
Quantitative and Graphical Prediction of Atom Distribution and Lattice Distorting Behavior of FCC_CoCuNi Multi-Principal Element Alloys Based on Inherent Sublattice Preference

Xiangyan Su , Xiaolin Zhou , [Minliang Gao](#) , Dehua Wu , Hui Guo , [Xuan Fang](#) , Anqi Ji , Xingyu Chen , Xiaoqiong Zhang , Hehua Que , Haoran Han , Jinkun Chen , [Bo Wu](#) * , [Baisheng Sa](#) , Yu Tang , [Chuangshi Feng](#) , [Fuxiang Zhang](#) * , [Limei Cha](#) , [Xiaolan Yang](#) , Chen Dong , [Jiankang Huang](#) * , [Yue Shen](#) , [Ming Wen](#) *

Posted Date: 10 February 2026

doi: 10.20944/preprints202602.0788.v1

Keywords: multi-principal element alloys (MPEAs); alloy thermodynamics; sublattice preference; microstructure at atomic level; lattice distorting behavior; computational materials science



Preprints.org is a free multidisciplinary platform providing preprint service that is dedicated to making early versions of research outputs permanently available and citable. Preprints posted at Preprints.org appear in Web of Science, Crossref, Google Scholar, Scilit, Europe PMC.

Copyright: This open access article is published under a [Creative Commons CC BY 4.0 license](#), which permit the free download, distribution, and reuse, provided that the author and preprint are cited in any reuse.

Disclaimer/Publisher's Note: The statements, opinions, and data contained in all publications are solely those of the individual author(s) and contributor(s) and not of MDPI and/or the editor(s). MDPI and/or the editor(s) disclaim responsibility for any injury to people or property resulting from any ideas, methods, instructions, or products referred to in the content.

Article

Quantitative and Graphical Prediction of Atom Distribution and Lattice Distorting Behavior of FCC_CoCuNi Multi-Principal Element Alloys Based on Inherent Sublattice Preference

Xiangyan Su ¹, Xiaolin Zhou ¹, Minliang Gao ², Dehua Wu ³, Hui Guo ⁴, Xuan Fang ¹, Anqi Ji ¹, Xingyu Chen ², Xiaoqiong Zhang ², Hehua Que ², Haoran Han ², Jinkun Chen ², Bo Wu ^{1,2,*}, Baisheng Sa ², Yu Tang ⁵, Chuangshi Feng ⁵, Fuxiang Zhang ^{5,*}, Limei Cha ⁶, Xiaolan Yang ⁷, Chen Dong ⁸, Jiankang Huang ^{8,*}, Yue Shen ⁹ and Ming Wen ^{9,*}

¹ Materials Design and Manufacture Simulation Facility, School of Advance Manufacturing, Fuzhou University, Jinjiang, 362200, China

² Multiscale Computational Materials Facility, Materials Genome Engineering Institute, School of Materials Science and Engineering, Fuzhou University, Fuzhou, 350100, China

³ School of Computer Science and Technology, Hainan University, Haikou, 570228, China

⁴ Key Laboratory of Pico Electron Microscopy of Hainan Province, Center for Advanced Studies in Precision Instruments, Haikou, 570228, China

⁵ Songshan Lake Materials Laboratory, Dongguan 523808, China

⁶ Material Science and Engineering Department, Guangdong Technion Israel Institute of Technology, Shantou, Guangdong 515063, China

⁷ School of Physics and Electronic Science, Zunyi Normal College, Zunyi 563006, China

⁸ School of Materials Science and Engineering, Lanzhou University of Technology, Lanzhou, 730050, China

⁹ State Key Laboratory of Precious Metal Functional Materials, Kunming, Yunnan, 650106, China

* Correspondence: wubo@fzu.edu.cn (B.W.); zhangfuxiang@sslabor.org.cn (F.Z.); sr2810@163.com; (J.H.); wen@ipm.com.cn (M.W.)

Highlights

1. The inherent sublattice preference behavior of FCC_CoCuNi multi-principal alloys are predicted theoretically.
2. Sublattice preference consideration extends beyond the commonly believed yet unreasonable randomly mixing hypothesis.
3. Atom distribution and lattice distorting behaviors are quantitatively and graphically characterized based on sublattice preference.
4. The even and odd layers of MPEA may show considerable different atom distributing behavior due to sublattice preference.

Abstract

The inherent temperature-dependent sublattice preference of constituent atoms in FCC_CoCuNi multi-principal element alloys (MPEAs) is theoretically predicted by combining a two-sublattice model based on the L1₂AuCu₃ prototype with computational thermodynamics, which extends beyond the commonly-believed, yet unreasonable randomly mixing solid solution hypothesis. Based on the predicted sublattice occupied fractions (SOFs) and available computer resource, two MPEAs atom distributing models with different sizes are established for different applications, respectively, where the bigger size model is further employed to analyze statistically the atom distributing character quantitatively and graphically, while the smaller size model is employed to study the lattice distortion of MPEAs further using first-principles calculations density functional theory. The atom distributing configurations of some representative heat treatment temperatures, as well as the

hypothetical randomly mixing structure are compared. It is revealed that FCC_CoCuNi MPEAs exhibit strong temperature-dependent ordering behavior. The SOFs-based configurations are $(\text{Ni}_{1.0000})_{1a}(\text{Co}_{0.4445}\text{Cu}_{0.4444}\text{Ni}_{0.1111})_{3c}$, $(\text{Co}_{0.0653}\text{Cu}_{0.0721}\text{Ni}_{0.8626})_{1a}(\text{Co}_{0.4227}\text{Cu}_{0.4204}\text{Ni}_{0.1569})_{3c}$, and $(\text{Co}_{0.1574}\text{Cu}_{0.1593}\text{Ni}_{0.6833})_{1a}(\text{Co}_{0.3920}\text{Cu}_{0.3913}\text{Ni}_{0.2167})_{3c}$ at 100 K, 900 K, and 1400 K, respectively. Overall, Ni atoms always prefer to 1a sublattice and the preference tendency reduce a little bit at considerable high temperatures. The configurational entropies of FCC_CoCuNi MPEAs increase with the increase of heat treatment temperature, while they are considerably lower than that of the hypothetical ideal random solid solution. Based on the atom distributing model of MPEAs, the local atomic cluster characteristics are further investigated by statistically analyzing the coordination numbers of the constituent atom coordinated with the same type of atoms. The radial distribution function (RDF) further verified the atom aggregating behavior. For most family of crystal planes in FCC_MPEAs, except {1 1 1}, there are obviously different atom distributing characters between the even and odd layers. The atom distributing model of some representative bulk structure and surface structure are afforded valuably for reference and application both in experimental and theoretical investigation further. Thus, rich and indispensable structural genome data are afforded for the further research and development of the promise FCC_CoCuNi MPEAs intensively.

Keywords: multi-principal element alloys (MPEAs); alloy thermodynamics; sublattice preference; microstructure at atomic level; lattice distorting behavior; computational materials science

1. Introduction

Over the past two decades, high-entropy alloys (HEAs), synthesized by mixing multiple principal elements in equimolar or near-equimolar proportions, have been shown to possess exceptional properties [1–4]. Among them, CoCuNi have emerged as promising candidates for various advanced applications [5–7]. Benefiting from synergistic effects, potential application in the field of catalysis compared to conventional oxides [8]. For instance, catalysts composed of low-cost CoCuNi MPEAs display excellent performance, close to the noble metal-based catalysts RuO₂ or IrO₂ in the hydrogen evolution reaction (HER) [9,10]. In addition, owing to their distinctive magnetic and magnetoresistive properties, Co-Cu alloys are recognized as robust candidate systems for synthesizing magnetic heterostructures [11], which can be potentially applied as materials for magnetic devices such as MEMS [12]. The incorporation of Ni contributes to enhancing the magnetic properties of Co-Cu systems [13–15], compared with that of Cr, Fe, or Mn. Karpuz et al. discussed the correlation of magnetic properties from the perspective of microstructure [16], it is found that adjusting the deposition potential exerts a crucial influence on the film composition, microstructure, and magnetic properties of ternary CoCuNi alloys simultaneously. Mondal et al. [17] prepared nanoscale ternary Cu₅₀Co₂₅Ni₂₅ alloys at different annealing temperatures, verifying the correlation between microstructure and magnetic properties.

FCC_CoCuNi MPEAs have been successfully prepared via traditional vacuum arc melting methods, as well as new approaches including electrodeposition [18] and microemulsion [19] methods. However, till now, the inherent composition and temperature-dependent sublattice preference, or the atom distributing characteristics remain unclear, which hinders the intensive understanding and modulating the heat treatment process, microstructure, diverse properties and potential applications for this inexpensive MPEAs. Traditionally, atoms in MPEAs are generally assumed to be randomly distributed on the full crystal lattice structure, but in our view, such a hypothesis is unreasonable, since the inherent differences exist both for the various constituent sublattices and the various constituent atoms, let alone the influence of heat treatment temperature, are neglected in total, thus, severe miscalculations are inevitable. Most recently, Ding emphasis that the study of MPEAs should be switch from the traditional disorder-believed to ordered structure character care [20]. In fact, we realized this issue since 2011 [21], and sustained explorations have been carried out [21–31]. In our previous work, the possibilities of forming FCC high entropy alloys

in equal-atomic systems CoFeMnNiM and CoFeMnNiSmM have been explored by considering the criteria of Gibbs free energy of formation and the configurational entropies simultaneously, due to the limitation of available computer resource, only the total energy at ground state were calculated using first-principles calculation based on Density functional theory (DFT). After carrying out long-time explorations, we proposed a general sublattice model that integrates computational thermodynamics with first-principles calculations based on combining DFT and density functional perturbation theory (DFPT) to predict sublattice preference and its order-disorder transitions [22]. The framework has been successfully applied to investigate the mechanical or chemical properties of some typical intermetallic compounds and MPEAs. For example, Hamid et al. [23] revealed that in Ni₃Al-based γ' phase (L1₂ structure) superalloys, Cr can significantly improve the microhardness of the alloy, while Mn exerts the most pronounced effect on reducing the bulk modulus and shear modulus based on the sublattice preference. Chen et al. [24,25] investigated the atom distributing behavior, lattice distorting behavior and mechanical properties of CoCrNi, CoNiV and CoCrFeNi MPEAs. For FCC_CoNiV MPEAs, Zhang et al. [26] found that the predicted temperature-dependent hardness of SOFs-based structure agree well with the available experimental results, while the special quasirandom structure (SQS) model is lower about 50%. Qiao et al. [27] revealed the non-periodic diffusion energy barrier waves for the C atom diffusing along the neighboring octahedra in FCC_CoNiV MPEA with (V_{1.0000})_{1a}(Co_{0.4445}Ni_{0.4444}V_{0.1111})_{3c}. Weng et al. systematically investigated the oxygen evolution reaction (OER) of FCC_CoFeGaNiZn [28], and HER of FCC_CoCrFeNi [29], and Su et al. [30] systematically investigated the OER of FCC_CoCuFeNiPd and CoCuFeNiRu. by systematically analyzing the intermediate adsorption behavior and free energy changes surface adsorption sites, they revealed that the average overpotential is in excellent agreement with the available experimental value for the SOFs-based model, significantly outperforming the results obtained from the SQS model. Qian et al. [31] revealed the influence of N content on structures and mechanical properties of FCC_(AlCrMoTiV)_{1-x}N_x high entropy nitrides, and the surface oxidation mechanism and mechanical properties of lightweight MPEAs AlCrMoTi and AlCrMoTiV based on sublattice preference. Even for the complex intermetallics with three sets of sublattices [32] or four sets of sublattice [33], the predicted SOFs agree well with the available experimental data.

In this work, the temperature-dependent sublattice preference of constituent atoms of FCC_CoCuNi MPEAs is predicted quantitatively and graphically. Based on the predicted SOFs, the atomic distribution characteristics and associated lattice distorting behavior are analyzed. The fundamental and essential structure model of some representative bulk structures and surface structures at atom scale are established based on the sublattice preference, which are expected to facilitate the potential application to explore the microstructure and diverse properties of FCC_CoCuNi MPEAs from experimental and theoretical aspects, promote especially the potential applications in catalytic and magnetic research fields.

This paper comprises four sections. Following the introduction in Section 1, Section 2 briefly outlines the theoretical models and the computational parameters used in calculations. Section 3 presents a detailed analysis of temperature-dependent sublattice preference, local ordering behavior, lattice distorting behaviors, and surface models. Finally, the conclusions of the study are summarized in Section 4.

2. Materials and Methods

2.1. Sublattice Model of MPEAs with FCC Structure

The crystal lattice structure information of the L1₂-AuCu₃ prototype employed in simulating the FCC MPEAs is presented in Table 1, and the fundamental information of structures and properties of stable elements at room temperature involved in this study is shown in Table 2.

Table 1. The crystal lattice structure information of the L1₂AuCu₃ prototype employed in simulating the FCC MPEAs.

Phase	Prototype	Pearson's Symbol	Strukturbericht Designation	Space Group	Wyckoff positions		
				Symbol	Number	Multiplicity	Wyckoff letter
FCC	AuCu ₃	cP4	L1 ₂	Pm3m	#221	1	a
						3	c

Table 2. The fundamental information of structures and properties of stable elements reference (SER) at room temperature involved in this study.

Metal	Stable structure	Space No.	Space Group	Radius(Å)	χ	Atomic mass	Outer Ele.	Melting(K)
Co	HCP_A3	194	P6 ₃ /mmc	1.25	1.88	58.93	3d ⁷ 4s ²	1768
Cu	FCC_A1	225	Fm3m	1.28	1.90	63.55	3d ¹⁰ 4s ¹	1358
Ni	FCC_A1	225	Fm3m	1.25	1.91	58.69	3d ⁸ 4s ²	1726

As mentioned in Section 1, considering the obvious difference between the constituent sublattice 1a and 3c, the difference between the three kinds of constituent atoms HCP_Co, FCC_Cu, and FCC_Ni, as well as the tremendous influence of heat treatment temperature on the microstructure and properties, in this work, the temperature-dependent sublattice preference of the different kind of constituent atoms of FCC_CoCuNi MPEAs are predicted theoretically by combining the two-sublattice model based on the AuCu₃ prototype with L1₂ structure (L1₂AuCu₃) and computational thermodynamics, where the thermodynamic process of MPEAs formed from the constituent atoms is described quantitatively. The general approach has been reported in detail previously and summarized briefly here for following easily.

The general two-sublattice model of multi-component alloy phase is presented in Equation (1), the variable $y_{M_i}^{S_k}$ in the two-sublattice model, denotes the SOFs of element M_i on sublattice S_k , while M_i represents the constituent elements within the alloy system, and S_k corresponds to distinct sublattices defined by Wyckoff positions. and the corresponding FCC_CoCuNi MPEA is shown in Equation (2). The synthesis reaction equation of FCC_CoCuNi MPEA synthesized from the pure elements with stable crystal structure is shown in Equation (3). This equation expresses the overall stoichiometry of the alloy as a weighted distribution of SOFs across distinct Wyckoff positions, with 1/4 of the lattice sites belonging to the 1a sublattice and the remaining 3/4 to the 3c sublattice.

$$\left(M_{1,y_{M_1}^{S_1}}, M_{2,y_{M_2}^{S_1}}, \dots, M_{i,y_{M_i}^{S_1}} \right)_{S_1} \left(M_{1,y_{M_1}^{S_2}}, M_{2,y_{M_2}^{S_2}}, \dots, M_{i,y_{M_i}^{S_2}} \right)_{S_2}, \quad (1)$$

$$\left(Co_{y_{Co}^{1a}}, Cu_{y_{Cu}^{1a}}, Ni_{y_{Ni}^{1a}} \right)_{1a} \left(Co_{y_{Co}^{3c}}, Cu_{y_{Cu}^{3c}}, Ni_{y_{Ni}^{3c}} \right)_{3c}, \quad (2)$$

$$0.3333Co+0.3333Cu+0.3334Ni=0.25[y_{Co}^{1a}(Co)+y_{Cu}^{1a}(Cu)+y_{Ni}^{1a}(Ni)] \\ +0.75[y_{Co}^{3c}(Co)+y_{Cu}^{3c}(Cu)+y_{Ni}^{3c}(Ni)]. \quad (3)$$

The Gibbs energy of formation of the synthesis reaction equation of FCC_CoCuNi MPEAs prepared from the pure elements with stable crystal lattice structure is independent of intermediate reaction pathways and depends solely on the initial and final states of the system. Based on these characteristics of state function, an alternative computational approach for Gibbs energy of formation is adopted: first, the Gibbs energies of formation of the end-member compounds are calculated. These are then transformed into complex alloy phases via a two-stage synthesis process. As an example, the chemical reaction pathway for the formation of CoCuNi MPEAs with an FCC structure from pure elements is illustrated in Figure 1. The total Gibbs energy of the system is subsequently calculated using Equation (4).

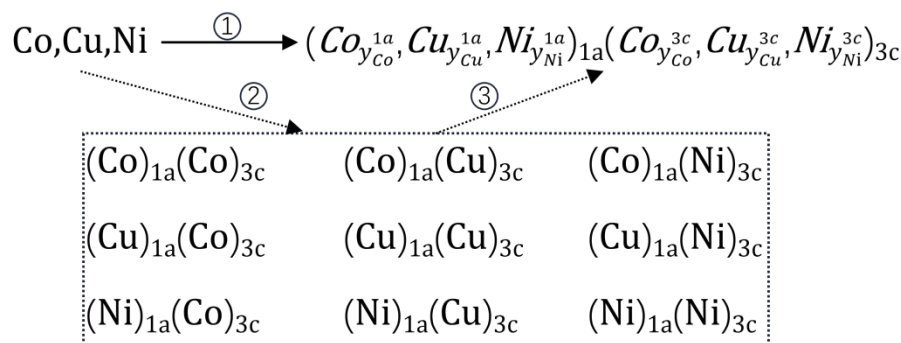


Figure 1. Alternative calculating path of thermodynamic function denoting ① = ② + ③.

$$\Delta G = \sum_{i=1,2,\dots,n} \sum_{j=1,2,\dots,n} y_{M_i}^{1a} y_{M_j}^{3c} \Delta G_{(M_i)_{1a}(M_j)_{3c}} - T \cdot (-R \sum_{i=1,2,\dots,n} (0.25 * y_{M_i}^{1a} * \ln y_{M_i}^{1a} + 0.75 * y_{M_i}^{3c} * \ln y_{M_i}^{3c})) + \Delta G_{phy.} + \Delta G^E, \quad (4)$$

where the $\Delta G_{(M_i)_{1a}(M_j)_{3c}}$ constitutes a critical parameter, representing the formation energy of the ordered end-member compound $(M_i)_{1a}(M_j)_{3c}$ formed from stable elements at ambient temperature. The units of ΔG are normalized to (eV/atom) when the thermodynamic data are processed, and subsequently converted to J/(mol·atom). $y_{M_i}^{S_k}$ represents the SOFs on distinct sublattice. In this work, the thermodynamic database of end-member Gibbs free energies previously established by our research group is directly applied to calculate the alloy thermodynamics under phase equilibrium conditions, and thus the thermodynamic properties, SOFs, and configurational entropy at different temperatures can be obtained. ΔG^E in Equation (4) is the excess Gibbs free energy of formation describes the remaining part of the real Gibbs energy of formation of the phase when the first three terms have been subtracted from the real Gibbs energy, which is ignored in this paper. The main reason is that the excess Gibbs free energy is normally treated using some special polynomial involving interaction parameters, and the interaction parameters are optimized by fitting the available thermodynamic properties of the considered system. However, in this work, the available structural information such as sublattice preference and vacancy concentration, and thermodynamic properties of the considered systems are rather insufficient. We employed the quasi-harmonic approximation (QHA) calculations to consider the main part of thermodynamic properties at a definite temperature, so we ignored excess Gibbs free energy in this study although it is necessary to consider precisely in the future. As for the physical contribution to $\Delta G_{phy.}$ in the present work, consider the complexity of the sublattice occupied configuration, the contribution of magnetic entropy is ignored. It is worth noting that the SOFs obtained based on the thermodynamic database were calculated using the Thermo-Calc software [34].

2.2. First-Principles Calculations

All first-principles calculations presented in this work are performed using the Vienna Ab initio Simulation Package (VASP) [35] based on DFT. Due to the presence of 3d transition metals in the studied systems, spin polarization is included. A plane-wave kinetic energy cutoff of 400 eV is applied for all calculations. Structural relaxations are performed using the conjugate gradient (CG) algorithm, with electronic convergence achieved when the total energy change is less than 1×10^{-5} eV. Structural convergence is defined by a force tolerance criterion of 0.05 eV/Å. The RMM-DIIS algorithm is used for the iterative solution of the Kohn-Sham equations. Sampling over the Brillouin zone employed a $2 \times 2 \times 2$ Monkhorst-Pack k-point mesh [36], which yielded 4 irreducible k-points for the MPEAs modelled bases on the $3 \times 3 \times 3$ supercell of FCC_L12_AuCu₃ prototype.

3. Results and Discussion

3.1. Temperature-Dependent Sublattice Preference of FCC_CoCuNi MPEAs

For the CoCuNi alloy with an FCC lattice structure, the sublattice occupied behavior of alloying atoms on the different kinds of sublattices is predicted and plotted as temperature-dependent SOFs, based on a thermodynamic database of end-member Gibbs free energy of formation functions established in this work, which has been described in our early publications.[22,23,25]. The temperature-dependent SOFs are presented in Figure 2.

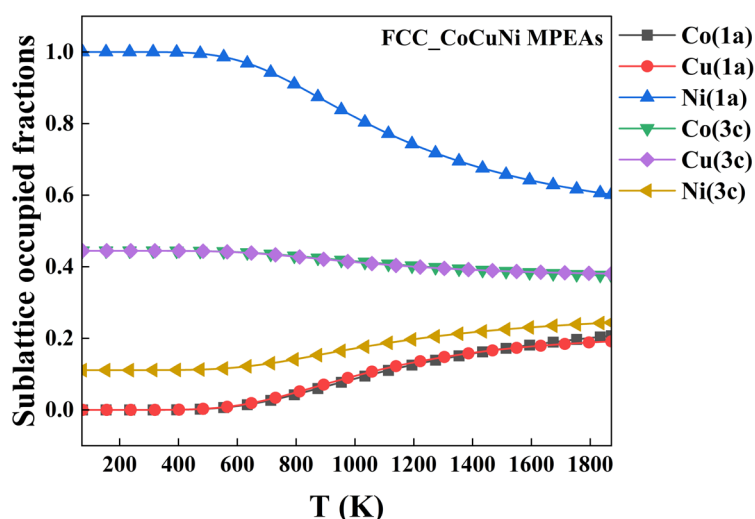


Figure 2. The temperature-dependent SOFs of FCC_CoCuNi MPEAs.

From Figure 2, the obvious temperature-dependent sublattice preference behavior is observed in FCC_CoCuNi MPEAs. For example, the SOFs-based configurations are determined as $(\text{Ni}_{1.0000})_{1a}(\text{Co}_{0.4445}\text{Cu}_{0.4444}\text{Ni}_{0.1111})_{3c}$, $(\text{Co}_{0.0653}\text{Cu}_{0.0721}\text{Ni}_{0.8626})_{1a}(\text{Co}_{0.4227}\text{Cu}_{0.4204}\text{Ni}_{0.1569})_{3c}$, and $(\text{Co}_{0.1574}\text{Cu}_{0.1593}\text{Ni}_{0.6833})_{1a}(\text{Co}_{0.3920}\text{Cu}_{0.3913}\text{Ni}_{0.2167})_{3c}$ at 100 K, 900 K, and 1400 K, respectively. Overall, Ni atoms predominantly occupy the 1a sublattice over the entire temperature range, whereas Co atoms and Cu atoms occupy the 3c sublattice, which exhibit analogous temperature-dependent trends. At low temperature below 500 K, Ni atoms occupy the full 1a sublattice, and the minor rest Ni atoms occupy the 3c sublattice, whereas all the Co and Cu atoms occupy the 3c sublattice. At middle temperature from 500 K to 1200 K, the sublattice preference of Ni change a little bit, that is, gradually shifts from strong preferring to 1a sublattice to slight preferring to 1a sublattice, some of the Ni atoms replace sublattice with some of the Co and Cu atoms. When the heat treatment is carried out above 1200 K, the atom site preferences are weak considerably although the dominant preferred sublattice of each kind of constituent element is maintained. Detailed digital temperature-dependent SOFs data are provided further application in the electronic Supplementary Materials.

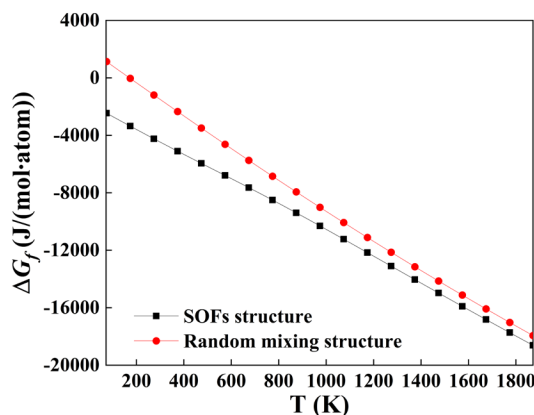
The corresponding thermodynamic properties of formation of the FCC_CoCuNi MPEAs formed from the constituent atoms are predicted based on the formula Equation (4), where the stable structures at room temperature are taken as reference (SER), i.e., the reference state defined in CALPHAD community. The results are plotted in Figure 3. Including the temperature-dependent Gibbs free energy of formation (Figure 3a), enthalpy of formation (Figure 3b), entropy of formation (Figure 3c), configurational entropy (Figure 3d). For comparison, the temperature-dependent Gibbs free energy of formation (Figure 3a) and the configurational entropy (Figure 3d) of the hypothesis randomly mixing structure are also calculated and imposed, and the two kinds of configurational entropies are calculated based on Equations (5) and (6), where the SOFs of the randomly mixing structure of MPEAs is actually equal to the alloy composition, and for the ternary equimolar alloy, all the data are 0.333. We can see that temperature-dependent Gibbs free energy of formation of

randomly mixing structure is always more positive than the SOFs structure, which means the SOFs structure is more stable in thermodynamics than the randomly mixing structure. Meanwhile, the randomly mixing structure over estimates the configurational entropies.

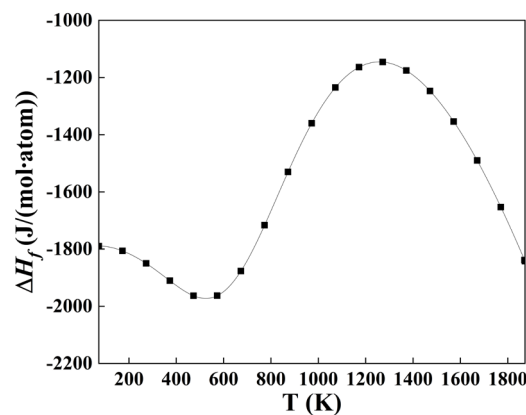
Normally, the perfect or ideal randomly mixing in real alloy systems can not achieve due to the inherent competitive bonding behaviors exist between the different types of the constituent atoms [37]. This observation indicates that the configurational entropy calculated from the randomly mixing configuration only predicts the atomic arrangement of the alloy at high temperatures and fails to capture the thermodynamic evolution of configurational entropy with the increase of heat treatment temperature. Although the reduced configurational entropy tends to increase the Gibbs free energy of formation, the magnitude of the decrease in the enthalpy of formation, as shown in Figure 3b, is substantially larger. This dominant effect of enthalpy on the thermodynamic equilibrium leads to a more negative overall the Gibbs free energy of formation, which suggests that the formation of the FCC_CoCuNi MPEAs within the SOFs framework possesses a stronger thermodynamic driving force. Overall, the configuration based on SOFs can more realistically reflect the thermodynamic behavior of MPEAs, since it takes into account the intrinsic atomic interactions and sublattice preferences inherent to these multi-component systems.

$$S_{Random_mixing_conf} = -R \cdot \sum_{i=1}^n (x_i \cdot \ln(x_i)), \quad (5)$$

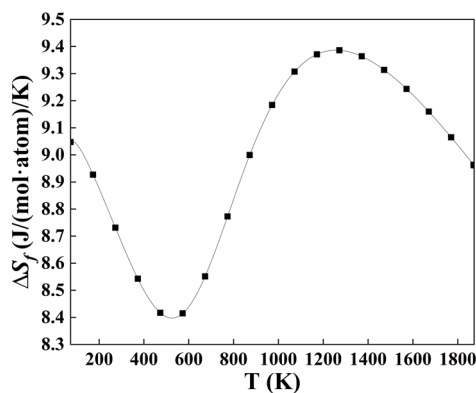
$$S_{FCC_SOFs_conf} = -R \cdot (0.25 \cdot \sum_{i=1}^n y_{M_i}^{1a} \cdot \ln y_{M_i}^{1a} + 0.75 \cdot \sum_{i=1}^n y_{M_i}^{3c} \cdot \ln y_{M_i}^{3c}), \quad (6)$$



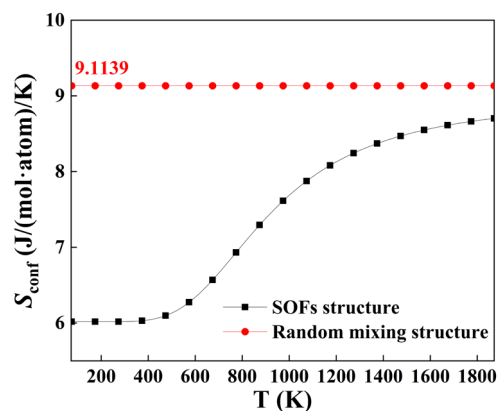
(a) The temperature-dependent of Gibbs free energy of formation



(b) The temperature-dependent of enthalpy of formation



(c) The temperature-dependent of entropy of formation



(d) The temperature-dependent of configurational entropy

Figure 3. Thermodynamic properties of SOFs-Structured FCC CoCuNi MPEAs as a function of heat treatment temperature: (a) Gibbs energy of formation, (b) enthalpy of formation, (c) entropy of formation, and (d) configurational entropy, all compared with the randomly mixing solid solution alloy.

3.2. Graphical Characterization of the Atom Distribution and Local Range Ordering Behavior

To quantitatively characterize the sublattice preferences of the different atoms on the different kinds of sublattices, the atomic-scale spatial arrangement is visualized based on the SOFs predicted from thermodynamic equilibrium calculations in Section 3.1. For the FCC_CoCuNi MPEAs, atomic configurations at three different temperatures are modeled, which correspond to the phase equilibrium states under different heat treatment. The atom configurations based on SOFs of three representative heat treatment temperatures are determined as $(\text{Ni}_{1.0000})_{1a}(\text{Co}_{0.4445}\text{Cu}_{0.4444}\text{Ni}_{0.1111})_{3c}$ at 100 K, $(\text{Co}_{0.0653}\text{Cu}_{0.0721}\text{Ni}_{0.8626})_{1a}(\text{Co}_{0.4227}\text{Cu}_{0.4204}\text{Ni}_{0.1569})_{3c}$ at 900 K, and $(\text{Co}_{0.1574}\text{Cu}_{0.1593}\text{Ni}_{0.6833})_{1a}(\text{Co}_{0.3920}\text{Cu}_{0.3913}\text{Ni}_{0.2167})_{3c}$ at 1400 K, respectively.

Considering the available computational resource limitations and statistical requirements, a $30\times 30\times 30$ supercell model is constructed based on the ordered FCC $\text{L}_{12}\text{-AuCu}_3$ prototype structure, as illustrated in Figure 4. The model contains a total of 108,000 atoms and strictly satisfies the compositional constraints of each sublattice, thereby accurately representing the probabilistic occupancy of atoms under thermal equilibrium at the target temperature. Figure 5 presents the three-dimensional atomic spatial distributions of the FCC_CoCuNi MPEAs at different equilibrium temperatures. The scale bar is calibrated to reflect the actual integer dimensions, with annotations indicating the corresponding lattice nesting structure, the SOFs of different elements in various lattices, and the actual number of atoms occupying each sublattice. Through the visual analysis of this spatial distribution, the enrichment tendency of atomic types at each kind of sublattices can be identified directly.

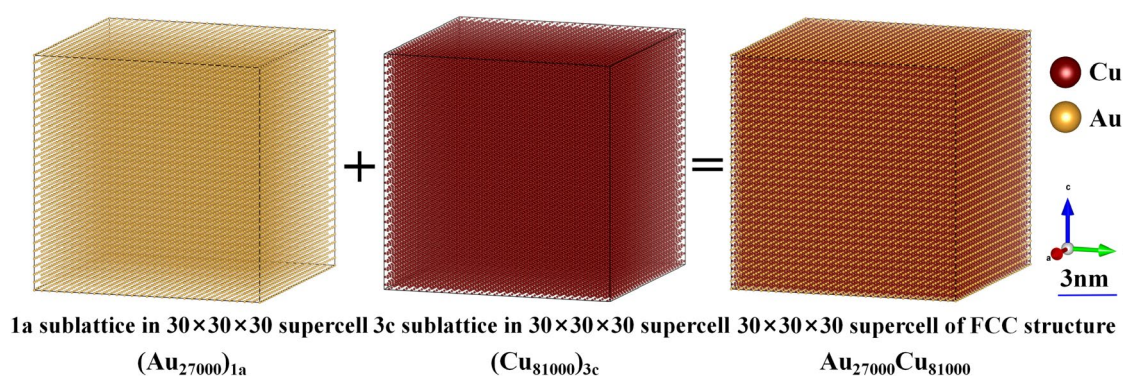
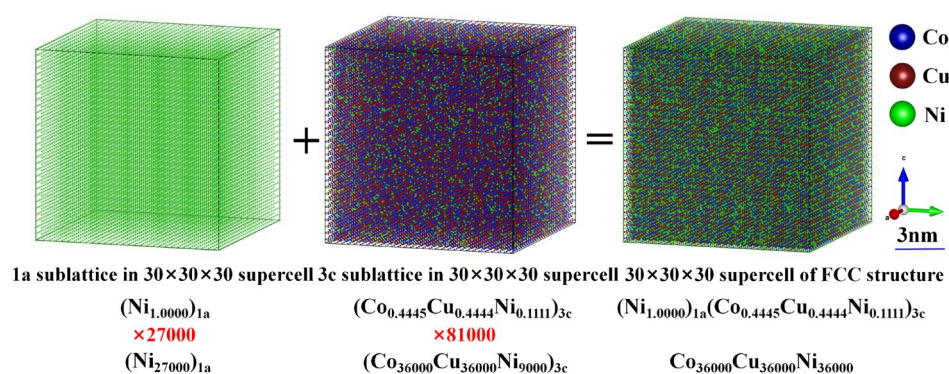


Figure 4. The supercell of the ordered L_{12} prototype structure.



(a) Construction of a $30\times 30\times 30$ FCC supercell based on the prototype of $\text{L}_{12}\text{-AuCu}_3$ for FCC_CoCuNi MPEAs at 100 K

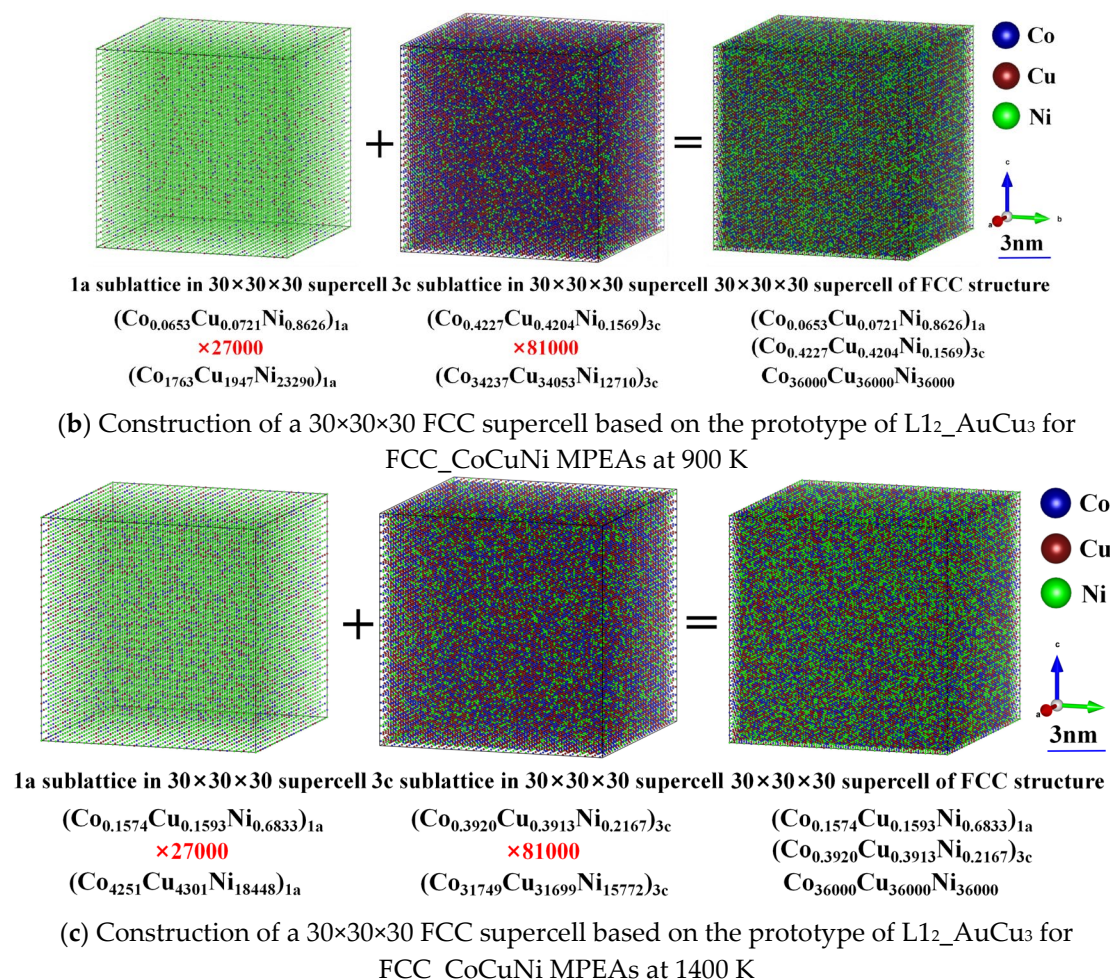


Figure 5. Construction of a $30 \times 30 \times 30$ supercell based on the prototype of $L1_2_AuCu_3$ for FCC_CoCuNi MPEAs at (a) 100 K, (b) 900 K, and (c) 1400 K, respectively.

To explore the so-called chemical short-range order (CSRO) or local ordering behavior, which is the emerging issue in MPEAs, we further quantitatively and graphically characterize the atom distributions by statistically analyzing the coordination environments of various constituent element in FCC_CoCuNi MPEAs at several representative heat treatment temperatures. We simplify the issue initially by focusing only on the first nearest neighbor (1NN) shell of the prescribed central atom M_i^* . To ensure the reliability of the statistical analysis, here we construct three isolated cases based on SOFs at each temperature and comparing them with the ideal randomly mixing structure. See the detail number list in Table 3, where in atom pairs of $M_i^* - nM_i$, the atom marked with a star (*) denotes the central atom of the same type M_i , surrounded by n equidistant atoms (only the 1NN distance is considered for simplification) that form $M_i^* - nM_i$ pairs. It should be noted that the counts for small coordination numbers in Table 3, the atoms agree with the large coordination numbers are included accumulatively, that is, the $M_i^* - nM_i$ configurations include atomic pairs of $M_i^* - nM_i$ and above.

Table 3. Statistical analysis of 1NN coordination characteristics of different central atoms (M^*) coordinated with the same type of atoms $M_i^* - nM_i$ included accumulatively in FCC_CoCuNi MPEAs containing 108,000 atoms under different equilibrium heat treatment conditions.

M* nM	Cluster group number											
	SOFs structure									Randomly mixing structure		
	100K			900K			1400K			At any temperature		
	Case 1	Case 2	Case 3	Case 1	Case 2	Case 3	Case 1	Case 2	Case 3	Cas e 1	Cas e 2	Cas e 3
Co*- 10C	0	0	0	0	0	0	0	0	0	1	1	4
Co*- 9Co	0	0	0	2	6	2	6	13	4	18	16	22
Co*- 8Co	5	6	5	30	25	21	59	63	47	94	73	84
Co*- 7Co	93	80	75	160	148	148	263	274	242	401	358	370
Co*- 6Co	461	497	430	667	669	655	917	940	896	1268	1197	1173
...	-	-	-	-	-	-	-	-	-	-	-	-
Cu*- 10C	0	0	0	0	0	0	0	0	0	4	2	1
Cu*- 9Cu	0	0	0	3	2	3	10	6	5	18	18	11
Cu*- 8Cu	6	3	5	27	23	20	48	54	52	95	81	66
Cu*- 7Cu	66	70	61	157	163	140	230	258	235	383	387	346
Cu*- 6Cu	438	460	411	662	705	657	914	919	902	1229	1254	1176
...	-	-	-	-	-	-	-	-	-	-	-	-
Ni*- 10N	0	0	0	0	0	0	0	0	0	2	2	2
Ni*- 9Ni	0	0	1	3	4	4	11	9	11	19	15	12
Ni*- 8Ni	17	13	9	36	36	34	71	58	71	84	90	76
Ni*- 7Ni	117	124	116	244	233	242	343	362	385	347	367	348
Ni*- 6Ni	729	684	688	1070	1036	1055	1327	1353	1366	1186	1224	1162
...	-	-	-	-	-	-	-	-	-	-	-	-

As we know, the coordination number of a pure metal atom in FCC_L1₂ is 12. Nevertheless, Statistical analysis reveals that for FCC_CoCuNi MPEAs in both phase equilibrium ordered and randomly mixing configurations, the 1NN count of like-atom pairs in the $M_i^* - nM_i$ never exceeds 10, thus far from the full coordination number of 12. Since both Co and Cu atoms are predicted to occupy the 3c sublattice at low temperatures, thereby forming only eight types of 3c-3c coordination

pairs centered on 3c sublattices. thereby limiting the maximum coordinating number $n=8$. In contrast, Ni atoms occupy both the 1a and 3c sublattices, so Ni*-nNi pairs make a higher coordinating chance with the same kind of constituent atom than Co and Cu.

From Table 3, it is seen that when FCC_CoCuNi MPEAs were subjected to equilibrium heat treatment at 100 K, the maximum coordinating numbers n for Co*-nCo, Cu*-nCu, and Ni*-nNi clusters are 8, 8, and 9, respectively. For equilibrium heat treatment both at 900K and 1400 K, all the maximum coordinating numbers n for Co*-nCo, Cu*-nCu, and Ni*-nNi clusters are 9. Further analyze the cluster group number in FCC_CoCuNi MPEAs, indicates that they are temperature-dependent, the cluster group numbers for Co*-8Co, Cu*-8Cu, and Ni*-8Ni in Case 1 at 100 K were 5, 6, and 17, respectively. In contrast, the group numbers for Co*-9Co, Cu*-9Cu, and Ni*-9Ni in Case 1 at 1400 K were 6, 10, and 11, respectively. These results demonstrate that increasing the equilibrium temperature promotes a more uniform sublattice occupied distribution of each kind of element, which in turn increases both the maximum coordinating number within clusters and the cluster group number in FCC_CoCuNi MPEAs. In contrast, in the randomly mixing configuration, the maximum coordinating number n for Co*-nCo, Cu*-nCu, and Ni*-nNi clusters is consistently 10, which is also less than 12. Furthermore, as illustrated in Figure 7, the total number of coordination pairs in the disordered structure is significantly higher than that in the ordered SOFs structure, indicating that the randomly mixing configuration generally overestimates both the maximum cluster group number and the number of coordination pairs. Thus, in comparison to the unreasonable randomly mixing model, constructing large supercells based on SOFs better reflect the fine microstructure at the atomic scale affected by heat treatment temperature, and thereby provides more accurate atomic distribution configurations. These configurations are crucial for the reliable prediction of various properties of MPEAs.

The probability of a kind of constituent atom involved in the group with maximum coordinating number of $M_i^* - nM_i$ can be calculated by combining the maximum coordination number n_{max} and cluster group numbers. For example, when the maximum coordinating number is 10, and the cluster group number is N_g , the probability of a kind of constituent atom involved in the group with maximum coordinating number of $M_i^* - nM_i$ is,

$$P(M_i^* - 10M_i) = [N_g \times (1 + n_{max})/36000] \times 1000\%, \quad (7)$$

where the $1 + n_{max}$ means 1 central atom plus n_{max} coordinating atoms, 36,000 means there are 108,000 atoms in total, and 36,000 atoms for each type of the constituent atom in the equimolar ternary MPEAs based on $30 \times 30 \times 30$ supercell of FCC_L1₂ AuCu₃ prototype. Similarly, when the maximum coordinating number is 9 or 8, and the cluster group number is N_g , the probability of a kind of constituent atom involved in the group with maximum coordinating number of $M_i^* - nM_i$ is,

$$P(M_i^* - 9M_i) = [N_g \times (1 + 9)/36000] \times 1000\% = 0.278N_g\%, \quad (8)$$

$$P(M_i^* - 8M_i) = [N_g \times (1 + 8)/36000] \times 1000\% = 0.250N_g\%. \quad (9)$$

For FCC_CoCuNi in case 3 at 1400 K, the maximum coordination is $M_i^* - 9M_i$, with the probability of a kind of constituent atom involved in the group with maximum coordinating number of $M_i^* - 9M_i$ is calculated in the following,

$$P(Co^* - 9Co) = N_g \times 0.278\% = 4 \times 0.278\% = 1.112\%, \quad (10)$$

$$P(Cu^* - 9Cu) = N_g \times 0.278\% = 5 \times 0.278\% = 1.390\%, \quad (11)$$

$$P(Ni^* - 9Ni) = N_g \times 0.278\% = 11 \times 0.278\% = 3.058\%. \quad (12)$$

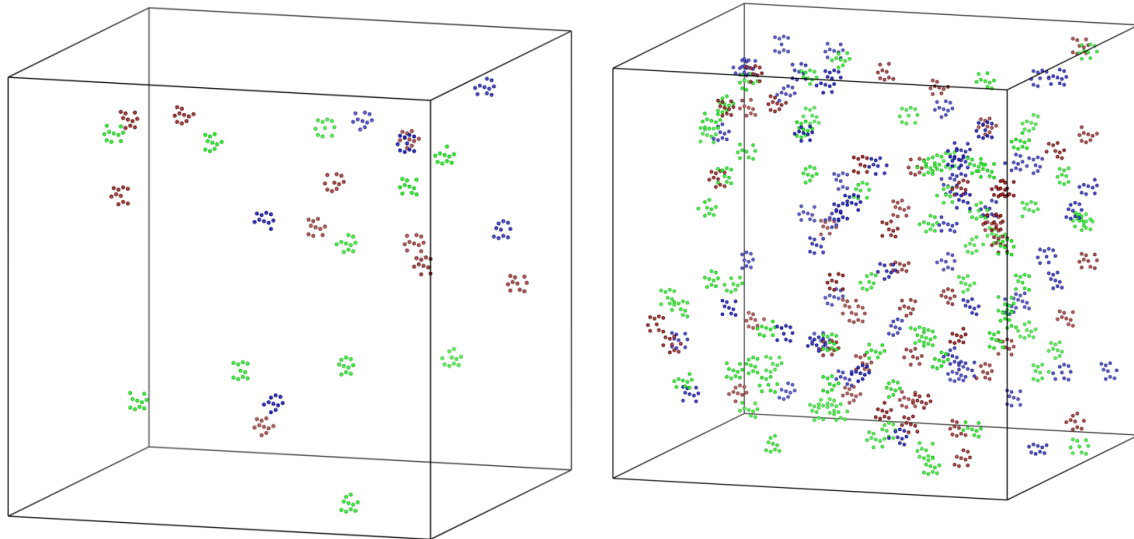
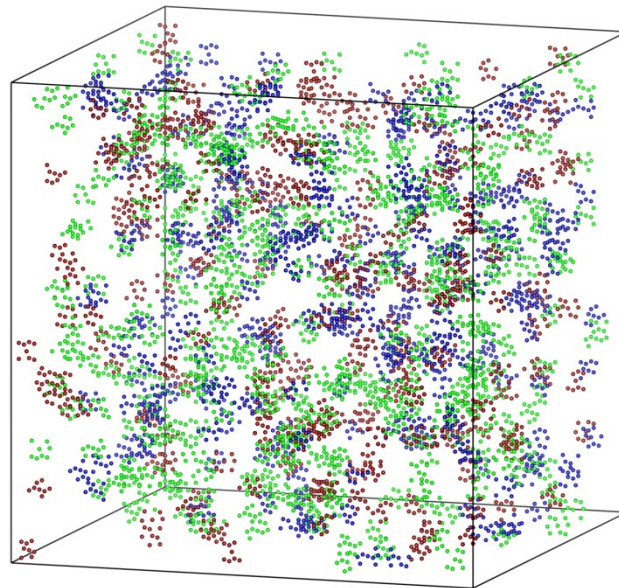
(a) The $M_i^* - 9M_i$ coordinating clusters(b) The $M_i^* - 8M_i$ and above (containing $M_i^* - 9M_i$) coordinating clusters(c) The $M_i^* - 7M_i$ and above (containing $M_i^* - 8M_i$ and $M_i^* - 9M_i$) coordinating clusters

Figure 6. The considerably large coordinating clusters in a sublattice preferring configuration of FCC_CoCuNi MPEAs with a $30 \times 30 \times 30$ supercell based on the prototype of $L1_2\text{-AuCu}_3$ containing 108,000 atoms at 1400 K. (a) The $M_i^* - 9M_i$ coordinating clusters; (b) The $M_i^* - 8M_i$ and above (containing $M_i^* - 9M_i$) coordinating clusters; (c) The $M_i^* - 7M_i$ and above (containing $M_i^* - 8M_i$ and $M_i^* - 9M_i$) coordinating clusters.

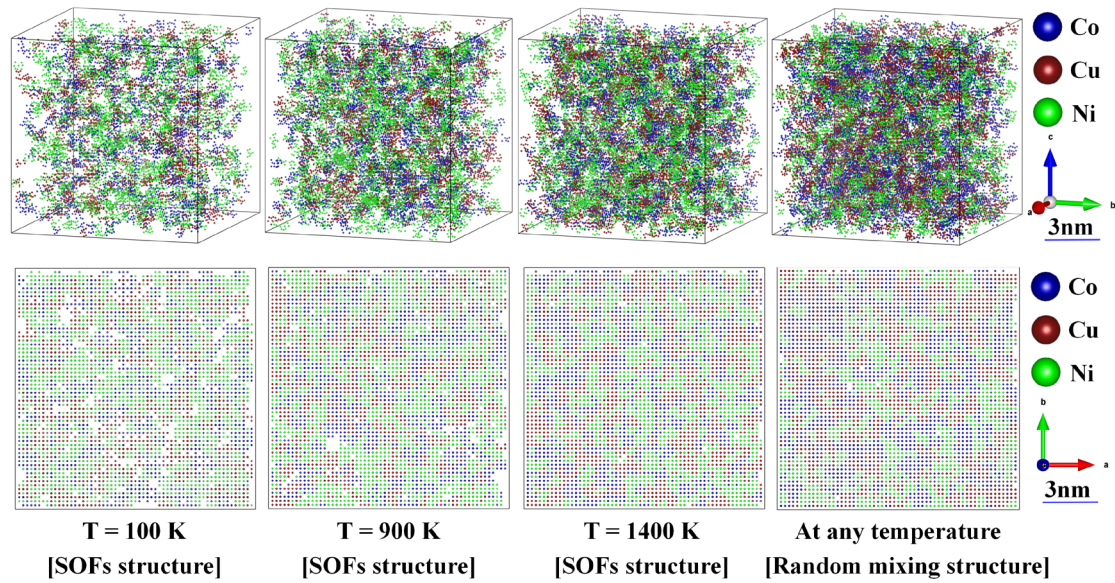


Figure 7. The $M_i^* - 6M_i$ and above (containing $M_i^* - 7M_i$, $M_i^* - 8M_i$, and $M_i^* - 9M_i$) coordinating clusters in FCC_CoCuNi MPEAs structure based on SOFs and randomly mixing configuration at different temperatures, along with their corresponding (0 0 1) plane projection diagrams.

Radial distribution analysis for various atomic pairs is performed for the FCC_CoCuNi MPEAs based on the 30×30×30 supercell model. The radial distribution function (RDF) quantifies the spatial arrangement of the constituent atoms. It represents the ratio of the local particle density at a specific distance r from a reference particle to the average global density of that particle type. Specifically, $g_{AB}(r)$ denotes the density of B type atoms at a radial distance r from a A type atom center, as defined by Equation (13):

$$g_{AB}(r) = \frac{dN_{AB}}{\rho_B 4\pi r^2 dr} \quad (13)$$

where dN_{AB} is the number of B atoms within a spherical shell of thickness dr at distance (r), and ρ_B represents the average bulk density of B atoms. Figure 8a-c present the RDF analysis for the FCC_CoCuNi MPEAs with SOFs structure. The leftmost peak corresponds to the 1NN shell. Peak intensity scales directly with the relative atomic pair density. As shown in Table 3, the high-coordination number ($n \geq 6$) clusters decreases in the order of $\text{Ni} > \text{Co} \approx \text{Cu}$. However, if including low-coordination number ($n < 6$) clusters, the overall cluster abundance follows the sequence $\text{Co} \approx \text{Cu} > \text{Ni}$. This distribution trend is consistent with the atomic coordination characteristics revealed by the RDF; further details are provided in the electronic Supplementary Materials. These findings reveal the inherent chemical short range ordering characters in FCC_MPEAs. Moreover, the RDF profiles confirm not only the ordered atomic arrangement within the 1NN shell but also provide important insights into the coordination features of the second and higher neighbor shells. In contrast, RDF analysis of the randomly mixing structure (see Figure 8d) can only capture the peak differences determined by the component content, but fails to present the shell specificity between atomic pairs revealed in the SOFs model. Consequently, the SOFs approach provides a more accurate description of the local atomic environment. This fidelity is crucial for precise understanding and prediction of material microstructure and resultant properties.

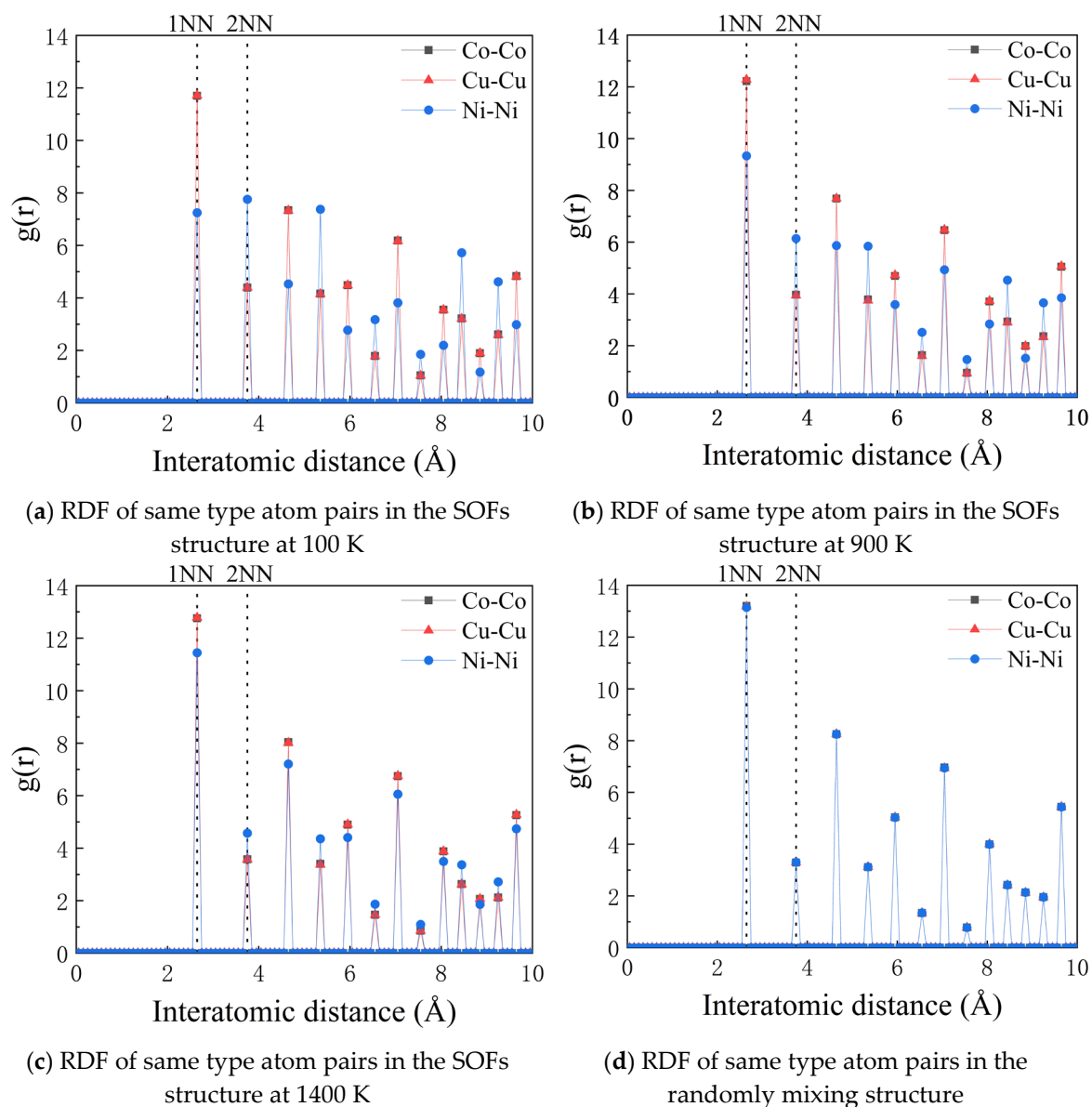
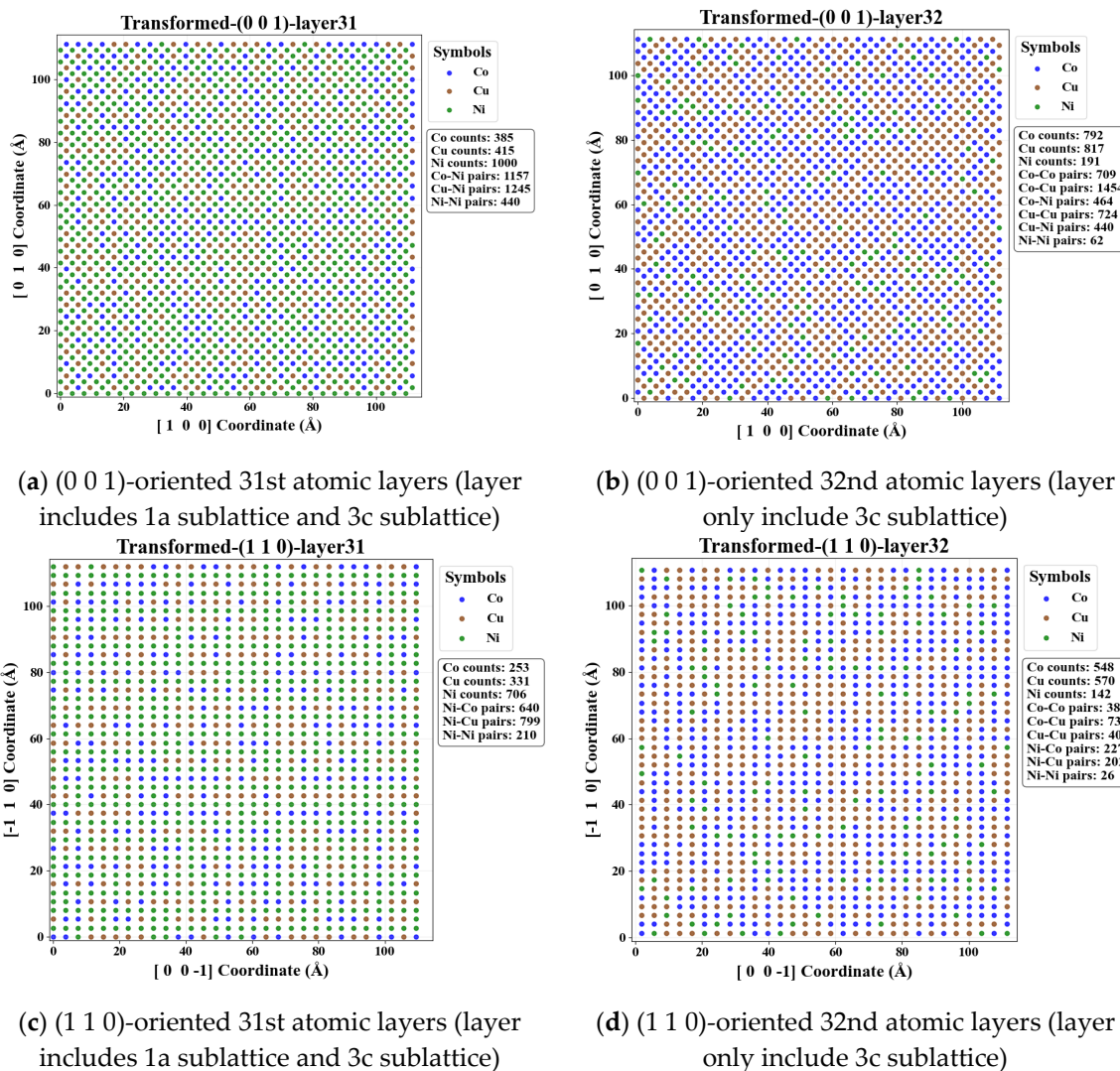


Figure 8. Radial distribution functions of same type atom pairs. (a) SOFs structure at 100 K; (b) SOFs structure at 900 K; (c) SOFs structure at 1400 K; (d) randomly mixing structure.

To elucidate the local distribution characteristics at the atomic scale, a systematic layer-by-layer analysis is performed for FCC_CoCuNi MPEAs based on a $30 \times 30 \times 30$ supercell model of the $L1_2$ _AuCu₃ prototype and SOFs along different crystallographic planes. To minimize the influence of random errors, the 31st and 32nd atomic layers are selected as representative examples for analyzing the planar distribution features. Quantitative statistical results, as illustrated in Figure 9, reveal significant differences in the population distribution of different atomic species between odd and even layers within the $\{0\ 0\ 1\}$ and $\{1\ 1\ 0\}$ plane families. Specifically, the relative abundance of Ni atoms is markedly higher in odd-numbered layers, whereas Co and Cu atoms exhibit a pronounced preference for occupying even-numbered layers. This distribution behavior is primarily attributed to the sublattice preference. As illustrated in Figure 10, Ni atoms tend to predominantly occupy the 1a sublattices of the FCC $L1_2$ _AuCu₃ prototype, Co and Cu atoms predominantly occupy the 3c sublattices of the FCC $L1_2$ _AuCu₃ prototype. Notably, no significant disparity is observed between adjacent layers in the $\{1\ 1\ 1\}$ plane family, the atomic distribution in these planes closely resembles a randomly mixing model, indicating a high degree of interlayer uniformity. Furthermore, this distribution trend remains consistent in different odd layers or different even layers, confirming the statistical adequacy of the supercell size employed in this study. Schematic illustrations of the atomic

distributions for various plane families at other different temperatures are provided in the electronic Supplementary Document.

Differences in compositional distribution across adjacent atomic layers inevitably leads to fundamentally different local chemical environments on the surface. This finding carries important implications for the study of catalytic properties in MPEAs, the bulk region and the near-surface region cannot be simply regarded as completely random solid solutions. The sublattice preference should be considered and thus the difference of the neighbor oven layer and odd layer should be cared when we further study the fine-microstructure and diverse properties experimentally and theoretically. These features must be incorporated as a fundamental premise in constructing accurate models to rationally simulate the adsorption behaviors on catalyst surfaces.



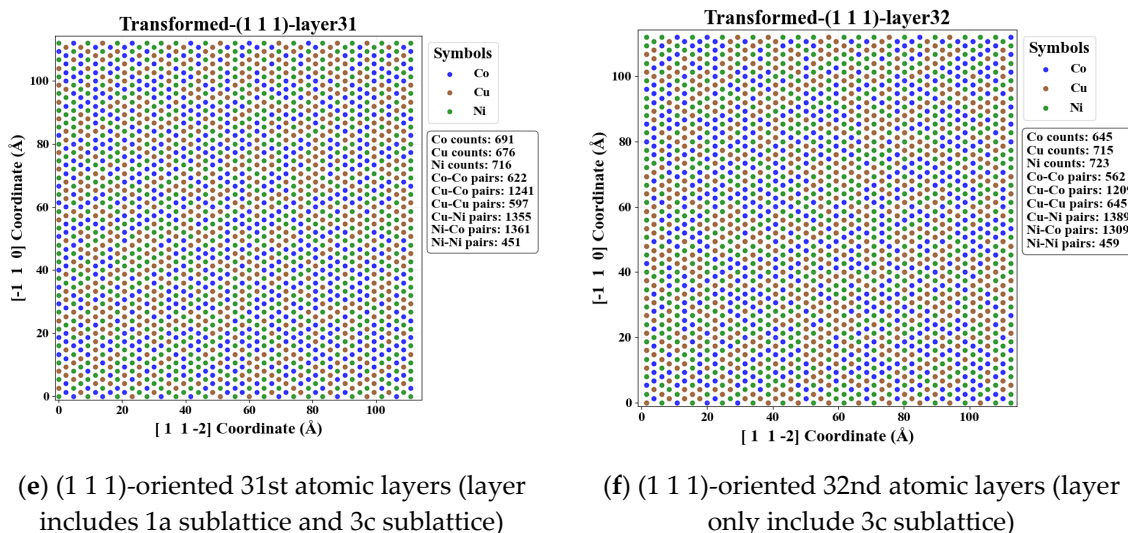


Figure 9. Adjacent atomic layers of FCC_CoCuNi MPEAs with a $30 \times 30 \times 30$ supercell at 100 K. (a-b) (0 0 1)-oriented 31st and 32nd atomic layers; (c-d) (1 1 0)-oriented 31st and 32nd atomic layers; (e-f) (1 1 1)-oriented 31st and 32nd atomic layers.

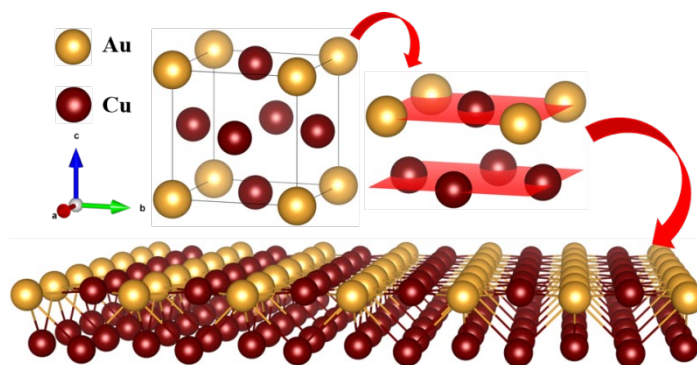
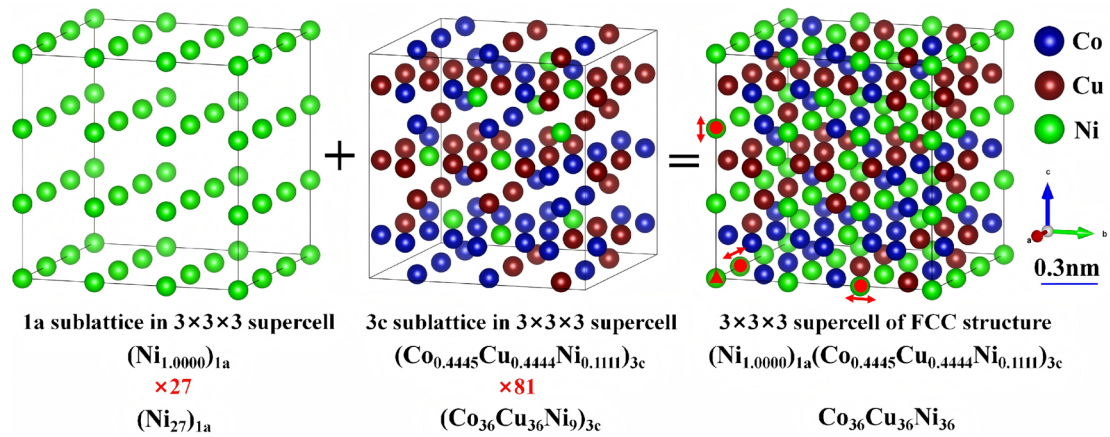


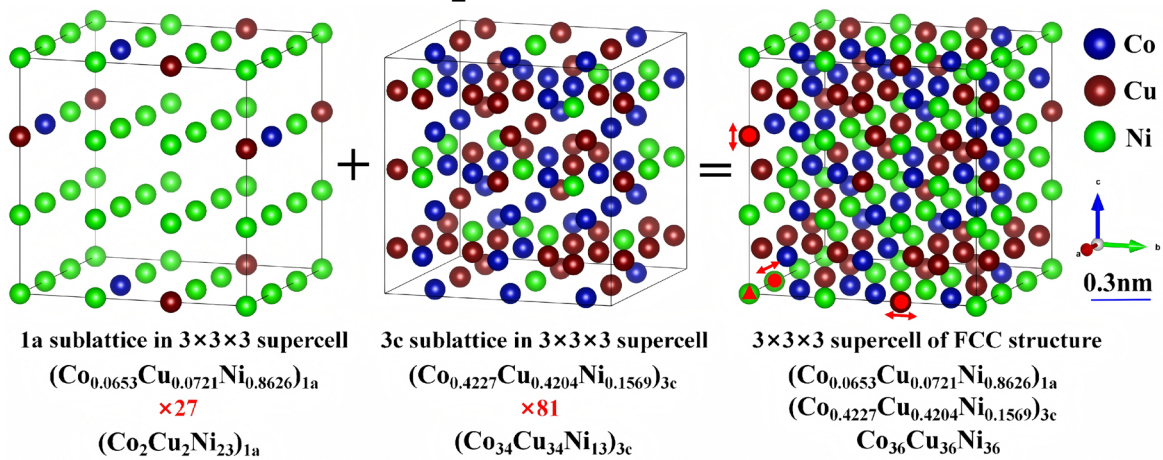
Figure 10. Interlayer atomic sublattice differences of FCC_L12_AuCu₃ supercell.

3.3. Quantitative and Graphical Characterization of the Lattice Distortion of MPEAs

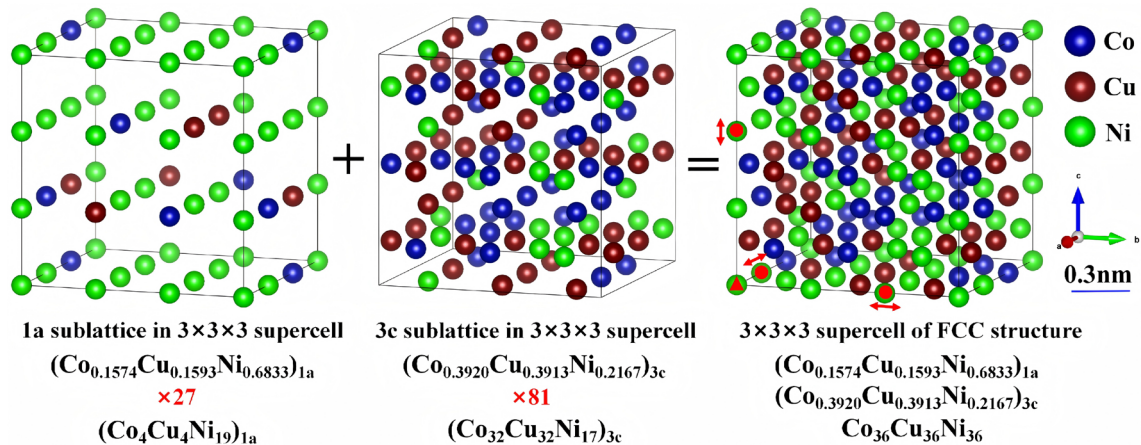
Considering computational resource constraints, $3 \times 3 \times 3$ supercells are constructed based on the FCC_L12_AuCu₃ prototype and the corresponding SOFs, following the same framework as the $30 \times 30 \times 30$ supercells. The calculations are performed for FCC_CoCuNi MPEAs at 100 K, 900 K, and 1400 K. To achieve an optimal balance between computational cost and accuracy, a stepwise optimization strategy is employed. First, atomic positions and unit cell shape are fixed while the volume is optimized (ISIF = 7, NSW = 20; hereafter referred to as R7), yielding the equilibrium lattice parameters for the undistorted configuration. Subsequently, based on the optimized structure from the first step, a full relaxation is performed in which volume, cell shape, and atomic positions are all allowed to vary (ISIF = 3, NSW = 20; hereafter referred to as R3), thereby attaining global energy minimization. It should be noted that during the full relaxation calculation, a selective dynamics method is employed, where one atom is fixed as the original point, while three atoms are constrained to slide along the X, Y, and Z axes, respectively, to suppress the overall crystal rotation and avoid the shift of the full lattice. In Figure 11, the atoms marked with red triangles are fixed at the origin coordinates, while those indicated by red solid circles are only permitted to move along the X, Y, and Z directions. All atomic positions are described using Cartesian coordinates to preserve the spatial vector characteristics of lattice distortions, while distortion values are normalized using 1NN distances to ensure cross compositional comparability of distortion magnitudes.



(a) Construction of a $3 \times 3 \times 3$ FCC supercell based on the prototype of $\text{L1}_2\text{-AuCu}_3$ for FCC_CoCuNi MPEAs at 100 K



(b) Construction of a $3 \times 3 \times 3$ FCC supercell based on the prototype of $\text{L1}_2\text{-AuCu}_3$ for FCC_CoCuNi MPEAs at 900 K



(c) Construction of a $3 \times 3 \times 3$ FCC supercell based on the prototype of $\text{L1}_2\text{-AuCu}_3$ for FCC_CoCuNi MPEAs at 1400 K

Figure 11. Nested supercell model of a $3 \times 3 \times 3$ FCC_CoCuNi MPEAs based on the $\text{L1}_2\text{-AuCu}_3$ prototype and SOFs at (a) 100 K, (b) 900 K, and (c) 1400 K (Atoms fixed or constrained by selective dynamics are highlighted in red.).

The system underwent initial volume relaxation followed by complete structural relaxation. The corresponding lattice parameters, angles, volumes, and total energies are summarized in Table 4. To quantitatively characterize lattice distortion, the 1NN distance d_o between adjacent atom pairs in the volume relaxing structure is adopted as the reference. The relative distortion is defined by Equation (14).

$$Dr = \frac{\sum_{i=1}^n \sqrt{(x_{i,disto.} - x_{i,undisto.})^2 + (y_{i,disto.} - y_{i,undisto.})^2 + (z_{i,disto.} - z_{i,undisto.})^2}}{(n-1) \times d_o} \times 100\% \quad (14)$$

where, n denotes the total number of atoms in the supercell. For the 3×3×3 FCC supercell derived from the L1₂-AuCu₃ prototype, $n = 108$. Since the coordinates of one atom are constrained at the origin, the number of displaceable atoms corresponds to $n-1$. The position vectors $(x_{i,disto.}, y_{i,disto.}, z_{i,disto.})$ and $(x_{i,undisto.}, y_{i,undisto.}, z_{i,undisto.})$ represent atomic coordinates of atom i in the undistorted and distorted configurations, respectively. The parameter d_o denotes the 1NN distance in the volume relaxing reference structure. Thus, lattice distortion parameters are computed quantitatively from the simulation outputs using these definitions. The resulting distortion metrics are presented in Table 5. Upon completion of full structural relaxation, the crystal structure is optimized to its equilibrium state, resulting in a volume change and a reduction in the total energy of the system. As for the fundamental lattice parameters, the changes in lattice constants and angles are found to be minimal even after full relaxation. Therefore, it can be concluded that the FCC_CoCuNi MPEAs essentially retains its simple cubic structure.

Table 4. The calculated crystal lattice structure data of FCC_CoCuNi MPEAs based on 3×3×3 supercell of L1₂-AuCu₃ prototype.

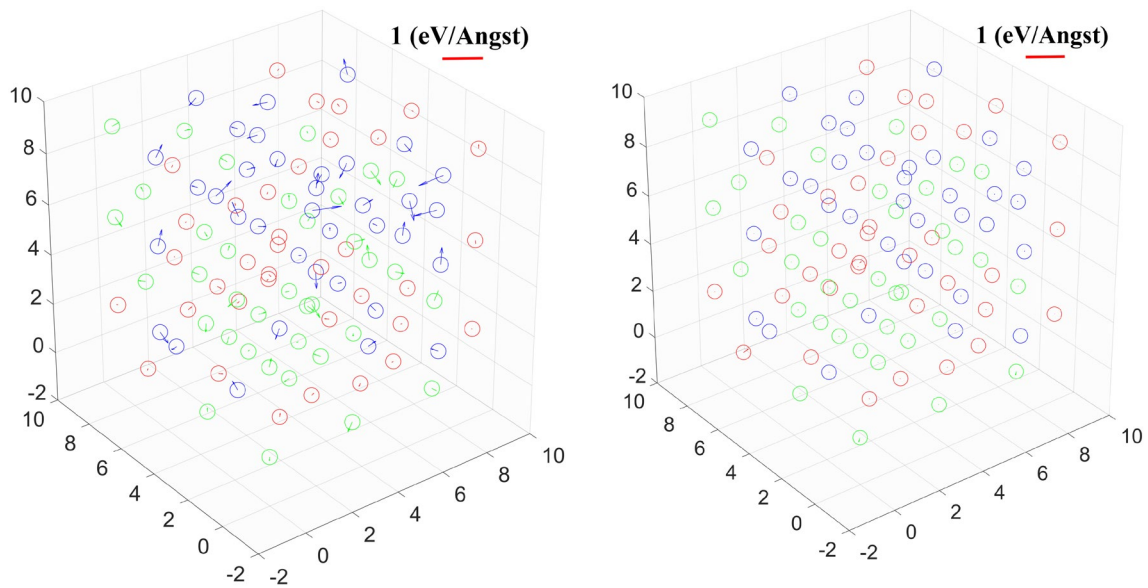
Temperature (K)	Relaxing mode	a (Å)	b (Å)	c (Å)	α (°)	β (°)	γ (°)	V (Å ³)	E _{tot} (eV/atom)	Magmom (uB)
100	Only volume relaxin	10.66	10.66	10.66	90.00	90.00	90.00	1213.11	-5.396	80.132
	Full relaxin	10.67	10.68	10.67	90.00	89.99	89.99	1217.54	-5.403	79.991
900	Only volume relaxin	10.66	10.66	10.66	90.00	90.00	90.00	1213.24	-5.387	80.347
	Full relaxin	10.67	10.68	10.67	89.96	89.94	89.97	1217.85	-5.396	80.352
1400	Only volume relaxin	10.66	10.66	10.66	90.00	90.00	90.00	1211.95	-5.387	80.473
	Full relaxin	10.67	10.67	10.67	90.01	90.00	89.99	1217.01	-5.395	80.453

Table 5. The calculated lattice distortion data of FCC_CoCuNi MPEAs based on 3×3×3 supercell of L1₂-AuCu prototype.

Temperature (K)	Average lattice constant (Å)	d_0 (Å) (Volume relaxing)	d_0 (Å) (Full relaxing)	Absolute lattice distortion per atom (Å)	Relative lattice distortion per atom (%)	Distortion energy (eV)	Unit atomic distortion energy (eV/atom)
100	3.559	2.510	2.507	0.038	1.50%	0.741	0.007
900	3.560	2.510	2.507	0.042	1.67%	0.852	0.008
1400	3.559	2.510	2.507	0.040	1.58%	0.889	0.008

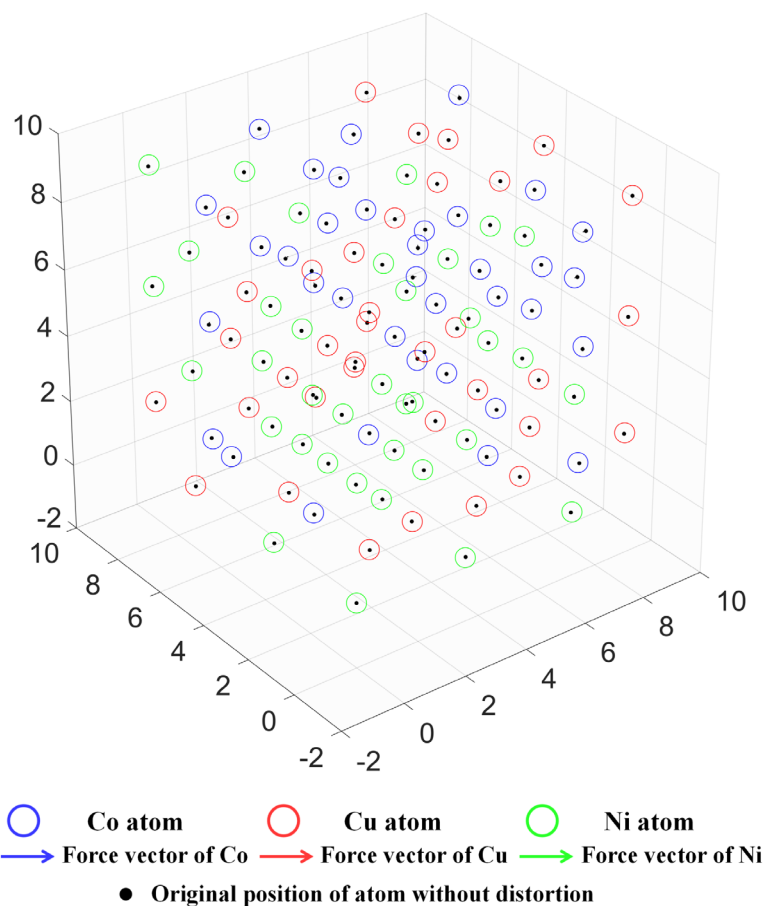
To gain deeper insights into the micromechanical origin of lattice distortion, this study visually characterized the atomic resultant forces and distorted displacements of individual atoms in FCC_CoCuNi MPEAs before and after structural relaxation, as illustrated in Figure 12. In the unrelaxed initial configuration (R7) where atomic positions are constrained by the lattice, mere volume expansion is insufficient to eliminate the atomic-scale stress inhomogeneity induced by variations in the local chemical environment. Under these conditions, Co and Ni atoms experience significant forces due to the atomic size mismatch effect, with the resultant force acting on each atom denoted by arrows (Figure 12a). After full relaxation (R7 + R3), it reaches an equilibrium state with the minimum energy, where the degrees of freedom of atomic positions are fully released. Except for the atoms fixed by the selective dynamics method, which still sustain a small residual force, the forces acting on most atoms are nearly eliminated (Figure 12b), confirming that the optimization calculations meet the required standards. Notably, the lattice distortion of FCC_CoCuNi MPEAs is not significant in terms of the lattice parameters in Table 5. For the force acting on atom, specifically, Co atoms experience the largest force, followed by Ni atoms, while Cu atoms bear the weakest force. Meanwhile, the ranking of atomic distortion displacement is consistent with the above force distribution results. To characterize the slight atomic distortion displacement, hollow spheres with different colors are used to represent the atomic positions after lattice distorting whereas the solid black dots denote their initial positions before lattice distortion. At this stage, the geometric centers of individual atoms have displaced from their initial positions, indicating the presence of significant atomic distorted displacements (Figure 12c). The rearrangement of atomic positions by adjusting local bond lengths and bond angles effectively alleviates the non-equilibrium stress field in the initial configuration, leading to a systematic reduction in the net forces acting on all atoms.

In summary, lattice distortion in MPEAs is inevitable due to the non-equilibrium force fields experienced by the different types of constituent atoms, which is reflected in nature, that is, the total energy difference before and after distortion. However, these local atomic-scale strain fluctuations due to the sublattice preference of the different constituent atoms are one of the key factors governing the properties of MPEA. Therefore, quantitative and graphical studies on lattice distortion are crucial for clarifying its underlying mechanisms. Furthermore, based on the relaxed bulk structure, representative surface structural models of FCC crystals are cleaved. All constructed surface models are three-atomic-layer configuration with their stacking sequences explicitly labeled in the corresponding figures (see Figure 13), which can be adopted to simulate the surface phenomenon in diverse application with considerable reliability. Notably, two distinct stacking sequence models are established for the {0 0 1} and {1 1 0} surfaces, respectively. Three stacking sequence models are established for the {1 1 1} close-packed surface. The three-atomic-layer structure effectively balance electronic structure calculation precision with computational efficiency, and mitigates interference from bulk-phase atoms. These models are indispensable for the subsequent simulations of surface oxidation, nitridation, and catalytic behaviors.



(a) Resultant force acting on each atom of FCC_CoCuNi MPEAs without lattice distortion (R7) at 900 K

(b) Resultant force acting on each atom of FCC_CoCuNi MPEAs with lattice distortion (R7 + R3) at 900 K



(c) Distorted displacements of FCC_CoCuNi MPEAs with lattice distortion (R7 + R3) at 900 K

Figure 12. Atomic resultant forces and distorted displacements of FCC_CoCuNi MPEAs with and without lattice distortion based on the SOFs at 900 K (a) resultant force acting on each atom without lattice distortion (R7); (b) resultant force acting on each atom with lattice distortion (R7 + R3); and (c) distorted displacements with lattice distortion (R7 + R3).

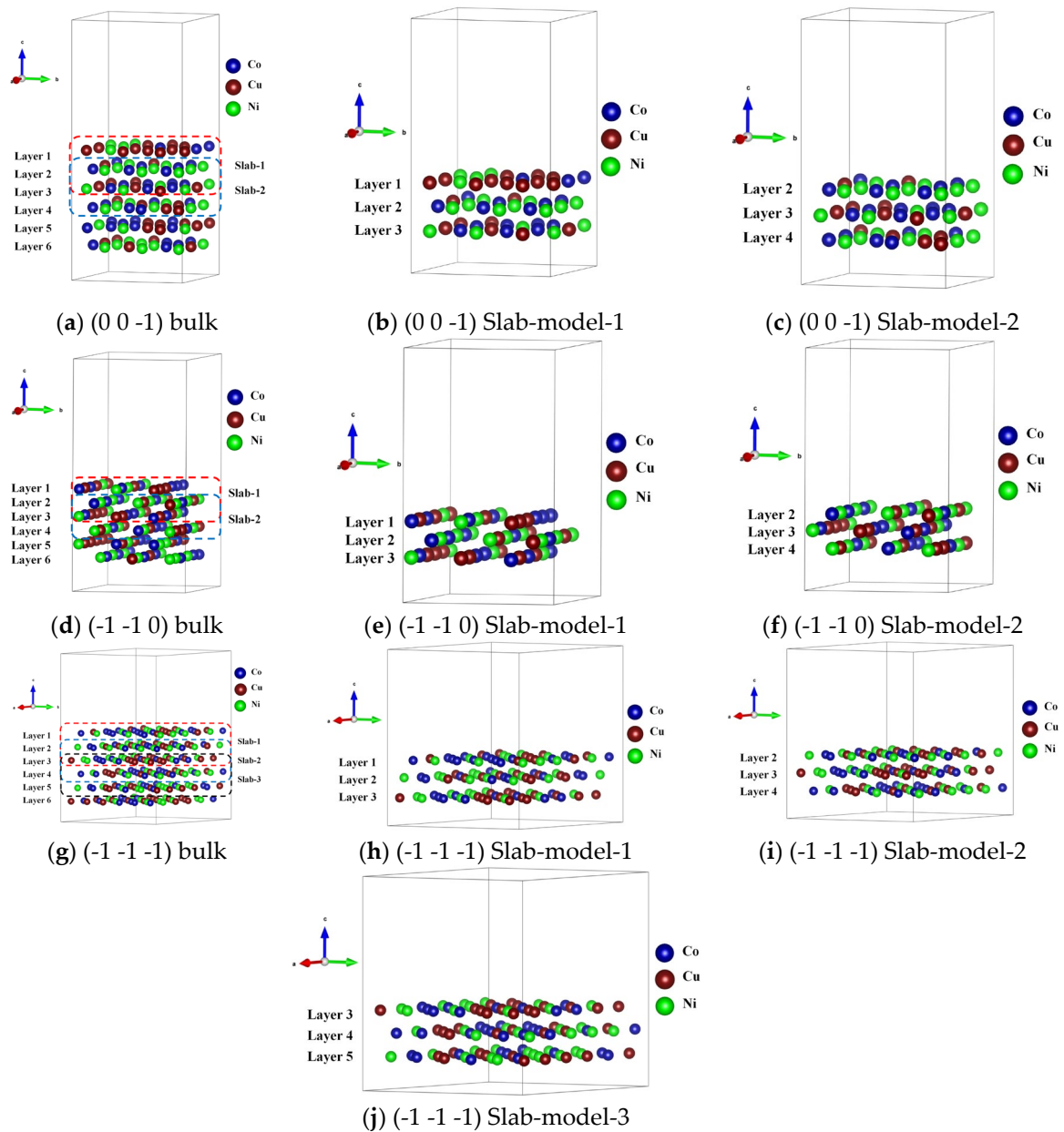


Figure 13. Distinct stacking sequence models of the representative surface in FCC_CoCuNi MPEAs at 900 K. (a-c) (0 0 -1) bulk structure, Slab-model-1 and 2; (d-f) (-1 -1 0) bulk structure, Slab-model-1 and 2; (g-j) (-1 -1 -1) bulk structure, Slab-model-1, 2, and 3.

4. Conclusions

The atom distributing configuration and lattice distortion behaviors of FCC_CoCuNi MPEAs are theoretically investigated based on the inherent sublattice preference of the different constituent atoms on different constituent sublattices. The sublattice preference are significantly affected by heat treatment temperatures. The sublattice preferences change continuously with the increase of the heat treatment temperature. The SOFs configurations are $(\text{Ni}_{1.0000})_{1a}(\text{Co}_{0.4445}\text{Cu}_{0.4444}\text{Ni}_{0.1111})_{3c}$, $(\text{Co}_{0.0653}\text{Cu}_{0.0721}\text{Ni}_{0.8626})_{1a}(\text{Co}_{0.4227}\text{Cu}_{0.4204}\text{Ni}_{0.1569})_{3c}$, and $(\text{Co}_{0.1574}\text{Cu}_{0.1593}\text{Ni}_{0.6833})_{1a}(\text{Co}_{0.3920}\text{Cu}_{0.3913}\text{Ni}_{0.2167})_{3c}$ at 100 K, 900 K, and 1400 K, respectively. Thus, Ni predominantly occupies the 1a sublattice across the entire temperature range, while the 3c sublattice is mainly occupied by Co and Cu atoms, Increasing temperature, Ni tends to migrate to the 3c sublattice a little bit, and the occupation proportions of Co and Cu on the 1a sublattice increase synchronously.

The configurational entropy of FCC_CoCuNi MPEA increases with the increase of heat treatment temperature, while it is considerably lower than that of the hypothetical structure with

randomly mixing solid solution. For example, the configurational entropies are 6.017, 7.383, and 8.399 J/(mol·K) at 100 K, 900 K, and 1400 K, respectively, while it is 9.114 J/(mol·K) in randomly mixing case.

Coordination environment analysis indicates that in the ordered structure based on SOFs, the maximum coordinating number n is 9 for Co^*-nCo , Cu^*-nCu , and Ni^*-nNi , respectively. In contrast, randomly mixing models overestimate both the maximum cluster group number and the number of coordination pairs. Lattice distorting behaviors of the MPEAs subjected to heat treatment to the equilibrium state at 100 K, 900 K, or 1400 K and then quench to the ground state (0 K) are compared quantitatively and graphically. For instance, for the sample is heat treated at 900 K and then quenched to 0 K, the average atomic distorting energy is 0.008 eV/atom and the relative lattice distortion relative to the first nearest neighbor distance is 1.67%, and The corresponding changes of driving force field on atom are visualized.

Based on the relaxed bulk structure, some representative surface structural models are cleaved, which are indispensable structure models employed for further simulation on the surface oxidation, nitridation and catalyst behaviors. In particular, we emphasize that for most family of crystal planes of FCC_MPEAs, except {1 1 1}, there are obviously different atom distributing characters between the even and odd layers. Thus, it is necessary to model at least one even layer and one odd layer, and then assess the surface properties of the even and odd layers of MPEAs combinatorially to obtain the comprehensive surface properties of the corresponding MPEAs.

Current work intensively explores the temperature-dependent fine microstructure based on the inherent sublattice preference of constituent atoms on the different types of sublattice. Essential structure data and model are afforded for investigate and modulate the fine microstructure and diverse properties in the future.

Supplementary Materials: The following supporting information can be downloaded at: Preprints.org.

Author Contributions: Conceptualization, B. W., M. W. and F.-X. Z.; validation, Y. T., C.-S.F., F.-X. Z. and L.-M. C.; investigation, X.-Y. S., X.-L. Z., X. F., A.-Q. J., X.-Q. Z., H.-H. Q., H.-R. H., J.-K. C., H. G., X.-L. Y., C. D., and Y. S.; data curation, X.-Y. S., M.-L. G. and X.-Y. C.; writing—original draft preparation, X.-Y. S., X.-L. Z., A.-Q. J., and X.-Q. Z.; writing—review and editing, B. W., B.-S. S., J.-K. H., M. W. and F.-X. Z.; visualization, M.-L. G. and D.-H. W.; supervision, B. W., M. W. and F.-X. Z. All authors have read and agreed to the published version of the manuscript.

Funding: This research was funded by the National Natural Science Foundation of China (50971043, 51171046), Key Research and Development Program of China (CISRI-21T62450ZD), Natural Science Foundation of Fujian Province (2021J01590), Student Research and Training Program (SRTP) of Fuzhou University (31234), and the Zunyi Normal University Research Project (ZunShi BS [2025]03).

Data Availability Statement: Data is contained within the article or Supplementary Material.

Conflicts of Interest: The authors declare no conflicts of interest.

References

1. Miracle, D.B.; Senkov, O.N. A critical review of high entropy alloys and related concepts. *Acta Materialia* 2017, 122, 448-511, doi:10.1016/j.actamat.2016.08.081.
2. Ali, N.; Zhang, L.; Liu, D.; et al. Strengthening mechanisms in high entropy alloys: A review. *Mater Today Commun* 2022, 33, 104686, doi:10.1016/j.mtcomm.2022.104686.
3. Fu, Y.; Liu, P.; Zhang, H.; Ding, X.; Sun, J. Accelerated design of high-strength refractory multi-principal element alloys from first-principles calculations. *Journal of Materials Research and Technology* 2025, 36, 10520-10534, doi:10.1016/j.jmrt.2025.05.259.
4. Zhang, H.; Cai, D.; Sun, X.; et al. Solid solution strengthening of high-entropy alloys from first-principles study. *Journal of Materials Science & Technology* 2022, 121, 105-116, doi:10.1016/j.jmst.2021.11.076.

5. Wang, M.M.; Liu, L.J.; Wen, J.T.; et al. Multimetallic CuCoNi Oxide Nanowires In Situ Grown on a Nickel Foam Substrate Catalyze Persulfate Activation via Mediating Electron Transfer. *Environ Sci Technol* 2022, 56, 12613-12624, doi:10.1021/acs.est.2c04312.
6. Murakami, Y.; Murase, K.; Fukami, K. Smooth Thin Film of a CoNiCu Medium-Entropy Alloy Consisting of Single Nanometer-Sized Grains Formed by Electrodeposition in a Water-in-Oil Emulsion. *The Journal of Physical Chemistry C* 2023, 127, 4696-4703, doi:10.1021/acs.jpcc.2c08033.
7. Söğüt, Ö.; Dönük, Ç.; Apaydın, G.; Bakkaloğlu, Ö.F. Examination of CoNiCu thin films by using XRF and XRD. *Canadian Journal of Physics* 2014, 92, 435-439, doi:10.1139/cjp-2012-0538.
8. Katiyar, N.K.; Biswas, K.; Yeh, J.W.; Sharma, S.; Tiwary, C.S. A perspective on the catalysis using the high entropy alloys. *Nano Energy* 2021, 88, 106261, doi:10.1016/j.nanoen.2021.106261.
9. Chu, F.; Wang, J.; He, J.; et al. Rare-Earth-Induced Charge Polarization in Medium-Entropy Alloy Driving Fast Hydrogen Generation. *Advanced Functional Materials* 2025, e15235, doi:10.1002/adfm.202515235.
10. Ma, J.; Lu, B.; Wang, S.; et al. MOF-derived CuCoNi trimetallic hybrids as efficient oxygen evolution reaction electrocatalysts. *New Journal of Chemistry* 2020, 44, 2459-2464, doi:10.1039/C9NJ05562B.
11. Maeda, A.; Tanuma, T.; Kume, M.; Shimizu, R.; Doi, A. GMR in corrugated Co/Cu multilayers. *IEEE Transactions on Magnetics* 1997, 33, 3535-3537, doi:10.1109/20.619489.
12. Duch, M.; Esteve, J.; Gómez, E.; Pérez-Castillejos, R.; Vallés, E. Electrodeposited Co-Ni alloys for MEMS. *Journal of Micromechanics and Microengineering* 2002, 12, 400-405, doi:10.1088/0960-1317/12/4/309.
13. Karahan, I.; Bakkaloğlu, Ö.; Bedir, M. Giant magnetoresistance of electrodeposited Cu-Co-Ni alloy films. *Pramana* 2007, 68, 83-90, doi:10.1007/s12043-007-0009-5
14. Pané, S.; Gómez, E.; Vallés, E. Magnetoresistive granular Cu-Co-Ni coatings prepared by electrodeposition. *Journal of Electroanalytical Chemistry* 2006, 596, 87-94, doi:doi.org/10.1016/j.jelechem.2006.07.009.
15. Yu, Z. Giant magneto resistance for CuCoNi granular films prepared by electrode position. In *Proceedings of the IOP Conference Series: Materials Science and Engineering*, 2019; p. 042091.
16. Karpuz, A.; Kockar, H.; Alper, M. Microstructure dependence of magnetic properties on electrochemically produced ternary CuCoNi alloys. *Journal of Materials Science: Materials in Electronics* 2014, 25, 4483-4488, doi:10.1007/s10854-014-2191-9.
17. Mondal, B.N.; Basumallick, A.; Chattopadhyay, P.P. Correlation of microstructure and magnetic properties in Cu-Co-Ni alloys. *Materials Science and Engineering: B* 2010, 166, 174-179, doi:10.1016/j.mseb.2009.11.003.
18. Gómez, E.; Pané, S.; Vallés, E. Electrodeposition of Co-Ni and Co-Ni-Cu systems in sulphate-citrate medium. *Electrochimica Acta* 2005, 51, 146-153, doi:10.1016/j.electacta.2005.04.010.
19. Saha, S.; Ramanujachary, K.V.; Lofland, S.E.; Ganguli, A.K. Cu-Co-Ni alloys: an efficient and durable electrocatalyst in acidic media. *Materials Research Express* 2016, 3, 016501, doi:10.1088/2053-1591/3/1/016501.
20. Ding, J. Order or disorder, that is the question in high-entropy alloys. *Nature Reviews Materials* 2026, 1-2, doi:10.1038/s41578-025-00887-y
21. Zhang, C.-h.; Lin, M.-h.; Wu, B.; et al. Explore the possibility of forming fcc high entropy alloys in equal-atomic systems CoFeMnNiM and CoFeMnNiSmM. *Journal of Shanghai Jiaotong University (Science)* 2011, 16, 173-179, doi:10.1007/s12204-011-1113-8.
22. Wu, B.; Zhao, Y.; Ali, H.; et al. A reasonable approach to describe the atom distributions and configurational entropy in high entropy alloys based on site preference. *Intermetallics* 2022, 144, 107489, doi:10.1016/j.intermet.2022.107489.
23. Ali, H.; Chen, R.; Wu, B.; et al. The site preference and doping effect on mechanical properties of Ni₃Al-based γ' phase in superalloys by combing first-principles calculations and thermodynamic model. *Arabian Journal of Chemistry* 2022, 15, doi:10.1016/j.arabjc.2022.104278.
24. Chen, R.; Weng, L.; Zhang, C.; et al. The influence of site preference on the elastic properties of FCC_CoCrFeNi multi-principal element alloy. *Journal of Alloys and Compounds* 2023, 965, 171426, doi:10.1016/j.jallcom.2023.171426.
25. Chen, R.; Xie, T.; Wu, B.; et al. A general approach to simulate the atom distribution, lattice distortion, and mechanical properties of multi-principal element alloys based on site preference: Using FCC_CoNiV and

- CoCrNi to demonstrate and compare. *Journal of Alloys and Compounds* 2023, 935, 168016, doi:10.1016/j.jallcom.2022.168016.
26. Zhang, C.-b.; Qian, C.; Ye, Z.-a.; et al. Influence of ordering behaviors on thermodynamic and mechanical properties of FCC_CoNiV multi-principal element alloys. *Transactions of Nonferrous Metals Society of China* 2025, 35, 2320-2331, doi:10.1016/s1003-6326(25)66817-8.
 27. Qiao, Y.; Chen, X.; Wu, B.; et al. A general approach to qualitatively and graphically characterize the diffuse behavior of interstitial nonmetallic atoms in multi-principal element alloys based on site preference. *Materials Genome Engineering Advances* 2025, 3, doi:10.1002/mgea.70021.
 28. Weng, L.; Su, L.; Xu, N.; et al. The preferred adsorption sites and catalytic mechanism of FCC_CoFeGaNiZn multi-principal element alloy for oxygen evolution reaction catalysis based on site preference of constituent atom on sublattice. *Intermetallics* 2024, 165, doi:10.1016/j.intermet.2023.108132.
 29. Weng, L.; Zhang, X.; Su, L.; et al. Prediction of the catalytic mechanism of hydrogen evolution reaction enhanced by surface oxidation on FCC_CoCrFeNi and $\text{Co}_{0.35}\text{Cr}_{0.15}\text{Fe}_{0.2}\text{Mo}_{0.1}\text{Ni}_{0.2}$ multi-principal element alloys based on site preference. *Applied Surface Science* 2024, 672, doi:10.1016/j.apsusc.2024.160730.
 30. Su, L.; Que, H.; Qian, C.; et al. Prediction of oxygen evolution reaction activity of FCC_CoCuFeNiPd and CoCuFeNiRu multi-principal element alloys based on sublattice preference of constituent atoms and the site preference of intermediates. *Physical Chemistry Chemical Physics* 2025, 27, 22064-22081, doi:10.1039/d5cp02461g.
 31. Qian, C.; Chen, X.; Su, L.; et al. The influence of N content on structures and mechanical properties of FCC_(AlCrMoTiV)_{1-x}N_x high-entropy nitrides: A density functional theory (DFT) study based on site preference. *Computational Materials Science* 2025, 251, doi:10.1016/j.commatsci.2025.113787.
 32. Wu, B.; Zinkevich, M.; Aldinger, F.; Chu, M.; Shen, J. Prediction of the ordering behaviours of the orthorhombic phase based on Ti₂AlNb alloys by combining thermodynamic model with ab initio calculation. *Intermetallics* 2008, 16, 42-51, doi:10.1016/j.intermet.2007.07.007.
 33. Zheng, Y.; Wu, B.; Zhang, C.; Dai, P. Prediction of the site occupations of the ThMn₁₂-type intermetallics YFe_{12-x}Mo_x by combining thermodynamic model with ab-initio calculations. *Intermetallics* 2010, doi:10.1016/j.intermet.2010.03.036.
 34. Andersson, J.O.; Helander, T.; Höglund, L.; Shi, P.; Sundman, B. Thermo-Calc & DICTRA, computational tools for materials science. *Calphad* 2002, 26, 273-312, doi:10.1016/s0364-5916(02)00037-8.
 35. Kresse, G.; Furthmüller, J. Efficient iterative schemes for ab initio total-energy calculations using a plane-wave basis set. *Phys Rev B Condens Matter* 1996, 54, 11169-11186, doi:10.1103/physrevb.54.11169.
 36. Kratzer, P.; Neugebauer, J. *The Basics of Electronic Structure Theory for Periodic Systems*. *Front Chem* 2019, 7, 106, doi:10.3389/fchem.2019.00106.
 37. Han, Y.; Chen, H.; Sun, Y.; et al. Ubiquitous short-range order in multi-principal element alloys. *Nat Commun* 2024, 15, 6486, doi:10.1038/s41467-024-49606-1.

Disclaimer/Publisher's Note: The statements, opinions and data contained in all publications are solely those of the individual author(s) and contributor(s) and not of MDPI and/or the editor(s). MDPI and/or the editor(s) disclaim responsibility for any injury to people or property resulting from any ideas, methods, instructions or products referred to in the content.