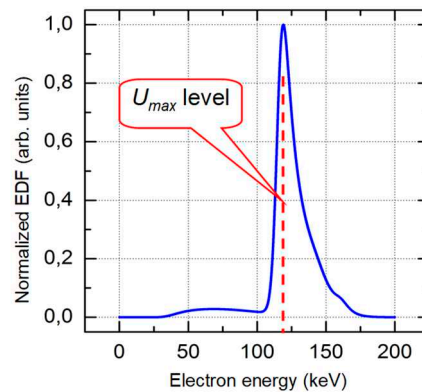


Figure 5. Calculated integral spectrum of fast electrons on the anode behind the 10- μm Al foil.

A quite large part of electrons with the so-called anomalously high energies [8,9,14] can be seen in the runaway electron spectrum. However, this observed effect has natural explanation clearly understood from 3 phase portraits shown in Figure 3 [68].

For the one-dimensional problem with coaxial discharge gap geometry, a number of intermediate conclusions can be made based on the results of fast breakdown modeling.

1) The energies of the overwhelming part of runaway electron flow are taken from the high-energy tail of the plasma ensemble under the action of the strong electric field near the cathode (with small curvature radius). This process takes place at the plasma front near the cathode where the high plasma electron density is combined with the high electric field strength.

2) In the process of plasma front propagation, the maximum strength in its vicinity decreases, and the intensity of fast electron generation decreases noticeably.

3) The runaway electrons at the dense plasma front create secondary electrons which also multiply like an avalanche. A fast plasma production in the zone between the plasma front and anode promote leveling of the field strength, which in this case, cannot provide the transition of plasma electrons to the continuous acceleration mode.

4) The field strength continues to increase due to the field compression between the quickly moving plasma front and the anode, thereby providing additional acceleration of a part of the runaway electrons to anomalously high energies.

Taking into account the theoretical pattern, it is possible to analyze constructively various experimental results.

4. Experimental installations and measurement procedures

4.1. Generators, cathodes, and collectors for forming and measuring the RAEB

In the first works [10–16] in which X-ray and RAEB were registered, generators of high voltage pulses with comparatively long fronts and large diameters of transmission lines and gas diodes were used with the cathode and anode design non-optimal for obtaining the runaway electron beam currents of several ten amperes (see Figure 5.1.1 of work [16]). In addition, the RAEB registration sensors and the employed oscilloscopes had insufficient time resolution. Over the last 20 years, the generators, beam registration sensors, and gas diode designs have been significantly improved, and the oscilloscopes with picosecond time resolution have appeared. All this has allowed the researchers to obtain experimentally the main laws of changes in the RAEB parameters attendant to changes of the amplitude and voltage pulse front as well as the pulse shape, cathode and gas diode designs, gas type and pressure, voltage pulse repetition frequency of the generator, and its life time. The registered RAEB pulse durations were analyzed in Chapter 7 of work [112] and in works [31,40,95,97]. Data on the RAE bremsstrahlung and characteristic x-rays were obtained (see collective monographs [32,109,112]). It was established that under conditions of RAEB generation, the diffusion discharge is formed in the gaps with non-uniform electric field filled by different gases at high pressure due to the development of wide streamers [30]. All this allowed new data on the RAEB parameters to be obtained with high accuracy.

To analyze the obtained experimental results in more details, we consider the design of one of the generators specially created for RAEB investigation (see Chapter 4 of work [32]). The generator with a system of capacitive dividers provided registration of voltage pulses in the discharge gap and was also equipped by the collector system for measuring the beam current pulses or the runaway electron number density. The number of electrons emitted from the entire anode foil surface was measured, and the RAEB pulses were measured with subnanosecond or picosecond time resolution by reducing the size of the receiving collector part. Note that to obtain the picosecond time resolution, suitable connectors and cables of minimal length should be used (for example, see Chapter 7 of work [112]). To register the discharge current, the foil and the collector were removed, and the shunt based on film chip resistors or strip lines with time resolution up to ≈ 100 ps was inserted.

The design of the SLEP-150M generator (see Chapter 4 of work [32]) forming voltage pulses of ≈ 1 -ns duration at half maximum and 0.25-ns pulse duration at the levels 0.1–0.9 of the front amplitude is shown in Figure 6.

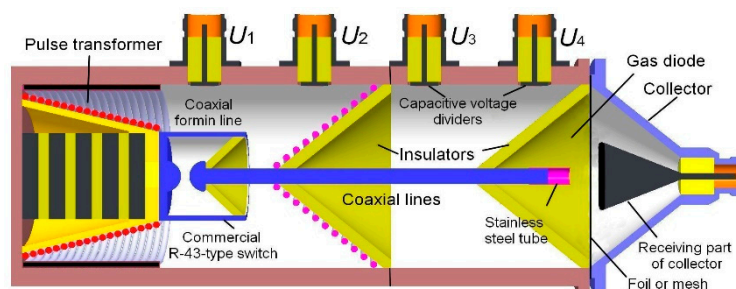


Figure 6. Block diagram of the SLEP-150M generator comprising the sensors U_1 , U_2 , U_3 , and U_4 that allow reconstructing the voltage pulse shape in the gap; the short transmission line with the sensor U_2 and the additional transmission line with the sensors U_3 and U_4 ; the gas diode built into the transmission line; and the collector with the receiving part 20 mm in diameter providing time resolution of ≈ 80 ps arranged near the foil.

The SLEP-150M generator differed from the SLEP-150 generator by the additional transmission line. In the generators, the circuit with the pulse transformer was used, inside which dielectric ring ferrite sheets were placed. The voltage pulses with amplitudes of ~ 4 kV generated by the additional capacitor not shown in the figure are fed to the primary winding made of the foil. The high-voltage output of the secondary winding is connected to the high-pressure spark gap R-43 shaped as a beaker. Its external surface together with the generator housing formed the coaxial line 4 cm long with an impedance of 20Ω charged by the pulse transformer. After the breakdown of the R-43 spark gap, the voltage pulse is formed which through the short and additional transmission lines having a $100\text{-}\Omega$ impedance passes to the gas diode with the cathode and the foil anode. The pulse transformer and the forming and transmission lines are filled with transformer oil.

The tubular cathode 6 mm in diameter made of the thin foil with a thickness of $100 \mu\text{m}$, fixed to the internal wire of the additional coaxial line, is also shown in Figure 6. Other cathodes the shapes and sizes of which affected the RAEB parameters, including cone-type cathodes with different apex angles, cathodes made of sewing needles, shaving edges, mesh cathodes made of thin wires, and spherical cathodes were also used.

To measure the voltage pulse parameters, capacitive sensors U_1 , U_2 , U_3 , and U_4 described in details in works [28,113] were used. Their time resolution at small receiving part diameters in the coaxial line (≤ 1 cm) reached ≈ 100 ps. The shunt based on the chip resistors or strip lines connected in parallel was used to measure the current running through the discharge gap, including the capacitive current, dynamic capacitive current, and conduction current (see Chapter 4 of work [32]). Such shunts allowed registering the current across the gas diode with subnanosecond time resolution.

The RAEB current was measured with collectors having different diameters of the receiving part. When the diameter was about 1 mm and the special cable had a small length, the time resolution of the collector was not worse than 10 ps. When the diameter of the receiving collector part increased to 2 cm (see Figure 6), its time resolution worsened to 80 ps, but the anode foil area, behind which the beam current was recorded, increased.

In addition, in a number of experiments with this generator, the coaxial limiting spark gap was placed on the left end face of the additional transmission line, which allowed the voltage pulse duration at half maximum to be reduced to 0.1 ns, and the durations of the leading and trailing pulse edges to be reduced to 100 ps. However, in this case, the voltage pulse amplitude also decreased.

For the gas diode filled with atmospheric air, it was found that the change in the pressure, humidity, and air temperature in a laboratory room can affect the RAEB parameters. Therefore, it would be better to carry out comparative experiments in air under identical weather conditions with monitoring of these parameters.

Note that the RAEB in works [25,28,31] were called supershort avalanche electron beam (SAEB). The term *supershort* was proposed because of its small duration, and the term *avalanche* was used because the electron avalanches appearing at the cathode play an important role in its formation. Furthermore, in the Section devoted to the study of the RAEB, we use both terms (SAEB and RAEB). Note also that in a number of publications, the term *supershort* was sometimes translated from the Russian language by the term *ultrashort*; as a result, the RAE beam was also named the UAEB.

4.2. Measurement of the parameters of the voltage pulses, discharge currents, and SAEB

The knowledge of the voltage pulse shape and amplitude on the gas diode allows interpreting correctly the results obtained. Figure 7 shows a series of waveforms of voltage pulses and SAEB obtained using the SLEP-150M accelerator with the tubular cathode.

From the waveforms of the voltage pulses of the capacitive dividers U_2 and U_3 , it can be seen that the voltage pulse fronts and amplitudes of the incident wave before arrival of voltage pulses reflected from both dividers coincide. However, the voltage pulses U_{ref} , reflected from the gap, arrived at different times. The delay of U_{ref} depends on the distance between the gas diode and the capacitive divider, and it is greater for the voltage pulse U_2 registered from the capacitive divider. The difference between the pulses U_2 and U_3 yields U_{ref} . Moreover, it is not distorted by other reflections within the first 800 ps. The summation of U_2 and U_{ref} with synchronized fronts allows the shape of the voltage pulse U across the gap to be determined. The simultaneous measurements of the electron beam, displacement current, and dynamic displacement current allows synchronization to be performed.

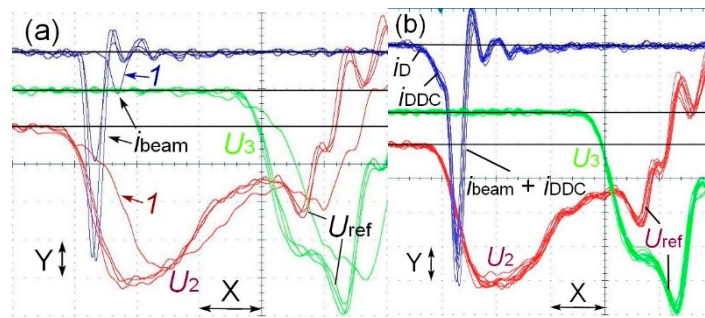


Figure 7. Waveforms of the voltage measured on capacitive voltage dividers (U_2 and U_3) and of the electron beam current pulse (i_{beam}) (a) and the same voltage pulses (b) for the sum of the electron beam, displacement current (i_D), and dynamic displacement current (DDC) ($i_{beam} + i_{D+D}$) [31,44] for the pulse measured on the collector with the receiving part 5 mm in diameter for the diode with a tubular cathode. Scales: $i_{beam} - 0.008$ A/div; $U_2 - 32.4$ kV/div; $U_3 - 30.4$ kV/div (Y); and time - 400 ps/div (X). The voltage pulses and SAEB are synchronized with picoseconds accuracy, but delays between them were not determined.

In Figure 7a, the beam currents significantly decrease because of a *bad* response of the spark gap and an increase in the voltage pulse front and decrease in its amplitude (pulses 1). In Figure 7b, the SAEB pulses are shown together with the dynamic capacitive current depending on the transparency of the grid anode. The anode grid cell (0.6×0.6 mm) was chosen so that the DDC was several times less than the SAEB.

Using the difference between the voltage pulses U_2 and U_3 , the reflected voltage pulse was selected, and its front was superimposed on the incident voltage wave. This allowed the voltage pulse across the discharge gap to be reconstructed. This method is widely used in pulse technique [115], including the study of generation of runaway electron beams (see Chapter 7 of work [112]).

To affix the beam current pulses to the voltage pulses with picosecond accuracy, the DDC and capacitive currents were used. Figure 8a shows the reconstructed voltage pulse U across the gap, the discharge current pulse I_d registered with the shunt, and the beam current pulse behind the anode foil registered with the collector having the receiving part with a diameter of 3 mm.

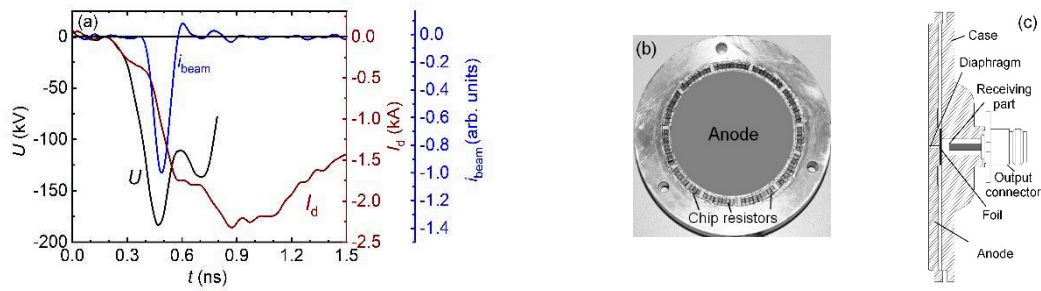


Figure 8. Waveforms of the voltage across the gap U , discharge current I_d , and electron beam current i_{beam} behind the foil at the pulser SLEP-150M with tubular cathode.

All three pulses were synchronized. It can be seen that the beam current is registered near the maximum of the voltage pulse and remains sufficiently high after termination of the beam current. The shunt design is shown in Figure 8b. It was used instead of the collector and simultaneously served as the anode. The high time resolution of the collector was reached by application of the film chip resistors connected in parallel. The collector with the receiving part 3 mm in diameter (Figure 8c) was used to register beam current pulses with time resolution up to 20 ps. The SAEB pulse shown in Figure 3a was limited with the collector. From the U and i_{beam} waveforms shown in Figure 8a, it can be seen that the limitation of the SAEB duration is due to the discharge gap short-circuited by the plasma. This is in agreement with results of modeling presented in Section 3.

The comparison of the reconstructed voltage pulses and pulses U_4 registered with the capacitive divider located opposite the center of the discharge gap (see Figure 6) showed that U_4 allows registering sufficiently accurately the voltage pulse front and its amplitude, but significantly distorts only its decay. Hence, the SLEP-150 (without additional transmission line and capacitive divider U_2) and the SLEP-150M (with capacitive divider U_4) type generators can be used to obtain dependences of the SAEB parameters on the voltage on the gas diode without application of the reconstruction technique based on reflected pulses.

5. Experimental data

5.1. Influence of various factors on the SAEB parameters

5.1.1. Influence of the pulse amplitude and front duration on the voltage pulse

As is well known from experimental researches and modeling of the parameters of runaway electron beams, the beam current, electron energy, and pulse duration are influenced by various factors (for example, see [16,32,109,112]). In this Section, changes in the SAEB parameters accompanying variations in the voltage pulse amplitude and front duration are demonstrated. The SAEB were measured behind the thin foil anode, and in some cases, behind the dense grid anode. The grid anode was used for simultaneous registration of the capacitive current and dynamic capacitive current used to affix the SAEB to the voltage pulse [31,32,44]. In addition, the use of the grid anode allowed one to register beams with low electron energy, at the level of 10–20 keV and less, generated at low reduced electric field strengths or when the voltage pulse duration increased to hundreds of nanoseconds. It was established (for example, see works [31,32]) that the SAEB amplitude depends significantly on the voltage pulse amplitude and its current front duration.

The results of measurements using the SLEP-150M generator (Figure 6) with subnanosecond time resolution are shown in Figure 9.

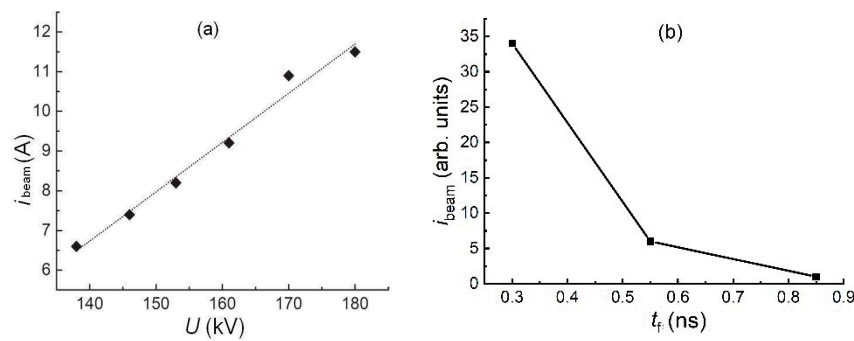


Figure 9. Dependence of the SAEB current amplitude behind the aluminum foil with a thickness of 10 μm on the voltage on the interelectrode gap (a) and voltage pulse front duration (b) for the tubular cathode with a diameter of 6 mm and the interelectrode gap length $d = 12$ mm at the air pressure $p = 100$ kPa.

Since the first works [10–14] (see also monographs [16,32] and the references in them) in which results of investigations of X-ray, runaway electron beam, and bremsstrahlung parameters were studied under the influence of the SAEB, it was established that the runaway electron current increased with the voltage amplitude on the gas diode. The dependence obtained for the cone shaped collector with a receiving part diameter of 2 cm is shown in Figure 9a. However, it should be kept in mind that similar dependences were obtained only in measurements of the voltage on the cathode-anode gap. In the dependence of the beam current amplitude on the generator voltage amplitude, the beam current decreased with increasing generator voltage [36]. This is due to the breakdown of the gap at the voltage pulse front.

The improved time resolution of the registration system allowed one to establish a significant effect of the voltage pulse front duration on the SAEB amplitude (Figure 9b). Moreover, the decrease of the beam current was affected not only by a decrease in the breakdown voltage with increasing voltage pulse front duration, but also by processes occurring in the gas diode. The dependence shown in Figure 9b was obtained at the same voltage (≈ 200 kV) on the gap due to choice of voltage pulses with the same amplitudes and corresponding beam current pulses from the series of ~ 100 accelerator switches on. From the figure it can be seen that the reduction of the voltage pulse front to 0.3 ns leads to a significant increase in the SAEB amplitude. Systematic studies of the effect of the voltage pulses with durations of 0.2 ns and less on the beam current amplitude have not yet been carried out. However, from the data of work [116] in which the voltage pulse with an amplitude of 1.4 MV and 0.1 ns rise time was used, the runaway electron beam current behind the anode foil did not exceed 16 A, whereas in Chapter 4 of monograph [32] it was reported that the SAEB current with an amplitude of 100 A and pulse duration at half maximum of 100 ns was recorded behind the Al foil 10 μm thick, which corresponded to the RAE number behind the foil equal to $6.2 \cdot 10^{10}$. In these conditions, the generator voltage pulse amplitude was 400 kV, and the voltage pulse rise time on the level 0.1–0.9 was 0.25 ns.

5.1.2. Runaway electron energy distribution

This parameter is very important for understanding of physical processes occurring during RAE generation and for practical application of the SAEB. However, experimental data on the runaway electron beam spectra obtained by various scientific groups differ significantly. Results of investigations performed at the HCEI showed that in the SAEB spectrum generated in air at atmospheric pressure, two-three groups of electrons with different energies can be identified [28,31,32]. The basic (second) group of electrons has energies in the range $eU_m/3 < T_2 \leq eU_m$, where U_m is the maximum voltage on the gap and e is the electron charge. The first group of electrons has energies $T_1 \leq eU_m/3$. To measure the electrons of the first group, thin foils or metal grids with small cell sizes (less than 0.2×0.2 mm) should be used. This allows one to avoid the effect of the dynamic

displacement current on the collector readings [44]. The electrons of the third group have energies $T_3 > eU_m$; they are called the electrons with *anomalous* energy. The number of electrons in each group depends on the experimental conditions, voltage pulse parameters, and design of the cathode and gas diode. To increase the number of electrons in the third group, the voltage pulse rise time should be reduced and cathodes with increased curvature radius should be used. However, even in conditions close to optimum for SAEB generation, the number of electrons of the third group is low and does not exceed 10% of the electron number behind the aluminum anode foil with a thickness of 10 μm .

Figure 10 shows results of investigations of the runaway electron beam spectra generated in the gas diodes; a part of them was presented in work [121].

Three sections designated by the figures can be seen in all experimental curves, with obvious inflections in transitions from one section to another. Section 1 reflects the contribution of the electrons of the first group with comparatively low energies. Section 2 corresponds mainly to the electrons of the second group – the main group in the SAEB. Section 3 indicates the electrons with energies $T_3 > eU_m$ and shows that their number is comparatively low.

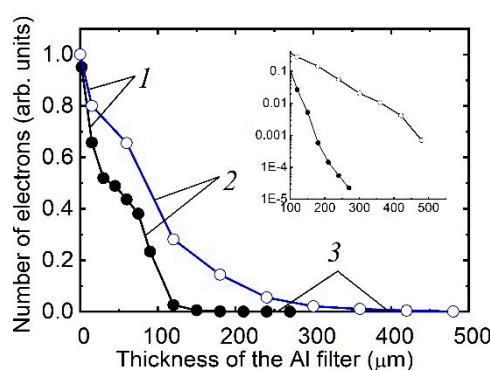


Figure 10. Dependences of the SAEB amplitude on the thickness of the aluminum tubular filter which served as the anode for the tubular cathode with a diameter of 6 mm manufactured from the foil with a thickness of 100 μm (closed circles) and for the spherical cathode with a diameter of 9.5 mm (open circles). Both cathodes were made of stainless steel. The dependences are shown on linear and semilogarithmic scales. Numbers 1, 2, and 3 indicate electrons of different groups; $d = 12$ mm for the tubular cathode and 8 mm for the spherical cathode of the SLEP-150M generator.

To reconstruct the spectrum, the method developed by A. V. Kozyrev and V. Yu. Kozhevnikov [117] was used that allows the electron beam spectra to be determined under minimal *a priori* assumptions using regularization of the ill-posed problem solution of the Fredholm integral equation of the first order. The main requirement for the reconstruction of the electron spectrum is sufficiently smooth decay curve. Therefore, to calculate the spectrum, the experimental decay curve, if required, should be approximated by a smooth dependence.

5.1.3. Influence of the cathode material and shape on the SAEB parameters

The electrode material and design affect significantly the parameters of supershort avalanche electron beams generated by nanosecond discharges in air and other gases at atmospheric pressure. Systematic studies of the influence of the cathode material on the SAEB amplitude and X-ray density were carried out in work [45] for tubular cathodes, gas diodes filled with air at atmospheric pressure, and high voltage pulses with different rise times (0.3, 1, and 15 ns). The gap was formed by the flat anode and tubular cathode made of different metals (stainless steel, permalloy, titanium, niobium, copper, brass, or aluminum). On the installation with voltage pulse rise time of 0.3 ns, it was established that the voltage amplitude on the gap depends on the tubular cathode material and reaches its maximum value for the stainless steel cathode. The maximum SAEB amplitudes were reached, with other things being the same, in the conditions of the maximum voltage on the gap. It

was assumed that the voltage amplitude on the gap changes due to different thresholds for electron emission from a metal surface. For voltage pulse rise time of 1 ns and less, the SAEB amplitude increased for the metal cathodes with low work function.

When the voltage pulse rise time increased to 15 ns and the interelectrode gap length increased to 8 cm, the cathode material ceased to affect the voltage amplitude on the gap and the intensity of X-ray from the gas diode. The X-ray density, measured in work [45] using a NaI scintillator and a photo multiplier, was independent of the cathode material.

The results similar to those reported in work [45] were also obtained using the SLEP-150M generator with the cone cathode and voltage pulse rise time of 0.3 ns, and the effect of the interelectrode gap was also demonstrated. In these experiments, the SAEB amplitudes and the voltage amplitudes on the gap were measured during SAEB generation. The cone cathodes, made of copper, aluminum, and stainless steel with cone apex angles of 90° were used. The dependences of the SAEB amplitude registered through the collimator hole with a diameter of 1 mm placed after the anode foil on the interelectrode gap length are shown in Figure 11 for the indicated cone cathode materials.

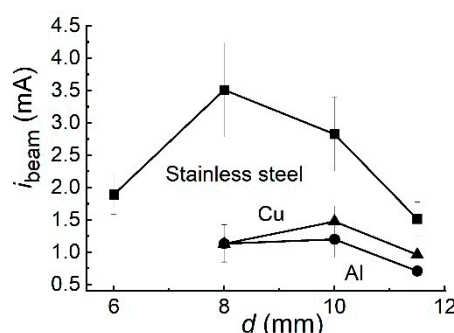


Figure 11. Dependences of the SAEB current amplitude on the interelectrode gap length for the indicated cone cathode materials. The discharge was initiated in air at atmospheric pressure. The collimator hole diameter was 1 mm.

Each point was averaged over 10 pulses. The optimum interelectrode gap length was 8 mm for the cone stainless steel cathode, whereas for the copper and aluminum cathodes, it was 10 mm. The average voltage pulse amplitude on the gap, reconstructed from the incident and reflected waves for the interelectrode gap 10 mm long and the cone stainless steel cathode, was ~ 120 kV, whereas for the copper and aluminum cathodes, it was ~ 100 kV. In what follows that the maximum SAEB currents were obtained for the cone stainless steel cathode providing the maximum voltage on the gap. This coincides with the results of work [45] in which the tubular cathodes were investigated. Unlike the results of measurements of the beam current from the foil surface with a diameter of 2 cm with the tubular cathode (see Chapter 1 of [112]), the interelectrode gap had no significant influence on the SAEB pulse duration on the gas diode axis in measurements of the beam current transmitted through the collimator hole 1 mm in diameter with the cone cathode. The current pulse duration at half maximum was greater than the limiting time resolution of the registration system and was ~ 30 ps at half maximum. The distinctive feature of the SLEP-150 generator with the cone cathode is formation of a clearly pronounced cathode spot at the cone apex and the reduction of the SAEB current amplitude.

The influence of the cathode shape on the SAEB amplitude was studied in ample detail using the SLEP-150 and SLEP-150M generators (see Chapters 1 and 4 of work [32] and Chapters 1 and 7 of work [112]). The RADAN-220 [113] and FID generators [118] were also used. Six cathodes were applied. Cathode No. 1 (tubular one) represented the stainless steel tube 6 mm in diameter made of the foil with a thickness of 100 μm . Cathode No. 2 (spherical one) represented the steel sphere with a diameter of 9.5 mm. Cathode No. 3 (grid one) represented the grid with a step of 4 mm from parallel wires 0.2 mm in diameter fixed on the end face of the hollow cylinder 3 mm high, 40 mm in diameter,

and disk bottom. The distance from the wires to the bottom was 1.5 mm. Stainless steel cathode No. 4 (cone one) had an apex angle of 82° and rounding radius of the cone apex of ~ 0.1 mm. The cone base had a diameter of 6 mm and passed into the cylinder of the same diameter. Cathode No. 5 (blade one) was fabricated from a razor blade 7 mm long fixed on the end face of the tube made of the foil 6 mm in diameter. Tubular cathodes of large diameter (up to 60 mm) were also used, including the cathodes consisting of several tubes of different diameters coaxial with the central axis [25].

The flat anode of the gas diode (Figure 6) was made of the aluminum foil with a thickness of $10\ \mu\text{m}$ reinforced by the grid with transparency up to 90% or the diaphragm. To obtain the maximum beam current amplitude, the anode should be made of the metal with small atomic number and the least thickness. At the same time, it should have high strength to maintain the pressure drop between the gas diode and collector. In addition, the shock waves generated by diffusion or spark discharges in gas diodes should be taken into account.

It was found that to increase the SAEB amplitude, it is necessary to use cathodes with a long sharp edge, including cathodes with several coaxial tubes of different diameters (Figure 12a).

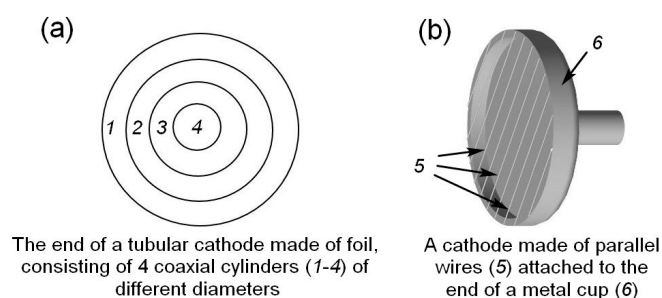


Figure 12. Designs of the cathodes fabricated from tubes (a) and wires (b) with a long sharp edge.

The maximum amplitudes were obtained using grid cathode made of parallel stainless steel wires (Figure 12b). The SAEB current with amplitude of ≈ 100 A and duration at half maximum of 100 ns, which corresponded to the RAE number behind the foil equal to $6.2 \cdot 10^{10}$, was obtained behind the Al foil with a thickness of $10\ \mu\text{m}$. With this cathode, the exposition X-ray dose was measured for the copper foil anode with a thickness of $20\ \mu\text{m}$. The largest exposition dose was 1.8 mR per pulse. The optimum interelectrode gap to obtain the maximum SAEB amplitude was ~ 4 mm. The SAEB amplitude decreased with increasing interelectrode gap, but the average electron energy increased. Therefore, the optimum interelectrode gap to obtain the maximum exposition dose was longer (~ 5 mm) than that for the maximum SAEB amplitude.

Note that the optimum interelectrode gap depends on the design and sizes of the cathode, amplitude and rise time of the generator voltage pulse, and gas type and pressure. For the SLEP-150 generator with the tubular electrode 6 mm in diameter, it was 12 mm.

5.1.4. Influence of the gas pressure and type on the SAEB parameters

Typical dependences of the SAEB current pulse amplitude on the pressure are shown in Figure 13.

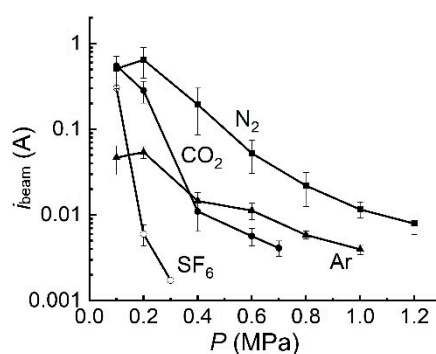


Figure 13. Dependences of the SAEB current pulse amplitude on the pressure for the indicated gases for $d = 4$ mm and tubular cathode obtained using the SLEP-150M generator.

An increase in the gas pressure usually lead to the decrease of the SAEB amplitude [119]. This is connected with the decrease of the reduced electric field strength and the increase of the electron energy losses by collisions. However, there can be exceptions for some sections of the experimental dependences. Thus, the beam current increases when the nitrogen and argon pressure in Figure 13 increases from one to two atmospheres. In this case, this is due to the increased number of the cathode spots on the tubular cathode edge and the improved discharge uniformity.

The maximum SAEB current amplitudes were reached when the diode is filled with light gases (helium and hydrogen), and the minimum amplitudes were observed for gases with large atomic number (krypton and xenon) [31] as well as for molecular gases consisting of a large number of atoms (Figure 13)

5.1.5. Generation of an RE beam in the direction opposite to the anode

This mode was implemented using a high-voltage flat anode and a grounded grid cathode, see Chapter 5 in [112]. The design of a gas diode for generating a RE beam in the direction opposite to the anode is shown in Figure 14.

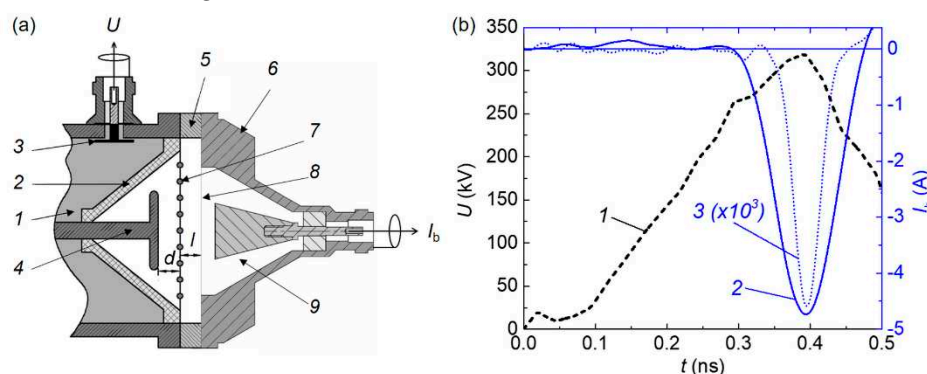


Figure 14. (a) The design of a gas diode for generating a RAE in the direction opposite to the anode. 1 – high-voltage line; 2 – insulator; 3 – capacitive voltage divider; 4 – high-voltage flat anode made of Ta; 5 – metal ring; 6 – collector housing; 7 – grounded grid cathode; 8 – Al foil; 9 – collector receiving part. (b) Waveforms of the voltage U (1) and RAE current I_b in the direction opposite to the anode recorded with 20-mm-diameter (2) and 3-mm-diameter (3) collectors. SLEP-150 (positive polarity). $d = 4$ mm. $l = 3$ mm.

In this mode, the main part of the current from the grid cathode enters the flat anode, causing bremsstrahlung X-ray radiation. However, the beam current in the direction opposite to the anode, which in its characteristics corresponds to the SAEB and is recorded behind an Al foil, reached several amperes. When only a fraction of a RAE current is measured by a collector with a small diameter (3 mm) of the receiving part, its FWHM duration decreases (waveform 3, Figure 14b). An important feature of this mode is the effect of the anode material on the beam current. When using a tantalum Ta anode, the beam current was four times higher than that when using an aluminum one, and the exposure dose of X-ray radiation during a discharge in atmospheric-pressure air was 3.5 mR. Apparently, X-ray radiation affects the formation and movement of an ionization wave in the direction opposite to the anode. With an increase in the intensity of X-ray radiation with the Ta anode, the beam current in the direction opposite to the anode increases.

6. Discussion

Based on our analysis of the experimental and theoretical works devoted to runaway electron generation in centimeter gaps filled with high- pressure gases cited in the present review, we can conclude that the main regularities of this phenomenon has been established by the present time. In

addition, in many works the importance was indicated of runaway electron generation for the formation of various discharge forms, primarily diffusion discharges [16,32]. However, when studying the RAEB in high-pressure gases, primarily in air at atmospheric pressure, discussions constantly arose on the electron energy distribution, the RAEB pulse duration, and the mechanism of runaway electron generation. By the present time, the number of debatable questions has decreased. This is due to improved equipment and sensors used in experimental research as well as refined theoretical models. Let us consider in more details the results for which new data have been obtained.

The amplitude and duration of the RAEB pulse are important parameters for the runaway electron generation. We have already pointed out that in the first works [12–16] in which the runaway electron beams (RAEB) were registered in air at atmospheric pressure, the generators of high-voltage pulses with comparatively long rise time, large diameters of the transmission line and gas diode, and cathode and gas diode designs non-optimal for obtaining runaway electron beam currents of several ten amperes were used (see Figure 5.1.1 of work [16]). In addition, sensors used for RAEB registration and employed oscilloscopes had insufficient time resolutions. Over the last 10 years, the generators, sensors for beam registration, and the gas diode design have been significantly improved. In addition, the oscilloscopes appeared with picoseconds time resolution. It was found that to obtain beams with a great number of runaway electrons behind the anode foil and hence, a high RAEB amplitude, not only high reduced electric field strengths and voltage pulses with short rise times, but also the cathodes with extended edges and a great number of emission centers are required [31,32,112]. Moreover, it has been established that the beam current increases for the optimum design of the gas diode shown in Figure 12 and the longitudinal electric field [97]. In the gas diode shown in Figure 12, the runaway electrons propagating at large angles to the longitudinal cathode axis [28] charge the insulator surface, thereby increasing the number of electrons registered behind the anode foil. In addition, the loss of electrons that go to the side wall of the gas diode is reduced by increasing the area of the cathode with a sharp edge, see Figure 12.

The conducted researches confirmed that the minimum duration of the runaway electron beam current were registered behind the anode foil only when measuring a part of the electron beam transmitted through a hole in the anode diaphragm the diameter of which should be 1 mm or less [120]. It was found that the RAEB pulses having two peaks were registered in some cases (see Chapter 4 of work [32]) with small diaphragms placed at the anode and cathode having extended edge with small curvature radius. This mode can be explained by non-simultaneous emission along the sharp edge of the cathode with small curvature radius. It was shown that for voltage pulses with rise times of 0.3 and 0.7 ns, the least RAEB durations were observed with cone or spherical cathodes having a radius of ~1 cm, and one emission center was formed at the electric field maximum [120].

The occurrence of electrons with anomalous energy was caused by the Askaryan effect. The results of calculations presented in [8,9] showed that a part of electrons in the electric discharge in gases can acquire additional acceleration due to synchronous movement with electrons of the streamer or ionization wave front. This mechanism was experimentally confirmed by registration of electrons with anomalous energy (exceeding eU , where U is the voltage on the discharge gap; see Figure 10) as well as by the results of theoretical modeling shown in Figures 4 and 5. However, in works [121,122] (see also work [16]), it was declared that the electron energy distribution maximum corresponds to an energy of 290 keV for the interelectrode gap of 2 cm and the voltage on the gap $U_m = 190$ kV. Moreover, work [121] erroneously stated that the monoenergetic runaway electron beam is generated in air at atmospheric pressure. In that case, the main part of electrons in the beam had the energy exceeding eU_m [122]. This error was repeated in the recent work [123] of this group.

There was also the third point of view on the possibility of generation of runaway electrons with anomalous energy presented in works [34,124]. The authors of these publications considered that the maximum energy of runaway electrons generated in air at atmospheric pressure cannot exceed eU_m . As already pointed out above, the results of simulations (see Figures 4 and 5 in Section 3) together with experimental measurements shown in Figure 10 demonstrate generation of runaway electrons with different energies, including the energy exceeding eU . As can be seen from the calculated results shown in Figure 5, the ratio of the number of runaway electrons with anomalous energy to that with

energy $\leq U$ is greater than in the experimental conditions. This is due to the fact that calculations were performed for a simplified geometry of the gas diode disregarding the RAE generation at different angles.

Let us schematically describe the mechanism of runaway electron generation in the SAEB generation mode in which the maximum beam current amplitude behind the foil anode has been successively obtained to date. Four stages of the SAEB generation can be distinguished in the discharge development. The first stage corresponds to the auto-electron emission from the cathode that arises at voltage pulse amplitude of hundreds of kilovolts at the pulse front due to macro- and micro-inhomogeneities on the cathode. As already pointed out above, the cathode should have sharp edges and long length of the emitting surface for generation of SAEB with maximum amplitudes. In the second stage, the electrons emitted from the cathode go over to the mode of running away due to the electric field concentration on micro- and macro-inhomogeneities of the cathode. These electrons ionize the gas near the cathode and create initial electrons from which, together with the auto-emission electrons, electron avalanches develop transforming into a spherical streamer (an ionization wave). Accordingly, a dense cloud of diffusion plasma is formed near the cathode in a short time. In this stage, the discharge current together with the displacement current with subnanosecond voltage pulse front reaches several hundreds of amperes (Figure 8), and the auto-electron emission has time to convert into explosive one [125]. At voltage pulse durations of 0.1–0.2 ns, the corona diffusion discharge is observed near the cathode together with bright spots arising on the cathode surface. In addition, the current from the cathode is influenced by near-cathode plasma radiation. The influence of the photoemission on the beam current generation leads to the approach of the diffuse discharge to the lateral surface of the cathode (see Figure 6 in Chapter 1 of work [32]). Note that the electric field near the cathode is additionally amplified by the positive ion charge, and this also can lead to fast electron generation, including the region near the lateral cathode wall. The main RAE number is generated in the third phase and is caused by the electron acceleration between the dense polarized plasma front (the streamer front) and the anode. In the beginning, this occurs at the cathode, and for a high rate of voltage change, in the gap and near the anode. The electrons moving at the ionization wave front and in the gap are affected by both negative charge of the avalanche heads and the voltage on the anode. Note that the electric field in the gap is amplified when the streamer front approaches to the anode. In the fourth stage, the ionization wave front reached the anode, the electric field distribution in the gap becomes more uniform, and the electron beam generation stops. In addition, after the ionization wave front reached the anode, the voltage on the gap decreased. The voltage decay on the gap depends on the gas pressure and type. It was experimentally established that using the SLEP-150 generator, the voltage on the gap starts to decrease in 200–500 ps (Figure 8a). In this time, the streamer front and the electron beam reached the anode, and the ionization energy increased. Under these conditions, the ionization wave velocity reached ~ 10 cm/ns [126]. The different RAE generation modes were described in detail in work [127].

By the present time, it has been established that the **first** electrons in pulsed discharges in centimeter intervals are initiated from the cathode with small curvature radius due to auto-electron emission. In this case, the electron emission can be amplified due to microinhomogeneities appearing on the cathode owing to the explosive electron emission [128], and as shown in new works, the influence of mechanical stresses [129] and small particles sputtered from the cathode [130] can be observed. The electrons start to accelerate to high energies in the near-cathode zone with enhanced electric field after occurrence of the first electron avalanches transforming into a spherical streamer. Furthermore, the energy of a part of initially accelerated electrons continued to increase in the decreasing electric field. At subnanosecond high voltage pulse fronts, the runaway electron number can increase when the wide streamer front approaches to the anode [30]. And this increase of the runaway electron number is manifested through the increase of not only RAE amplitude, but also its duration.

7. Conclusions

Since the origin of C. T. R. Wilson's idea [1,24] on the possibility of electron acceleration to high energies in atmospheric discharges, the runaway electron generation has been studied for about a hundred years. His idea had a significant impact on the understanding of processes occurring in gas discharges at high electric field strengths. The runaway electron generation in gases is a fundamental physical process which influences the gas medium breakdown. To realize the runaway electron mode in air or other gases at high pressure, the reduced electric field strength should exceed its threshold value. This is most easily reached in a non-uniform electric field using the cathodes with small curvature radius. In the beginning, the electrons are accelerated in the zones of the maximum electric field, and then their acceleration continues in the lower field zone due to the reduced electron energy losses with increase of their velocity. The reduced threshold electric field strength necessary for the formation of beams with the maximum number of runaway electrons is about 10 times higher compared to the conventional reduced electric field strength [53,54,56].

The modes of runaway electron beam generation are very diverse and depend on the voltage pulse parameters, gas type and pressure, cathode and gas diode designs, and cathode material. The RAEB amplitudes of ~100 A have already been reached in air at atmospheric pressure [31] and can be further increased. The RAEB pulses with amplitudes of several units of kiloamperes and subnanosecond pulse duration can be obtained by decreasing the gas pressure in the diode. The runaway electrons allow pulsed diffuse discharges with high specific energy contribution to be obtained that can be used to create pulsed lasers and excilamps as well as to process metal, dielectric, and semiconductor surfaces.

In conclusion, note that currently there are little-studied discharge aspects significantly affected by the runaway electron beam generation, in particular, the atmospheric discharges [16,32,131]. The runaway electron generation limits the plasma heating in installations for studying the thermonuclear synthesis. The problem of improving the existing theoretical models is also relevant, first of all, the development of three-dimensional models which will allow one to describe more accurately the obtained experimental results and to predict new modes of runaway electron generation.

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