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## Article

# Processing of Bulk Hemp Seeds by Estimating the Optimum Input and Output Parameters and the Description of the Theoretical Deformation Energy Under Uniaxial Compression Loading

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## Abstract

This present study adopted the Box-Behnken Design (BBD) with Response Surface Methodology (RSM) to identify the optimum input processing factors (heating temperature: 40, 50 and 60 °C, heating time: 30, 45 and 60 min and pressing height: 60, 80 and 100 mm) for estimating the oil output parameters (mass of oil, oil yield and oil expression efficiency) and deformation energy. The mechanical properties examined were the hardness and secant modulus of elasticity. Based on the full quadratic model, which includes both significant and non-significant terms, the optimal input processing factors were determined to be a heating temperature of 60 °C, a heating time of 52.5 min, and a sample pressing height of 100 mm, with coefficient of determination ( $R^2$ ) values ranging from 0.68 to 0.95. The linear models with the significant terms predicted the mass of oil of 33.36 g, oil yield of 21.5 %, oil expression efficiency of 65.47 % and the experimental deformation energy of 1080.82 J. The percentage error values between the experimental and theoretical deformation energies were from 1.35 to 28.31%, suggesting that the varying input processing factors affected the coefficients of the tangent curve model for fitting the experimental force-deformation curves. The hardness and secant modulus of elasticity values ranged between 3.65 and 7.09 kN/mm and 123.98 to 150.39 MPa, indicating that the varying input processing factors had a significant effect on the stiffness of the bulk hemp seeds. These findings are useful for modelling and optimising the mechanical behaviour of oilseeds using a mechanical screw press to enhance oil recovery efficiency.

**Keywords:** compression process; Box-Behnken design; response surface regression; mechanical properties; mathematical models

## 1. Introduction

Hemp or industrial hemp (*Cannabis sativa* L.) is a multipurpose plant grown for many applications, including biofuel production [1–3]. It is a species in the Cannabaceae family in which the level of tetrahydrocannabinol (THC) is very low, according to the provisions under the Common Agricultural Policy (CAP) [4,5]. In the EU, the THC content is not allowed to exceed 0.3% of dry matter [4]. Hemp has been cultivated for millennia, dating back to approximately 10,000 years [6–9]. The hemp plant has grown across Europe for centuries mainly for textiles, ropes and other industrial applications, with a significant increase in cultivation from 20,540 ha in 2015 to 33,020 ha in 2022. In the same period, the production of hemp increased from 97,130 tonnes to 179,020 tonnes. France is the largest producer, accounting for more than 60% of EU production, followed by Germany (17%) and the Netherlands (5%) [4,5,10]. The global industrial hemp market size was estimated at USD 5.49 billion in 2023 and is projected to reach USD 16.82 billion by 2030, growing at a CAGR (Compound Annual Growth Rate) of 17.5% from 2024 to 2030 [11]. The growth is driven by the rising product

demand from application industries such as food and beverages, personal and animal care, across the globe. The top five hemp-producing countries in the world are China, Canada, the United States, France and Chile [12]. Hemp cultivation is beneficial for the environment and biodiversity due to its short cropping period, high resistance to harmful organisms, less water requirement compared to other fibre plants, and it can be grown in a wide range of weather and geographical conditions [13–15].

Hemp seeds, an edible hemp product, are notable for their oil (25–35%), protein (20–25%), carbohydrates (25–30%), insoluble fibre (10–15%) and an average phytate content of 2.80 g/100 g, which are of vital nutritional and bioactive importance [13,16]. Dehulled hemp seeds can contain up to 50% oil, with polyunsaturated fatty acids making up 80% of their total fatty acid content [13,17,18]. Hemp seeds are rich in polyunsaturated fatty acids, including omega-6 fatty acids, such as linoleic acid (18:2), and omega-3 fatty acids, particularly  $\alpha$ -linolenic acid (18:3) [16]. In addition, hemp seeds are known to support overall health and exhibit anti-inflammatory properties. Omega-3 and omega-6 fatty acids offer protection against heart disease, alleviate inflammation in joints, aid in treating dermatitis, and contribute to maintaining skin moisture and balance [16,19].

The oil extraction process can be performed at room temperature (cold pressing) and increased temperature (hot pressing); the latter provides higher oil yield, but oil properties can be hindered at elevated temperatures [20]. Currently, both conventional and advanced technologies are used for oil extraction [21,22]. Conventional extraction methods such as screw press, Soxhlet extraction and hydro distillation have been used for extended periods. However, these methods are cost-effective in terms of machinery requirements, time-consuming extraction process, high energy requirement, greenhouse gas (GHG) emissions, considerable residual oil in oil press cakes and inferior oil quality [21,23,24]. Advanced methods, including enzyme-assisted, pulsed electric field pretreatment; microwave-assisted extraction, microwave-assisted hydro distillation, supercritical fluid extraction, ultrasound-assisted hydro distillation and sonication-assisted hydro distillation, are preferred to the conventional methods due to the lower requirement of the organic solvent, short extraction time, higher percentage oil recovery and retention of heat-sensitive compound quality of extract [21,25–31]. Particularly, to extract oil from hemp seeds, the screw press extraction, Soxhlet extraction, microwave-assisted solvent extraction and supercritical CO<sub>2</sub> have been utilised [16,32–36].

Another promising oil extraction technique is the uniaxial compression process [37], which has been utilized for extracting oil under cold and hot-pressing conditions from oil-bearing plant seeds/kernels such as flax, hemp, rape, pumpkin, hazelnut, sunflower and jatropha [38–43]. To understand the mechanical properties, oil recovery efficiency and deformation energy requirement of the oilseeds/nuts based on their experimental and theoretical force-deformation curves in relation to the varying input processing factors such as compressive force, speed, heating temperature, heating time, diameter of pressing vessel, samples pressing height and moisture content, it is ideal to use the uniaxial compression process. This process has not been adequately explored for hemp seeds coupled with optimization statistical techniques. The statistical optimization technique using response surface methodology combined with an experimental design such as Box-Behnken has been recently employed by several researchers to optimize the input processing factors and their corresponding output parameters [20,25,44–52]. Therefore, the objectives of the present study were to determine: the oil recovery efficiency, the mechanical properties, the theoretical deformation energy and the optimum input processing factors (heating temperature, heating time and pressing height) with their corresponding output parameters (mass of oil, oil yield, oil expression efficiency and experimental deformation energy) of bulk hemp seeds under uniaxial compression loading.

2. Materials and Methods

2.1. Sample

Samples of bulk hemp seeds were used for the study. The samples were purchased from Vitalcountry.cz, Plzenská, Štěnovice, Czech Republic. The samples packaged in transparent plastic bags were kept under laboratory conditions before the experiments.

2.2. Determination of Moisture Content

The moisture content of the samples was determined using Eq. (1) [45,53].

$$MC = \left( \frac{m_b - m_a}{m_b} \right) \cdot 100 \tag{1}$$

where *MC* is the moisture content of samples (% w.b.), *m<sub>a</sub>* and *m<sub>b</sub>* are the masses of the samples before and after oven drying (g) for 17 h at 105 °C [54].

2.3. Determination of Oil Content

The oil content of the samples was determined using Eq. (2) following the Soxhlet extraction procedure with the use of petroleum ether [41,55–57].

$$OC = \left( \frac{m_o}{m_b} \right) \cdot 100 \tag{2}$$

where *m<sub>o</sub>* is the mass of oil extracted (g) and *m<sub>b</sub>* is the initial mass of the ground sample.

2.4. Box-Behnken Experimental Design

The input processing factors (heating temperature, heating time and pressing height) at three levels each were designed using STATISTICA 13 software [58] by employing the Box-Behnken experimental design (BBD) [59]. The heating temperature values were 40, 50 and 60 °C, the heating time values were 30, 45 and 60 min, and the pressing height values were 60, 80 and 100 mm. The overall design generated 17 experimental runs (Table 1) comprising twelve combinations of factors and five replications at the centre points using Eq. (3) [44,48,51].

Table 1. Box-Behnken experimental design with twelve combinations and five replications.

Run	Input processing factors			Coded values using Eq. (2)		
	<i>H<sub>TP</sub></i> (°C)	<i>H<sub>TM</sub></i> (min)	<i>P<sub>HT</sub></i> (mm)	<i>H<sub>TP</sub></i> (°C)	<i>H<sub>TM</sub></i> (min)	<i>P<sub>HT</sub></i> (mm)
1	40	30	80	−1	−1	0
2	60	30	80	1	−1	0
3	40	60	80	−1	1	0
4	60	60	80	1	1	0
5	40	45	60	−1	0	−1
6	60	45	60	1	0	−1
7	40	45	100	−1	0	1
8	60	45	100	1	0	1
9	50	30	60	0	−1	−1
10	50	60	60	0	1	−1
11	50	30	100	0	−1	1
12	50	60	100	0	1	1
13*	50	45	80	0	0	0
14*	50	45	80	0	0	0



15*	50	45	80	0	0	0
16*	50	45	80	0	0	0
17*	50	45	80	0	0	0

\* Repetitions at the centre points of factor levels;  $H_{TP}$ : Heating temperature;  $H_{TM}$ : Heating time and  $P_{HT}$ : Initial pressing height of the sample.

$$N = 2k \times (k - 1) + C_0 \rightarrow 2 \times 3(3 - 1) + 5 = 17$$

(3)

where  $k$  is the number of input factors and  $C_0$  is the number of central points. The factors-levels stated above were coded from  $-1$  (low value) to  $+1$  (high value) with  $0$  being the centre value according to Eq. (4) [51,59,60].

$$x_i = \frac{X_i - X_0}{\Delta X}$$

(4)

where  $x_i$  is the coded value of the  $i^{th}$  variable,  $X_i$  is the uncoded value of the  $i^{th}$  test variable,  $X_0$  is the uncoded value of the  $i^{th}$  test variable at the centre point, and  $\Delta X$  is the step change in the real value of the variable  $i$  corresponding to the variation in a unit for the dimensionless value of the variable  $i$ . The polynomial regression model of a second order, defining the responses as a function of the input processing factors, is expressed in Eq. (5).

$$Y = \beta_0 + \sum_{i=1}^k \beta_i X_i + \sum_{i=1}^k \beta_{ii} X_i^2 + \sum_{i_1 < j}^k \sum_j^k \beta_{ij} X_i X_j$$

(5)

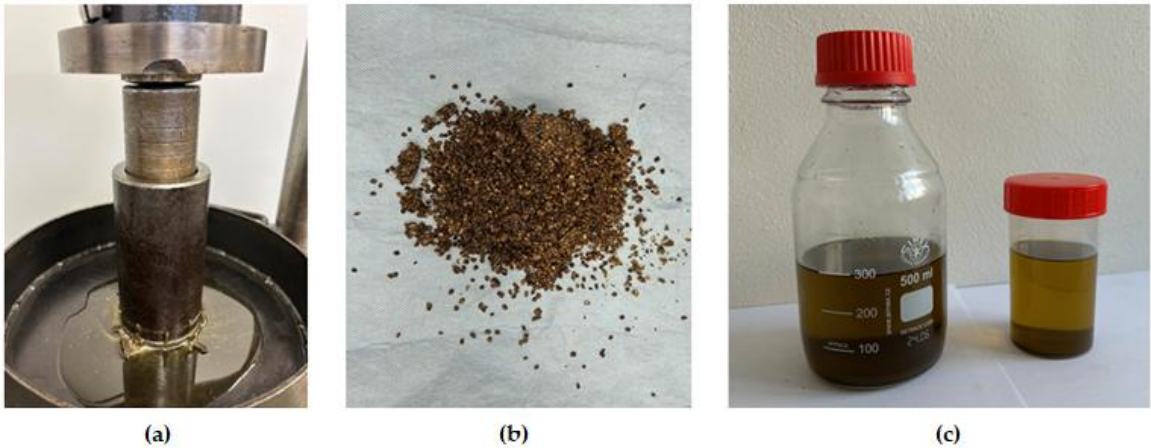
where  $Y$  is the response variable;  $\beta_0, \beta_i, \beta_{ii}$  and  $\beta_{ij}$  are the regression coefficients of the intercept, linear, quadratic and interaction terms, respectively;  $X_i$  and  $X_j$  are the independent variables, and  $k$  is the number of factors.

2.5. Pretreatment of Samples Using Standard Oven

The samples of hemp seeds were preheated following the design presented in Table 1 using the standard oven equipment (MEMMERT GmbH + Co. KG, Buechenbach, Germany). The fan and the restrictor air flap in the oven were set at 30% to control the air circulation during the drying process.

2.6. Compression Tests of Samples After Pretreatment

The universal compression testing machine (ZDM 50, Czech Republic) of a maximum load of 500 kN and a pressing vessel of diameter 60 mm with a plunger were used for extracting the hemp seed oil (Figure 1a–c) following the Box-Behnken design (Table 1). Based on preliminary tests, the maximum input force required for hemp seeds was set at 300 kN at a pressing speed of 5 mm/min.



**Figure 1.** (a) Uniaxial compression test for extracting the oil, (b) seedcake of bulk hempseeds sample, (c) extracted oils from the 17 experimental tests/runs conducted.

### 2.6.1. Oil Yield

The oil yield was determined using Eq. (6) [25,59,61].

$$O_{YD} = \left[ \left( \frac{M_{OL}}{M_{SP}} \right) \cdot 100 \right] \quad (6)$$

where  $O_{YD}$  is oil yield (%),  $M_{OL}$  is the mass of oil determined as the difference between the mass of the seedcake and the initial mass of the sample  $M_{SP}$  (g).

### 2.6.2. Oil Expression Efficiency

The oil expression efficiency was determined using Eq. (7) [62].

$$O_{EF} = \left[ \left( \frac{O_{YD}}{O_{CT}} \right) \cdot 100 \right] \quad (7)$$

where  $O_{EF}$  is the oil expression efficiency (%) and  $O_{CT}$  is the percentage oil content (%) in the hemp seeds sample determined by Soxhlet extraction.

### 2.6.3. Deformation Energy

The deformation energy was determined using Eq. (8) [63–65].

$$E_{NG} = \sum_{n=0}^{n=i-1} \left[ \left( \frac{F_{n+1} + F_n}{2} \right) \cdot (x_{n+1} - x_n) \right] \quad (8)$$

where  $E_{NG}$  is the deformation energy (J),  $F_{n+1} + F_n$  and  $x_{n+1} - x_n$  are the compressive force (kN) and deformation (mm),  $n$  is the number of data points, and  $i$  is the number of sections in which the axis deformation was divided.

### 2.6.4. Force and Deformation

The force,  $F_R$  (N) and deformation  $D_F$  (mm) values were obtained directly from the compression tests' output data.

### 2.6.5. Hardness

The hardness,  $H_{DN}$  (kN/mm) of the samples was calculated using Eq. (9) [53,66,67].

$$H_{DN} = \frac{F_{RC}}{D_{FX}} \quad (9)$$

### 2.6.6. Strain

The strain,  $\varepsilon_{ST}$  (-) of the samples was calculated using Eq. (10) [53,66,67].

$$\varepsilon_{ST} = \frac{D_{FX}}{H_{PT}} \quad (10)$$

### 2.6.7. Compressive Stress

The stress,  $\sigma_{SS}$  (MPa) of the samples was calculated using Eq. (11) [53,66,67].

$$\varepsilon_{ST} = \frac{F_{RC}}{A_{PV}} \quad (11)$$

where  $A_{PV}$  is the area of the pressing vessel, which was calculated to be 2827.43 mm<sup>2</sup>.

### 2.6.8. Secant Modulus of Elasticity

The secant modulus of elasticity,  $E_{SM}$  of the samples was calculated based on Hooke's law using Eq. (12) [53,66,67].

$$E_{SM} = \frac{\sigma_{SS}}{\varepsilon_{ST}} \quad (12)$$

where  $E_{SM}$  is the secant modulus of elasticity (N/mm<sup>2</sup> = MPa) and  $\varepsilon_{ST}$  is the strain (-).

### 2.7. Utilisation of Tangent Curve Model

The tangent curve model (Eq. 13) [43] was used to describe the experimental force-deformation curves and energy of bulk hempseeds as a function of the input processing factors.

$$F_D(X) = A_D \cdot [\tan(B_D \cdot X)]^n \quad (13)$$

where  $F_D(X)$  is the compression force (N) for the deformation of the bulk oilseeds,  $X$  (mm),  $A_D$  is the force coefficient of mechanical behaviour (N),  $B_D$  is the deformation coefficient of mechanical deformation behaviour (mm<sup>-1</sup>) and  $n$  is the model's fitting exponent (-).

### 2.8. Statistical Analysis

The experimental data obtained were evaluated statistically using STATISTICA 13 [58] by employing the response surface regression technique at a 0.05 significance level. The theoretical fitting of the experimental force-deformation curves and the statistical metrics were done using MathCAD 14 (PTC Software, Needham, MA, USA) [43,68]. The graphical illustrations were also done by the above-mentioned statistical packages.

## 3. Results and Discussion

### 3.1. Calculated Moisture Content and Oil Content

The moisture content and the oil content of the samples of hemp seeds were determined to be  $7.49 \pm 0.08$  (% w.b.) and  $32.84 \pm 0.70$  %, respectively. The determined moisture content is within the optimum levels reported in the literature for different oilseeds before oil extraction. However, both higher and lower moisture content levels could result in an increase or a decrease in the percentage oil yield [69]. For instance, Moslavac et al.[69] mentioned that the lowest moisture content of 5.52 % produced the highest oil yield of rapeseeds in comparison with sunflower seeds, where the highest amount of oil yield was achieved at seeds moisture content of 6.77 %, which was also in agreement with the study reported by [Bamgoye and Adejumo (2011) [70] on sunflower seeds.

### 3.2. Calculated Responses from the BBD Experimental Runs

Following the BBD experimental runs in relation to the input processing factors combinations (Table 1), the calculated responses were the mass of oil, oil yield, oil expression efficiency and deformation energy using equations (Eq. 5) to (Eq. 7). The oil expression efficiency is dependent on the mass of oil, oil yield and oil content of the seeds, hence, the need to estimate all the oil output parameters. Based on the twelve factors combinations (runs 1 to 12) without any repetitions at the centre points, the highest amount of the oil expression efficiency of 67.27 % was obtained at run 6 (heating temperature: 60 °C, heating time: 45 min and pressing height of 60 mm) followed by run 10 (heating temperature: 50 °C, heating time: 60 min and pressing height of 60 mm) producing an amount of 65.12 % and then run 4 (heating temperature: 60 °C, heating time: 60 min and pressing height of 80 mm) generating 65.55%. However, the five repetitions of the input factors at the centre points recorded an average amount of  $61.96 \pm 4.08$  %. Their corresponding deformation energies were 818.03, 722.55, 972.28 and  $913.74 \pm 55.04$  J. It was observed that the highest deformation energies of 1179.6 and 1143.53 J were obtained from run 7 (heating temperature: 40 °C, heating time: 45 min and pressing height of 100 mm) and run 8 (heating temperature: 60 °C, heating time: 45 min and pressing

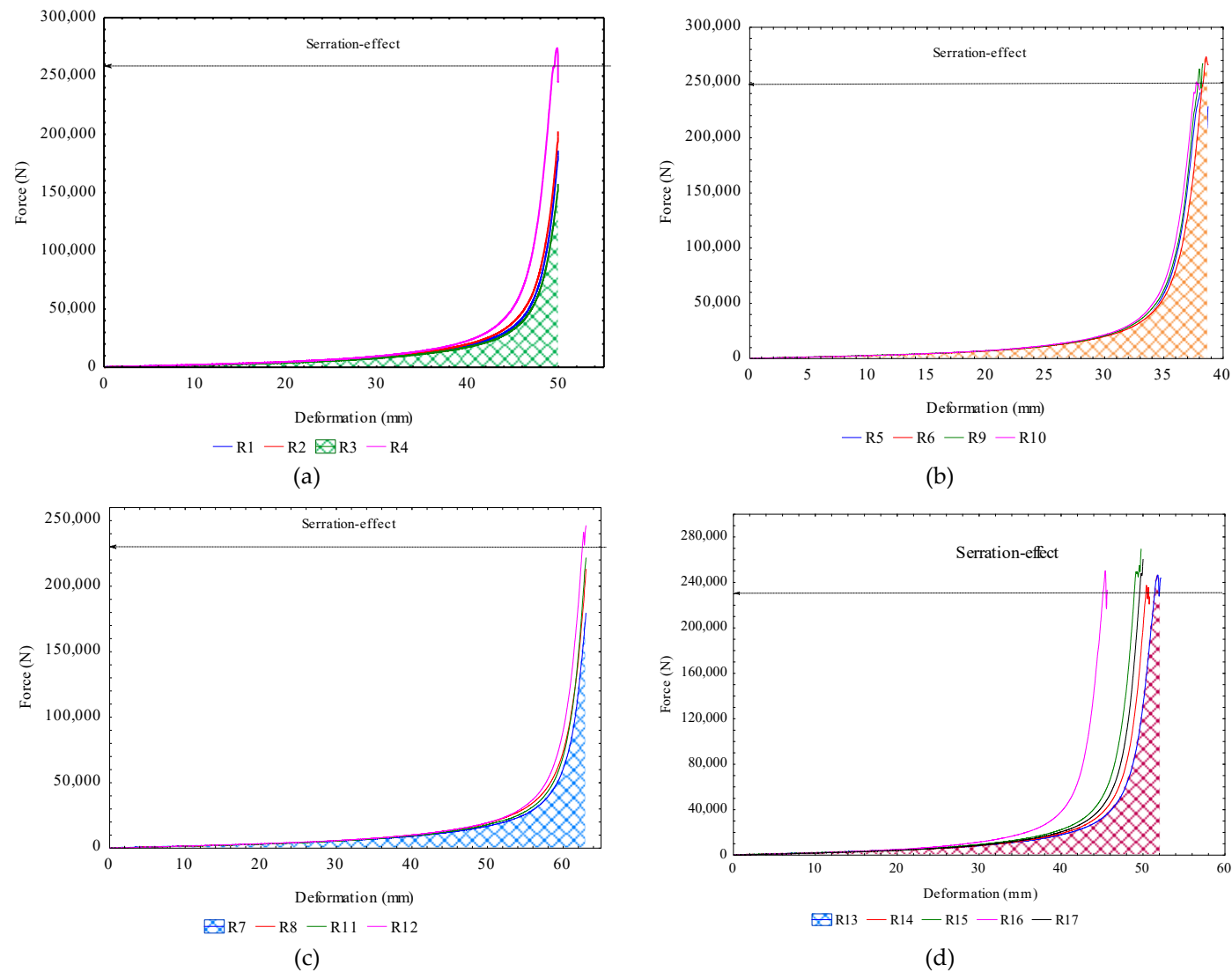
height of 100 mm) with oil expression efficiency amounts of 59.74 % and 65.12 % respectively. The area under the force-deformation curve (Figure 2) is the deformation energy for extracting the oil under uniaxial compression loading.

**Table 2.** Determined amounts of oil output parameters and deformation energy of bulk hempseeds from the BBD.

Run	Input processing factors			Calculated output parameters			
	$H_{TP}$ (° C)	$H_{TM}$ (min)	$P_{HT}$ (mm)	$M_{OL}$ (g)	$O_{YD}$ (%)	$O_{EE}$ (%)	$E_{NG}$ (J)
1	40	30	80	20.53	15.94	48.55	850.21
2	60	30	80	26.46	20.55	62.57	934.74
3	40	60	80	25.26	19.62	59.73	829.49
4	60	60	80	27.72	21.53	65.55	972.28
5	40	45	60	20.87	21.15	64.40	811.15
6	60	45	60	21.8	22.09	67.27	818.03
7	40	45	100	31.88	19.62	59.74	1143.53
8	60	45	100	34.75	21.39	65.12	1179.6
9	50	30	60	20.96	21.24	64.68	778.24
10	50	60	60	21.37	21.66	65.94	722.55
11	50	30	100	32.26	19.85	60.45	1051.14
12	50	60	100	31.25	19.23	58.56	1092.21
13*	50	45	80	25.33	19.67	59.90	1009.82
14*	50	45	80	25.15	19.53	59.47	876.28
15*	50	45	80	26.89	20.88	63.59	909.25
16*	50	45	80	24.73	19.20	58.48	886.91
17*	50	45	80	28.92	22.46	68.39	886.46

\* Repetitions at the centre points of factor levels;  $H_{TP}$ : Heating temperature;  $H_{TM}$ : Heating time;  $P_{HT}$ : Initial pressing height of sample;  $M_{OL}$ : Mass of oil extracted;  $O_{YD}$ : Percentage oil yield;  $O_{EE}$ : Percentage oil expression efficiency and  $E_{NG}$ : Deformation energy.





**Figure 2.** Force-deformation curves of bulk hempseeds at (a) various pressing heights (b) at various input processing factors at constant pressing height,  $H = 80$  mm, (c)  $H = 60$  mm, (d)  $H = 100$  mm and (e) centre values of the input processing factors. The area under the curve represents the deformation energy.

3.3. Calculated Mechanical Properties from the Force-Deformation Curves

Each experimental run generated the force-deformation curve as shown in Figure 2a–d where the mechanical properties, namely the force, deformation, hardness, strain, stress and secant modulus of elasticity of the hemp seeds were calculated using equations (Eq. 8) to (Eq. 11) (Table 3). The hardness is dependent on the force and the deformation relation, whereas the secant modulus of elasticity is derived from the stress and strain ratio. The secant modulus is used for materials that exhibits non-linear relationship, and it thus explains the stiffness of the material, which is calculated over a specific operating range up to a chosen point on the non-linear curve [67]. Considering the mean values of the input factors center points (runs 13–17) and the individual input factors combinations (runs 1–12), the overall hardness and secant modulus of elasticity values ranged between 3.65 and 7.09 kN/mm and 123.98 to 150.39 MPa indicating that the varying input processing factors had significant effect on the stiffness of the bulk hemp seeds. It is important to mention that preceding the maximum compressive force is the serration-effect (Figure 2), which was characterised by the ejection of seedcake through the pressing holes mainly due to higher pressure leading to a vibration of the compression machine. Other factors such as moisture content, pressing speed, vessel diameter and quality of raw material could contribute to the serration effect characteristics [42,64,65]. Usually, the serration effect does not produce any significant amount of oil; hence, the compression process has to be discontinued to prevent insufficient use of input energy. The knowledge of the mechanical properties of oilseeds under the uniaxial compression process is relevant for understanding the pressure threshold in the screw press and its design and optimisation mechanisms [40,64–66,71].

Table 3. Determined mechanical properties of bulk hempseeds from the BBD.

Input processing factors					Calculated output parameters				
Run	$H_{TP}$ (° C)	$H_{TM}$ (min)	$P_{HT}$ (mm)	$F_{RC}$ (kN)	$D_{FX}$ (mm)	$H_{DN}$ (kN/mm)	$\epsilon_{ST}$ (-)	$\sigma_{ST}$ (MPa)	$E_{SM}$ (MPa)
1	40	30	80	223.52	50.49	4.43	0.63	79.05	125.26
2	60	30	80	250.17	50.57	4.95	0.63	88.48	139.97
3	40	60	80	222.72	50.83	4.38	0.64	78.77	123.98
4	60	60	80	257.77	49.46	5.21	0.62	91.17	147.46
5	40	45	60	251.11	38.36	6.55	0.64	88.81	138.92
6	60	45	60	273.34	38.57	7.09	0.64	96.68	150.39
7	40	45	100	239.16	64.28	3.72	0.64	84.59	131.59
8	60	45	100	266.93	63.66	4.19	0.64	94.41	148.30
9	50	30	60	262.22	38.02	6.90	0.63	92.74	146.35
10	50	60	60	241.16	37.55	6.42	0.63	85.29	136.29
11	50	30	100	230.83	63.3	3.65	0.63	81.64	128.97
12	50	60	100	241.23	62.71	3.85	0.63	85.32	136.05
13*	50	45	80	246.62	51.81	4.76	0.65	87.22	134.68
14*	50	45	80	237.37	50.43	4.71	0.63	83.95	133.18
15*	50	45	80	249.49	49.17	5.07	0.61	88.24	143.57
16*	50	45	80	250.18	45.43	5.51	0.57	88.48	155.81
17*	50	45	80	248.00	49.87	4.97	0.62	87.71	140.70

\* Repetitions at the centre points of factor levels;  $H_{TP}$ : Heating temperature;  $H_{TM}$ : Heating time;  $P_{HT}$ : Initial pressing height of sample;  $F_{RC}$ : Compression force;  $D_{FX}$ : Deformation;  $H_{DN}$ : Hardness;  $\epsilon_{ST}$ : Strain;  $\sigma_{ST}$ : Stress and  $E_{SE}$ : Secant modulus of elasticity.

3.4. ANOVA Analysis of Calculated Responses and Their Regression Coefficients

The ANOVA results of the response surface regression analysis of the calculated parameters (mass of oil, oil yield, oil expression efficiency and deformation energy) are provided in Tables 4 to 7. The coefficients of the intercept, linear, quadratic and interaction terms of the input processing factors (heating temperature, heating time and sample pressing height) for each parameter model showed both significant (p-value < 0.05) and non-significant (p-value > 0.05). For the mass of oil model parameter, the intercept, heating temperature and the sample pressing height indicated significant, whereas the other terms were non-significant. For the oil yield and oil expression efficiency model parameters, only the intercept and the heating temperature indicated significant, whereas the other terms were non-significant. The deformation energy model parameter showed that the intercept and the sample pressing height were significant, whereas the other terms were non-significant. The coefficient of determination ( $R^2$ ) values confirm the models' coefficients ranged between 0.68 and 0.95, implying their adequacy for prediction.

Table 4. ANOVA results for the  $M_{OL}(g)$  parameter at a 0.05 significance level.

Effect	Model <sup>a</sup> coefficients	Standard error	t-value	Sum of squares	df	Mean square	F- value	p- value
Intercept	26.20	0.77	33.89	292.5	9	32.50	10.87	0.00*
$H_{TP}$ (L)	1.52	0.61	2.49	18.57	1	18.57	6.25	0.04*
$H_{TP}^2$ (Q)	-0.17	0.84	-0.21	0.13	1	0.13	0.04	0.84**
$H_{TM}$ (L)	0.67	0.61	1.10	3.63	1	3.63	1.22	0.31**
$H_{TM}^2$ (Q)	-1.04	0.84	-1.23	4.54	1	4.54	1.53	0.26**
$P_{HT}$ (L)	5.64	0.61	9.23	254.70	1	254.70	85.65	0.00*
$P_{HT}^2$ (Q)	1.29	0.84	1.54	7.05	1	7.05	2.37	0.17**
$H_{TP} \cdot H_{TM}$	-0.87	0.86	-1.00	3.01	1	3.01	1.01	0.35**
$H_{TP} \cdot P_{HT}$	0.49	0.86	0.56	0.94	1	0.94	0.32	0.59**
$H_{TM} \cdot P_{HT}$	-0.36	0.86	-0.41	0.50	1	0.50	0.17	0.69**
Residual				20.92	7	2.99		
Lack of Fit				9.03	3	3.01	1.01	0.47**
Pure Error				11.89	4	2.97		
Total				313.42	16			

$H_{TP}$ : Heating temperature;  $H_{TM}$ : Heating time;  $P_{HT}$ : Initial pressing height of sample; L: Linear term; Q: Quadratic term; <sup>a</sup>: Coefficient of determination ( $R^2$ ) = 0.93 for mass of oil,  $M_{OL}(g)$ ; \*: p-value < 0.05 or higher F-value means significant and \*\*: p-value > 0.05 or lower F-value means non-significant.

Table 5. ANOVA results for the  $O_{YD}(\%)$  parameter at a 0.05 significance level.

Effect	Model <sup>a</sup> coefficients	Standard error	t-value	Sum of squares	df	Mean square	F-value	p- value
Intercept	20.35	0.59	34.40	25.6	9	2.84	1.62	0.00*
$H_{TP}$ (L)	1.15	0.47	2.47	10.64	1	10.64	5.93	0.04*
$H_{TP}^2$ (Q)	-0.19	0.64	-0.29	0.15	1	0.15	0.08	0.78**
$H_{TM}$ (L)	0.56	0.47	1.19	2.47	1	2.47	1.38	0.27**
$H_{TM}^2$ (Q)	-0.75	0.64	-1.17	2.39	1	2.39	1.33	0.28**
$P_{HT}$ (L)	-0.76	0.47	-1.62	4.57	1	4.57	2.55	0.15**
$P_{HT}^2$ (Q)	0.90	0.64	1.40	3.41	1	3.41	1.90	0.21**
$H_{TP} \cdot H_{TM}$	-0.67	0.66	-1.02	1.82	1	1.82	1.01	0.34**
$H_{TP} \cdot P_{HT}$	0.21	0.66	0.31	0.17	1	0.17	0.09	0.76**
$H_{TM} \cdot P_{HT}$	-0.26	0.66	-0.39	0.27	1	0.27	0.15	0.71**

Residual	12.24	7	1.75		
Lack of Fit	5.07	3	1.69	0.94	0.49**
Pure Error	7.17	4	1.79		
Total	37.82	16			

$H_{TP}$ : Heating temperature;  $H_{TM}$ : Heating time;  $P_{HT}$ : Initial pressing height of sample; L: Linear term; Q: Quadratic term; <sup>a</sup>: Coefficient of determination ( $R^2$ ) = 0.68 for oil yield,  $O_{YD}$ (%); \*: p-value < 0.05 or higher F-value means significant and \*\*: p-value > 0.05 or lower F-value means non-significant.

Table 6. ANOVA results for the  $O_{EF}$ (%) parameter at a 0.05 significance level.

Effect	Model <sup>a</sup> coefficients	Standard error	t-value	Sum of squares	df	Mean square	F- value	p- value
Intercept	61.96	1.80	34.40	237.2	9	26.35	1.62	0.00*
$H_{TP}$ (L)	3.51	1.42	2.47	98.62	1	98.62	5.93	0.04*
$H_{TP}^2$ (Q)	-0.57	1.96	-0.29	1.37	1	1.37	0.08	0.78**
$H_{TM}$ (L)	1.69	1.42	1.19	22.91	1	22.91	1.38	0.27**
$H_{TM}^2$ (Q)	-2.29	1.96	-1.17	22.17	1	22.17	1.33	0.28**
$P_{HT}$ (L)	-2.30	1.42	-1.62	42.37	1	42.37	2.55	0.15**
$P_{HT}^2$ (Q)	2.74	1.96	1.40	31.59	1	31.59	1.90	0.21**
$H_{TP} \cdot H_{TM}$	-2.05	2.01	-1.02	16.83	1	16.83	1.01	0.34**
$H_{TP} \cdot P_{HT}$	0.63	2.01	0.31	1.57	1	1.57	0.09	0.76**
$H_{TM} \cdot P_{HT}$	-0.79	2.01	-0.39	2.49	1	2.49	0.15	0.71**
Residual				113.54	7	16.22		
Lack of Fit				47.02	3	15.67	0.94	0.49**
Pure Error				66.51	4	16.63		
Total				350.69	16			

$H_{TP}$ : Heating temperature;  $H_{TM}$ : Heating time;  $P_{HT}$ : Initial pressing height of sample; L: Linear term; Q: Quadratic term; <sup>a</sup>: Coefficient of determination ( $R^2$ ) = 0.68 for oil expression efficiency,  $O_{EF}$ (%); \*: p-value < 0.05 or higher F-value means significant and \*\*: p-value > 0.05 or lower F-value means non-significant.

Table 7. ANOVA results for  $E_{NG}$ (J) parameter at a 0.05 significance level.

Effect	Model <sup>a</sup> coefficients	Standard error	t-value	Sum of squares	df	Mean square	F- value	p- value
Intercept	913.76	20.20	45.25	252777	9	28086.33	13.77	0.00*
$H_{TP}$ (L)	24.94	15.97	1.56	4977	1	4977	1.64	0.16**
$H_{TP}^2$ (Q)	38.82	22.01	1.76	6345.4	1	6345.4	2.09	0.12**
$H_{TM}$ (L)	-8.57	15.97	-0.54	587	1	587	0.19	0.61**
$H_{TM}^2$ (Q)	-38.22	22.01	-1.74	6151.2	1	6151.2	2.03	0.13**
$P_{HT}$ (L)	167.06	15.97	10.46	223282.4	1	223282.4	73.58	0.00*
$P_{HT}^2$ (Q)	35.49	22.01	1.61	5304.2	1	5304.2	1.75	0.15**
$H_{TP} \cdot H_{TM}$	32.25	22.58	1.43	4159.6	1	4159.6	1.37	0.20**
$H_{TP} \cdot P_{HT}$	7.30	22.58	0.32	213	1	213	0.07	0.76**
$H_{TM} \cdot P_{HT}$	24.19	22.58	1.07	2340.6	1	2340.6	0.77	0.32**
Residual				14275.38	7	2039.34		
Lack of Fit				2137.3	3	712.4	0.23	0.87**

Pure			
Error	12138	4	3034.5
Total	267052.4	16	

$H_{TP}$ : Heating temperature;  $H_{TM}$ : Heating time;  $P_{HT}$ : Initial pressing height of sample; L: Linear term; Q: Quadratic term;  $a$ : Coefficient of determination ( $R^2$ ) = 0.95 for deformation energy,  $E_{NG}(J)$ ; \*: p-value < 0.05 or higher F-value means significant and \*\*: p-value > 0.05 or lower F-value means non-significant.

The coefficients of the full quadratic and reduced models are described in equations (Eq.14–Eq.21). The full quadratic models' coefficients, including both the significant and non-significant terms of the intercept, linear, quadratic and interactions (Eqs.14, 16, 18 and 20), are useful for identifying the optimal input factors. The adequacy of the full quadratic models was determined by the lack of fit  $P$ -values, which were greater than 0.05 (Tables 4 to 7). Similar evaluation of the quadratic model was reported in the studies by Todorovic et al. [20], [Chanioti and Tzia [59] and Ocholi et al.[60]. The reduced model coefficients comprising only the significant terms (Eqs.15, 17, 19 and 21) are effective for prediction and experimental validation. For mass of oil (Eq. 15), the dominant effect was the heating temperature and pressing height, whereas for oil yield (Eq. 17), and oil expression efficiency (Eq. 19), the dominant effect was the heating temperature, and for deformation energy (Eq. 21), the dominant effect was the pressing height.

$$M_{OL}(g) = 26.20 + 1.52 \cdot H_{TP} - 0.17 \cdot H_{TP}^2 + 0.67 \cdot H_{TM} - 1.04 \cdot H_{TM}^2 + 5.64 \cdot P_{HT} + 1.29 \cdot P_{HT}^2 - 0.87 \cdot H_{TP} \cdot H_{TM} + 0.49 \cdot H_{TP} \cdot P_{HT} - 0.36 \cdot H_{TM} \cdot P_{HT} \quad (14)$$

$$M_{OL}(g) = 26.20 + 1.52 \cdot H_{TP} + 5.64 \cdot P_{HT} \quad (15)$$

$$O_{YD}(\%) = 20.35 + 1.15 \cdot H_{TP} - 0.19 \cdot H_{TP}^2 + 0.56 \cdot H_{TM} - 0.75 \cdot H_{TM}^2 - 0.76 \cdot P_{HT} + 0.90 \cdot P_{HT}^2 - 0.67 \cdot H_{TP} \cdot H_{TM} + 0.21 \cdot H_{TP} \cdot P_{HT} - 0.26 \cdot H_{TM} \cdot P_{HT} \quad (16)$$

$$O_{YD}(\%) = 20.35 + 1.15 \cdot H_{TP} \quad (17)$$

$$O_{EF}(\%) = 61.96 + 3.51 \cdot H_{TP} - 0.57 \cdot H_{TP}^2 + 1.69 \cdot H_{TM} - 2.29 \cdot H_{TM}^2 - 2.30 \cdot P_{HT} + 2.74 \cdot P_{HT}^2 - 2.05 \cdot H_{TP} \cdot H_{TM} + 0.63 \cdot H_{TP} \cdot P_{HT} - 0.79 \cdot H_{TM} \cdot P_{HT} \quad (18)$$

$$O_{EF}(\%) = 61.96 + 3.51 \cdot H_{TP} \quad (19)$$

$$E_{NG}(J) = 913.76 + 24.94 \cdot H_{TP} + 38.82 \cdot H_{TP}^2 - 8.57 \cdot H_{TM} - 38.22 \cdot H_{TM}^2 + 167.06 \cdot P_{HT} + 35.49 \cdot P_{HT}^2 + 32.25 \cdot H_{TP} \cdot H_{TM} + 7.30 \cdot H_{TP} \cdot P_{HT} + 24.19 \cdot H_{TM} \cdot P_{HT} \quad (20)$$

$$E_{NG}(J) = 913.76 + 167.06 \cdot P_{HT} \quad (21)$$

### 3.5. Profiles of Predicted Values Based on Optimal Input Factors and Desirability

The predicted and desirability profiles of the full quadratic models are illustrated in Figures 3–6, respectively. The mass of oil regression model (Eq. 14) predicted an amount of 34.976 g with the optimal input factors (heating temperature: 60 °C (+1), heating time: 45 min (0) and sample pressing height: 100 mm (+1)) with a desirability value of 1 (Figure 3). The oil yield regression model (Eq. 16) predicted an amount of 22.647 % with optimal input factors (heating temperature: 60 °C (+1), heating time: 52.5 min (0.5) and sample pressing height: 60 mm (–1)), achieving the desirability value of 1 (Figure 4). The oil expression efficiency regression model (Eq. 18) predicted an amount of 68.96 % with optimal input factors (heating temperature: 60 °C (+1), heating time: 52.5 min (0.5) and sample

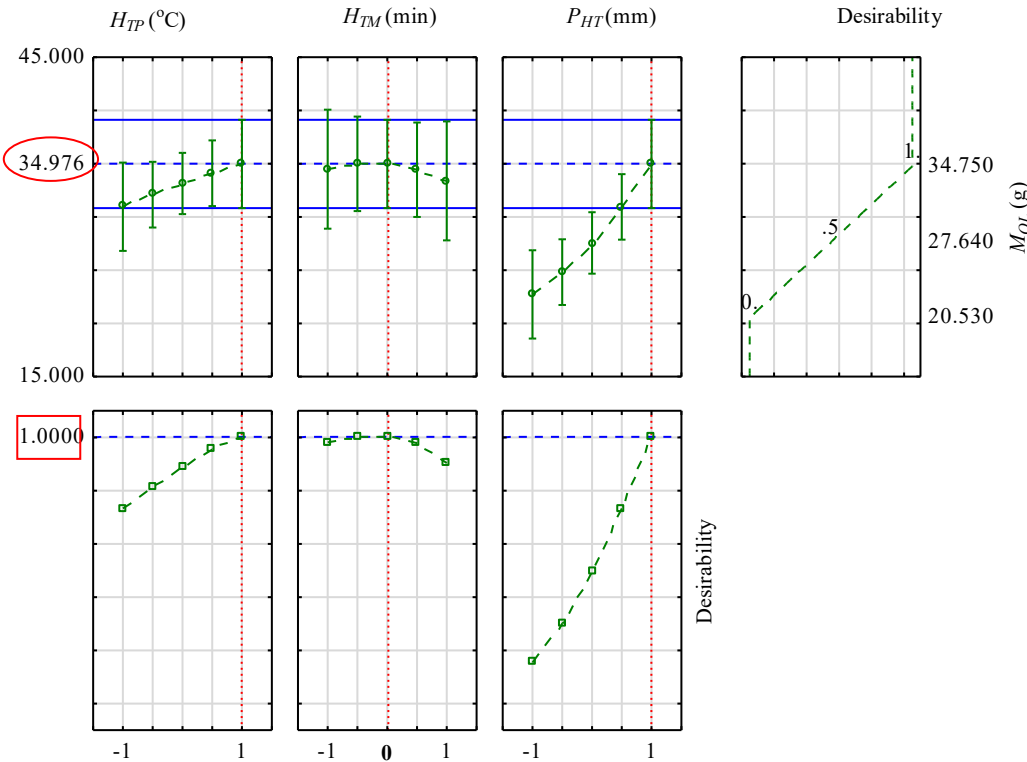


pressing height: 60 mm (−1) achieving the desirability value of 1 (Figure 5). The deformation energy regression model (Eq. 20) predicted an amount of 1197 (J) with optimal input factors (heating temperature: 60 °C (+1), heating time: 60 min (+1) and sample pressing height: 100 mm (+1)), giving the desirability value of 1 (Figure 6). The desirability value of 1 was identified in all cases, implying that all the responses simultaneously achieved their individual optima without any existence of trade-offs [59,60]. However, the reduced regression models (Eqs.15, 17, 19 and 21), considering only the significant terms from the full quadratic models, produced the mass of oil of 33.36 g, oil yield of 21.5 %, oil expression efficiency of 65.47 % and deformation energy of 1080.82 J. The differences between the full quadratic model and the reduced model predictions were determined using absolute and relative differences (Table 8). For all the model responses, relative differences were below 10%, indicating close agreement between the two regression models.

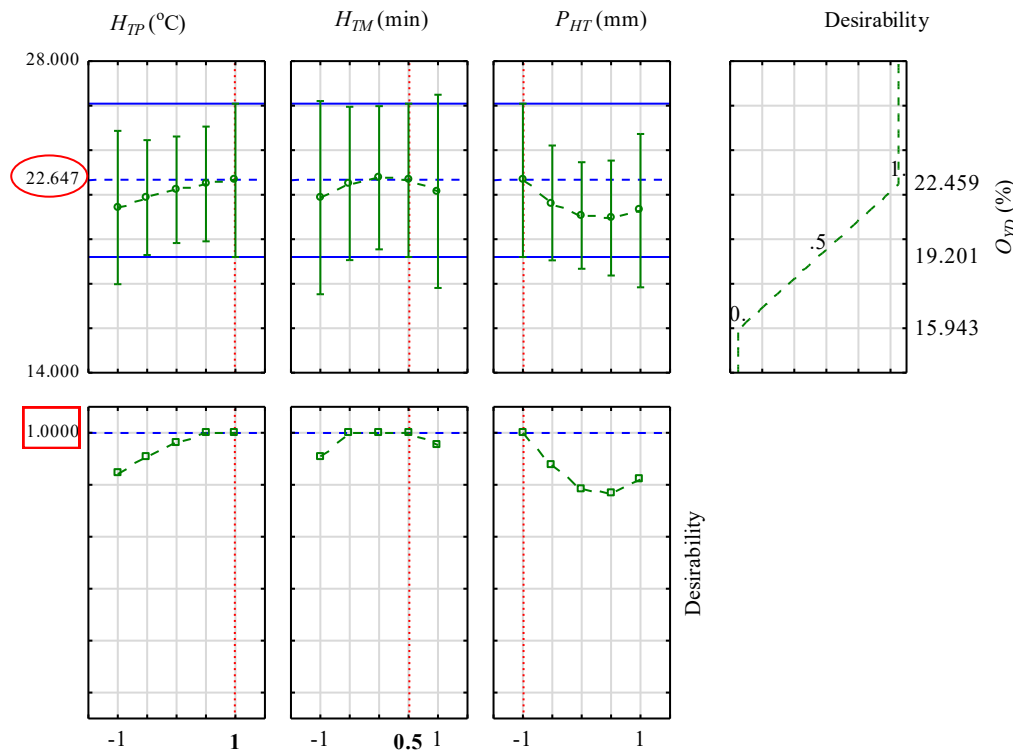
**Table 8.** Prediction comparison between the full quadratic model and the reduced model.

Model responses	Full quadratic model (Eqs.14, 16, 18 and 20)	Reduced model (Eqs.15, 17, 19 and 21)	Absolute difference	Relative difference (%)
$M_{OL}(g)$	34.98	33.36	1.62	4.62
$O_{YD}(\%)$	22.65	21.50	1.15	5.06
$O_{EE}(\%)$	68.96	65.47	3.49	5.06
$E_{NG}(J)$	1197.00	1080.82	116.18	9.71

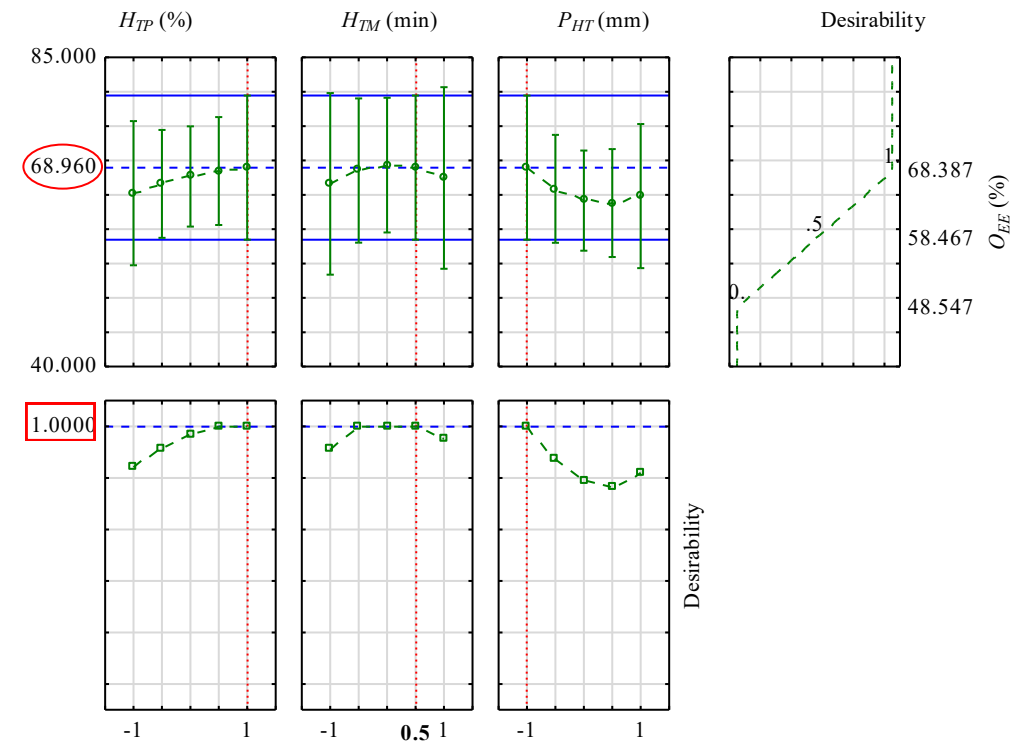
$M_{OL}$ : Mass of oil;  $O_{YD}$ : Oil yield;  $O_{EE}$ : Oil expression efficiency and  $E_{NG}$ : Deformation energy.



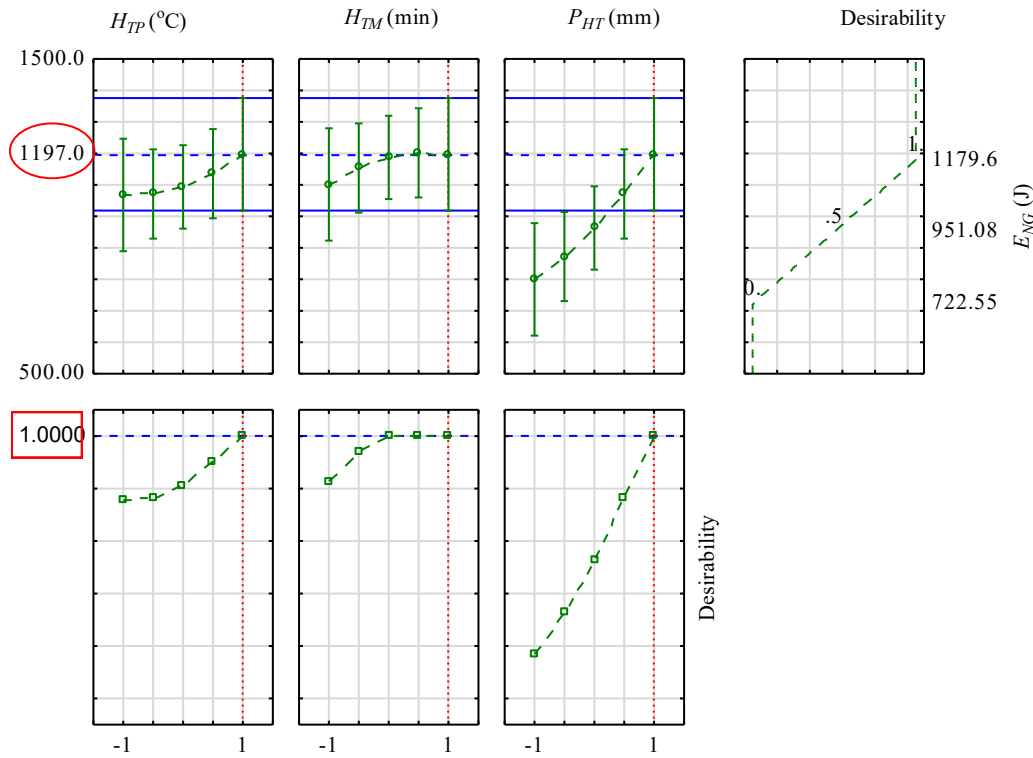
**Figure 3.** Profiles of predicted values (blue dotted lines) and desirability (red dotted lines) of the mass of oil,  $M_{OL}$  parameter;  $H_{TP}$ : Heating temperature (+1: optimal level of 60 °C);  $H_{TM}$ : Heating time (0: optimal level of 45 min) and  $P_{HT}$ : Initial pressing height of sample (+1: optimal level of 100 mm). The dotted blue line.



**Figure 4.** Profiles of predicted values (blue dotted lines) and desirability (red dotted lines) of oil yield,  $O_{YD}$  parameter;  $H_{TP}$ : Heating temperature (+1: optimal level of 60 °C);  $H_{TM}$ : Heating time (0.5: optimal level of 52.5 min) and  $P_{HT}$ : Initial pressing height of sample (-1: optimal level of 60 mm).



**Figure 5.** Profiles of predicted values (blue dotted lines) and desirability (red dotted lines) of oil expression efficiency,  $O_{EE}$  parameter;  $H_{TP}$ : Heating temperature (+1: optimal level of 60 °C);  $H_{TM}$ : Heating time (0.5: optimal level of 52.5 min) and  $P_{HT}$ : Initial pressing height of sample (-1: optimal level of 60 mm).



**Figure 6.** Profiles of predicted values (blue dotted lines) and desirability (red dotted lines) of deformation energy,  $E_{NG}$  parameter;  $H_{TP}$ : Heating temperature (+1: optimal level of 60 °C);  $H_{TM}$ : Heating time (+1: optimal level of 60 min) and  $P_{HT}$ : Initial pressing height of sample (+1: optimal level of 100 mm).

3.6. Observed, Predicted, Residuals and Percentage Error

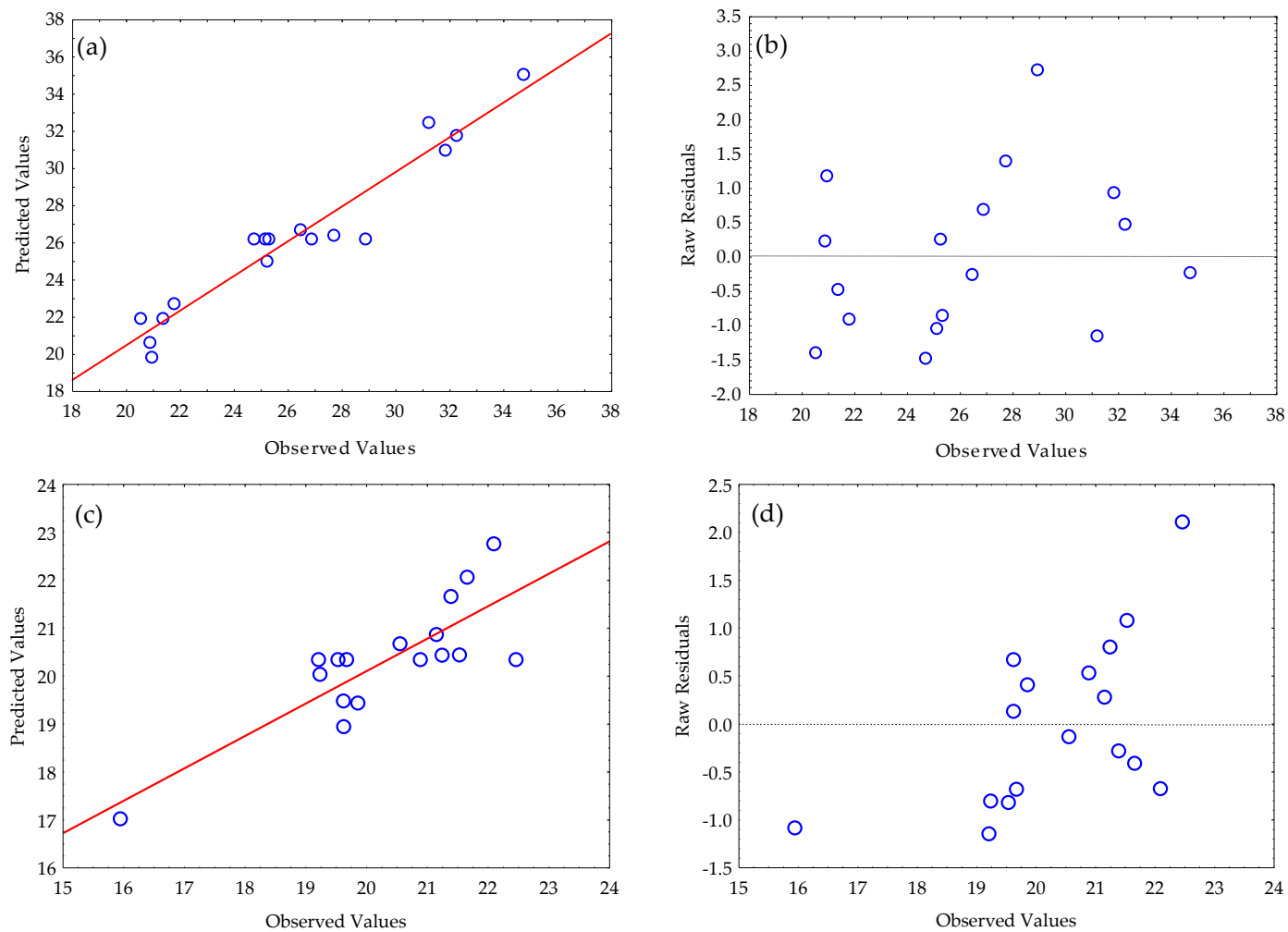
The residuals from the observed and predicted based on the full quadratic models (Eqs.11, 13, 15 and 17) for the individual experimental runs and their percentage error are presented in Tables 9 and 10 and subsequently illustrated in Figure 7a–h. A positive residual means the model underpredicts the observed value, whereas a negative residual means the model overpredicts the observed value. However, randomly distributed residuals around the zero line and the lower percentage error values between 0.14 and 10.52 indicate a good model performance [45].

Table 9. Observed, predicted, residuals and absolute percentage error values of mass of oil and oil yield.								
Runs	Mass of oil, $M_{OL}(g)$				Oil yield, $\theta_{YD}(\%)$			
	Observed	Predicted	Residuals	% Error	Observed	Predicted	Residuals	% Error
1	20.53	21.93	−1.40	6.37	15.94	17.03	−1.08	6.36
2	26.46	26.71	−0.25	0.94	20.55	20.68	−0.13	0.64
3	25.26	25.01	0.25	1.00	19.62	19.48	0.13	0.67
4	27.72	26.32	1.40	5.31	21.53	20.44	1.08	5.30
5	20.87	20.64	0.23	1.10	21.15	20.87	0.28	1.34
6	21.80	22.72	−0.92	4.05	22.09	22.76	−0.67	2.96
7	31.88	30.96	0.92	2.98	19.62	18.95	0.67	3.55
8	34.75	34.98	−0.23	0.65	21.39	21.66	−0.28	1.29
9	20.96	19.79	1.17	5.92	21.24	20.44	0.80	3.94

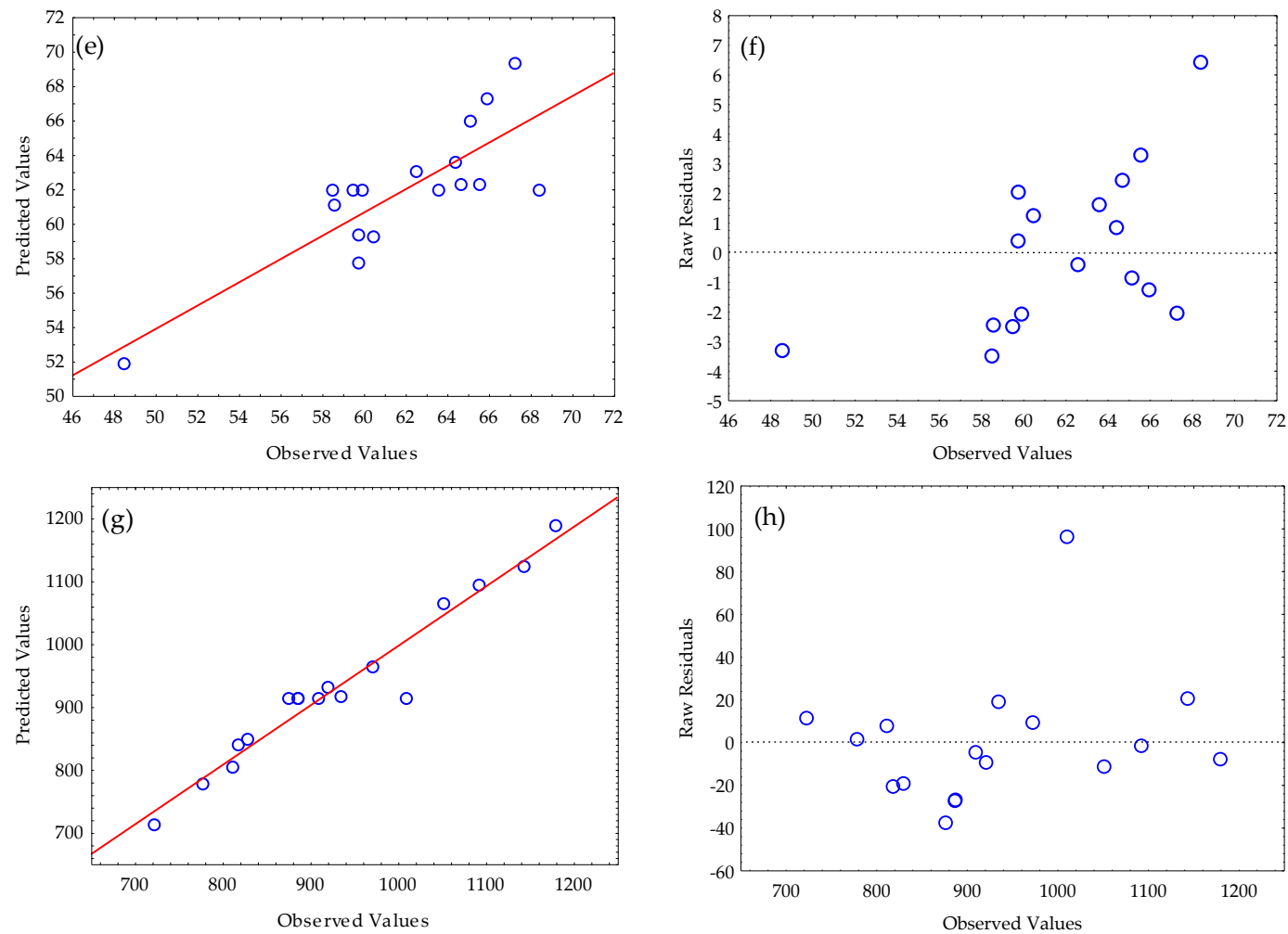
10	21.37	21.85	−0.48	2.18	21.66	22.07	−0.41	1.86
11	32.26	31.78	0.48	1.50	19.85	19.44	0.41	2.11
12	31.25	32.42	−1.17	3.61	19.23	20.04	−0.80	4.01
13	25.33	26.20	−0.87	3.34	19.67	20.35	−0.68	3.34
14	25.15	26.20	−1.05	4.02	19.53	20.35	−0.82	4.02
15	26.89	26.20	0.69	2.62	20.88	20.35	0.53	2.62
16	24.73	26.20	−1.47	5.63	19.20	20.35	−1.14	5.63
17	28.92	26.20	2.72	10.36	22.46	20.35	2.11	10.36

**Table 10.** Observed, predicted, residuals and absolute percentage error values of oil expression efficiency and deformation energy.

Runs	Oil expression efficiency, $O_{EE}$ (%)				Deformation energy, $E_{NG}(J)$			
	Observed	Predicted	Residuals	% Error	Observed	Predicted	Residuals	% Error
1	48.55	51.85	−3.30	6.36	920.94	930.23	−9.29	1.00
2	62.57	62.97	−0.40	0.64	934.74	915.62	19.12	2.09
3	59.73	59.33	0.40	0.67	829.49	848.61	−19.12	2.25
4	65.55	62.25	3.30	5.30	972.28	962.99	9.29	0.97
5	64.40	63.55	0.85	1.34	811.15	803.37	7.78	0.97
6	67.27	69.32	−2.05	2.96	818.03	838.66	−20.63	2.46
7	59.74	57.69	2.05	3.55	1143.53	1122.90	20.63	1.84
8	65.12	65.97	−0.85	1.29	1179.60	1187.38	−7.78	0.66
9	64.68	62.23	2.45	3.94	778.24	776.73	1.51	0.19
10	65.94	67.19	−1.25	1.86	722.55	711.22	11.33	1.59
11	60.45	59.21	1.25	2.11	1051.14	1062.48	−11.34	1.07
12	58.56	61.01	−2.45	4.01	1092.21	1093.72	−1.51	0.14
13	59.90	61.96	−2.07	3.34	1009.92	913.76	96.16	10.52
14	59.47	61.96	−2.49	4.02	876.28	913.76	−37.48	4.10
15	63.59	61.96	1.62	2.62	909.25	913.76	−4.51	0.49
16	58.48	61.96	−3.49	5.63	886.91	913.76	−26.85	2.94
17	68.39	61.96	6.42	10.36	886.46	913.76	−27.30	2.99







**Figure 7.** Observed versus predicted and observed versus residuals of mass of oil (a, b), oil yield (c, d), oil expression efficiency (e, f) and deformation energy (g, h).

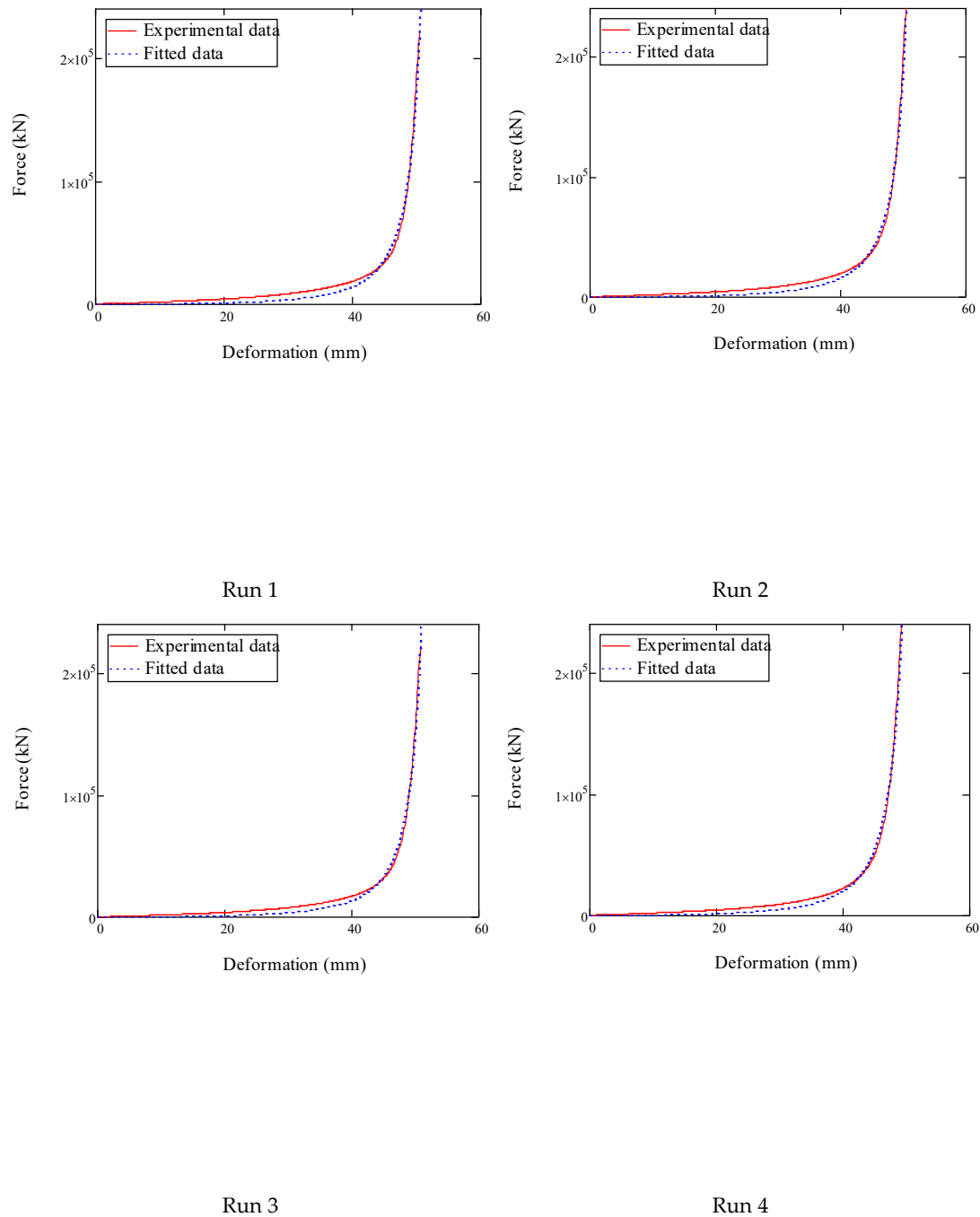
3.7. Theoretical Force-Deformation Curves and Deformation Energy

The experimental force-deformation curves were described theoretically by employing the tangent curve model (Eq.13). The determined coefficients and statistical metrics of the model are presented in Table 7. The force coefficients of mechanical behaviour,  $A_D$  (kN) ranged from 2.504 and 4.26 kN whiles the deformation coefficients of mechanical behaviour,  $B_D$  ranged from 0.023 to 0.039 (mm<sup>-1</sup>). The fitting exponent value of the tangent model was found to be 2, which defines the shape or steepness of the force-deformation curve. The force coefficient of the mechanical behaviour influences the slope of the deformation characteristic, whereas the deformation coefficient of mechanical behaviour influences the range of deformation. These two coefficients indicate the initial rigidity of the pressing process [43]. The tangent model coefficients were statistically significant (F-value < F-critical or P-value > 0.05) with high coefficients of determination ( $R^2$ ), confirming their adequacy for describing the mechanical behaviour of bulk oilseeds or bulk agricultural materials under compression loading. The experimental and theoretical fitted curves for runs 1–4 are shown in Figure 7, which were similar to experimental runs 5–17.

**Table 7.** Determined coefficients of the tangent curve model and statistical metrics for describing the force-deformation curve of bulk hempseeds against the input processing factors of the BBD.

Run	$X$ (mm)	$A_D$ (kN)	$B_D$ (mm <sup>-1</sup> )	$n$ (-)	F-value	F-critical	P-value	$R^2$
1	50.49	2.759	0.029	2	1.341	3.851	0.247	0.993
2	50.57	3.094	0.029	2	0.882	3.851	0.348	0.995
3	50.83	2.687	0.029	2	0.946	3.851	0.331	0.995
4	49.46	3.477	0.029	2	0.695	3.851	0.405	0.996
5	38.36	4.260	0.038	2	0.184	3.851	0.668	0.989
6	38.57	4.000	0.038	2	0.327	3.851	0.368	0.996
7	64.28	2.895	0.023	2	0.630	3.851	0.428	0.991
8	63.66	2.923	0.023	2	0.913	3.851	0.340	0.995
9	38.02	3.809	0.038	2	0.458	3.851	0.499	0.995
10	37.55	3.726	0.039	2	0.633	3.851	0.427	0.996
11	63.30	2.504	0.023	2	1.202	3.851	0.273	0.993
12	62.71	2.867	0.023	2	1.101	3.851	0.294	0.995
13	51.81	3.487	0.028	2	0.532	3.851	0.466	0.993
14	50.43	2.913	0.029	2	0.963	3.851	0.327	0.995
15	49.17	3.166	0.030	2	0.872	3.851	0.351	0.996
16	45.43	3.724	0.032	2	0.407	3.851	0.524	0.996
17	49.87	2.899	0.029	2	0.835	3.851	0.361	0.995

$X$  is the experimental deformation,  $D_{FX}$  (mm),  $A_D$  is the force coefficient of mechanical behaviour (kN),  $B_D$  is the deformation coefficient of mechanical behaviour (mm<sup>-1</sup>),  $n$  is the model's fitting exponent (-), F-value < F-critical or P-value > 0.05 means significant, and  $R^2$  is the coefficient of determination of the tangent model.



**Figure 7.** Experimental and fitted data of the force-deformation curves of bulk hempseeds for runs 1–4 representing similar curves obtained for experimental runs 5–17.

Based on the theoretically fitted curves, the theoretical deformation energies were calculated (Table 8) using the integral form of Eq. (13) as expressed in Eq. (22) for  $n = 2$ .

$$\int F(X)dx \rightarrow \frac{A \cdot (\tan(B \cdot X) - B \cdot X)}{B} \quad (22)$$

The percentage error values between the experimental and theoretical deformation energies ranged from 1.35 and 28.31%, suggesting that the varying input processing factors thus influence the coefficients of the tangent model. However, the efficiency of the tangent model was between 98.65% and 71.69%, which confirms its suitability for describing the mechanical behavior of oilseeds [43,72,73].

**Table 8.** Determined amounts of experimental and theoretical energy of bulk hempseeds against the input processing factors of the BBD.

Run	Input processing factors			Experimental and theoretical energy		
	$H_{TP}$ (° C)	$H_{TM}$ (min)	$P_{HT}$ (mm)	$E_{NG}$ (J)	$TE_{NG}$ (J)	Error (%)
1	40	30	80	850.18	749.91	11.79
2	60	30	80	934.71	863.07	7.66
3	40	60	80	829.50	818.34	1.35
4	60	60	80	972.37	701.21	27.89
5	40	45	60	811.21	823.42	1.50
6	60	45	60	818.06	843.24	3.08
7	40	45	100	1141.28	1170	2.52
8	60	45	100	1179.66	1001	15.14
9	50	30	60	778.22	646.27	16.69
10	50	60	60	722.49	749.91	4.51
11	50	30	100	1051.16	784.87	25.33
12	50	60	100	1095.25	785.18	28.31
13	50	45	80	1009.84	851.14	15.72
14	50	45	80	876.21	776.742	11.35
15	50	45	80	909.29	943.75	3.79
16	50	45	80	886.90	820.62	7.47
17	50	45	80	886.16	653.78	26.22

$H_{TP}$ : Heating temperature;  $H_{TM}$ : Heating time;  $P_{HT}$ : Initial pressing height of sample;  $E_{NG}$ : Experimental deformation energy,  $TE_{NG}$ : Theoretical deformation energy.

4. Conclusions

The processing of bulk hemp seeds under uniaxial compression loading by applying the Box-Behnken Design and response surface methodology revealed the following findings. The maximum compressive force of 273.34 kN was obtained at the input factor combinations (heating temperature: 60 °C, heating time: 45 min and pressing height: 60 mm) in the absence of the serration-effect behaviour characterised by seedcake ejection without oil yield. Full quadratic and reduced (linear) regression models were described for the mass of oil, oil yield, oil expression efficiency and deformation energy. The quadratic models of a second order included both the significant and non-significant terms of the intercept, linear, quadratic and interactions of the input factors for assessing the models adequacy based on the lack-of-fit p-values > 0.05. The linear models included only the significant terms useful for prediction and experimental validation. Based on the full quadratic models, the mass of oil was predicted as 34.976 g at optimal factor levels (heating temperature: 60 °C (+1), heating time: 45 min (0) and sample pressing height: 100 mm (+1)). The oil yield was predicted as 22.647 g at optimal factor levels (heating temperature: 60 °C (+1), heating time: 52.5 min (0.5) and sample pressing height: 60 mm (-1)). The oil expression efficiency was predicted at 68.96 (%) with optimal factor levels (heating temperature: 60 °C (+1), heating time: 52.5 min (0.5) and sample pressing height: 60 mm (-1). The energy was predicted as 1197 (J)) at optimal factor levels (heating temperature: 60 °C (+1), heating time: 60 min (+1) and sample pressing height: 100 mm (+1)). All the optimal factor levels achieved a desirability value of 1, and the coefficient of determination (R<sup>2</sup>) values were between 0.68 and 0.95, indicating the models’ adequacy. The tangent curve model showed a good fit for describing the experimental force-deformation curves with (R<sup>2</sup>) values closer to 1. However, the theoretical deformation energies obtained from the tangent curve model compared to the experimental deformation energies showed percentage error values between 1.35 and 28.31%,

which indicated that the varying input factors tend to affect the coefficients of the tangent curve model. The study approach will be validated in the mechanical screw press by modelling and optimizing the input processing factors in relation to the oil recovery efficiency and minimum energy requirement. The results of the present study are an expansion of the conference paper [74] in the proceeding of 9<sup>th</sup> International Conference on Trends in Agricultural Engineering 2025.

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